

**Key Words:**

*Precipitation*

Filtration

Separation

Organic

**Retention:**

**Permanent**

**Key WTP R&T References:**

Test Specification: 24590-WTP-TSP-RT-01-029, Rev 0

Test Plan: SRT-RPP-2002-00054, Rev 0

Test Scoping Statement(s): S-132

Test Exception: 24590-WTP-TEF-TR-03-027

**FINAL REPORT: PILOT-SCALE CROSS-FLOW  
ULTRAFILTRATION TEST USING A HANFORD SITE  
TANK 241-AN-102 WASTE SIMULANT (U)**

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**MAY 6, 2003**

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Savannah River Site  
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Prepared for the U.S. Department of Energy Under Contract Number DE-AC09-96SR18500



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## **ACKNOWLEDGMENTS**

The author would like to thank all that were involved in this task. Mike Armstrong's care and dedication in running this experiment allowed it to be successfully completed. Support from the other Engineering Development Laboratory & other personnel: Vern Bush, Jimmy Mills, Jerry Corbett, Thaddeus Reown, and Mike Restivo, was instrumental in keeping the experiment on track and maintaining the test rig ready, from instrumental calibration to around-the-clock testing. A special thanks is in order to all those individuals just mentioned for the long hours they invested in the experiment, which at times disrupted their family life. The Lab supervisor, Susan Hatcher, is to be commended for keeping us safe, even when things seemed to be the most hectic. I would also like to thank Tim Steeper and Mike Williams for their assistance with the test and with providing the slurry simulant. The management of Dan Burns and Steve Wach made this task's successful completion a sure thing. Thanks is extended to Hector Guerrero, and Dan Burns who had the unenviable task of reviewing this report and to Linda-Lee DiVecchia who did a wonderful job of threading all the many pages into a usable form. Finally, I would like to thank my customer from the River Protection Project – Waste Treatment Plant Project, Paul Townson, for his support, which made this work possible.

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## LIST OF ACRONYMS

ADS	Analytical Development Section (part of WSRC/SRTC)
AN-102	Department of Energy Hanford Site Tank 241-AN-102
AN-102R2	Radioactive cold slurry simulant of AN-102 that was revised twice (R2) to be a better match to the actual radioactive waste. It was the principal simulant used for this test.
AN-107	Department of Energy Hanford Site Tank 241-AN-107. A simulant of this waste was used to precondition the cross-flow filter before testing began with AN-102R2
BC	Baseline Conditions (see Fig. 17)
BNI	Bechtel National, Inc.
CFD	Computational Fluid Dynamics
cP	Centipoise
cSt	Centistoke
CUF	Cells Ultrafiltration facility (bench-top cross-flow filter used with both radioactively cold and hot wastes)
°C	Degree Centigrade (or Celcius)
$\rho$	density, g/ml
D	Diameter
DF	Decontamination Factor: (Slurry Molarity / Filtrate Molarity)
DIF	Deionized and Filtered (0.1 micron) Water
DOE	United States Department of Energy
dP	Differential Pressure
ft	Foot
$\gamma$	Shear Rate, sec <sup>-1</sup> (Rheology Parameter)
i.d. or ID	Inside Diameter
IS	insoluble solids
in.	inch
hr	Time: Hour
HLW	High Level (Activity) Waste
l or L	Liter
LAW	Low (Level) Activity Waste
$\mu$	Dynamic Viscosity, cP, (Rheology Parameter)
$\mu_0$	Consistency or Plastic Viscosity, cP, (Rheology Parameter)
NOC	Newly Optimized Conditions (see Fig. 17)
m	Meter
M	Molar
min	Time: Minute
ml or mL	Milliliter
mm	Millimeter
nominal	The word “nominal” for a filter rating is a vague term because its meaning is manufacturer dependent. Further, a “nominal” rating does not give an exact size to a filter medium, but rather an approximation to the expected performance of a filter. In the case of Mott, a nominal rated 0.1- $\mu$ m filter means that approximately 95% of particles greater than 0.1 $\mu$ m will not pass the filter.
NTU	Nephelometric Turbidity Unit

**LIST OF ACRONYMS**  
**(Continued)**

Pa	Pascal
PJM	Pulse Jet Mixer
PSD	Particle Size Distribution
psi	Pounds Per Square Inch
psig	Pounds Force Per Square Inch Gauge
psid	Pounds Force Per Square Inch Difference
PXU	Pilot-scale Cross-flow Ultrafiltration facility
QA	Quality Assurance
Re	Reynolds number, $Re = \rho VD/\mu$ , non-dimensional number
RPP	River Protection Project (at the DOE Hanford Site)
o.d. or OD	Outside Diameter
s or sec	Time: Second
SRTC	Savannah River Technology Center (part of WSRC)
Sr/TRU	Strontium/Transuranic
Std Dev	Standard Deviation
$\tau$	Shear Stress, dynes/cm <sup>2</sup> , (Rheology Parameter)
$\tau_0$	Yield Stress (Shear Stress at Shear Rate = 0), dynes/ cm <sup>2</sup> , (Rheology Parameter)
TS	Total Solids
EDL	Engineering Development Laboratory (part of WSRC/SRTC)
TMP	Transmembrane Pressure (the average pressure drop across the thickness of the filter medium – perpendicular to the slurry flow.)
TRU	Transuranic
TTR	Technical Task Request
UF	Ultrafiltration
ug	microgram
V	Velocity of the slurry flow along the length of the filter tubes
WGI	Washington Group International
WTP	Waste & Immobilization Treatment Plant
WSRC	Westinghouse Savannah River Company

## **1.0 SUMMARY OF TESTING**

### **1.1 OBJECTIVES**

This report discusses the results of cross-flow filter operation in a pilot-scale experimental facility that was designed, built, and run by the Engineering Development Laboratory of the Westinghouse Savannah River Company Savannah River Technology Center. This filter technology was evaluated for its inclusion in the pretreatment section of the nuclear waste stabilization plant being designed by Bechtel National, Inc. The waste treatment plant will be built at the U.S. Department of Energy's Hanford Site as part of the River Protection Project.

The test objectives, which are listed in the task plan (Duignan, 2002a), were to demonstrate using a simulated waste of AN-102R2:

- Separation of insoluble solids
- Filterability during simulant dewatering after precipitation
- Concentration of the simulant to above 15 wt%
- Filterability of the concentrated simulant during a steady-state solids loading
- Washing the slurry

### **1.2 CONDUCT OF TESTING**

The general test matrix was as follows:

- Baseline the filter with water
- Baseline the filter with a standard slurry
- Dewater simulant from ~ 1 wt% to >15 wt% insoluble solids
- Filter simulant at the highest concentration of solids at steady state solids loading
- Wash slurry
- Acid Clean Filter

Four batches of AN-102R2 simulant, precipitated under different conditions, were tested, but only one, Batch 3B, completed all the steps above due to its good filterability. This reports discusses in detail the problems and successes with each of those batches.

### **1.3 RESULTS AND PERFORMANCE AGAINST OBJECTIVES**

The filter element under study was manufactured by the Mott Metallurgical Corporation in Connecticut. The filter unit was made of seven 316 stainless steel sintered metal tubes. Each tube was a nominal-rated 0.1-micron filter with an inside diameter of 0.5 inch, an outside diameter of 0.625 inch, and a porous length of 90 inches. These dimensions give an active filter surface area of 6.7 ft<sup>2</sup>. At the time of this task these aforementioned dimensions were given as prototypic; therefore, each filter tube was considered full size to the filter, which

would be built for the plant. Only the number of tubes was expected to change. [Current plans call for 241 tubes (~231 ft<sup>2</sup> of filter area) in each of the cross-flow filter bundles of which there will be 3 bundles in series for each of the two filtration flow loops.]

The filter was tested with a simulated nuclear waste of Tank 241-AN-102, which is referred to as an Envelope C waste. The recipe for the simulant was developed by the SRTC Waste Treatment Technology Department and the simulant was procured and prepared by EDL personnel specifically for this task. The supernatant portion of the simulant contained numerous inorganic salts, soluble organics, had a pH  $\approx$  12, and a sodium molarity of approximately 6.0 M. Insoluble solids were added to the supernatant to simulate entrained solids in the real waste. The particle size distribution was designed to be bimodal; one group ranged from 1 to 2 microns and the other ranged from 5 to 10 microns. Finally, to this slurry three precipitating agents were added: Sodium Hydroxide, Strontium Nitrate, and Sodium Permanganate, which raised the pH to approximately 14. After all the additions, the insoluble solids loading started at 0.8 to 1.6 wt% and after dewatering it was eventually raised to about 25 wt%. The total solids ranged from as low as 28 wt% for post-washed slurry to as high as 49 wt% for the pre-washed slurry. At 25°C and a solids loading of 1.0 wt%, this slurry had a density of approximately 1.29 g/mL, a viscosity of 4 cP, and Newtonian rheological characteristics. However, as the solids loading increased, a yield stress was present. At the highest loading, the slurry rheology showed time dependent characteristics of a thixotropic fluid, e.g., certain paints, inks, and foods like ketchup. The flow conditions for the test varied as follows: Axial slurry velocities ranged from 7 ft/s to 15 ft/s (2.1 m/s to 4.6 m/s) and transmembrane pressures ranged from 20 psid to 60 psid (138 kPa to 414 kPa) at a temperature of 25°C.

### **1.3.1 Filter Baseline and Acid Cleaning**

Before each test the filter was tested with inhibited (0.01 M NaOH) water and a standard slurry (5 wt% SrCO<sub>3</sub>) to baseline its operation. After each test the filter was acid cleaned with 2 M HNO<sub>3</sub> and retested with water and the standard slurry. The summary results are:

#### **1.3.1.1 Inhibited Water**

Inhibited water tests before and after each slurry test indicated a return to “clean” filter fluxes.

#### **1.3.1.2 Standard Slurry**

The use of a standard slurry to show a filter’s return to cleanliness was confounded by the level of cleanliness of not just the filter but of the entire filter system. Unless the entire filtration loop was clean, then determining the cleanliness of just the in-line filter may not be possible.

### 1.3.1.3 Acid Cleaning

The method used, two 90-minute circulations of 2 M nitric acid, cleaned most of the solids away from the filter but there were always some remaining solids. The complex wastes may need more targeted cleaning to remove all waste remnants

### 1.3.2 Solids Separation

With respect to insoluble solids separation the results were excellent. Turbidity for all filtrate samples measured considerable less than 1 NTU and generally ranged from 0.1 to 0.3 NTU.

### 1.3.3 Filterability

With respect to filterability, the results ranged from unacceptable to good as compared to the target mean filtrate flux of 0.020 gpm/ft<sup>2</sup> at 15 wt% insoluble solids and as explained below.

#### 1.3.3.1 Dewatering

Under the flow conditions of a slurry velocity of 12.0 ft/s and a transmembrane pressure of 40 psid (3.7 m/s and 275 kPa), the observed filtrate flux during dewatering ranged from one unacceptable test (Batch 3C) to three acceptable tests (Batches 3A, 3B, and 4A, with 3B giving the best results) when compared to the target mean filtrate flux of 0.020 gpm/ft<sup>2</sup>. The results are summarized in Fig. 75, which is reproduced here for convenience. There can be many reasons why the filtration results varied among the batches, some of which are discussed herein, but the largest difference was between the poor filterability of Batch 3C, which had the lowest concentration of free hydroxide, and the good filterability of Batch 3B, which had a higher free hydroxide concentration and was precipitated at a higher temperature, i.e., 50°C. The filterability of remaining two batches fell between the extremes. They both had the higher level of free hydroxide, but Batch 3A was precipitated at the lower temperature of 25°C and Batch 4A used a pulse jet mixer during precipitation instead of an impeller agitator.

Batch Number	Precipitation Conditions*	Precipitation Mixing	Precipitation Temp, °C	Final Conc of Free OH <sup>-</sup>	Final Conc of SrNO <sub>3</sub>	Final Conc of NaMnO <sub>4</sub>	Filter Flux (gpm/ft <sup>2</sup> )			Location
							at 2 wt%	at 15 wt%	Avg to 15 wt%	
3C	NOC =	well	25	0.3 M	0.03 M	0.03 M	0.019	0.005**	0.010***	(Fig. 38)
3B	BC =	well	50	1.0 M	0.075 M	0.050 M	0.066	0.024	0.049	(Fig. 40)
3A	BC @ 25°C =	well	25	1.0 M	0.075 M	0.050 M	0.052	0.019	0.020	(Fig. 42)
4A	BC w/PJM =	PJM	50 > 25	1.0 M	0.075 M	0.050 M	0.021	0.014	0.020	(Fig. 44)

\* These are the dewatering results and the precipitation conditions nomenclature can be found in Fig. 17  
 \*\* Batch 3C only went to 8.3 wt% but flux was constant from 5 to 8.3 wt%  
 \*\*\* Batch 3C average assumes the filtrate flux continues at 0.005 gpm/ft<sup>2</sup> to 15 wt%

Figure 75. Dewatering results

### **1.3.3.2 Steady State**

Steady state tests at high concentrations of insoluble solids (>20 wt%) indicated that slurry axial velocity is an important parameter in filtrate flux, while the transmembrane pressure is less so. Flow parameters of 12 ft/s and 40 psid are reasonable. With hourly backpulsing the filter depth fouling decreased the filtrate flux by approximately 60% after 24 hours of continuous operation.

### **1.3.4 Washing**

A test to wash slurry with an equal volume of water showed good removal of sodium; approximately 65%.

### **1.3.5 Scaling**

Comparisons made with the small amount of existing data from similar small and pilot-scale tests show that relating small to plant-scale operation may not be possible.

### **1.3.6 Recommendations**

It is recommended that:

1. Axial slurry velocity be greater than 11 ft/s and the transmembrane pressure more than 30 psid. Higher velocities will filter slurries faster, but higher transmembrane pressures will not increase filter fluxes significantly.
2. Baseline conditions (BC in Fig. 75) be used when precipitating Envelope C-type wastes like AN-102 to obtain the best filterability.
3. Backpulsing be minimized because increasing backpulsing increases depth fouling of the filter and thus reduces time between acid cleanings.
4. A more effective cleaning method be determined than the use of 2 M nitric acid, alone.

## **1.4 QUALITY REQUIREMENTS**

This work was conducted in accordance with the RPP-WTP Quality Assurance requirements specified for work conducted by SRTC as identified in DOE IWO MOSRLE60. Researchers followed the WSRC QA program, which has been approved by WTP, and the WSRC QA Management Plan (WSRC-RP-92-225). The program applied the appropriate QA requirements for this task, as indicated by the QA Plan Checklist in section IX of the Task Technical and Quality Assurance Plan (Duignan, 2002a).

Analytical sample labeling and tracking complied with established procedures (WSRC Manual L1, Procedure 7.15). The SRTC Analytical Development Section (ADS) conducted all analyses using the routine level QA program. Calibrated measuring and test equipment

were utilized for all flow rate, pressure, and temperature measurements on the Pilot-scale Cross-flow Ultrafiltration Facility.

The Task Technical & QA Plan provided the quality requirements for this work (Duignan, 2002a). NQA-1 1989, part 1, Basic and Supplementary Requirements and NQA-2a 1990, Part 2.7 were applied as appropriate.

## **1.5 ISSUES**

Originally, this task was planned to filter only two slurry simulant batches, i.e., Batches<sup>†</sup> 3 and 4. Those batches only differed by how well they would be mixed during the precipitation process. Batch 3 was to be well mixed with a mechanical agitator and Batch 4 was to be mixed with pneumatically driven pulse jet mixer (PJM). Previous work (Duignan, 2000b) with Envelope C-type simulants using well mixed baseline precipitation conditions has already been shown to attain an acceptable level of decontamination and filterability. Since RPP-WTP has been designed to use PJM to agitate the precipitating wastes; therefore, it was important to show its effects on decontamination and filterability. Unfortunately, the Batch 3 test demonstrated very poor filterability, which necessitated changes to the precipitation process and thus increased the number of tests to four batches<sup>‡</sup>, i.e., 3C, 3B, 3A, and 4A.

## **2.0 CD-ROM ENCLOSURES**

The report is contained on a CD-ROM in the following file format:

Microsoft Word, Version 97  
Adobe Acrobat, Version 5.0

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<sup>†</sup> Batches 1 and 2 were strictly related to the precipitation task (Steeper and Williams, 2003) and were not part of this task.

<sup>‡</sup> The batch numbering nomenclature is arbitrary and the sequence shown above is the chronological order in which the batches were tested. Batch 4 is referred to 4A because a 4B was planned in the event Batch 4A indicated that more testing was needed. Batch 4B was not required.

## 3.0 DISCUSSION

### 3.1 INTRODUCTION

Bechtel National, Inc. (BNI) has been contracted by the Department of Energy (DOE) to design a Waste Treatment and Immobilization Plant (WTP) to stabilize liquid radioactive waste that is stored at the Hanford Site as part of the River Protection Project (RPP). Because of its experience with radioactive waste stabilization, the Savannah River Technology Center (SRTC) of the Westinghouse Savannah River Company (WSRC) is working with BNI and Washington Group International (WGI), to help design and test certain parts of the waste treatment facility. One part of the process is the separation of radioactive solids from the liquid wastes by cross-flow ultrafiltration. This task tested a cross-flow filter, prototypic in porosity, length and diameter, with a simulated radioactive waste, made to prototypically represent the chemical and physical characteristics of a Hanford waste in tank 241-AN-102 (AN-102) and precipitated under prototypic conditions.

This technical baseline research and development work was initiated by a Technical Task Request (TTR) (Duignan, 2002a) that was issued in April of 2002. This TTR is a result of a WGI test specification (Townson, 2002a) to test a simulated radioactive waste in an existing pilot scale cross-flow filtration system in the Engineering Development Laboratory (EDL) of SRTC. With the initial documentation in place (Blunt, 2002; Duignan, 2002a,b,c,d; Edmunds, 2002) the task began by first preconditioning the filter. Since the first test would be using a brand new filter it was subjected to the flow of an archived simulant (AN-107) in order to attain a "used" filter state, which would be more prototypic of actual plant daily use. That is, a new filter could give falsely high filtrate flux rates, which would not be conservative. The preconditioned filter was then used to filter the AN-102R2 simulant. This waste simulant, along with other complexant containing wastes, like the preconditioning simulant, is referred to as Envelope C (see Eibling and Nash (2001) for a description of the entire range of radioactive wastes and their simulants). How well this simulant matched the actual waste is beyond the scope of this task and not addressed; it was used as given input. However, details can be found in Steeper and Williams (2003), which is a report that deals with the preparation and precipitation of AN-102R2. Finally, to this simulant several compounds were added to simulate the step of precipitating Strontium and Transuranic constituents. After precipitation, the simulant was ready for filtering, which began the test.

The simulant of AN-102R2 was the second in a series of two Envelope C-type wastes that have been tested. The first (AN-107) has been previously tested by Duignan (2000b) and these two tests followed an Envelope A (AN-105) simulant test (Duignan, 2000a). This report deals solely with the AN-102R2 simulant.

The chosen filter was manufactured by the Mott Metallurgical Corporation to meet RPP-WTP specifications (Townson, 2002a), as follows:

- 7 filter tubes with each having an inside diameter of 0.5-inch
- 90-inch porous length for each filter tube and made of stainless steel
- Nominal rated 0.1 micron filter element (the List of Acronyms explains 'nominal')

and the pilot test rig was designed to have the following:

- Maximum axial velocity through filter tubes of 4.6 m/s (15 ft/s)
- Maximum transmembrane pressure (TMP) of 60 psid
- Maximum axial velocity to be achievable at the maximum TMP
- Instrumentation to monitor the axial velocity, the filtrate flow rate, the TMP, and the slurry temperature
- All materials to be compatible with the high-caustic simulants and the 2 M nitric acid cleaning solution

All specifications were met or exceeded.

A summary of EDL task activities is as follows:

- Draft WGI Test Specification Received – May 8, 2001
- Order placed (P.O. AC26481A) for filter from Mott Incorporated – May 17, 2001
- Arrival of the filter from Mott Incorporated – August 15, 2001
- Approved WGI Test Specification Received – January 16, 2002
- WSRC Task Technical & Quality Assurance Plan Approved – April 9, 2002
- Principal shakedown activities began – October 1, 2002
- Test Procedure Approved – September 5, 2002 (Revision 0)
- Activities for preconditioning filter with AN-107 – September 9-29, 2002
- Activities for AN-102R2, Batch 3C test – September 30 - October 17, 2002
- Activities for AN-102R2, Batch 3B test – October 21 – November 5, 2002
- Activities for AN-102R2, Batch 3A test – November 6 – November 26, 2002
- Activities for AN-102R2, Batch 4A test – February 12-18 & March 12-26, 2003
- Final test activities (post calibrations) ended – April 15, 2003
- Draft final report completed and sent for review to WGI – May 14, 2003

## **3.2 EXPERIMENTAL**

### **3.2.1 Equipment**

The equipment assembled for this task was done to conform to the Task Plan (Duignan, 2002a). To facilitate understanding of the experimental equipment an explanation of the salient features follows.

### 3.2.1.1 Test Rig

Figure 1 is a partial drawing (Restivo, 2003) of the as-built test rig and Fig. 2 is a simplified schematic of the test rig. The facility stands approximately 25-feet tall and is serviced by a two-level mezzanine. The test rig is taller than the 90-inch tall filter element because it originally was used to test a 10-foot tall filter (Steimke, 1994). Several modifications were made in order to install the current cross-flow filter. The entire test rig was made of 300 series stainless steel with the majority being of 304 stainless steel.

The test rig is made up of three basic flow loops:

1. Slurry loop, which contains the filter and its housing and serves as the primary flow path for circulating slurries. This loop has an internal volume of approximately 26 liters, excluding the reservoir tank. It is made of primarily\* 1.5-inch sch 40 pipe, which has an inside diameter of 1.610 inches.  
[\*Some sch10 pipe was used, which has an inside diameter of 1.682 inches.]
2. Filtrate loop, which begins at the filter housing, allows the separated filtrate liquid to flow through the backpulse pulse pot before circulating back to the slurry reservoir to close the circuit. This loop has an internal volume of approximately 15 liters. It is made of primarily\* 0.375-inch tubing.  
[\*The pulse pot is made from 6-inch sch 80 pipe. The backpulse will be described in more detail after this section.]
3. Cleaning loop was not used for this test but is mentioned to point out valves that exist, but were not used, i.e., V8, V10, V12, and V19.

Two other flow circuits that are subsections of the other loops are the recirculation and the backpulse loops:

1. The recirculation loop is part of the slurry loop (by using valve V6) and is used to better control the slurry flow. The recirculation loop helps to increase mixing and to maintain a well mixed slurry.
2. The backpulse loop is part of the filtrate loop and stands ready to reverse the flow of filtrate. A pulse forces filtrate back through the seven filter elements in order to knock off built-up slurry cake on the inside diameter of the porous tubes. [The loop underwent significant changes to make it more prototypic to planned WTP operation; therefore, a more detailed explanation of the modified backpulse loop follows this section.]



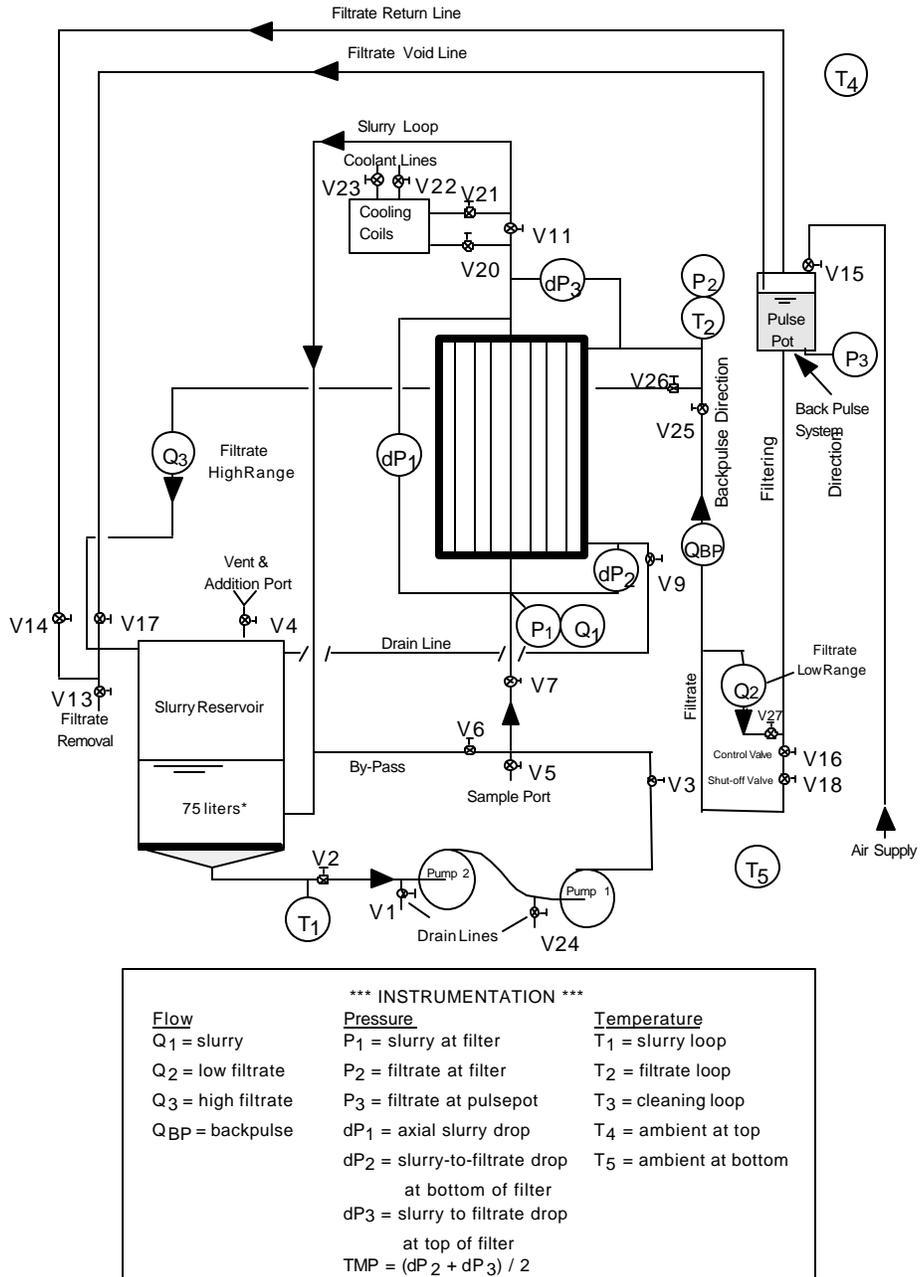


Figure 2. Schematic of the Pilot-scale Cross Flow Ultrafiltration Test Facility

The test rig is controlled through a series of valves, which are described below:

- V1: Drains slurry from the test rig at pump 2.
- V2: Isolates the slurry reservoir from the pumps
- V3: Isolates the slurry loop from the pumps
- V4: Allows liquid to be introduced to the slurry reservoir
- V5: Allows slurry to be sampled (not used for this test)
- V6: Recirculates slurry to the reservoir
- V7: Directs slurry to the filter; 3-way valve
- V8: Not in use – see below
- V9: Drains the filtrate loop
- V10: Not in use – see below
- V11: Controls the slurry flow downstream of the filter
- V12: Not in use – see below
- V13: Sample port for filtrate
- V14: Shut off for filtrate return line
- V15: Allows air to pressurize the pulsepot
- V16: Preset pressure drop for backpulse filtrate line
- V17: Allows liquid evacuation of pulsepot in preparation for backpulsing
- V18: Actuates a backpulse
- V19: Not in use – see below
- V20: Upstream slurry flow to heat exchanger
- V21: Downstream slurry flow from heat exchanger
- V22: Upstream coolant flow to heat exchanger
- V23: Downstream coolant flow from heat exchanger
- V24: Drains slurry from the test rig at pump 1
- V25: Shut low-flow filtrate line when high filtrate flows are needed (e.g. water)
- V26: Directs high filtrate flow to slurry reservoir and flow meter
- V27: Shuts filtrate flow to low-flow meter during a backpulse

Note: Valves V8, V10, V12, and V19 are for the cleaning loop, which was not used.

To circulate slurries in the test rig two 10 hp Galigher centrifugal pumps were used. The impeller and impeller housing were made from EPDM to be compatible with both the pH=14 slurry to be tested and the 2 M nitric acid cleaning solutions. The two pumps were used in series on the slurry loop to attain a head of 70 psig at 60 gpm (~ 4.6 m/s in each filter tube).

### **3.2.1.2 Cross Flow Filter**

The heart of this entire experimental task was the cross-flow filter element that was to be tested to define its operational characteristics under required flow conditions when using the Sr/TRU precipitation simulant. There were several candidates that could have been used for this test but due to availability and past experience in robust designs, a Mott filter was chosen. The specifications for the filter unit were:

Material: 316 stainless steel (sintered metal)  
Porosity: nominal rated 0.1 micron  
Length: 90 inches  
Diameter: 1/2-inch I.D., 5/8-inch O.D.  
Number: 7 tubes

The unit which was received from Mott met the requirements. Figure 3 and 4 show the 90-inch length was made from four 22.5-inch lengths that were welded together.



Figure 3. 7-tube bundle of a nominal rated 0.1 micron filter, 1.2" i.d., 5/8" o.d., 90" long



Figure 4. Adjoined filter tube sections

Besides the inter-tube weldments, Fig. 5b, the 7 tube bundle was welded together with the tube sheets, Figs 5a, d, and extra support was made with stabilizing plates and supporting solid metal 1/4-inch rods which ran the length of the tube bundle, Fig. 5c.

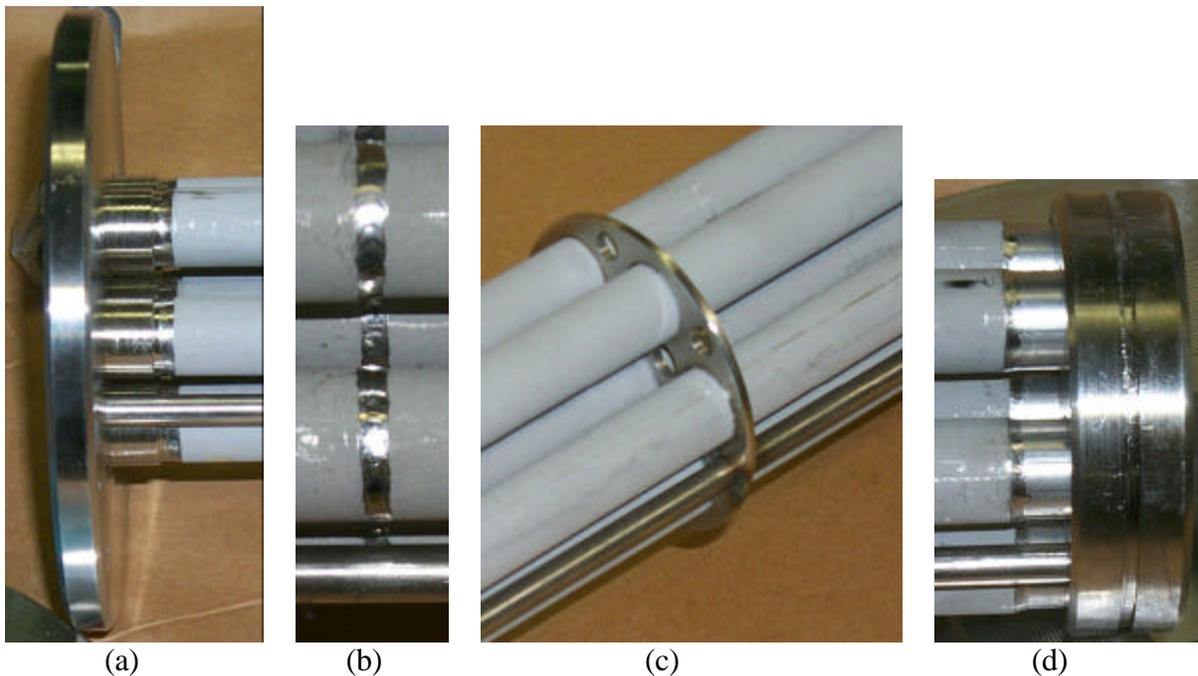


Figure 5: (a) Large-tube sheet, (b) tube-to-tube weldment, (c) tube supports, (d) small-tube sheet.

The stainless steel sintered surface has a fairly robust construction. Figure 6 shows an enlargement of two different pore-size filter elements, 0.5 and 100 microns. (Mott did not

have a picture of a nominal rated 0.1 micron filter but stated that the appearance is identical to the larger sizes.)

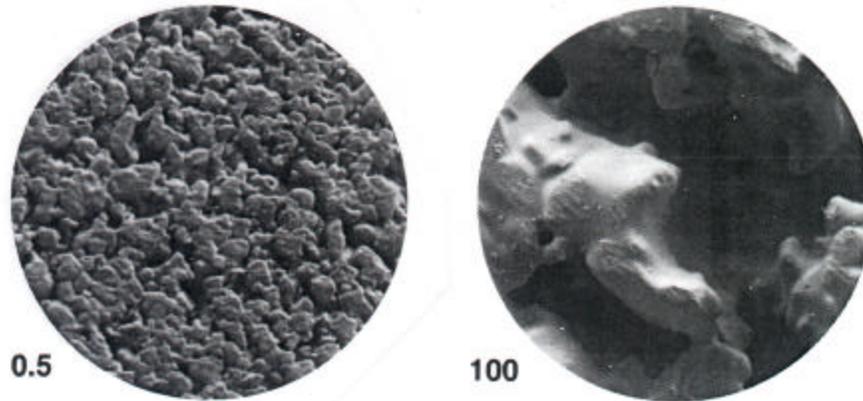


Figure 6. Magnified views (approximately 150x) of surfaces of two different pore-size rated Mott filters (the number to the left of each figure is the pore-size rating in microns)

When the test rig is in operation, slurry enters the porous tubes at the small tube sheet, Figs. 5d and 7b, and exits the tubes at the large tube sheet, Figs. 5a and 7a. Each tube sheet is sealed to a 1.5-inch to 3-inch plenum.

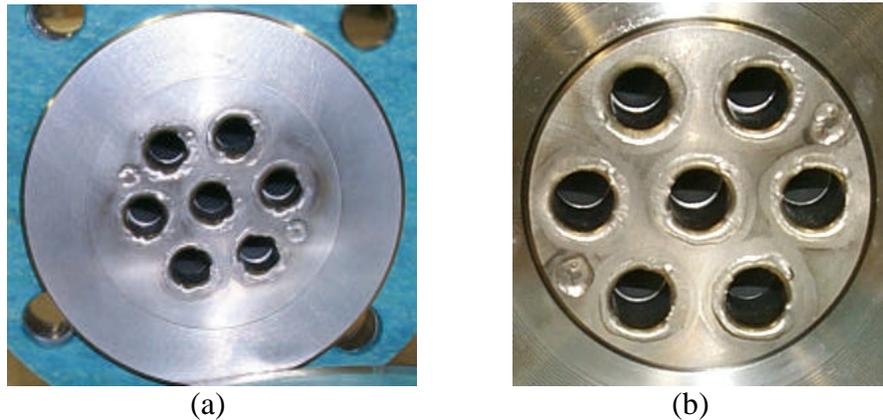


Figure 7: Tube-sheet profiles (a) Downstream (b) Upstream

The tube housing, Fig. 8, was made from a 3-inch schedule 10 pipe with two pipes connected at either end to remove filtrate. For this test the filter unit was oriented vertically in the test rig, see Figs. 1, 2, and 8. The tube bundle sat in the housing such that the large tube sheet, Figs. 5a and 7a, was secured to the top flange of the housing; this tube sheet also supported the weight of the assembly. The smaller, lower, tube sheet, Fig. 5d and 7b, was able to pass through the housing and separated the slurry side of the flow channel from the filtrate side with an “O” ring between the outer perimeter of the lower tube sheet and the inside diameter of the filter housing.



Figure 8. Installed 90-inch tall cross-flow filter housing

### 3.2.1.3 Backpulse System

On March 20, 2002 the RPP-WTP customer requested that the backpulse system be changed from the piston-type, used for previous tests (Duignan, 2000a, b), to a pneumatic-type that would be more prototypic of the current RPP-WTP design. That is, a filtrate system, which is normally liquid solid, would introduce a gas into a small vessel, called a pulse pot to evacuate some of the liquid so that it can then be pressured. When ready, a valve is opened very fast to allow the pressurized liquid to flow back, “pulsed,” into the crossflow filter. Figure 9 is a schematic of the RPP-WTP backpulse system and Fig 10 is a simplified operational procedure.

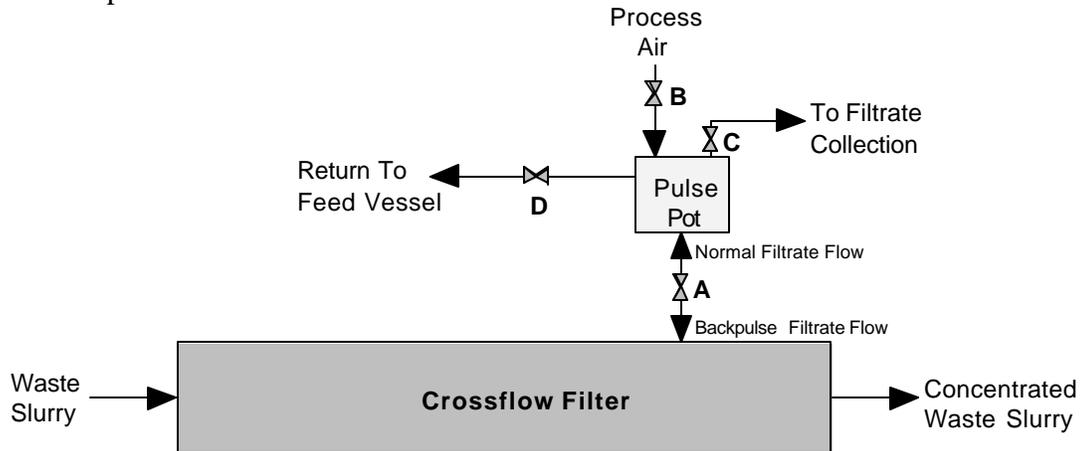


Figure 9. Planned RPP-WTP backpulse system

V / Mode V / Valve >>	A	B	C	D
Filtering	Open	Closed	Open	Closed
Stop Filtration	Closed	Closed	Closed	Closed
Void Pulsepot	Closed	Open	Closed	Open
Pressure Pulsepot	Closed	Open	Closed	Closed
Isolate Pulsepot	Closed	Closed	Closed	Closed
Back Pulse	Open	Closed	Closed	Closed
Resume Filtration	Open	Closed	Open	Closed

Figure 10. Procedure to operate backpulse system

The planned plant backpulse system is designed to have a:

1. Backpulse pressure 30 psi above the slurry pressure at the filter.
2. Pressure drop from the pulse pot to the filter of 10 psid during a backpulse.
3. Pulse liquid volume of at most  $2/3^{\text{rds}}$  of the total pulse pot volume.
4. Volume of the pulse liquid enough for efficient back pulsing.  
(This volume was stated to be a minimum of 70% of the volume of the porous tube walls.)
5. Back pulse cycle duration of 5 to 10 seconds.

The pilot test rig was changed to meet the above requirements. However, what could not be matched were the dynamic characteristics of the plant system. That is, because of differences

in scale, and therefore mass, the momentum of the plant system will be considerably different. The operation of the pilot system followed the sequence shown in Fig. 10 and it was designed to meet all five criteria above. For the volume of pulse liquid, past experience (Duignan, 2000a, b) has shown an effective volume to be 0.036 gallons per square foot of inside area of the cross-flow filter. Therefore, the volume used was:

$$(0.036 \text{ gal/ft}^2) \times (7 \text{ tubes}) \times \pi [(0.5 \text{ inch}/12)] \times 90 \text{ inches}/12 = 0.25 \text{ gal.}$$

By using the 4<sup>th</sup> criterion above the volume would be:

$$70\% \times [(7 \text{ tubes}) \times \text{volume of porous tube wall}] =$$

$$70\% \times [(7 \text{ tubes}) \times \pi/4 [(0.625 \text{ inch}/12)^2 - (0.5 \text{ inch}/12)^2] \times 90 \text{ inches}/12 \times 7.48 \text{ gal/ft}^3] = 0.21 \text{ gal.}$$

Therefore, using 0.25 gallon would be conservative to effectively removing the filter cake.

Designing for the 10 psid pressure drop from the pulse pot to the filter housing, during the backpulse, was a little harder to obtain and, therefore, the pilot system was made to have an adjustable pressure drop using a valve. Several tests were done before the experiment began to estimate how to set that valve so that the backpulse pressure drop was near the target 10 psid. To illustrate the backpulse system, Figure 11 shows a subset of Fig. 2 and valve letters corresponding to those in Fig. 10 are included to compare operation. Note that for the pilot system, the voiding line, leading to valve D, is through the top of the pulse pot instead of the side, Fig 9, in order to change the void space size if necessary.

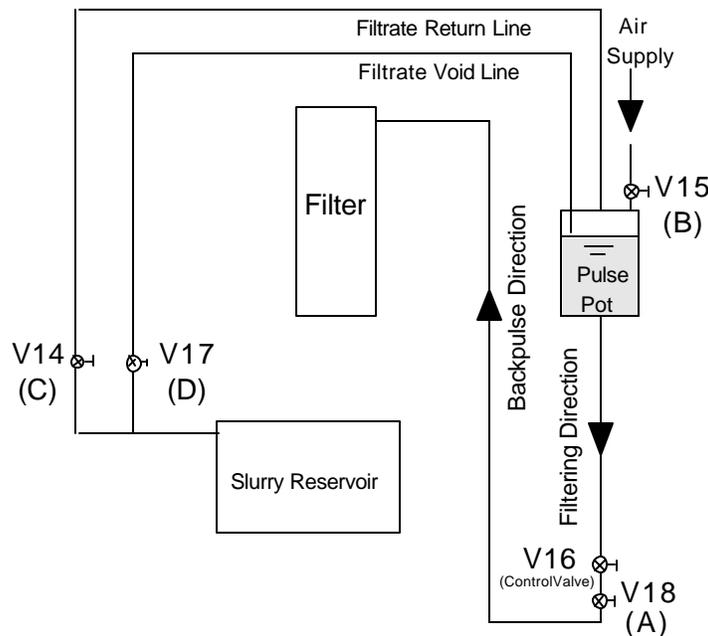


Figure 11. Pilot test rig backpulse loop, see also Fig. 2

To see how the system of Fig. 11 operates and how the pressure drop control valve, V16 was set see Fig. 12, which shows the data from one of the many shakedown tests done with water. The instrumentation indicated in Fig. 12 can be found in Fig. 2. It shows the slurry (water) pressure in the filter to be approximately 50 psig; therefore, the air overpressure (P3) was set at 90 psig, or approximately 30 psig at the filter housing when considering the pressure drop across the backpulse system at the highest backpulse flowrate. That is, as seen in Fig. 12, the backpulse flowrate peak after 2 seconds from opening valve A, at about 0.5 gpm/ft<sup>2</sup> and the backpulse pressure drop, i.e., P3-P2, was at approximately 10 psid.

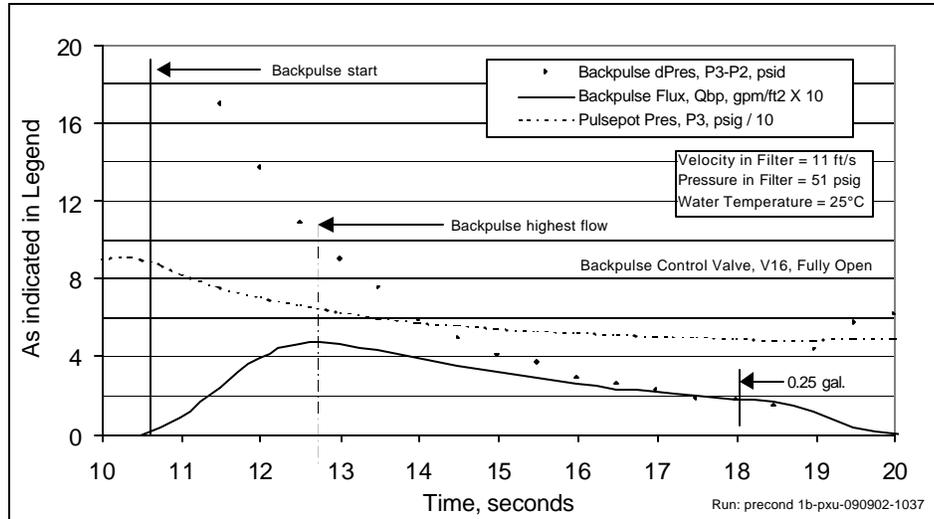


Figure 12. Pilot test rig backpulse operation with water

Figure 12 data show the sequence of events as indicated in Fig. 10, with the valves shown in Figs. 2 and 11:

1. Stop Filtration: Prior to data taking – all valves were closed.
2. Void Pulsepot: Prior to data taking – only valves B and D are open.
3. Pressurize Pulsepot: Prior to data taking – only valve B is left open.
4. Isolate Pulsepot: 0-10.5 seconds – all valves were closed.
5. Back Pulse: 10.5-18 seconds – valve A opened as fast as possible, then closed at some predetermined time, see Fig. 11.
6. Resume Filtration – valve C is opened, followed by opening valve A slowly.

Note that in step 6 valve C is opened first to relieve any residual pneumatic pressure and prevent further, albeit weak, backpulsing. Valve A is opened very slowly, over 60 seconds to uniformly form the filter cake when reestablishing filtrate flow.

As Fig. 12 indicates, the backpulse control valve was fully opened; therefore, this would be the position set for future slurry tests. Many tests were done to determine the number of seconds to leave the backpulse flow open before the 0.25 gallon of filtrate passed through the filter wall. When slurry was introduced into the test rig, the backpulse conditions were checked again. By trial and error the times in Fig. 13 were used to obtain 0.25 gpm of pulsed

filtrate for each run, which must change due to pressure of the slurry in the filter and thus leading to different air overpressures, leading to different values of backpulse flowrates.

Pressure at the filter (P1), psig	10	20	30	40	50	60	70
Duration of Pulse, seconds	9	11	12	14	15	17	18

Figure 13. Pilot test rig backpulse duration (time to hold valve A open)

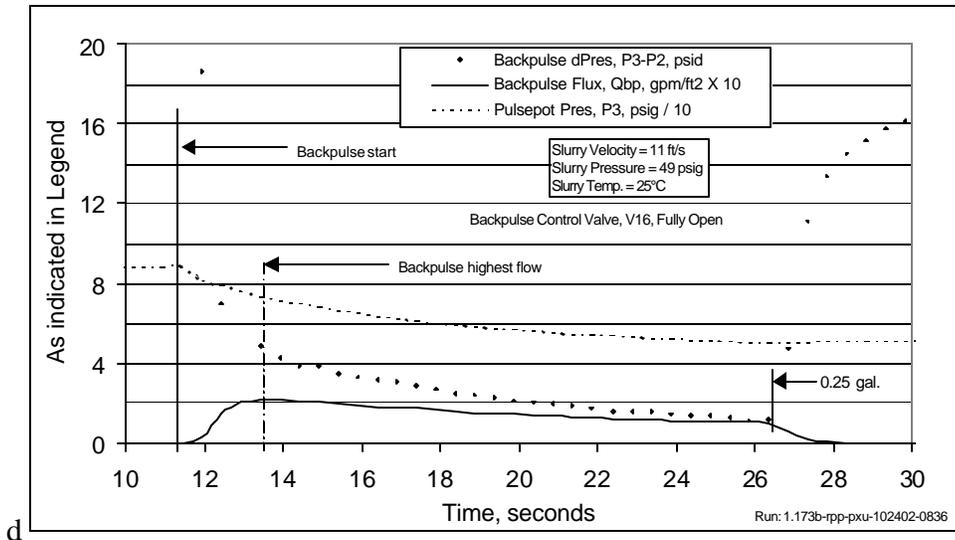


Figure 14. Pilot test rig backpulse operation with AN-102R2, Batch 3B

Figure 14 backpulse results were taken during one of the slurry tests (AN-102R2, Batch 3B) and indicates different results from those for water, basically because the slurry filtrate was 4 times more viscous than water. The peak backpulse flowrate occurred at almost the same time period as water, i.e., 2 seconds, but the rate only reached just under one half that of water. Moreover, at the peak flowrate, the backpulse system pressure drop was also about one half that of water, i.e., 5 psid. The times at which 0.25 gallon of filtrate passed back through the filter can be compared because both of the tests shown in Figs. 12 and 14 were done at a filter pressure of 50 psig. The water took 7.5 seconds and the slurry took 15 seconds. As can be verified in Fig. 13, the times shown are for slurry operation. Even though the backpulse system only presented a pressure drop of 5 psid at the peak filtrate flowrate, valve V16 was left open for all tests. The actual pressure that will exist in the full-size RPP-WTP backpulse piping will be considerably less than the assumed 10 psid because the project began a design change, making the filtrate flow paths much bigger. It is unlikely that the plant pressure drop will be more than 1 or 2 psid. Besides, if V16 were closed enough to attain a 10 psid it is unlikely that the filtrate momentum would be enough to affect the filter cake. As it is, the filtrate backpulse flowrate was only 0.2 gpm/ft<sup>2</sup> (or only 10 times greater than the target mean filtration rate of 0.02 gpm/ft<sup>2</sup>), which turned out not to be very effective in removing the Envelope C-type simulant filter cake.

### 3.2.1.4 Instrumentation

The measurement equipment used for this experiment was:

5 Type E thermocouples with average accuracies from\* 0.9 to 1.0°C,

6 Variable capacitance pressure transducers with average accuracies from\* 0.05 to 0.40 psi,  
and

4 Magnetic flow meters with accuracies from\* 0.005 to 0.5 gpm.

\*accuracies are a function of the instrument and calibration. The uncertainty introduced through the use of the 16-bit data acquisition system was insignificant (<0.1% reading) and was not included in the values above.

Figure H1, Appendix H, shows several tables which list all those instruments and data acquisition system (DAS) channels for each of the non-thermocouple instruments. The thermocouples had their own dedicated computer card to interface and convert the temperatures properly. The calibration of the DAS was checked and that information can also be found in Fig. H1, which includes tables and graphs that show the results and the transfer functions used for each channel.

From Figs. 1, H1, and H2 the location and the usage of each instrument can be determined, however the following list will better describe the placement and usage of all the measurement instruments:

T1 – A thermocouple located in the exit pipe of the slurry reservoir to measure the slurry temperature on its way to the filter.

T2 – A thermocouple located in the filtrate line at the end of the upper filter housing filtrate exit pipe to measure the filtrate temperature as it leaves the filter housing.

T3 – A thermocouple located in the cleaning loop at the exit of the cleaning loop<sup>†</sup> pump.

T4 – A thermocouple located outside of the top of the test rig to measure ambient temperature.

T5 – A thermocouple located outside at the bottom of the test rig to measure ambient temperature.

For the 6 pressure transducers also refer to Fig. H2 which indicate pressure-line locations as well as their heights.

P1 – A gauge pressure transducer located at the beginning of the filter housing to measure the pressure of the slurry just before entering the filter tubes.

P2 – A gauge pressure transducer located in the filtrate line at the top filter housing filtrate exit pipe to measure the pressure of the filtrate as it leaves the filter housing.

P3 – A gauge pressure transducer located at the bottom of the filtrate pulsepot to measure the pressure applied to produce a backpulse.

dP1 – A differential pressure transducer located across the slurry side of the filter to measure the drop in pressure along the filter tubes.

dP2 – A differential pressure transducer located across filter and housing at the filter to measure the transmembrane pressure at the beginning of the filter.

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<sup>†</sup> The cleaning loop in general was not used for this experiment, therefore its temperature measurement is generally irrelevant.

dP3 – A differential pressure transducer located across filter and housing at the filter to measure the transmembrane pressure at the end of the filter.

[The transmembrane pressure is determined from the average of dP2 and dP3.]

Q1 – A magnetic flowmeter located at the entrance of the filter to measure the slurry flowrate.

Q2 – A magnetic flowmeter located in the filtrate line between the exit of the filtrate housing and pulse pot to measure the low filtrate flowrates. This device was calibrated from 0 to 1.2 gpm (or a filtrate flux of 0 to 0.17 gpm/ft<sup>2</sup>), which covers most of the filtrate flux range expected for slurries.

Q3 – A magnetic flowmeter located in the filtrate line between the exit of the filtrate housing and the slurry reservoir tank, downstream of valve V26 to measure the high filtrate flowrates. This device was calibrated from 0 to 5 gpm (or a filtrate flux of 0.75 gpm/ft<sup>2</sup>), which covers all expected filtrate fluxes. This was used for water and nitric acid tests.

Qbp – A magnetic flowmeter located in the filtrate line between the filtrate housing and the pulsepot to measure the reversed filtrate flowrate during a backpulse. When a backpulse is made flowmeter, Q2, is isolated from the loop.

### **3.2.1.5 Measurement Uncertainty**

Appendix H has all the pertinent information on the uncertainties. The measurement uncertainties (95% confidence level) for the important calculated quantities are:

Slurry Velocity in a Filter Tube	=	V	± 6.2 %
Transmembrane Pressure	=	TMP	± 2.2 %
Temperature Corrected Filtrate Flux	=	Fc	± 5.4 %
Permeability	=	P	± 5.8 %

These number are based on pre- and post-test calibrations of the instruments.

### **3.2.2 Simulated Waste Slurry**

Beside the cross-flow filter, the most important aspect of this experiment was the slurry used to simulate a Hanford Site waste. The waste that was simulated is referred to as Envelope C. Envelope C are radioactive wastes that include tank 241-AN-102 from the Hanford Site, which is made up of organic and other complexants. The simulant used for this task was cold (non-radioactive), but chemically it was made as close as was known to actual waste. Once the base Envelope C simulant was ready for use, it was prepared for filtration by adding several precipitation reagents. Some information on the slurry tested will be given below but the goal of this task was to test filterability of a given waste simulant at a pilot scale and not to determine suitability of the simulant to the actual waste. Information of the actual waste can be found in Urie, et al. (2002), the development of the SRTC simulant can be found in Eibling (2003), and information on the preparation and precipitation of the simulant can be found in Steeper and Williams (2003).

Filterability, notwithstanding, to understand how this experiment was run it is necessary to know the general aspects of the slurries that were tested. This task tested one base simulated waste, which was subjected to four different methods of precipitation. The pilot-scale cross-flow facility was then used to filter each prepared simulant to determine the effect the methods had on filterability. The base simulant was developed by SRTC and it was made of many compounds, Fig. 15. The resulting mixture was deluted to a sodium concentration of 6.0 M.

Base Compound	Formula	Mol Wt	AN-102R2
Aluminum Nitrate	Al(NO <sub>3</sub> ) <sub>3</sub> ·9H <sub>2</sub> O	375.13	4.539E-01 M
Cadmium Nitrate	Cd(NO <sub>3</sub> ) <sub>2</sub> ·4H <sub>2</sub> O	308.48	4.096E-04 M
Calcium Nitrate	Ca(NO <sub>3</sub> ) <sub>2</sub> ·4H <sub>2</sub> O	236.15	9.257E-03 M
Cerium Nitrate	Ce(NO <sub>3</sub> ) <sub>3</sub> ·6H <sub>2</sub> O	434.22	2.411E-04 M
Cesium Nitrate	CsNO <sub>3</sub>	194.91	9.054E-05 M
Cobalt Nitrate	Co(NO <sub>3</sub> ) <sub>3</sub> ·6H <sub>2</sub> O	353.03	3.524E-05 M
Copper Nitrate	Cu(NO <sub>3</sub> ) <sub>2</sub> ·2.5H <sub>2</sub> O	241.60	2.783E-04 M
Ferric Nitrate	Fe(NO <sub>3</sub> ) <sub>3</sub> ·9H <sub>2</sub> O	403.99	5.662E-04 M
Lanthanum Nitrate	La(NO <sub>3</sub> ) <sub>3</sub> ·6H <sub>2</sub> O	433.01	2.097E-04 M
Lead nitrate	Pb(NO <sub>3</sub> ) <sub>2</sub>	331.20	6.784E-04 M
Manganous Chloride	MnCl <sub>2</sub> ·4H <sub>2</sub> O	197.90	4.028E-04 M
Neodymium Nitrate	Nd(NO <sub>3</sub> ) <sub>2</sub> ·6H <sub>2</sub> O	376.36	4.959E-04 M
Nickel Nitrate	Ni(NO <sub>3</sub> ) <sub>2</sub> ·6H <sub>2</sub> O	290.81	5.381E-03 M
Potassium Nitrate	KNO <sub>3</sub>	101.11	3.779E-02 M
Rubidium Nitrate	RbNO <sub>3</sub>	147.48	7.376E-05 M
Zinc Nitrate	Zn(NO <sub>3</sub> ) <sub>2</sub> ·6H <sub>2</sub> O	297.47	5.818E-05 M
Zirconyl Nitrate	ZrO(NO <sub>3</sub> ) <sub>2</sub> ·H <sub>2</sub> O	249.23	1.111E-04 M
EDTA	Na <sub>2</sub> C <sub>10</sub> H <sub>14</sub> N <sub>2</sub> O <sub>8</sub> ·2H <sub>2</sub> O	372.24	7.286E-03 M
HEDTA	Na <sub>3</sub> C <sub>10</sub> H <sub>15</sub> N <sub>2</sub> O <sub>7</sub>	278.26	1.524E-03 M
Sodium Gluconate	CH <sub>2</sub> OH(CHOH) <sub>4</sub> COONa	218.14	5.709E-03 M
Citric Acid	HOC(CH <sub>2</sub> CO <sub>2</sub> H) <sub>2</sub> CO <sub>2</sub> H	192.13	2.038E-02 M
Nitrilotriacetic Acid	N(CH <sub>2</sub> COOH) <sub>3</sub>	191.14	1.042E-03 M
Iminodiacetic Acid	HN(CH <sub>2</sub> CO <sub>2</sub> H) <sub>2</sub>	133.10	2.591E-02 M
Succinic Acid	C <sub>4</sub> H <sub>6</sub> O <sub>4</sub>	118.04	2.346E-04 M
Glutaric Acid	C <sub>5</sub> H <sub>8</sub> O <sub>4</sub>	132.12	3.786E-04 M
Adipic Acid	C <sub>6</sub> H <sub>10</sub> O <sub>4</sub>	146.14	1.288E-03 M
Azelaic Acid	C <sub>9</sub> H <sub>16</sub> O <sub>4</sub>	188.22	4.183E-03 M
Suberic Acid	C <sub>8</sub> H <sub>14</sub> O <sub>4</sub>	174.20	7.949E-03 M
Ammonium Acetate	NH <sub>4</sub> CH <sub>3</sub> COO	77.08	6.162E-03 M
Boric acid	H <sub>3</sub> BO <sub>3</sub>	61.83	2.575E-03 M
Sodium Chloride	NaCl	58.44	1.013E-01 M
Sodium Fluoride	NaF	41.99	6.846E-02 M
Sodium Sulfate	Na <sub>2</sub> SO <sub>4</sub>	142.04	9.953E-02 M
Potassium Molybdate	K <sub>2</sub> MoO <sub>4</sub>	238.14	3.561E-04 M
Sodium Hydroxide	NaOH	40.00	2.927E+00 M
Sodium Phosphate	Na <sub>3</sub> PO <sub>4</sub> ·12H <sub>2</sub> O	380.12	3.476E-02 M
Sodium Tungstate	Na <sub>2</sub> WO <sub>4</sub> ·2H <sub>2</sub> O	329.86	6.903E-04 M
Sodium Metasilicate	Na <sub>2</sub> SiO <sub>3</sub> ·9H <sub>2</sub> O	284.14	2.695E-04 M
Sodium Formate	NaHCOO	68.01	1.416E-01 M
Sodium Glycolate	HOCH <sub>2</sub> COONa	98.01	1.056E-01 M
Sodium Acetate	NaCH <sub>3</sub> COO·3H <sub>2</sub> O	136.08	3.737E-03 M
Sodium Oxalate	Na <sub>2</sub> C <sub>2</sub> O <sub>4</sub>	134.00	3.983E-03 M
Sodium Chromate	Na <sub>2</sub> CrO <sub>4</sub>	161.97	3.663E-03 M
Sodium Carbonate	Na <sub>2</sub> CO <sub>3</sub>	105.99	6.925E-01 M
Sodium Nitrate	NaNO <sub>3</sub>	84.99	9.594E-01 M
Sodium Nitrite	NaNO <sub>2</sub>	69.00	1.086E+00 M
Strontium Nitrate	Sr(NO <sub>3</sub> ) <sub>2</sub>	211.63	3.576E-05 M

Figure 15. Chemical make-up of the AN-102 simulant (AN-102R2)

To the base simulant, a very small amount of other solids, to remain mostly insoluble, were added to represent the entrained solids expected in the real waste, Fig. 16.

Entrained Solid (ES)*	Formula	Mol Wt	Mass %
Aluminum Oxide	Al <sub>2</sub> O <sub>3</sub>	101.96	15.12%
Barium Sulfate	BaSO <sub>4</sub>	233.4	0.02%
Calcium Oxalate	CaC <sub>2</sub> O <sub>4</sub> .H <sub>2</sub> O	146.11	0.13%
Calcium Tungstate	CaWO <sub>4</sub>	287.93	0.11%
Cerium Oxalate	Ce(C <sub>2</sub> O <sub>4</sub> ) <sub>3</sub> .9H <sub>2</sub> O	544.29	0.02%
Chromic Oxide	Cr <sub>2</sub> O <sub>3</sub>	151.99	0.93%
Ferric Hydroxide	FeO(OH)	88.85	0.68%
Lanthanum Oxalate	La <sub>2</sub> (C <sub>2</sub> O <sub>4</sub> ) <sub>3</sub> .10H <sub>2</sub> O	722.03	0.02%
Lead Sulfate	PbSO <sub>4</sub>	303.25	0.08%
Manganese Dioxide	MnO <sub>2</sub>	86.94	0.15%
Neodymium Oxalate	Nd <sub>2</sub> (C <sub>2</sub> O <sub>4</sub> ) <sub>3</sub> .10H <sub>2</sub> O	732.69	0.04%
Nickel Oxide	NiO	74.71	0.01%
Silicon Oxide	SiO <sub>2</sub>	60.09	0.05%
Sodium Carbonate	Na <sub>2</sub> CO <sub>3</sub> .H <sub>2</sub> O	124.01	42.71%
Sodium Fluoride	NaF	41.99	3.15%
Sodium Oxalate	Na <sub>2</sub> C <sub>2</sub> O <sub>4</sub>	134.00	16.10%
Sodium Phosphate	Na <sub>3</sub> PO <sub>4</sub> .12H <sub>2</sub> O	380.12	12.28%
Sodium Sulfate	Na <sub>2</sub> SO <sub>4</sub> .10H <sub>2</sub> O	322.04	8.35%
Zinc Oxalate	ZnC <sub>2</sub> O <sub>4</sub> .2H <sub>2</sub> O	189.45	0.02%
Zirconium Oxide	ZrO <sub>2</sub>	60.09	0.02%
Total* >			100.00%

\* Total ES added to be 0.1 wt% of simulant

Figure 16. Entrained solids added to the AN-102R2 simulant

The combination of the base simulant, Fig. 15, and the entrained solids, Fig. 16, represent the Hanford waste AN-102 that will be treated by the RPP-WTP. The initial treatment is precipitation. For organic-based wastes, like AN-102, three reagents are added to precipitate the strontium and transuranic components to decontaminate the wastes more effectively and to improve the wastes' filterability. Originally, this task was planned to filter only two slurry simulant batches, i.e., Batches<sup>†</sup> 3 and 4. Those batches differed only by how well they would be mixed during the precipitation process. Batch 3 was to be well mixed with a mechanical agitator and Batch 4 was to be mixed with a pneumatically driven pulse jet mixer (PJM). Previous work (Duignan, 2000b)<sup>‡</sup> with Envelope C-type simulants using well mixed baseline precipitation conditions, explained below, has already been shown to attain an acceptable level of decontamination and filterability. Since RPP-WTP has been designed to use PJM to agitate the precipitating wastes; therefore, it was important to show its effects on

<sup>†</sup> Batches 1 and 2 were strictly related to the precipitation task (Steeper and Williams, 2003) and are not part of this task.

<sup>‡</sup> The previous dewatering test with an Envelope C-type waste was done with a simulant of AN-107 from 30 November to 1 December of 1999 and the average filtrate flux was 0.045 gpm/ft<sup>2</sup> over the 28.5 hours of the test.

decontamination and filterability. Unfortunately, the Batch 3 test demonstrated very poor filterability<sup>†</sup>, which necessitated changes to the precipitation process and thus increased the number of tests to four batches<sup>‡</sup>, i.e., 3C, 3B, 3A, and 4A.

The reason the Batch 3 test did not show the same level of acceptable filterability is that the precipitation recipe was changed to minimize the amount of reagents. Those changes are referred to as the newly optimized conditions (NOC). The quantities of precipitating reagents which were previously shown to give good filterability (Duignan, 2000b) for Envelope C-type simulants also produced decontamination factors many times greater than were necessary. Hallen, Brooks, and Jagoda (2000) showed exceptionally high decontamination factors and recommended lowering the concentration of precipitation reagents to minimize the amount of chemicals that would have to be added to the wastes, thus creating more wastes. Those new concentrations are referred to as NOC. Unfortunately, while the NOC did produce acceptable levels of decontamination they had a deleterious effect on filterability. Once the low filtrate flux was obtained with the NOC Batch 3 the test scope was expanded to revisit precipitation with the successful baseline conditions (BC). The next three tests used BC with slight variations on the precipitation preparation in the way of mixing temperatures and agitation. Figure 17 lists the differences among the four batches of AN-102R2 simulant, which were ultimately tested. This report documents the filtering results of each of these batches.

Batch Number	Precipitation Conditions (1)	Precipitation Mixing (2)	Precipitation Temp, °C (3)	Final Conc of Free OH <sup>-</sup>	Final Conc of SrNO <sub>3</sub>	Final Conc of NaMnO <sub>4</sub>
3C	NOC =	well	25	0.3 M	0.03 M	0.03 M
3B	BC =	well	50	1.0 M	0.075 M	0.050 M
3A	BC @ 25°C =	well	25	1.0 M	0.075 M	0.050 M
4A	BC w/PJM =	PJM	50 > 25	1.0 M	0.075 M	0.050 M

Notes

(1) - Condition nomenclature:  
 NOC = newly optimized conditions (*to minimize volume of precipitating reagents*)  
 BC = baseline conditions (*known to obtain good decontamination and filterability*)  
 BC @ 25°C = baseline conditions but precipitated at 25°C  
 BC w/PJM = baseline conditions but mixed with a pulse jet mixer

(2) - Precipitation mixing nomenclature:  
 well = the precipitation solution was considered well mixed with a Lightin A-310 style impeller in a 42-inch diameter baffled tank rotating at 508 rpm (an impeller tip speed of 26.6 ft/s) imparting 4.3 hp/1000 gallons  
 PJM = pulse jet mixer which agitated the solution with pulses of air. The level of mixing is not know, but was less well mixed than with the impeller.

(3) Precipitation Temperature - after the last precipitating reagent was added the mixture was maintained at the listed temperature for four hours before filtration began. Additionally, batch 4A was further mixed another 18 hours as its temperature dropped from 50°C to 25°C before filtration began.

Figure 17. Nomenclature for the four AN-102R2 simulant batches

<sup>†</sup> The dewatering target was to have an average filtrate flux of 0.02 gpm/ft<sup>2</sup> or higher, with a final concentration of better than 15 wt% insoluble solids. As will be seen, the first Batch 3 test resulted in an average flux of 0.011 gpm/ft<sup>2</sup> over 45 hours of dewatering and the slurry was only concentrated to 8.5 wt% insoluble solids.

<sup>‡</sup> The batch numbering nomenclature is arbitrary and the sequence shown above is the chronological order in which the batches were tested. Batch 4 is referred to 4A because a 4B was planned in the event Batch 4A indicated a larger quantity was needed to reach 15 wt% insoluble solids. Batch 4B was not required.

### 3.2.3 Test Procedure/Matrix

Details of the test matrix and procedure that were carried out can be found in the Test Procedure (Duignan, 2002e), but an illustrated matrix is shown as Fig. 18.

Test No.	Test Activity	Trans-membrane Pressure (psid)	Slurry Velocity (ft/s)	Slurry Temp (°C)	Run Time (min.)
1.00A	Water (1)	10	12	25	20
1.00B	Water	20	12	25	20
1.00C	Water	30	12	25	20
1.01A	5 wt% SrCO <sub>3</sub> + Water	10	12	25	20
1.01B	5 wt% SrCO <sub>3</sub> + Water	20	12	25	20
1.01C	5 wt% SrCO <sub>3</sub> + Water	30	12	25	20
1.02	Water Rinse	20	12	25	60
1.03-1.15	Low solids concentration tests are no longer required (2)				
1.16	Dewater to 20 wt% (3)	40	12	25	(4)
1.17	20 wt%	40	12	25	120
1.18	20 wt%	40	12	25	120
1.19	20 wt%	40	12	25	120
1.20	20 wt%	30	9	25	60
1.21	20 wt%	30	13	25	60
1.22	20 wt%	50	13	25	60
1.23	20 wt%	50	9	25	60
1.24	20 wt%	40	12	25	120
1.25	20 wt%	40	7	25	60
1.26	20 wt%	40	15	25	60
1.27	20 wt%	20	12	25	60
1.28	20 wt%	60	12	25	60
1.29	20 wt%	40	12	25	120
Wash	(5)	40	12	30	(6)
1.30	> 20 wt%	40	12	25	(7)
1.31A	Water Rinse	40	12	25	60
1.31B	Acid clean (8)	40	12	25	90
1.31C	Acid clean	40	12	25	90
1.32	Water Rinse	20	12	25	60
1.33A	5 wt% SrCO <sub>3</sub> + Water	10	12	25	20
1.33B	5 wt% SrCO <sub>3</sub> + Water	20	12	25	20
1.33C	5 wt% SrCO <sub>3</sub> + Water	30	12	25	20
1.34A	Water	10	12	25	20
1.34B	Water	20	12	25	20
1.34C	Water	30	12	25	20

Notes:  
 (1) - The water was deionized, filtered with a 0.1-micron absolute filter, then made caustic to 0.01 M NaOH.  
 (2) - Before testing began a test exception (Townson, 2002b) to the test specification was issued to eliminate all low solids concentration tests.  
 (3) - wt% = weight percent of insoluble solids  
 (4) - Run time is the time to dewater the simulant from the low wt% to the final concentration. The only test specification requirement was to run for no less than 12 hours.  
 (5) - The concentrated slurry used for test 1.29 was washed with a volume of water (see note 1) equal to 21/18 x simulant volume. The water volume was broken down into 21 mini-washes.  
 (6) - The wash run time was the time necessary to introduce and remove all 21 subvolumes.  
 (7) - Test 1.30 run time was not fixed. Filtering was to continue until the simulant plugged the filter, or some test rig limit was reached.  
 (8) - 2 M nitric acid was used.

Figure 18. Test matrix used for AN-102R2 testing

Special attention should be given to test no. 1.16, dewatering. As will be seen in the results section and in the respective appendices, dewatering was the most important test. As previously mentioned, only 2 batches were originally planned, but as the number of batches grew to four, it was not necessary to carry out the entire test matrix listed in Fig. 18. The results section will discuss to what extent each batch was tested. Beside the test procedure, there were many Work Instructions issued to handle the daily changes that occurred. Those instructions can be found in the task notebook (Duignan, 2002b). To facilitate understanding the general operation of the test, a simplified version of the procedural steps is summarized below (see Figs. 1 and 2 for valve locations):

Daily pre-test activities –

1. Equipment is turned on to warm up if not already on.
2. The equipment was checked for functionality and after each of the four liquid-filled pressure sensing lines (see Fig. H2; Appendix H) were purged with 5 ml of distilled and filtered water, the transducers were checked at their zeroes for drift. The zeroes are recorded for 2 to 3 minutes by the DAS. Those data are included in each day's data sheets.

Daily testing activities for constant solids runs (high concentrations) –

3. Begin circulating the slurry in the recirculation loop until the temperature reached 25°C.
4. Turn on the reservoir cooling coil.
5. Allow the slurry to flow through the cross-flow filter.
6. Set the appropriate flow conditions as per the test procedure by iterating between the pumps' speeds and V11.
7. Set the DAS to read every minute.
8. Backpulse the filter. See the preceding backpulse section for its operation.
9. Allow the test rig to run for approximately 1 or 2 hours (as required).
10. Backpulse the filter once again.
11. Repeat from Step 6 for next set of flow conditions or shut down the test rig, if near the end of the work day.
12. End the test run.

Daily testing activities for wash test runs –

[Before beginning the test, prepare a volume of inhibited DIF water (i.e., deionized and filtered (0.1 micron filter) water to which caustic is added to obtain 0.01 M NaOH). The volume is to be 21/18 times the volume of slurry to be washed, which is broken down into 21 small volumes to be added to the slurry one at a time. With the wash water ready, do Steps 3 to 8 from above, then continue below.]

9. Add a small volume of wash water to the slurry in the test rig.
10. Switch valve V13 to the open-loop position so that the filtrate is not returned to the slurry loop, but is collected outside the test rig.
11. Allow the test rig to run until a volume of filtrate is removed that is equal to the volume of water that was put in. (Slightly more mass is taken out than was put in because of the filtrate's higher density.)
12. Maintain the axial filter velocity and the TMP constant.
13. Repeat Steps 9 through 12 for all 21 small volumes.

14. Switch valve V13 to the close-loop position.
15. Backpulse the filter once again.
16. End the test run.

Testing activities for pre-wash dewatering –

[Do Steps 3 to 8 from above.]

9. Switch valve V13 to the open-loop position so that the filtrate is not returned to the slurry loop, but is collected outside the test rig.
10. When the slurry level in the slurry reservoir drops to the 100-liter mark refill with more slurry from the precipitation test rig.
11. Repeat 10 until the entire contents of the prepared simulant is contained in the slurry reservoir of the filtration test rig.
12. If the filtrate flux drops below 0.015 gpm/ft<sup>2</sup> do a backpulse.
13. Continue concentrating the slurry until there is less than 75 liters or as otherwise indicated by the task lead.
14. Close V13 to stop slurry concentration and do a backpulse.
15. End the test run.

### 3.3 RESULTS

#### 3.3.1 Insoluble Solids Separation

The majority of the Results discussion concerns filterability because of the difficulties encountered, however, one absolute success of all the tests was the filter's ability to separate insoluble solids from the slurry simulants. The simulants' turbidity was measured at the beginning and end of each batch test and the result is:

Turbidity (for batches 3 and 4) = 0.17 NTU ±0.06 NTU (one standard deviation)

One source (Martino, 2001) that deals with 5.8 M Na<sup>+</sup> simulated wastes, which was used in research connected to the SRS Defense Waste Processing Facility at DOE's Savannah River Site, states that 5 NTU represents less than 6 ppm of insoluble solids. If this measure is used, then the 0.17 NTU would indicate that the filtrates obtained during the Batch 3 and 4 tests had less than 0.2 ppm of insoluble solids.

#### 3.3.2 Filterability

The actual events that took place to test all four simulated AN-102 batches did not follow the test matrix, Fig. 18<sup>†</sup>. The most important aspect was the dewatering test, i.e., 1.16; therefore,

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<sup>†</sup> A slurry test not shown in Fig. 18 was one that was done with archived AN-107 simulated slurry. Before any testing was done the filter, which was new, was subjected to filter this old slurry to put the filter in a "used" condition. Prior to preconditioning the filter it was baselined with water and the standard slurry and then a steady state slurry run was done for several days. The test number terminology used for preconditioning was similar to that used in Fig. 18, except that each test number was preceded with the word "precond."

that is the only test which all four simulants have data. In general, the matrix can be broken down into the following categories:

1. Baseline with water
2. Baseline with a standard slurry
3. Test slurry at a low concentration of solids (eliminated just before testing began)
4. Dewater
5. Test slurry at a high concentration of solids
6. Wash slurry
7. Dewater until pluggage
8. Acid Clean
9. Repeat step 2
10. Repeat step 1

Due to filterability difficulties and the change in the number of batches to test, the following is what actually occurred:

Batch 3C (test period: 1 to 3 October 2002)

1. Baseline with water
2. Baseline with a standard slurry
3. Dewatering from 0.8 wt% to 8.4 wt% insoluble solids (test stopped – poor filterability)
4. Acid Clean
5. Repeated step 2
6. Repeated step 1

Batch 3B (test period: 22 October to 5 November 2002)

The entire matrix was completed

Batch 3A (test period: 6 to 26 November 2002)

1. Baseline with water
2. Dewatering from 1.6 wt% to 25 wt% insoluble solids
3. Limited number of high concentration tests to verify operation
4. Acid Clean
5. Baseline with a standard slurry
6. Repeated step 1

Batch 4A (test period: 18 February & 12 to 26 March 2003)

1. Baseline with water (18 February)
2. Dewatering from 1.5 wt% to 18 wt% insoluble solids
3. Limited number of high concentration tests to verify operation
4. Acid Clean
5. Baseline with a standard slurry
6. Repeated step 1

The results for each of categories are discussed below. The discussion will first deal with baselining and cleaning, which will be then followed by the test data for the simulated waste.

### **3.3.2.1 Baseline with Water**

#### **3.3.2.1.1 Water and Cross-flow Filtration**

Normally a crossflow filter would not be used with just a liquid because there is nothing to filter. However, flowing water through a filter is useful in the sense of determining the cleanliness of the filter element. That is, to show if the same water filtrate flux is obtained before use and after use and after cleaning. Since there are no solids to deposit on the filter surface, and thus challenge the filter, water will produce results that seem counter-intuitive. This section will not discuss the nature of filtering without solids, since this has been dealt with in some depth elsewhere (Duignan, 2000a or b). Discussed here will be the data obtained with water throughout the tests with the AN-102R2 slurry simulant in the Pilot-scale Cross-flow Ultrafiltration (PXU) facility.

#### **3.3.2.1.2 Overall Evaluation**

At the start and end of each slurry test with the 0.1-micron Mott filter, it was required to test with water, as requested by the RPP-WTP customer (Townson, 2002a). Before use, the water was to be filtered with a 0.1-micron absolute filter and deionized. Further, the water was made mildly caustic to a concentration of 0.01 M NaOH (referred to as inhibited water). In most cases, the caustic addition was done, but there were some exceptions because the addition of even a small amount of caustic caused a significant reduction in filtrate flux when the inhibited water followed an acid cleaning. After using slurry, it was removed and then the slurry loop was cleaned with acid. The acid was followed with water rinses, however there could have been small pockets of slurry or acid solution left somewhere in the loop. The water with the mild caustic was thought to have caused some precipitation of solids that could not be totally removed from the slurry loop. Those solids would then affect the filtrate flux; confounding water-flux comparisons; therefore, some water runs did not include a caustic addition in order to see the effect.

To reiterate, the purpose of the water tests was to determine if the filter returned to the same level of cleanliness after being used with slurry. However, since water generally does not contain significant insoluble solids it does not act like a slurry; therefore it was followed by a standard slurry, 5 wt% SrCO<sub>3</sub>, to better determine the level of filter cleanliness. The standard slurry tests had their own problems and they will be discussed in the next section.

Water tests were actually done at several places in the test matrix, as already mentioned, see Fig. 18: at the very beginning (test 1.00), a rinse after the initial standard slurry tests (test 1.02), a rinse immediately after doing an entire slurry matrix (test 1.31A), another rinse after the acid cleaning (test 1.32), and the final test that comes immediately after the final standard slurry tests (test 1.34). The purpose of this section is to describe the before and after water tests, i.e., 1.00 and 1.34, but some of the rinses are included to better explain the,

sometimes conflicting, results as the filter went from a new state to some other level of cleanliness after its use.

For the testing of slurry simulant AN-102R2, there were a total of five batches of slurry runs: Preconditioning (with archived AN-107), AN-102R2 Batch 3C, AN-102R2 Batch 3B, AN-102R2 Batch 3A, AN-102R2 Batch 4A. [Note: For the preconditioning test, the test nomenclature is different. For example, while the initial water test number is 1.00, the initial preconditioning water test was called PreCond 1.] As mentioned, originally, there were only two tests planned and with preconditioning it would have been three: Preconditioning, AN-102R2 Batch 3, and AN-102R2 Batch 4. However, due to problems with filtering Batch 3 it was done three different ways, which wound up being three completely different batches. With so many tests run close together, there was no point doing water runs before and after each slurry test. Between any two tests, the final water test (1.34) of one slurry test would be used for the initial water test (1.00) for the next slurry test. There were some exceptions, which will be seen throughout the following presentation.

Figure 19<sup>†</sup> illustrates some of the data sets taken before and after each slurry test. (Note, each datum point in the figure is the time average filtrate flux over the period of each test, which lasted approximately 20 minutes each.) Ideally, a clear indication was expected on how effective the filter cleaning was, or if depth fouling progressed with time. While there is a tendency which indicates a return to the same clean level, the data do not elicit straight forward information. The separation among the two data sets before-Batch-3C (open and closed circles) and after-Batch-3C data (triangles) is significant. The main reason was that the slurry loop was very well cleaned after the end of the filter preconditioning, before starting with Batch 3C. This cleaning was not planned but there was a pump-liner failure, which forced the more thorough cleaning. After preconditioning the filter with the AN-107 slurry simulant, the filter was cleaned with 2 M nitric acid for 3 hours and then tested with the standard slurry, which was then followed by a water rinsing and the inhibited water test runs (open circles). The low filtrate flux was unexpected and was thought to be the result of chemicals that were left over from the cleaning that precipitated due to the caustic (0.01 M NaOH) added to the water. However, the acid cleaning caused the pump liners to fail during the water runs and needed replacing. Because pieces of the pump liner had to be removed from the entire filtration test rig, a very thorough cleaning was done. After the cleaning, the inhibited water runs were repeated before starting the slurry test with AN-102R2, Batch 3C. Those results show significantly higher filtrate fluxes (the closed circles). After filtering with Batch 3C slurry, the filter was cleaned once again with the standard method of 3 hours with 2 M nitric acid, followed by the standard slurry test, and then by a water rinsing and the inhibited water tests (triangles). Those subsequent water tests showed, once again, a low water flux. This low flux seemed to confirm the assumption of the presence of precipitated solids (e.g. aluminum). One option to return to the higher water flux was to ultraclean the slurry loop each time a slurry run is done, but that would have been very time consuming and the actual plant will not do such extensive measures unless it is absolutely necessary.

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<sup>†</sup> The data for all the figures in this section can be found in Appendix A.

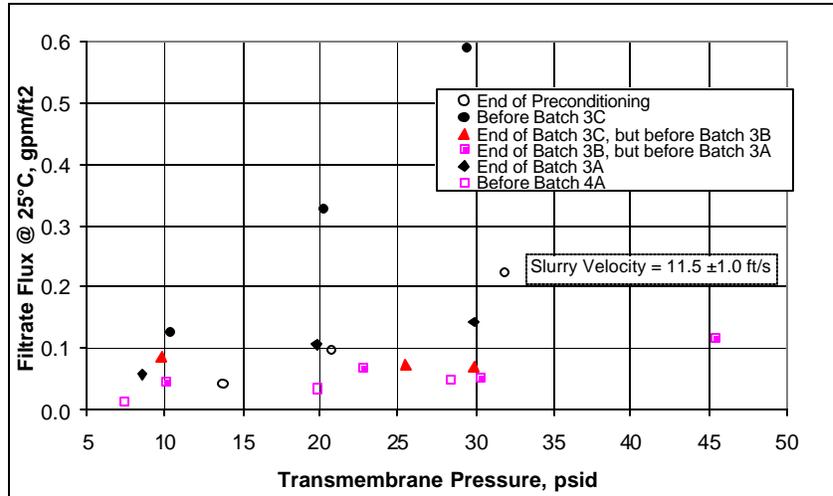


Figure 19. Water tests made before and after filtering several slurries. The filtered and deionized water was made mildly caustic (0.01 M NaOH).

The related data files are:

- Open Circles=tests after Preconditioning with AN-107 and before Batch 3C, tests: 8a, 8b, 8c
- Closed Circles=tests before slurry Batch 3C, tests: 1.00a-3C, 1.00b-3C, 1.00c-3C
- Triangles=tests before slurry Batch 3B, tests: 1.00a-3B, 1.00b-3B, 1.00c-3B
- Square=tests before slurry Batch 3A, test: 1.34a-3B, 1.34b-3B, 1.34c-3B
- Triangles=tests before slurry Batch 3B, tests: 1.00a-3C, 1.00b-3C, 1.00c-3C
- Open Squares=tests before slurry Batch 4A, tests: 1.00a-4A, 1.00b-4A, 1.00c-4A

The bottom five sets of data (open circles, diamonds, triangles, open squares, and closed squares) are much closer to each other than to the initial data set (closed circles). Considering that the level of filter cleanliness can change from one cleaning to the next, and that the filtrate flux is very sensitive to any debris in the filter, then the scatter seems understandable. Unfortunately, it is not possible to determine if depth fouling was increasing with time because the data sets do not chronologically become lower and lower. For instance, the set indicated by diamonds (after Batch 3A) is higher than the triangles and squares even though it was obtained after the sequence of Batch 3C, 3B, and 3A was complete. If depth fouling was increasing with time, its effect was confounded by other complications and not clearly observed.

### 3.3.2.1.3 Individual Evaluations

The different phases of testing where water runs were made are the following:

1. New Filter and the Effect of Inhibited Water after Nitric Acid Cleaning
2. Water Runs before and after Preconditioning with AN-107 slurry simulant
3. Water Runs before and after AN-102R2, Batch 3C slurry simulant
4. Water Runs before and after AN-102R2, Batch 3B slurry simulant
5. Water Runs before and after AN-102R2, Batch 3A slurry simulant
6. Water Runs before and after AN-102R2, Batch 4A slurry simulant

3.3.2.1.3.1 *New Filter and the Effect of Inhibited Water after Nitric Acid Cleaning*

Figure 20 shows data (diamonds) taken with inhibited water (IW = 0.01 M NaOH) just before testing it with the standard slurry of 5 wt% SrCO<sub>3</sub> and then data (squares) just after. However, the water after the standard slurry test did not have caustic and, in fact, was left mildly acidic (0.03 HNO<sub>3</sub>) because the addition of caustic caused the filtrate flux to drop significantly. The TMP was very low (4.9 psid) because the filtrate loop had a significant pressure drop. After the initial test the loop was modified to reduce the pressure drop. However, by that time the filter already experienced flow with the standard slurry of 5 wt% SrCO<sub>3</sub>. After the SrCO<sub>3</sub> tests were complete, and the slurry loop was flushed with water several times, the filtrate flux would not return to the higher values when using the IW; therefore a weak acid was used to prevent precipitation of solids to see if the filtrate flux could return to new-filter fluxes. Several water runs were done after adding the mild acid, as well as at the lower TMP to make a comparison to the new filter data. The two curves in Fig. 20 are significantly different but much closer to each other than when the water was made caustic.

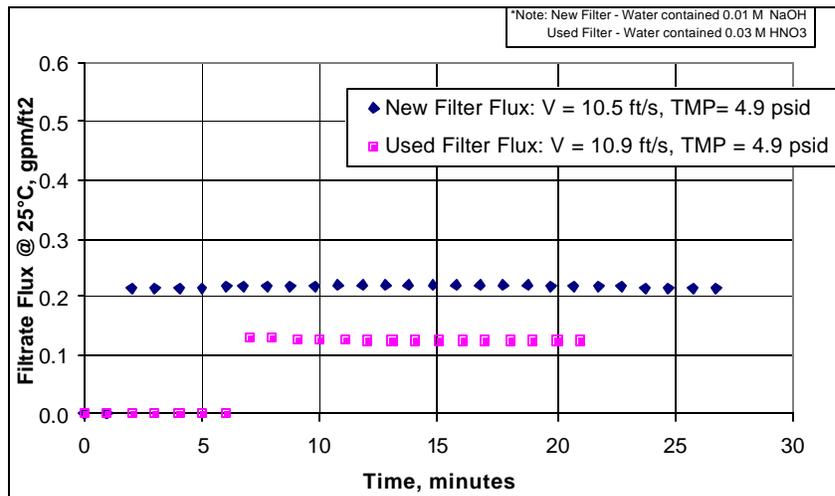


Figure 20. Water tests made on the new filter and after filtering with the standard slurry.

The water was filtered and deionized. The related data files are:

Diamonds=test on the new filter, and water had 0.01 M NaOH: PreCond 1a

Squares=test after standard slurry, and water had 0.03 M HNO<sub>3</sub>: PreCond 3

For example, see Fig. 21. After the standard slurry test and after rinsing the slurry with water, a fresh charge of IW was put into the test rig to do the water tests (PreCond 3a, 3b: squares in Fig 21, and 3c). Since the flux was very low, the test rig was cleaned with more acid and the runs were repeated (PreCond 3a;Rev.1, 3b;Rev1:diamonds in Fig. 21, and 3c) but the water was left slightly acidic (0.03 N HNO<sub>3</sub>). Both test runs in Fig. 21 were done at approximately the same flow conditions, therefore it was only the addition of caustic that made the difference. The presence of solids is evident from the lower data set in Fig. 21 by the drop in filtrate flux with time. As time goes by, the solids in the water are slowly accumulating on the surface of the filter.

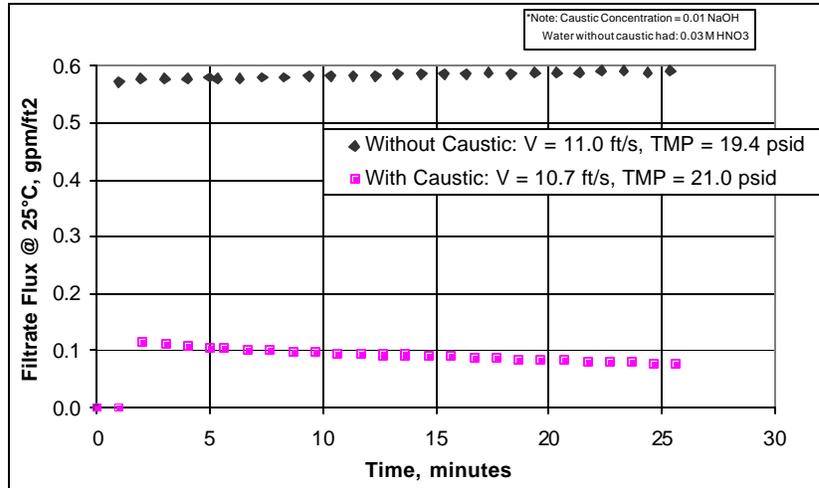


Figure 21. Water tests with and without caustic.  
 The water was filtered and deionized. The related data files are:  
 Diamonds=water had 0.03 M HNO<sub>3</sub>: PreCond 3b, Rev1  
 Squares=water had 0.01 M NaOH: PreCond 3b

The effect of adding caustic to a freshly cleaned and rinsed filter is further illustrated by Fig. 22. After Batch 3 testing was complete in November 2002, the test rig sat idle for about 3 months, until February of 2003, while waiting for Batch 4 simulant and the new precipitation mixing equipment to be ready. Just before Batch 4 testing began, the test rig was once again “baselined” with inhibited water. Those data are shown by the open squares in Fig. 22. Not only was the flux low for water, it was lower than any of the previously inhibited water test runs, see Fig. 19.

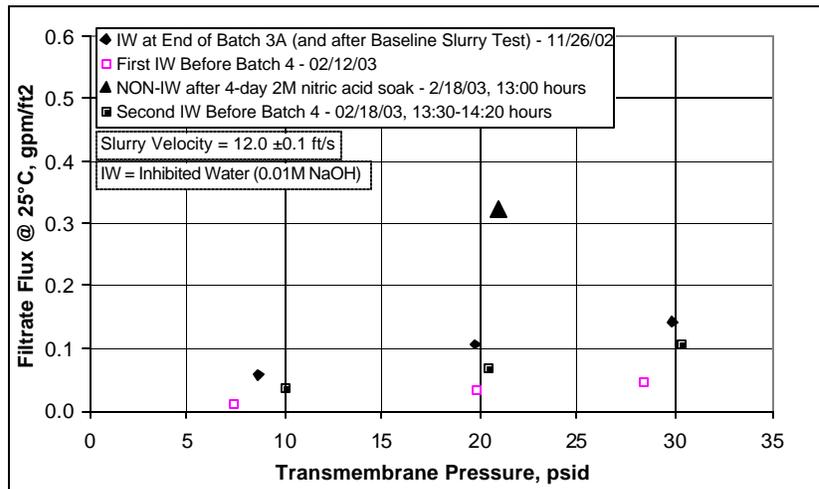


Figure 22. Water tests with and without caustic. Tests done between Batches 3 and 4.  
 Large triangle was obtained with filtered (0.1 micron) and demineralized water only.  
 For all other data the water had 0.01 M NaOH

The filled diamonds in Fig. 22 are the water data at the end of Batch 3A testing done on 11/26/2002. During time between the end of Batch 3A testing until next water data were

taken on 2/12/2003, the filter was submerged in inhibited water. It is not known why the data were lower. In an attempt to bring the flux up, the filter was soaked in 2 M nitric over a 4-day period<sup>†</sup> (2/14/03 to 2/17/03). Immediately before doing a new set of inhibited water runs an extra water test was done before adding the caustic. The single filled triangle at a TMP=20 psid shows the flux increased from about 0.05 gpm/ft<sup>2</sup> to just above 0.3 gpm/ft<sup>2</sup>! Caustic was subsequently added to have a concentration of 0.01 M NaOH and the full set of water runs was done. The flux immediately dropped and at TMP=20 psid the flux was approximately 0.075 gpm/ft<sup>2</sup>, which fell between the post Batch 3A water results and the water results of 2/12/02. The 4-day cleaning improved the flux slightly, but it still did not return to the November 2002 flux of just above 0.1 gpm/ft<sup>2</sup>. It seems that unless every single surface is cleaned in this type of filtration system, the addition of caustic will always reduce the filtrate flux.

3.3.2.1.3.2 Water Runs before and after Preconditioning with AN-107 Slurry Simulant

To put the filter in a “steady state” condition, it was preconditioned with a used slurry simulant (AN-107) so that its performance would be closer to a “used” filter. As for all other slurry tests the filter was checked before and after the slurry run for its water flux. Figure 23 depicts the data. Like the data of top curve in Figure 21, no caustic was added to the water to prevent solids from precipitating out of solution. The top curve of Fig. 23, (diamonds) was obtained just before running slurry through the filter. The bottom curve (circles) represent the filtrate flux after the filter experienced the slurry for many hours and underwent acid cleaning. The lower post-slurry curve must be attributed to some of the slurry not being removed with the acid.

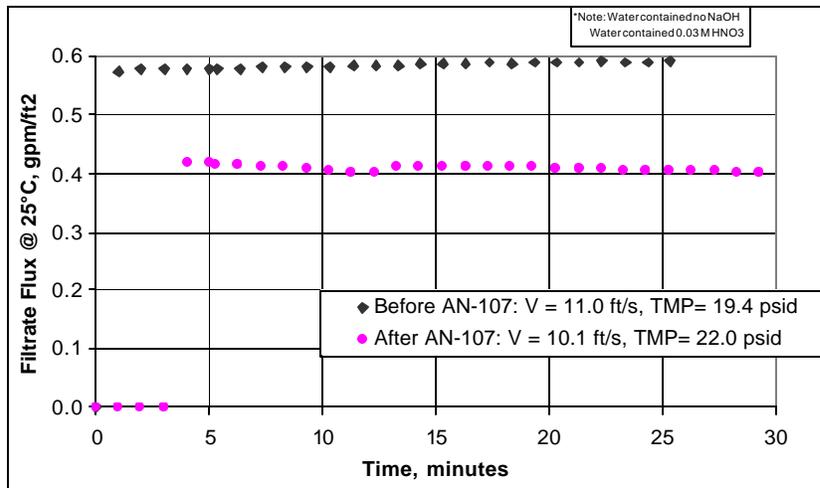


Figure 23. Water tests after cleaning the filter.

The water was filtered and deionized. The related data files are: Diamonds=water had 0.03 M HNO<sub>3</sub>: PreCond 3b, Rev1 Circles=water had 0.03 M HNO<sub>3</sub>: PreCond 6

<sup>†</sup> This cleaning was atypical. Generally, the filter would be subjected to two 90-minute cleanings with 2 M nitric flowing at 12 ft/s and a TMP = 20 psid. However, the upcoming Batch 4 slurry was expected to have poor filterability because of its preparation with poor mixing during the precipitation phase simulant using a Pulse Jet Mixer. SRTC and the RPP customer decided to clean the filter more thoroughly.

3.3.2.1.3.3 *Water Runs before and after AN-102R2, Batch 3C Slurry Simulant*

Just after the preconditioning slurry test and before the first Batch 3 test (3C) the filter was tested with water again. Figure 24 shows the data. These data sets are unique in that the test rig had a very thorough cleaning before the water test. During the first acid cleaning, after the preconditioning test, the coating on the impellers of the two slurry pumps began to break apart. It turned out that the 3-hour acid cleaning fatally degraded the pump liners, requiring replacement and upgrading of the liners.

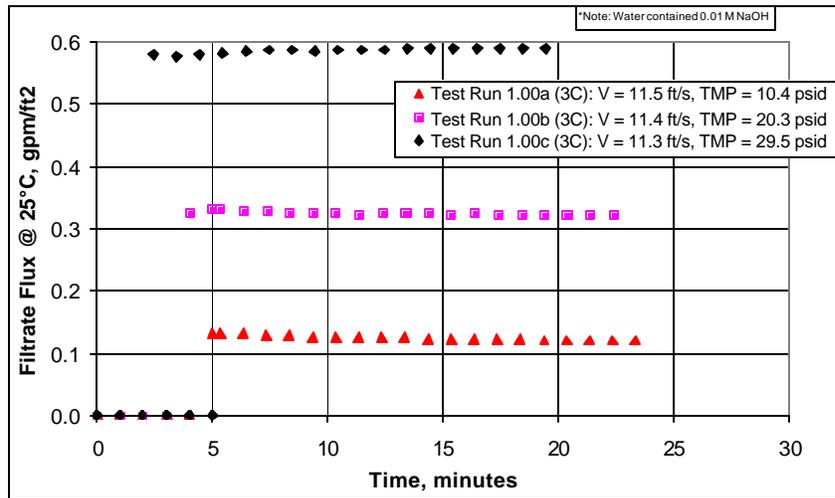


Figure 24. Water tests before test slurry AN-102R2, Batch 3C. The water was filtered and deionized.

The related data files are:

- Triangles=water had 0.01 M NaOH: Run 1a – 3C
- Squares=water had 0.01 M NaOH: Run 1b – 3C
- Diamonds=water had 0.01 M NaOH: Run 1c – 3C

During the replacement, the entire test rig underwent a thorough cleaning to remove all vestiges of the old pump liner. When it came time to test the filter with water again, IW water was used because it was thought that there would not be any solids in the slurry loop to precipitate when caustic was added. Indeed, this seems to be the case because the filtrate fluxes were relatively high, e.g., compare the middle data set of Fig. 24 (squares) to the data set with squares in Fig. 21, which had the same flow conditions, and had the same amount of caustic addition, i.e., 0.01 M NaOH. Also, evident in Fig. 24 is that the filtrate flux remained constant during the 20+ minutes of the tests, indicating the lack of insoluble solids.

3.3.2.1.3.4 *Water Runs before and after AN102, Batch 3B Slurry Simulant*

In contrast to the data in Fig. 24, Fig. 25 indicates a significant reduction in filtrate flux. There are three significant features to note: 1. The lower filtrate flux as compared to Fig. 23, 2. the almost independence on TMP, and 3. that the flux decreases with time.

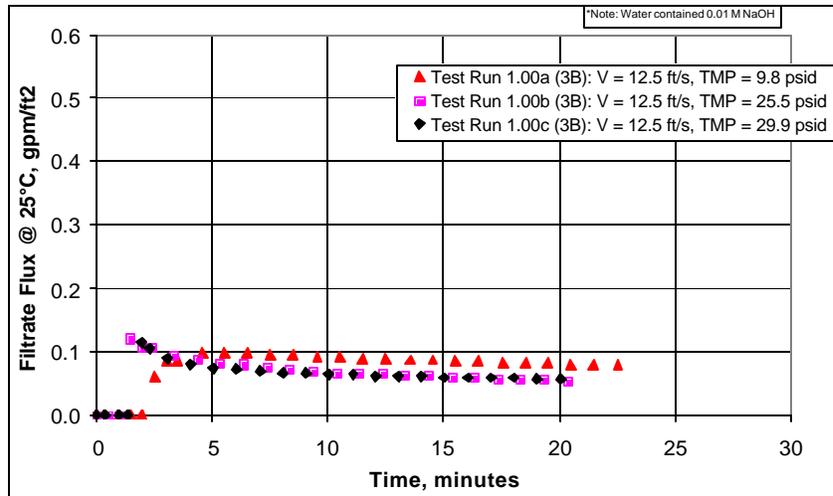


Figure 25. Water tests before test slurry AN-102R2, Batch 3B or after Batch 3C.

The water was filtered and deionized.

The related data files are:

Triangles=water had 0.01 M NaOH: Run 1a – 3B

Squares=water had 0.01 M NaOH: Run 1b – 3B

Diamonds=water had 0.01 M NaOH: Run 1c – 3B

The inhibited water data in Fig. 25 were obtained between two AN-102R2 Batches, i.e., 3C and 3B. As per the test specification (Townson, 2002a) requirements, the water was inhibited with 0.01 M NaOH, but as shown above, the caustic may have caused precipitation of solids that were left over from the 3 hours of nitric acid cleaning or the standard slurry test runs. Whether from precipitation or another cause, the filtrate flux was significantly reduced from clean test rig conditions (Fig. 24).

#### 3.3.2.1.3.5 Water Runs before and after AN-102R2, Batch 3A and 4A Slurry Simulant

The water results after other slurry tests, e.g. Batches 3A and 4A, were similar to those shown in Fig. 25, as can be seen from average data shown in Fig. 19. Those data are not shown here but the entire set of data can be found in Appendix A.

#### 3.3.2.1.4 Relationship between Water and Slurry Filtrate Fluxes

One other important thing to note on the relationship of filtrate flux between water and slurries is that there appears to be none. This is described in the following two bullets:

- For the water test just before the testing of AN-102R2, Batch 3C, Fig. 19 and Fig. 24 show the highest filtrate flux was approximately 0.6 gpm/ft<sup>2</sup> at an average slurry velocity of 11.3 ft/s and a TMP of 29.5 psid. Batch 3C slurry dewatering (Test 1.16 done on 1-3 Oct. 2002) with a velocity of 11.5 ft/s and a TMP of 41.8 psid, the filtrate flux started at 0.055 gpm/ft<sup>2</sup>. That is, the slurry filtrate flux started at an order of magnitude LESS than the water flux.

- For the water test just before the testing of AN-102R2, Batch 3B, Fig. 19 and Fig. 25 show the highest filtrate flux for all three tests was under 0.1 gpm/ft<sup>2</sup> at an average slurry velocity of 12.5 ft/s and a TMP from 9.8 to 29.9 psid. Batch 3B slurry dewatering (Test 1.16 done on 22-23 Oct. 2002) with a velocity of 12.1ft/s and a TMP of 40.5 psid, the filtrate flux started at 0.110 gpm/ft<sup>2</sup>. That is, the slurry filtrate flux started ABOVE the water flux, which further supports the theory that solids can stay in the test rig.

### 3.3.2.2 Baseline with Standard Slurry (5 wt% SrCO<sub>3</sub>)

Using a standard slurry to determine the level of cleanliness of the cross-flow filter was requested by the RPP-WTP customer. This standard slurry was a 5 wt% solution of Strontium Carbonate in water. Before making the slurry the water was to be deionized, filtered with a 0.1-micron absolute filter, then made caustic to 0.01 M NaOH.

The purpose of using a standard slurry was to determine if the filter, after being used and after it was cleaned with acid, would return to the same level of cleanliness. Using a standard slurry, instead of just water, was preferred because water generally does not contain any significant insoluble solids that will challenge the filter; therefore, it is not a true measure of filter performance. In concept, using a standard slurry is a good idea, however, in reality the filtrate flux obtained with any slurry is highly dependent not only on the level of filter cleanliness, but also on the slurry itself. The particles in the slurry are very important as to their size, shape, ability to deform, time stability, stickiness, etc.

The objective in conducting a standard slurry test before and after each test was to show that the filter returned to its original conditions before filtering. In this way permanent depth fouling could be measured. However, the variation from run to run was too large to make such a determination, except when the filter was new and after its first use. Figure 26<sup>†</sup> shows those data.

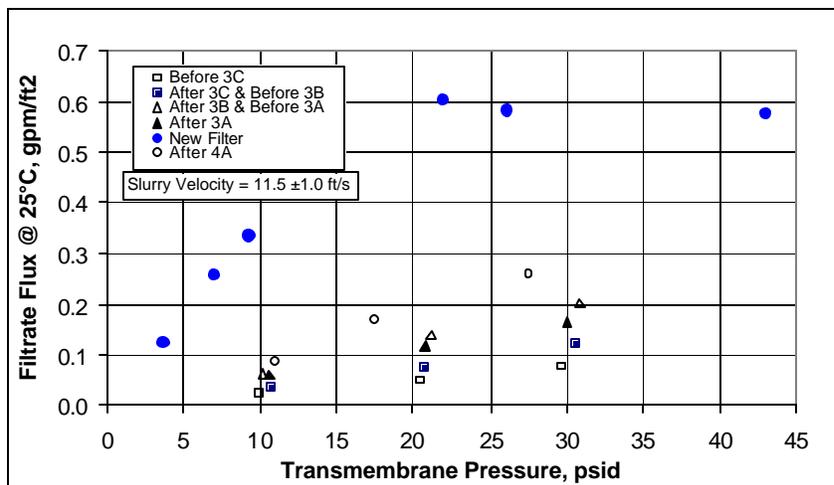


Figure 26. New and Used Filter Standard Slurry Filter Tests

<sup>†</sup> The data for all the figures in this section can be found in Appendix B.

A distinct feature in Fig. 26 is the large difference between the new-filter data and all the rest. With respect to the new-filter data, all used-filter data can be judged as the same. That is, the variation in the four sets of data is small compared to their filtrate flux magnitude, as compared to the new filter. This argument is made stronger by realizing that with a flux measurement uncertainty of approximately 5.4 %, the variation among the non-new filter data is still significant, but the significance is not large.

An interesting aspect of the new-filter data is the almost linear increase in flux with TMP up to 20 psid, at a constant slurry velocity of approximately 11 ft/s. To understand this effect, see Fig. 27, which is the time data for new-filter data in Fig. 26. For the three test runs with the lowest TMP, below 10 psid, it appears as if there is no slurry at all. It is as if just a liquid is flowing because the filter is not challenged at all. As the TMP increases to above 20 psid the typical crossflow Filtrate Flux vs. Time decay appears. This indicates that the first three points for the new-filter data in Fig. 26 represent the constant filtrate flux value, while the last three points represent an average of the decaying filtrate flux. It is possible the TMP=20 psid cut-off point indicates that fast settling SrCO<sub>3</sub> particles will not accumulate on the vertical filter surface until the TMP > 20 psid. (Note, from a well mixed condition the standard slurry solids settle out by gravity in only 1 minute and the particle density is 3.7 g/ml.). Another point of interest is for TMP>20 psid, where it appears that the filtrate flux is independent of TMP. The last three data points for the new filter in Fig. 26 are statistically the same. This similarity tends to imply that at 11 to 12 ft/s of slurry velocity the slurry cake cannot build up further (or is compressed) with increasing pressure, only with increasing time. As time increases, the filter cake becomes thicker, but for different TMP, above 20 psid, the thickness is the same for a given time period.

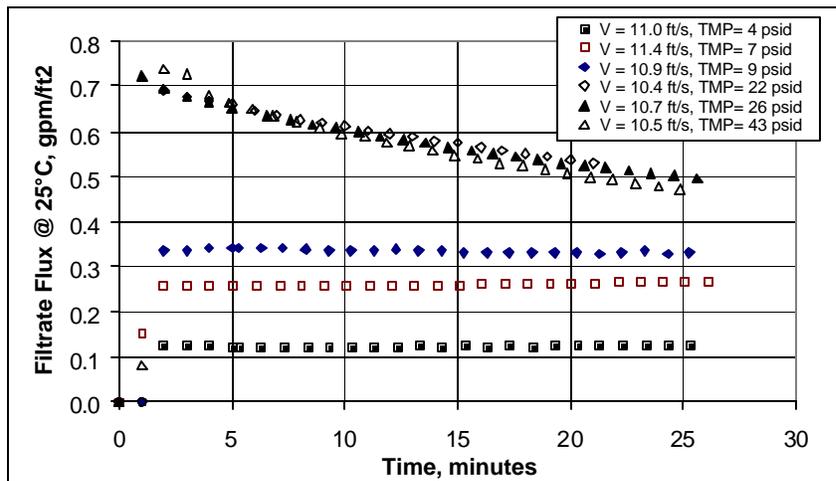


Figure 27. Filtering with Time After a Backpulse for the New Mott Filter

Because of the fast settling SrCO<sub>3</sub> particles, and their difficulty in forming a filter cake (or ease in being compressed), this material may not be the best candidate for a standard. For the used filter, after it had experience several different slurries, and was cleaned, the temporal

data are similar to the new filter, see Fig.28. The average values for these data are the black triangles in Fig. 26.

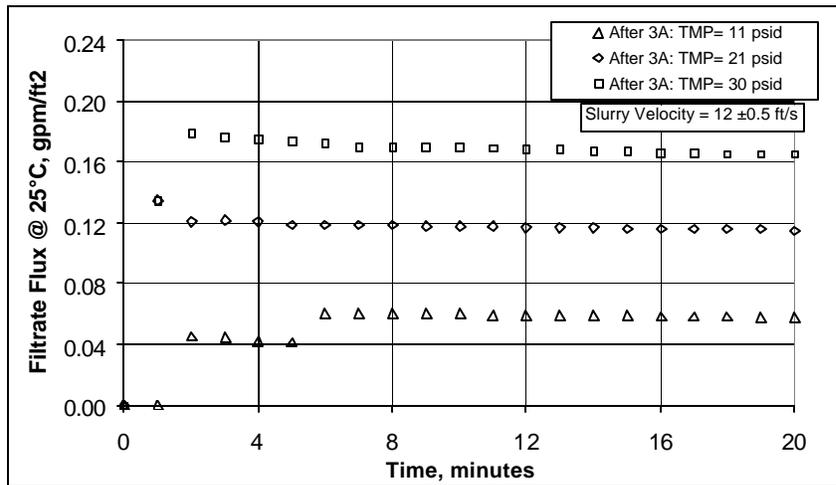


Figure 28. Filtering with Time After a Backpulse for the Used Mott Filter

The lowest data set shows that the filter is not being challenged, as well as the mid data set. However, the highest does show some reduction in flux with time. All other data sets for the used filter are similar, but the overall filtrate flux magnitude changes with the level of filter cleanliness.

A closer look at the used filter data is shown in Figure 29. Before and after each test with Batches 3 and 4 slurries, the standard slurry tests were done. To better understand the series of events, note the chronological order of the tests, i.e., 3C, 3B, 3A, and 4A. There were a total of 5 standard slurry tests.

As stated before, there is some significant difference among the five sets of data, but not by much, when compared to the new filter results shown in Fig. 26. In chronological order the earliest is the lowest set of data, before testing any of the slurry batches (i.e., before Batch 3C). The next lowest set was after completing sub-Batch 3C, but just before doing the second sub-Batch, 3B. The second highest set was obtained just before doing the last sub-Batch, i.e., 3A. Then the next set, which was just after 3A, was lower than the pre-3A test. This implies that time is not an issue, but that it is the level of cleanliness of the filter, which is important. That is, just before each standard slurry, the filter was cleaned with 2 M nitric acid for 3 hours. The acid does clean the filter but the filter does not return to its “new” state, as is evident in Fig. 26. How well the filter is cleaned is a function of several factors, like the level of fouling, and the type of material that is fouling the filter. The filter flux is very sensitive to any residual fouling or solids still in the slurry flow loop, therefore varying results of standard slurry testing are not surprising. The variation seen in the five data sets shown in Fig. 29 attest to the different level of filter cleanliness. This idea is further reinforced with the data obtained after the Batch 4A test. Just before the 4A test, the filter was soaked in 2 M nitric acid for 4 days, which may have left it slightly cleaner and therefore the baseline data were

slightly higher. With the limited cleaning protocol currently in practice, a standard slurry set of data cannot be expected to be more reproducible than that shown in Fig. 29.

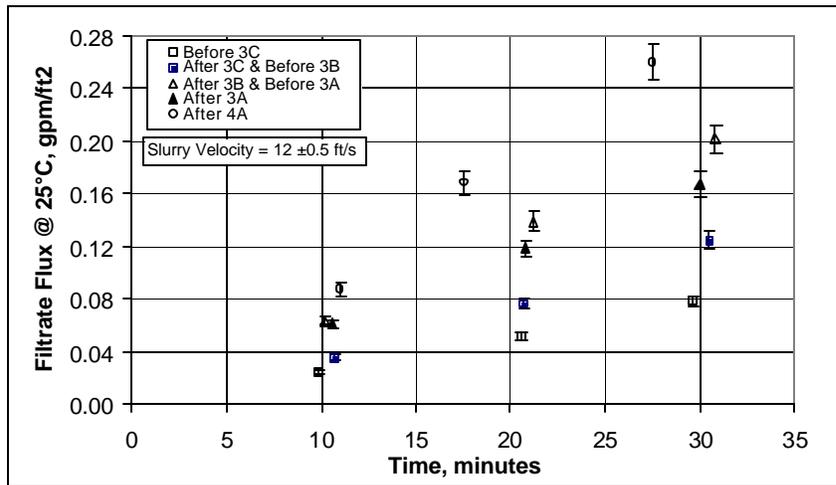


Figure 29. Used-Filter Standard Slurry Filter Tests

### 3.3.2.3 Cleaning the 0.01-micron Mott Filter with 2 M Nitric Acid

To clean the cross-flow filter a concentration of 2M nitric acid was requested by the RPP-WTP customer; no other requirements were made except to document the results, which are herein recorded. No method to clean the filter was specified, so the one used was based on early bench-top filter testing by using two batches, each circulating for 90 minutes. Other researchers (i.e., Zamecnik, 2003) have used longer cleaning intervals, like soaking for 24 to 48 hours, using different chemicals, or different nitric acid concentrations, but other methods are beyond the scope of this task. Being limited to 2 M nitric acid, then the 3-hour cleaning cycle was used because it was thought that the actual plant would not want to use longer cleaning periods due to expensive down time.

The purpose of cleaning the filter is to remove material, e.g., sludge, slurry, solids, etc., which would cause unacceptable filter fluxes, or operating pressures, that cannot be improved by either simply flushing with water or backpulsing. Backpulsing is the process of temporarily reversing the direction of filtrate flow by pulsing a fixed quantity through the filter wall to knock off built up filter cake from the inside surface of the filter tube. This material build-up occurs when fine slurry material is lodged in the filter wall, which is usually referred to as depth fouling. The wall thickness of the porous tubes used is 0.0625 inch or 1.5875 mm, which is 15,875 times larger than the nominal pore size of 0.1 micron; that is, there is considerable space in which to deposit solids.

To prepare the filter for use with the test slurry (AN-102R2), it was preconditioned with a similar slurry, AN-107, in order to start with a “used” filter, which would be more typical of daily plant operation. That is, a new filter was first subjected to AN-107 for a predetermined time interval (several days), then the filter was cleaned with 2 M nitric acid. For that first cleaning, the target acid flow parameters were an axial filter velocity (V) of 11 ft/s and a

transmembrane pressure (TMP) of 20 psid. Figure 30<sup>†</sup> shows the actual parameters used (filled and open diamonds). During the first period (filled diamonds), the filter was challenged during the first 10 minutes with undissolved solids and then the filtrate flux improved from about 0.42 gpm/ft<sup>2</sup> to above 0.45 gpm/ft<sup>2</sup>. After changing the nitric acid solution, the second period (open diamonds), there appears to be a reduced presents of solids, since the filter was not challenged as much. While there seemed to be a slight improvement in the filter cleanliness during the second period it appears that most of the cleaning occurred during the first period.

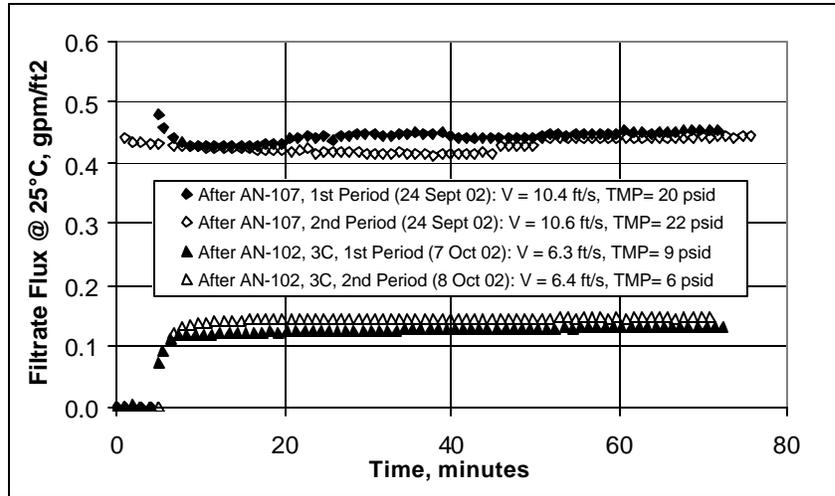


Figure 30. 2 M nitric acid cleaning after AN-107 & AN-102R2, Batch 3C

Unfortunately, the nitric acid cleaning after the preconditioning test damaged the pumps liners of the experimental test rig. While waiting for replacement liners that were of a material more impervious to nitric acid the filter had to be cleaned using a separate cleaning loop, which prevented acid from entering the pumps. That cleaning loop only had a small motor, which could not supply the energy necessary to attain the original flow parameters. Figure 30 shows that both V and TMP used for the Batch 3C acid cleaning were considerably less than those used for the preconditioning run. The post Batch 3C cleaning data are slowly increasing with time, but a plateau is not reached indicating that the filter may not have been brought to the same level of cleanliness as seen for the AN-107 cleaning.

Figure 31 shows a more dramatic effect from cleaning. After the second Batch 3 slurry test (3B), the first-period nitric acid cleaning shows how the filter was challenged during the first 60 minutes, after which the filtrate flux increased from 0.26 to 0.37 gpm/ft<sup>2</sup>. After replacing the nitric acid solution with a new charge, the second-period cleaning showed an improved filtrate flux and the filter was only mildly challenged for the first 15 minutes, then the flux increased to a steady value of approximately 0.56 gpm/ft<sup>2</sup>. This cleaning cycle implies that the two ninety-minute periods were necessary to clean the filter, but that further cleaning may not result in any significant filter performance. Note, the specified axial velocity was

<sup>†</sup> The data for all the figures in this section can be found in Appendix C.

increased by the customer from  $V = 11$  to  $V = 12$  ft/s and the high TMP for the first period, Batch 3B, cleaning, i.e., 43 psid, was done in error.

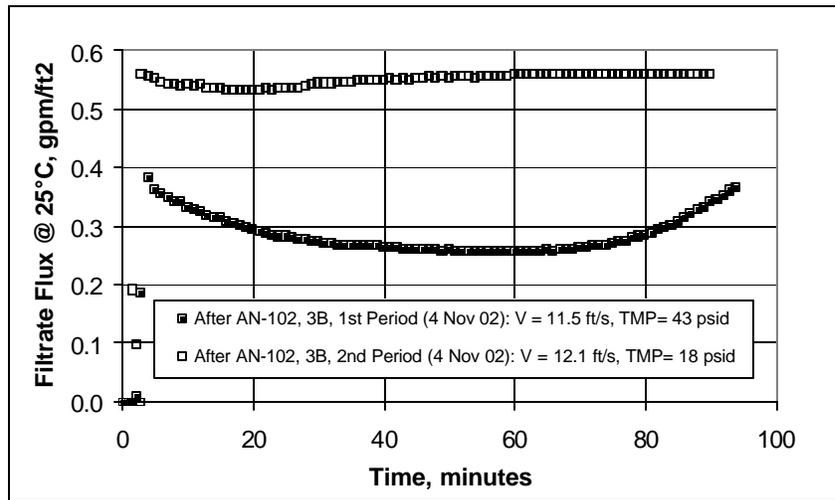


Figure 31. 2 M nitric acid cleaning after AN-102R2, Batch 3B

Figure 32 depicts another set of cleaning data, with the first period having the largest filtrate flux fluctuations and the second period indicating a basically clean filter. During the first cleaning period after Batch 3A the flux appears rather steady for about 35 minutes, but then it dropped for about 15 minutes before increasing.

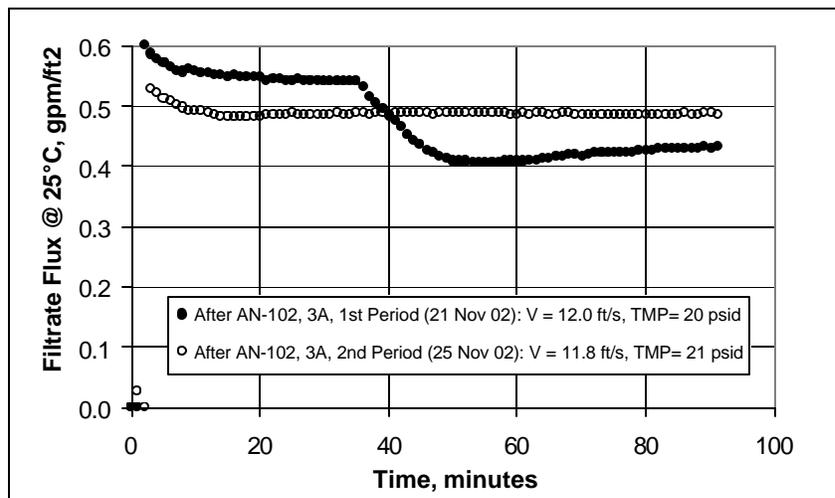


Figure 32. 2 M nitric acid cleaning after AN-102R2, Batches 3A

The reason for the sudden drop is not known, however, the test rig had a lot of small locations where slurry could have been lodged. It is possible that some slurry broke loose within the test loop and began challenging the filter. Once the slurry was circulating the solids would be dissolving in the nitric acid causing the filtrate flux to rise. During the

second cleaning period the slurry stops challenging the filter after 10 minutes and comes to steady state. This implies that there must have been some small amount of solids that were not dissolved by the nitric acid, but there was not enough to continue challenging the filter.

Just before doing the last AN-102R2 slurry test, Batch 4A, the filter was soaked for four days in 2 M nitric acid in an attempt to obtain better water fluxes. The water runs displayed the lowest filtrate fluxes since the 0.1 micron filters were first used in September 2002 (see the section on water runs). Figure 33 shows the results.

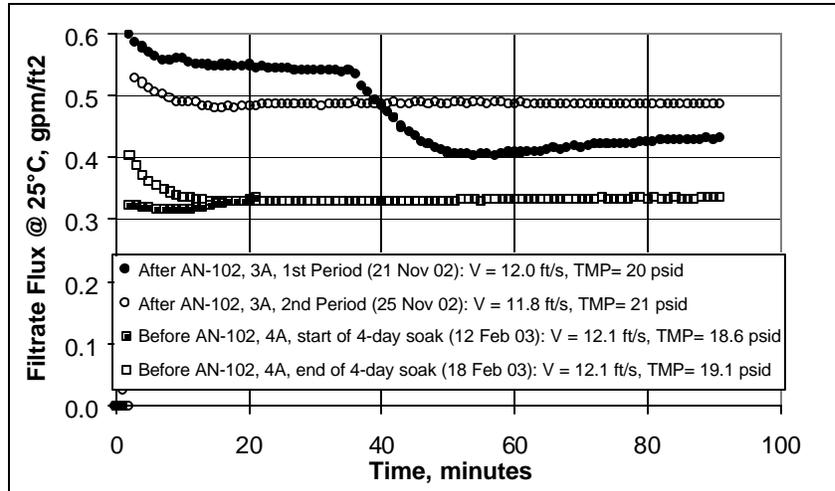


Figure 33. 2 M nitric acid cleaning after AN-102R2, Batches 3A & 4

Some interesting features of these pre-Batch 4A cleaning data are the lack of significant effects of the 4-day soaking and the lower filtrate flux values compared to the cleaning values done in November 2002. The test rig sat idle for approximately 3 months between the last Batch 3 slurry test (3A) and the acid cleaning done before the pre-Batch 4A test. During that time period, the filter was submerged in inhibited water. However, after the acid cleaning on 25 Nov 02 a standard slurry test (5 wt% SrCO<sub>3</sub>) was performed, also on 25 of November. While the test rig was rinsed out several times and had final inhibited water test runs, it is possible that pockets of slurry remained in the test rig. This could have contributed to the lower filtrate flux obtained on 18 Feb.03, as shown in Fig. 33. The fact that the post-soak (18 Feb.) results show the filter was challenged during the first 15 minutes indicate that there were still some insoluble solids in the acid which coated the filter. Furthermore, since the pre-soak (12 Feb.) and post-soak (18 Feb.) results indicate approximately the same steady state flux value, then the soak itself did very little to dissolve the solids remaining in the acid or lodged in the filter wall.

Figure 34 shows some confusing results. After the last batch of AN-102R2, i.e., 4A, was complete the filter was cleaned again. The initial 90-minute cleaning gave similar flux results as the cleaning flux just before Batch 4A was tested. The filled circles show how the filter was initially challenged and as the solids dissolved the filtrate flux first leveled out, which then increased to asymptotically approach the before-Batch 4A cleaning flux. Since this first period

of final cleaning was at the end of a workweek the test rig was emptied of acid and filled with deionized and filtered water. On the following Monday nitric acid was added to the water to bring the concentration to 2 M in order to begin the second 90-minute period of cleaning. Surprisingly, the filtrate flux was about double that from the previous period. Moreover, the very small flux drop during the first 30 minutes indicated the system had very little solids, after which the flux became stable. Somehow, the water soaking, over the weekend, and the second acid cleaning removed some material which caused to lower filtrate flux.

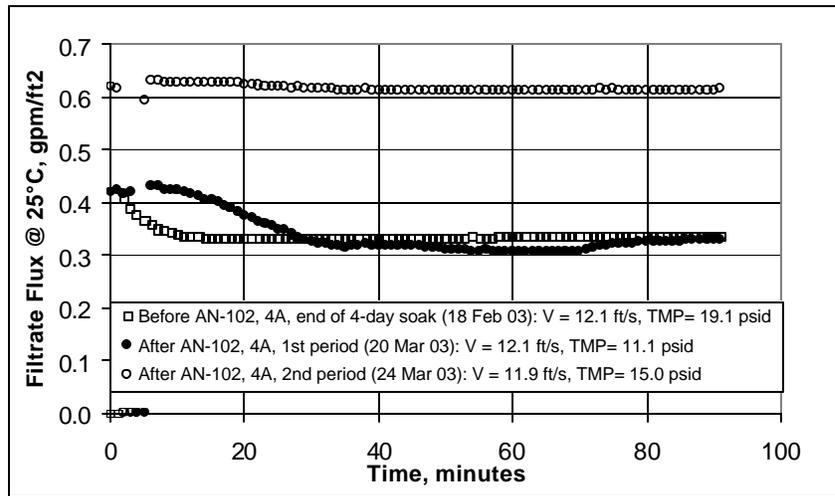


Figure 34. 2 M nitric acid cleaning after AN-102R2, before & after 4A

To conclude, Fig. 35 shows all the final period nitric acid cleanings that were done for the AN-102R2 simulant slurry tests, including the AN-107 filter preconditioning test.

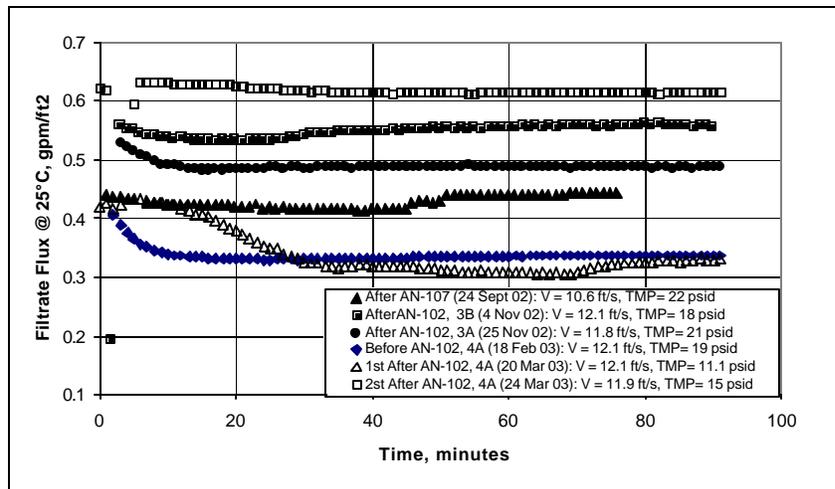


Figure 35. 2 M nitric acid cleaning of the AN-107 and AN-102R2 slurry tests

Neglecting the cleaning done on the filter after the preconditioning test the filtrate flux of acid chronologically becomes lower. The cleaning flux after the Batch 3B test is about 0.56 gpm/ft<sup>2</sup>, then after the Batch 3A test it goes to 0.49 gpm/ft<sup>2</sup>. Now from Batch 3A to Batch 4A the test rig sat idle so it was cleaned before 4A. The flux continued its downward trend to 0.33 gpm/ft<sup>2</sup>. Just after Batch 4A, the cleaning flux during the first cleaning period was slightly lower at about 0.32 gpm/ft<sup>2</sup>. This steady flux reduction with time may indicate that some of the solids are not soluble in 2 M nitric acid and are building up in the porous wall of the filter tubes. However, when the second cleaning was done after Batch 4A the flux doubled to close to 0.6 gpm/ft<sup>2</sup>! The reason why is not known, but something had to have been dissolved, which was previously in the system.

#### **3.3.2.4 Dewatering of AN-102R2 Slurry Simulant**

To reiterate, the principal reason for the pilot-scale cross-flow ultrafiltration test was to determine the filterability of different preparations of an organic-based precipitated slurry. The slurry was a simulant of waste in the Hanford Tank 241-AN-102. The particular simulant used is referred to as AN-102R2 because its original recipe was revised twice. See the Simulated Waste Slurry section for more information on the recipe.

The test runs described in this section deal with four batches of AN-102R2:

- 1.16, Batch 3C This AN-102R2 simulant was precipitated under NOC\*
- 1.16, Batch 3B This AN-102R2 simulant was precipitated under BC\*
- 1.16, Batch 3A This AN-102R2 simulant was precipitated under BC at 25°C
- 1.16, Batch 4A This AN-102R2 simulant was precipitated using PJM\*

\*See Fig. 17 for nomenclature and the number 1.16 refers to test 1.16 which is listed in the task plan (Duignan, 2002a) as the “dewatering” test.

After a slurry was made, all dewatering tests followed the same procedure:

1. Fill the pilot cross-flow test rig with slurry and take initial slurry and filtrate samples
2. Begin filtering while directing filtrate to a storage location so dewatering could commence.
3. Dewater until the insoluble solids concentration was > 15 wt% (but > 20 wt% was preferable).
4. Dewater for at least 12 hours and backpulse the filter when the filtrate flux < 0.015 gpm/ft<sup>2</sup>.
5. Stop dewatering and take final slurry samples.

Each of the dewatering tests result will be discussed in this section. Figure 36 shows the highlight results for each test as well as the simulant properties measured from samples taken before and after all four tests. They will be used throughout this section.

Batch of AN-102R2 Simulant>>	3C	3B	3A	4A
Date of Test	1-3 Oct. 02	22-23 Oct. 02	6-7, 11 Nov. 02	12-13 Mar. 02
Duration of Test	46 hours	12 hours	29 hours	20 hours
Volume of Slurry Dewatered	899 liters	900 liters	920 liters	650 liters
Mixing Conditions	Well Mixed/Agitator	Well Mixed/Agitator	Well Mixed/Agitator	Poorly Mixed/PJM
Slurry Precipitation Conditions	Newly Optimized	Baseline	Baseline (but 25°C)	Baseline
Highest Measured Filtrate Flux	0.06 gpm/ft1	0.11 gpm/ft2	0.06 gpm/ft2	0.05 gpm/ft2
Average Filtrate Flux over duration	0.011 gpm/ft1	0.048 gpm/ft2	0.019 gpm/ft2	0.019 gpm/ft2
<b>Low Solids Concentrations at the start of dewatering</b>				
Insoluble Solids	0.8 wt%	1.2 wt%	1.6 wt%	1.5 wt%
Total Solids	33.6 wt%	32.7 wt%	33.0 wt%	33.3 wt%
Slurry Consistency	3.6 cP	4.0 cP	4.1 cP	4.2 cP
Yield Stress	0 Pa	0 Pa	0 Pa	0 Pa
Filtrate Viscosity	2.7 cP	3.8 cP	3.7 cP	3.7 cP
Slurry Density	1.29 g/ml	1.29 g/ml	1.29 g/ml	1.29 g/ml
Filtrate Density	1.25 g/ml	1.279 g/ml	1.276 g/ml	1.277 g/ml
PSD [2] (by volume dist.): Mean	8.6 micron (68%) [1]	8.6 micron (48%) [1]	9.8 micron (42%) [1]	
PSD (by volume dist.): Mean	2.6 micron (32%) [1]	2.3 micron (52%) [1]	2.8 micron (58%) [1]	2.7 micron
PSD (by volume dist.): Std Dev	4.8 micron	4.3 micron	4.4 micron	1.9 micron
PSD (by volume dist.): spread	1 to 74 micron	1 to 52 micron	1 to 26 micron	0.8 to 37 micron
PSD (by number dist.): Mean	2.1 micron	1.9 micron	2.0 micron	1.8 micron
PSD (by number dist.): Std Dev	0.7 micron	0.5 micron	0.7 micron	0.6 micron
PSD (by number dist.): spread	1 to 22 micron	1 to 19 micron	1 to 19 micron	<0.7 to 16 micron
<b>High Solids Concentration at the end of dewatering</b>				
Insoluble Solids	8.4 wt% [3]	21.7 wt%	25.3 wt%	18.3 wt%
Total Solids	38.6 wt%	47.2 wt%	49.3 wt%	45.8 wt%
Slurry Viscosity	19 cP	20 cP	24 cP	14.8 cP
Yield Stress	7.5 Pa	8.6 Pa	24 Pa	7.7 Pa
Filtrate Viscosity	1.7 cP	3.7 cP	4.5 cP	3.8 cP
Slurry Density	1.31 g/ml	1.43 g/ml	1.45 g/ml	1.38 g/ml
Filtrate Density	1.276 g/ml	1.285 g/ml	1.283 g/ml	1.286 g/ml
PSD (by volume dist.): Mean	6.7 micron (51%) [1]	8.2 micron (13%) [1]		
PSD (by volume dist.): Mean	2.5 micron (49%) [1]	0.9 micron (87%) [1]	2.5 micron	2.1 micron
PSD (by volume dist.): Std Dev	3.0 micron	0.25 micron	1.8 micron	0.8 micron
PSD (by volume dist.): spread	<0.7 to 52 micron	<0.7 to 44 micron [4]	<0.7 to 26 micron	0.9 to 16 micron
PSD (by number dist.): Mean	1.9 micron	0.8 micron	1.8 micron	1.8 micron
PSD (by number dist.): Std Dev	0.7 micron	0.1 micron	0.5 micron	0.4 micron
PSD (by number dist.): spread	<0.7 to 16 micron	<0.7 to 2 micron [4]	<0.7 to 13 micron	0.9 to 11 micron
Notes: [1] - Bi-modal distribution, [2] - PSD = particle size distribution, [3] - Test stopped after 46 hours: poor filterability [4] - Ranges for 3B (only) should have been significantly less than 0.8 micron, but PSD method was limited to 0.7 micron				

Figure 36. Comparison among the four AN-102R2 dewatering tests

### 3.3.2.4.1 Filtering Batch 3C

Figure 37 is the time plot of the first Batch 3 test, which filtered very poorly and thus was stopped after about 46 hours of continuous filtering. The dewatering test began with the Envelope C-type slurry that was precipitated under what is referred to as “newly optimized conditions.” In short, the optimization was done to minimize precipitation reagents of sodium hydroxide, strontium nitrate, and sodium permanganate while still obtaining the needed decontamination factors for strontium and transuranic components. Unfortunately, the reduced concentration of reagents had a negative impact on filterability.

- Poor Filter Performance with Batch 3C

As stated above, at just under 46 hours of continuous filtering the cross-flow test rig was stopped and the test was terminated. The slurry that started out at about 1 wt% was only dewatered to an insoluble solids concentration of about 8.5 wt%; far short of the 15 wt% target. The overall filtrate flux average was 0.011 gpm/ft<sup>2</sup> for the 46-hour test but for the last 25 hours of the test the flux was below that value and for the last 10 hours it remained at 0.005 gpm/ft<sup>2</sup>, well below the target mean value of 0.02 gpm/ft<sup>2</sup>. It was decided to repeat the test with another Batch 3 slurry but at the original precipitation conditions where this type (another organic type simulated slurry: AN-107, see Duignan 2000b) of slurry had already been shown to filter well. In fact, two more tests were added, so that now there would be four AN-102R2 tests, instead of two.

Due to the poor filter performance and the inability to concentrate the slurry to 20 wt% in a reasonable time period, no steady-state filtration runs were done with Batch 3C, i.e., High Solids Concentration Test Runs Nos. 1.17 to 1.30 (Duignan, 2002a). These runs were to determine the filter operational parameters, V and TMP, that would give the highest filtrate flux. Steady state runs were put off until after the next slurry batch, or after the slurry batch that could be concentrated to at least 15 wt% of insoluble solids.

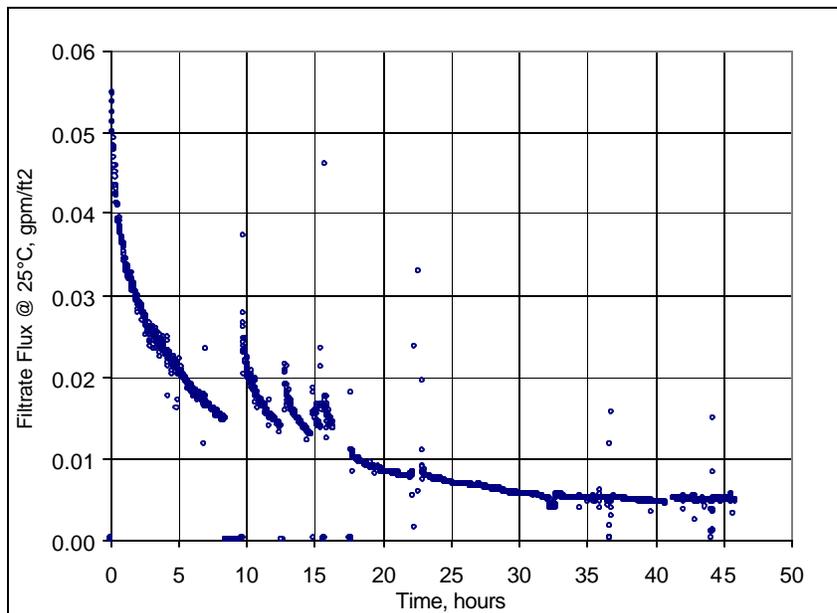


Figure 37. Batch 3C: Dewatering filter flux of AN-102R2 precipitated with the newly optimized conditions at 25°C.

Over the filtering period the average slurry velocity was  $V = 11.5$  ft/s, the average transmembrane pressure was  $TMP = 42$  psid, and the average slurry temperature was  $T = 26^\circ\text{C}$  (the filtrate flux was adjusted to  $T = 25^\circ\text{C}$ ). The test was done from 10/1 to 10/3/2002 and concentrated the insoluble solids from approximately 1 wt% to 8.5 wt%.

- Backpulsing did not prove useful

Figure 37 shows that after 5 hours of dewatering, the flux dropped precipitously to the target mean flux of 0.02 gpm/ft<sup>2</sup>. The criterion to initiate a backpulse was when the filtrate flux dropped below 0.015 gpm/ft<sup>2</sup> and this occurred after about 8.7 hours into the test and the solids concentration increased to just 2 wt%, Fig. 38. The backpulse increased the flux rate but after only 4 hours it returned to the criterion level again. The approximate 1-hour period that appears to show no flow in Fig. 37, just before the tenth hour, occurred because the filtrate flowmeter could only measure flow after the entire backpulse system was purged of air. That is, during that period the system was refilling, there was filtrate flow but it could not be measured since no liquid was flowing through the filtrate system flowmeter. (Note, after this test the filtrate flowmeter was relocated to begin measuring the filtrate immediately after a backpulse.) During a backpulse the filtrate flow actually is stopped and reversed for only a few minutes, then the flow reestablishes almost immediately. After the first backpulse, the filter was backpulsed four more times, each being less effective than the preceding one. After four backpulses that action was stopped. The increase in the filtrate flux and the fast return to the original low flux indicated that backpulsing was not effective. Actually, backpulsing was intended to be stopped after the second one, but at about the 16<sup>th</sup> hour (at 8 AM on Wednesday, 10/2/2003) the RPP customer was present and made two requests: to increase the slurry velocity from 11 ft/s to 12 ft/s to conform to the bench-top tests and to perform a backpulse to observe its operation and how it was being performed. Unfortunately, the filtrate flux returned to a low flux in less than an hour's time and then one more backpulse was done at 8:45 AM, resulting in similar response. No further backpulsing was to be done, but at about the 22<sup>nd</sup> hour a final backpulse was done with actuating air pressure increased from 30 psid to approximately 100 psid to see if the high pulse energy could dislodge the filter cake. As can be seen on Fig. 37 the increase of filtrate flow only lasted moments before it returned to the low filtrate flux. Backpulsing was totally ineffective and no longer used.

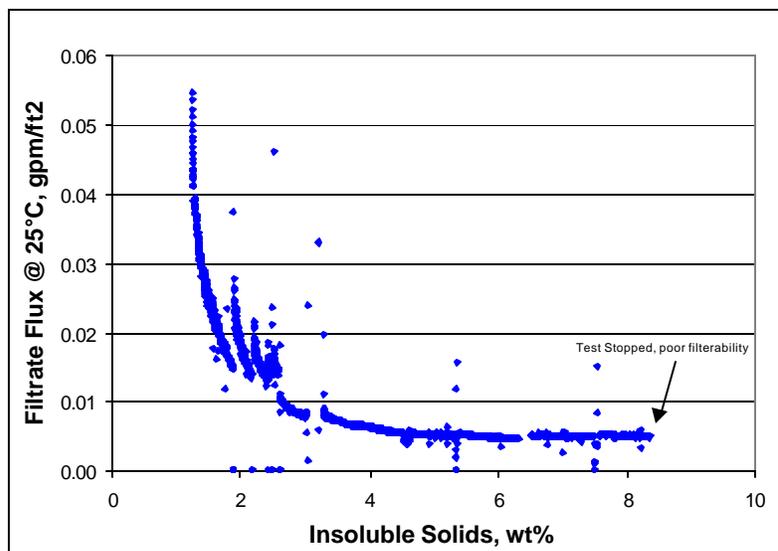


Figure 38. Pilot-scale X-flow UF Dewatering of AN-102R2, Batch 3C

### 3.3.2.4.2 Filtering Batch 3B

The second Batch 3 test (called 3B) followed the first Batch 3 test (called 3C) to confirm that good filterability could be attained with the organic based slurry by using baseline conditions, BC, during the precipitation step of the slurry preparation. The reluctance to initially use the BC slurry was because of the larger reagent quantities needed and the higher process temperature of 50°C, which were not necessary to attain the decontamination of the Strontium and Transuranic constituents from the slurry. However, using the newly optimized conditions, NOC (see above), resulted in an unfilterable slurry, but with BC Batch 3B, using the same flow parameters of  $V = 12$  ft/s and  $TMP = 40$  psid, an acceptable filter flux resulted.

Figure 39 shows a filtrate flux above the target mean of 0.02 gpm/ft<sup>2</sup> during the first 11.5 hours of the test. In fact, the entire test lasted just over 12 hours when the insoluble solids concentration went above 20 wt%, Fig. 40. The large drop off at the end was after the concentration was determined to be approximately 14 wt% and dewatering was continued until it went above 20 wt%. Even at the highest concentration the filtrate flux was still higher than the overall average of 0.011 gpm/ft<sup>2</sup> that was obtained during Batch 3C; therefore, the test was consider a success. Over the entire 12.2 hours of dewatering, the filtrate flux averaged at 0.048 gpm/ft<sup>2</sup>, or better than a factor of 4 over Batch 3C. Subsequently, the decontamination factors were measured for Batch 3B and were found to be acceptable (Steeper and Williams, 2003).

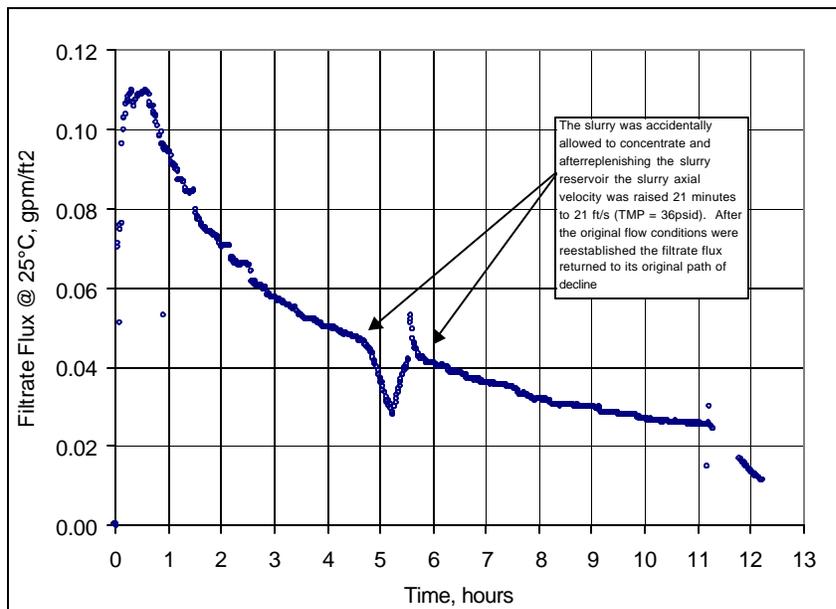


Figure 39. Batch 3B: Dewatering filter flux of AN-102R2 precipitated with the baseline conditions at 50°C.

Over the filtering period the average slurry velocity was  $V = 12.1$  ft/s, the average transmembrane pressure was  $TMP = 41$  psid, and the average slurry temperature was  $T = 26^\circ\text{C}$  (the filtrate flux was adjusted to  $T = 25^\circ\text{C}$ ). The test was done from 10/22 to 10/23/2002 and concentrated the insoluble solids from approximately 1 wt% to 22 wt%.

As a result of reaching the targeted solids concentration, this dewatering test run was followed by the steady-state runs, i.e., 1.17 to 1.29. These runs will be discussed in the next section of this report. Some other aspects of the Batch 3B dewatering test were: that no backpulse was done, a temporary drop of filtrate flow occurred around the 5<sup>th</sup> test hour, and a data gap at the 11.3 hour.

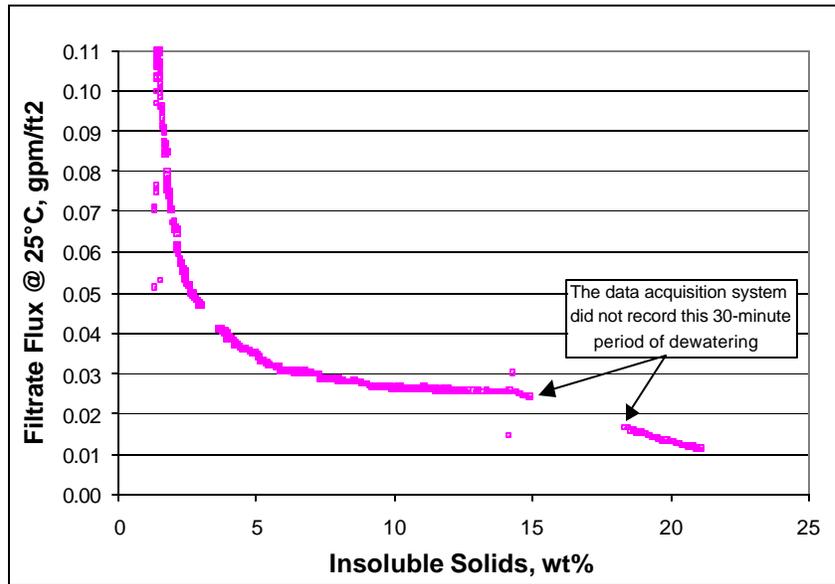


Figure 40. Pilot-scale X-flow UF Dewatering of AN-102R2, Batch 3B

- **No Backpulse**  
No backpulse was done for Batch 3B because the criterion of a filtrate flux below 0.015 gpm/ft<sup>2</sup> didn't occur during most of the test. At about the 12<sup>th</sup> hour the backpulse criterion was reached but by that time the test was all but complete, so a backpulse was not done.
- **Apparent data glitches were real events**  
At just past 4.5 hours into the test on Tuesday, 10/22/02, at around 8:15 PM the filtrate flux dropped precipitously, which continued until about 9:00 PM. During this time the slurry volume was not replenished and the slurry prematurely reached a high solids concentration. When the problem was discovered, more slurry was added to the test rig reservoir and the slurry axial velocity was increased from 12 to 21 ft/s for 21 minutes, in an attempt to recover the filtrate flux, without resorting to a backpulse which would have disturbed the filter cake. After 21 minutes, the filtrate flux appeared to be fully recovered, therefore the slurry velocity was returned to 12 ft/s. However, the filtrate flux continued to increase and then decrease to the original flux. At about 9:30 PM the excursion had passed and the flux was recovered. It appeared that the filter cake had returned to its appropriate thickness, as if the upset never occurred. On Wednesday, 10/23/2002, at 3:00 AM, 11.3 hours after starting the test, dewatering was stopped to evaluate the solids concentration and wait for another batch of simulant to be made. However, the solids concentration, turned out to be slightly more than 14 wt%. This was

deemed sufficiently high such that the remaining slurry could be concentrated above 20 wt%. This was very important because it meant the remaining chemicals on hand could be saved to make enough slurry to carry out a third test and save the program considerable expense. At about 6:00 PM on the same day, the Batch 3B test restarted to further concentrate the slurry. That last concentration process took about one hour. Unfortunately, during the first 30 minutes of dewatering the data logger was not operating, but it did capture the last 30 minutes (from 6:30 PM to the end at 7:00 PM), when the concentration reached 22 wt%. The actual final concentration was only known with a subsequent solids analysis. The actual filtrate flux, when the test rig was restarted at 6:00 PM, began above the final flux of 0.024 gpm/ft<sup>2</sup>, when the test was stopped at 3:00 AM earlier.

#### **3.3.2.4.3 Filtering Batch 3A**

After completing a successful Batch 3B test, it was important to know if filterability was sensitive to precipitation temperature. The reduced amount of simulant used for Batch 3B, approximately 1000 liters, enabled one more Batch 3 of approximately 900 liters to be made with the remaining chemicals. A third and final Batch 3 test (called 3A), was done, but the precipitation temperature of 50°C was lowered to 25°C. If good filterability could also be obtained at a lower temperature, then less hardware and energy would be needed by the Waste Treatment Plant.

The use of BC, while precipitating at 25°C, did obtain a filtrate flux better than Batch 3C, but unfortunately it was not as good as Batch 3B. Figure 41 shows the time plot of the entire data set as the insoluble solids concentration increased from 1.6 to 25 wt% as seen in Fig. 42, which plots filter flux as a function of insoluble solids wt%. The average filtrate flux over that period was 0.019 gpm/ft<sup>2</sup>, which is a factor of 1.7 better than Batch 3C, but only 40% that of Batch 3B. After only 8 hours of filtering, the flux dropped below the target mean of 0.02 gpm/ft<sup>2</sup>, and after 13 hours the flux dropped below the backpulsing criterion of 0.015 gpm/ft<sup>2</sup>, which initiated backpulsing. Over the next 7 hours the filter was backpulsed six times with each successive backpulse less effective. At the 21<sup>st</sup> hour, the RPP customer asked to stop backpulsing to see where the filtrate flux would end up as the concentration increased. At about the 26<sup>th</sup> hour, the flux reduced to close to 0.01 gpm/ft<sup>2</sup> and permission was obtained to stop the test on Thursday, 11/7/02. The test was then continued on the following Monday, 11/11/02. At that point the insoluble solids concentration was evaluated and found to be 15 wt%. For about 3 hours on Monday the slurry was concentrated from 15 to 25 wt%. Interestingly, the slurry filtrate flux increased from its value when the test was stopped on Thursday, 11/7/2003, of just above 0.01 gpm/ft<sup>2</sup> to just below 0.02 gpm/ft<sup>2</sup>. Something occurred during the 88 hours it sat idle, from Thursday evening at 5 PM until Monday morning at 9 AM. However after about one hour of filtering the filtrate flux dropped very fast as the solids concentration approached 20 wt% and then onto 25 wt%. It is possible that during the time period some of the filter cake fell off the filter surface since the filter was vertically oriented. At the end of Batch 3A filtering the filtrate flux dropped to the same rate that Batch 3C ended, i.e., 0.005 gpm/ft<sup>2</sup>. It seems clear from the three Batch 3 filtering tests that if a flux of better than 0.02 gpm/ft<sup>2</sup> is needed, it is very important to precipitate at the higher temperature, i.e., 50°C.

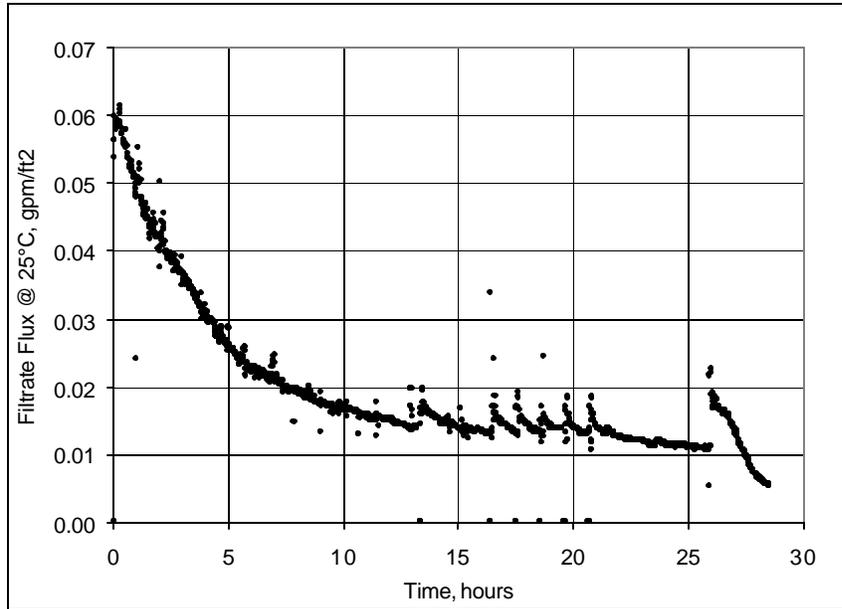


Figure 41. Batch 3A: Dewatering filter flux of AN-102R2 precipitated with the baseline conditions at 20°C.

Over the filtering period the average slurry velocity was  $V = 12.0$  ft/s, the average transmembrane pressure was  $TMP = 40$  psid, and the average slurry temperature was  $T = 25^\circ\text{C}$  (the filtrate flux was adjusted to  $T = 25^\circ\text{C}$ ). The test was done from 11/6 to 11/11/2002 and concentrated the insoluble solids from approximately 1.6 wt% to 25 wt%.

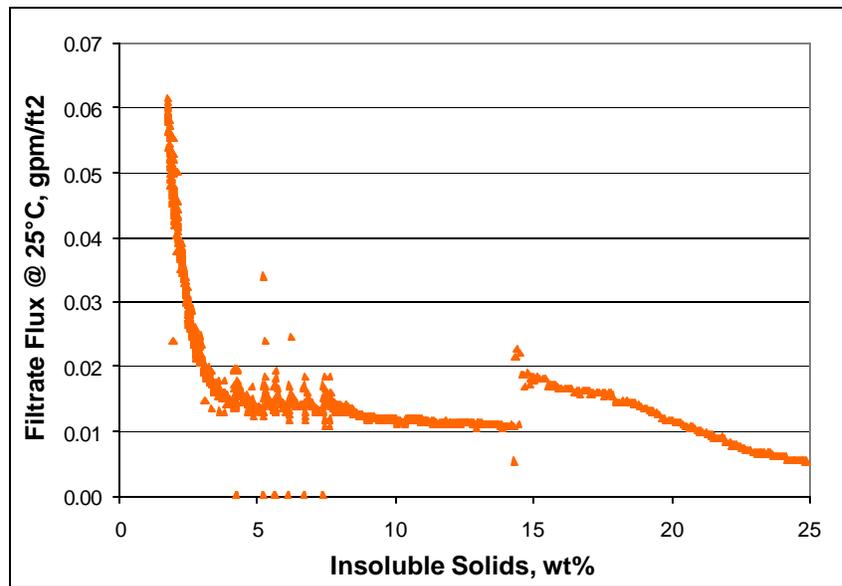


Figure 42. Pilot-scale X-flow UF Dewatering of AN-102R2, Batch 3A

### 3.3.2.4.4 Filtering Batch 4A

After completing the Batch 3 tests, for which the simulants were all prepared under well-mixed precipitation conditions, a Batch 4 test was planned to precipitate under more WTP-prototypic mixing conditions. That is, the WTP will use pulse jet mixers (PJM) that creates a completely different mixing environment as compared to standard impeller-type agitator. A new precipitation test rig was developed for this test (see Steeper and Williams, 2003). Two tests were planned, 1. Batch 4A, where the AN-102R2 simulant would be made at baseline conditions, and 2. Batch 4B, which would be done depending on the results of 4A.

Figure 43 shows the results of Batch 4A testing. The results were similar to Batch 3A, for which the filtrate flux was considered borderline acceptable. Figure 44 shows the entire data set as the insoluble solids concentration increased from 1.5 to 18 wt%, over the 19.5-hour period of dewatering. The average filtrate flux over that period was 0.019 gpm/ft<sup>2</sup>, which was the same as Batch 3A. That is, a factor of 1.7 better than Batch 3C, but only 40% that of Batch 3B. However, instead of only 8 hours of filtering, the flux dropped below the target mean of 0.02 gpm/ft<sup>2</sup>, in just under 5 hours! Conversely, even after 18 hours the flux still did not drop below the backpulsing criterion of 0.015 gpm/ft<sup>2</sup>. For this test the RPP-WTP customer requested a backpulse when the flux dropped below 0.02 gpm/ft<sup>2</sup>. This occurred at about 5.5 hours into the run. As before, the flux dropped very fast after the backpulse and after two more backpulses, around the 9<sup>th</sup> hour of filtering, there seemed to be no further advantage to backpulsing, therefore it was stopped

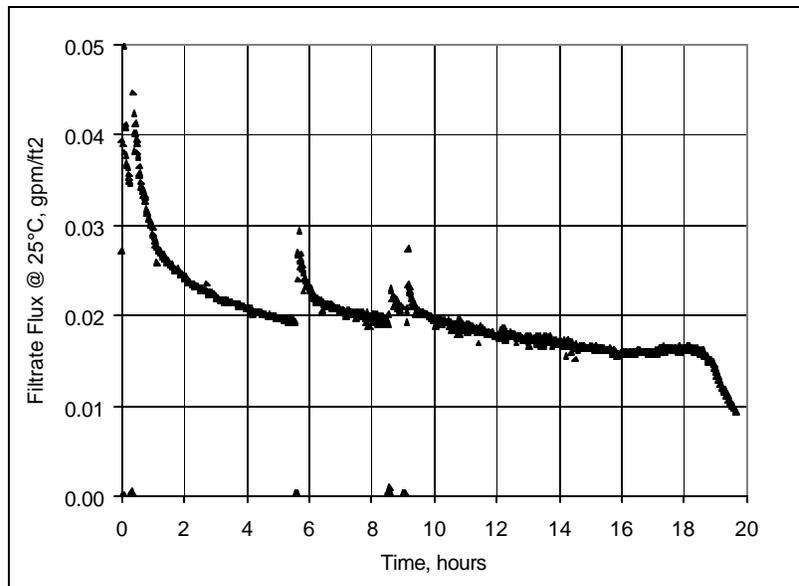


Figure 43. Batch 4A: Dewatering filter flux of AN-102R2 precipitated with the baseline conditions at 25°C.

Over the filtering period the average slurry velocity was  $V = 11.9$  ft/s, the average transmembrane pressure was  $TMP = 40$  psid, and the average slurry temperature was  $T = 25^\circ\text{C}$ . The test was done from 03/12 to 03/13/2003 and concentrated the insoluble solids from approximately 1.5 wt% to 18 wt%.

Batch 4A was smaller than the Batch 3, i.e., 650 liters, see Fig. 36; therefore there was no stopping point to see if the target insoluble solids concentration was reached. Because the filterability was only borderline the RPP-WTP customer decided not to have another batch of simulant made and that Batch 4A should be concentrated as high as possible in the hope of reaching the target 15 wt%. The slurry volume was reduced to just before the test rig reservoir began to aspirate air, which would have stopped slurry circulation and thus filtering. When the approximate 650 liters were reduced to 60 liters the test was stopped and slurry samples were taken. It turned out the target was exceeded, since the final concentration was 18.3 wt%. For dewatering operation, the test was a success.

Once again, the conclusion for Batch 4A is the same as for Batch 3A. That is, if a filtrate flux of better than 0.02 gpm/ft<sup>2</sup> is required then the precipitation mixing environment needs to be better. While Batch 3A needed to be mixed at the Batch 3B temperature of 50°C, Batch 4A needed to be mixed with more vigorous agitation than was available with the single pulse jet mixer. While the pilot test used only one PJM in the precipitation tank, the WTP plant has multiple PJM units planned for its precipitation tank. Creative uses of different mixing cycles for the many PJMs in the WTP tank may overcome the poor mixing results for this single PJM test.

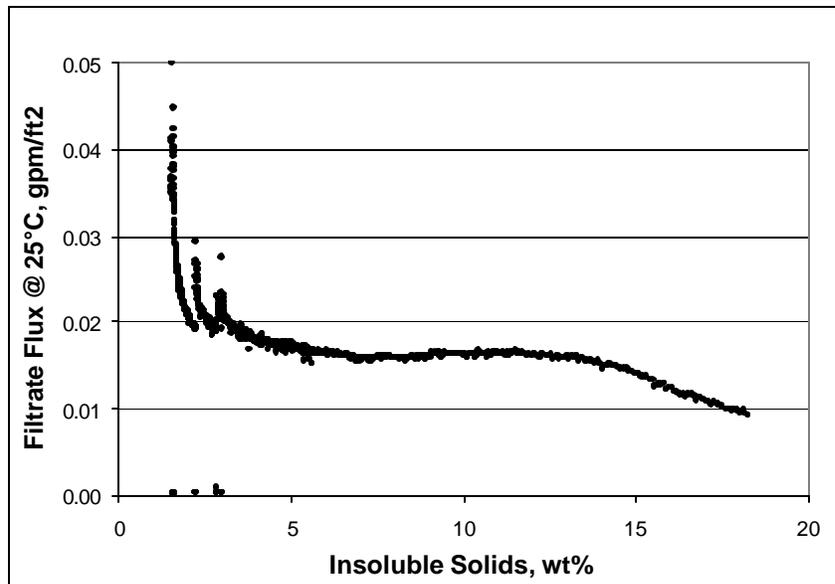


Figure 44. Pilot-scale X-flow UF Dewatering of AN-102R2, Batch 4A

#### 3.3.2.4.5 Overall Dewatering Results of AN-102R2

For comparison Fig. 45 combines the filtrate flux curves for all four runs. The slurry simulant that filtered the best was Batch 3B, which was precipitated under the original baseline conditions, and the worst was Batch 3C, which was done under a set of optimized conditions. Looking at the slurry data in Fig. 36 the reason for the disparity is not obvious. Out of all the simulants 3B had the smallest particles and was the only slurry where there was a significant reduction in the particle size after dewatering, i.e., from the low to high solids concentration. For all other properties the four simulants started at about the same

conditions, i.e., total solids of 33 wt%, viscosity of 4 cP and no yield stress, slurry density of 1.29 g/ml, bi-modal particle volume distribution of about half with particles between 8 to 10 microns and half between 2 and 3 microns (the exception was 4A which only had one particle size mean of 2.7 microns). Also, a scan of the rheological data characteristics in Appendix G does not elicit significant differences. All the simulants act as time-dependent pseudoplastics at the highest solids concentrations.

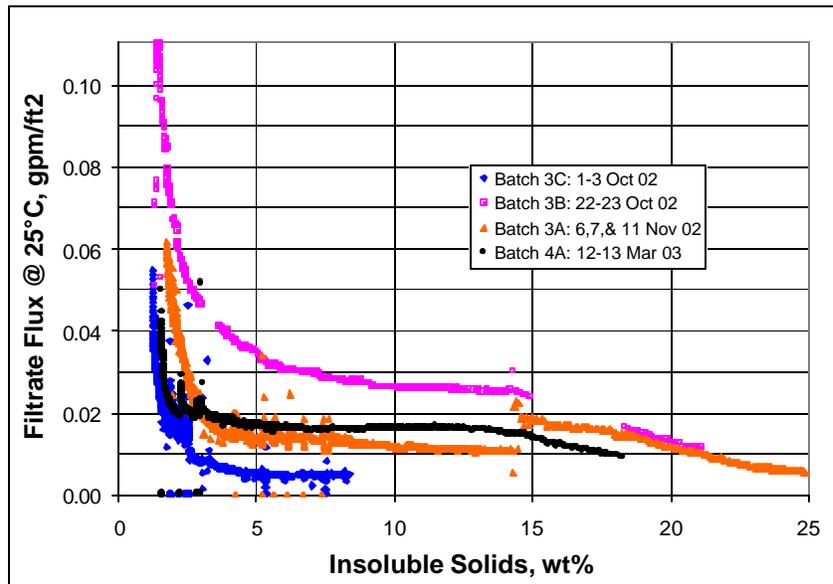


Figure 45. Pilot-scale X-flow UF Dewatering of AN-102R2, Batches 3 & 4

To definitively state why the filtrate fluxes differed among the simulants a lot more information would be needed about different chemical characteristics of the simulants. For instance, the particle-to-particle attractiveness. All the slurries appeared to be very sticky and thick as the solids concentration increased. How this affected the filter and the integrity of the filter cake is unknown. One telling feature was that backpulsing was not very affective. This indicates that much of the cake was not removed when a backpulse was made and as the cake became thicker backpulsing became completely ineffective. Small differences in a slurry's ability to adhere to the filter surface, and itself, very probably would lead to large differences in impeding filtrate from entering the porous substrate.

One notable feature in Fig. 45 is the sharp drop in filter flux when the insoluble solids concentration went beyond about 14 wt%. Roughly speaking there appears to be three distinct filtering regions:

1. From 0 to 5 wt% the filter flux drops precipitously as the filter cake forms and grows fast, relative to its initially formed thickness.
2. From 5 wt% to 15 wt% the filter flux is relatively stable. The filter cake is formed and further growth is slow, relative to the established thickness.

- Greater than 15 wt%, the filter flux begins to drop faster because the solids are close enough together to significantly increase the slurry viscosity, probably exponentially. See Fig. 46.

To understand these different regions it may help to look at some of the individual measured parameters shown in Fig. 36, or in Appendix G. Figure 46 shows one batch, Batch 3A, (using a modified Fig. 41) with some of the rheological data superimposed.

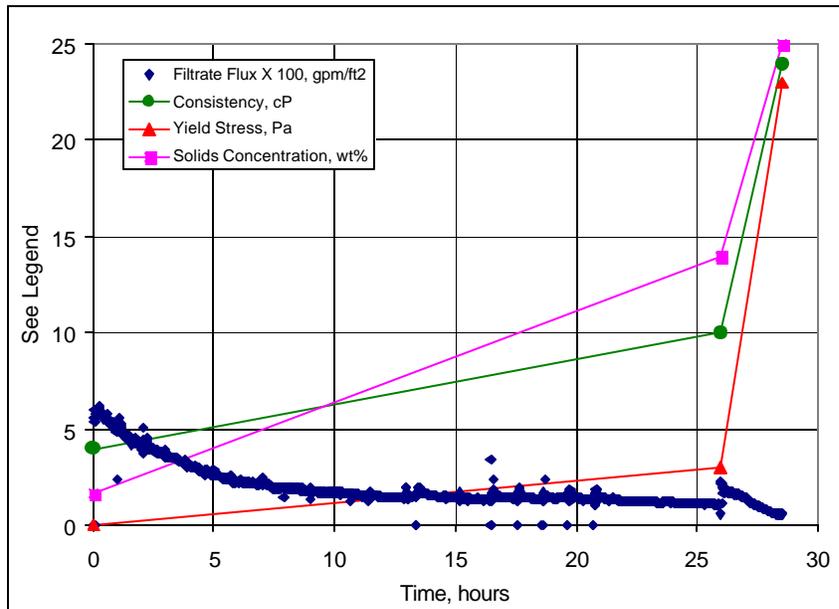


Figure 46. Batch 3A filtrate flux with selected rheological properties

It does appear that in region 3, after 14 wt% of insoluble solids, the rheological properties change significantly causing the filtrate flux to drop. Other differences among the different slurries are shown in Figs. 47 through 51 below.

Figures 47 and 48 show a distinct difference in the rheological properties of all the slurries made using baseline conditions (3B, 3A, and 4A) and the first test of 3C which was made with the newly optimized conditions. The much higher slurry consistency and yield stress was probably a major contributor in making 3C much harder to filter. This implies baseline conditions should be used during the precipitation of Envelope C slurries. However, the density for all the simulants seemed to be similar, Fig. 49.

From Figs. 50 and 51 it appears that all the slurries started with approximately the same size particles. That is, in the entire population of particles the mean particle size was very close to 2 microns and if particle volume is considered the particles were approximately equally distributed around two means, i.e., 2.5 microns and 9 microns.

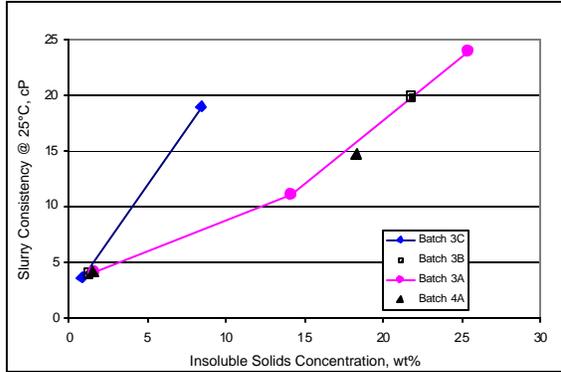


Figure 47. Batch 3&4 Slurry Consistency

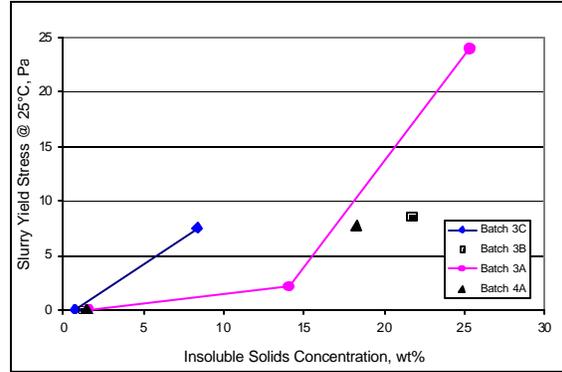


Figure 48. Batch 3&4 Slurry Yield Stress

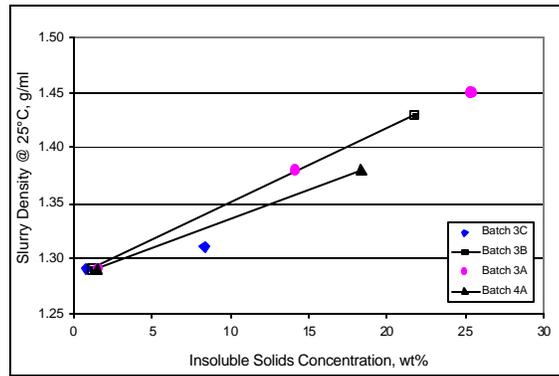


Figure 49. Batch 3&4 Slurry Density

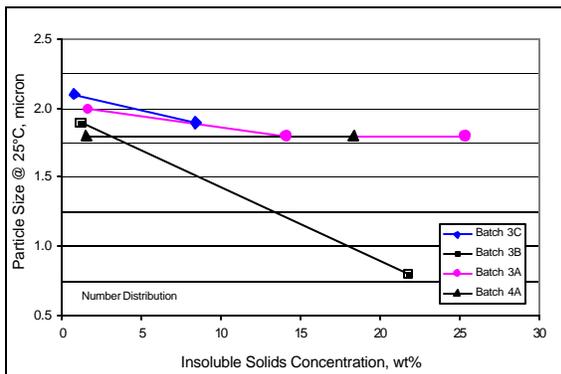


Figure 50. Batch 3&4 Mean Particle Size (by Number Distribution)

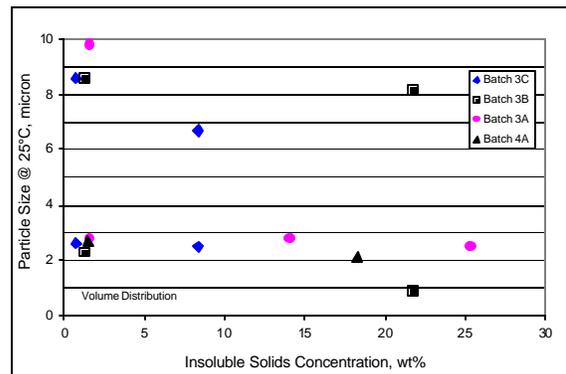


Figure 51. Batch 3&4 Mean Particle Size (by Volume Distribution)

As the simulants were circulated in the filtration facility some particle changes are evident. Figure 50 shows that mean population particle size did not change significantly for most of the simulants. However, Batch 3B stands out because its particles ended up to be less than one half as small. Remember, Batch 3B had the best filterability. With respect to the volumetric distribution of particles, all but Batch 4A started with bi-modal distributions. After dewatering the particle distributions for all but Batch 3B became mono-modal. (Actually they all did because the bi-modal distribution of Batch 3B was weak, i.e., only 13% of the particles had a distribution around the mean of 8 microns.) A notable difference was Batch 4A, which started and ended with a single mean particle size, though the size became slightly smaller, i.e., 2.2 microns to 0.9 microns.

### **3.3.2.5 Steady State Filtering of AN-102R2 Slurry Simulant**

The requirement of the Task Plan (Duignan, 2002a) was that after dewatering the Envelope C simulant to some high concentration of insoluble solids<sup>‡</sup>, it would be filtered while maintaining the solids concentration constant. In this way, a series of filter tests could be done to determine an optimum slurry velocity and transmembrane pressure.

#### **3.3.2.5.1 Typical Constant Insoluble Solids Concentration Steady-State Test Run**

Before discussing the overall steady-state results it is useful to look at one filter flux versus time to better understand the average data results. Figure 52 shows test run 1.17, for Batch 3B, which is a typical filter flux with time. While the other test runs have different magnitudes of filter fluxes the overall characteristics of filter flux with time are similar and therefore not shown here, but these can be found in Appendix E.

At the beginning of each steady-state run the typical operation is as follows: a backpulse is done in an attempt to start at the same point. However, due to depth fouling the filtrate flux will always decrease a small amount with each successive backpulse. This will be discussed later in this section. During the first few minutes there is no filtrate flux, while the filter is backpulsed. This then jumps to the highest flux, as a result of reestablishing filtrate flow after a backpulse. As soon as flow begins the flux drop precipitously as the filter cake begins to build. Within 30 to 40 minutes approximately 90% of the cake has been established (as indicated by the 90% drop in the filtrate flux from approximately 0.017 gpm/ft<sup>2</sup>, right after the backpulse, to 0.010 gpm/ft<sup>2</sup> after about 40 minutes) and then there is a very slow reduction in flux with time. After about 2 hours an asymptote is reached (Fig. 29 in Duignan (2000a) shows that after 8 hours the 2-hour flux is still basically the same). Note what appears to be a second backpulse just before the 10-minute mark. No second backpulse was given and this is a feature of how this particular filter test rig works. Just before the Batch 3B test the meter which measures filtrate flow was reoriented. Figure 2 shows the schematic of the test rig where the low flow filtrate flowmeter, Q2, is just downstream of valve V27. Originally the filtrate flowmeter was in the filtrate return line from the pulsepot, so that its large pressure drop would not affect the backpulse filtrate flow. Unfortunately, in that location it was necessary for the entire backpulse system to be liquid solid before the meter

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<sup>‡</sup> For dewatering the target insoluble solids concentration was 15 wt%, but a high concentration was preferable.

began registering a flow. For the unexpectedly very low flowrates experienced during the Batch 3C campaign, it took close to 30 minutes to replace the approximately 1.8 liters of filtrate evacuated during a backpulse. Having data during the first half an hour of operation is very important, as can be seen in Fig.52.

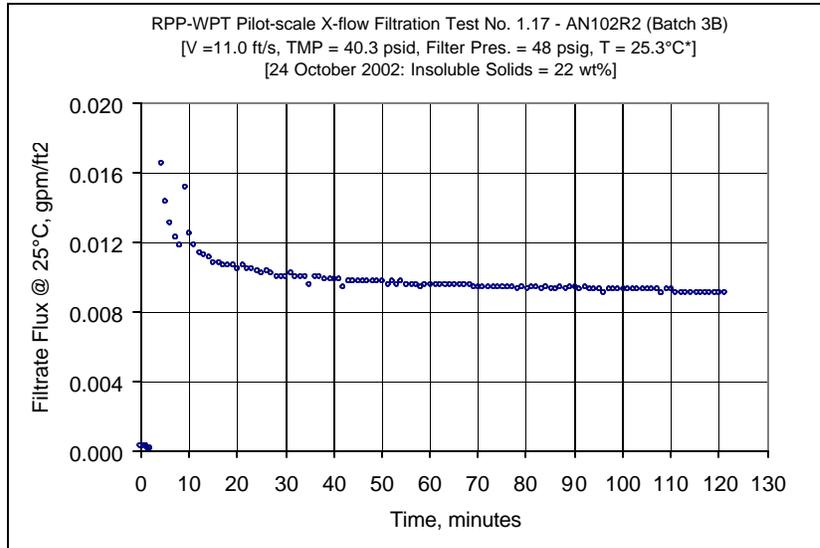


Figure 52. Batch 3B: Test Run 1.17

Over the filtering period the average slurry velocity was  $V = 11.0$  ft/s, the average transmembrane pressure was  $TMP = 40.3$  psid, and the average slurry temperature was  $T = 25.3^\circ\text{C}$  (the filtrate flux was adjusted to  $T = 25^\circ\text{C}$ ).

The low flow filtrate flowmeter was moved to the tubing between the filter housing and the pulsepot so immediate measurements could be taken; a special bypass line was used to valve out the flowmeter during a backpulse to avoid the high pressure drop that the meter would cause. Even though the new meter location allows the immediate measurement of filtrate flux, after filtrate flow is reestablished, the filtrate system still has a charge of air that needs to be expelled as the system is refilled with filtrate. In the case of test run 1.17 it took about 5 minutes to refill. Indeed, at 1.8 liters (= 0.48 gallons) the average flowrate over that time period of  $0.014$  gpm/ft<sup>2</sup> gives a time of  $0.48 / 0.014$  gal/min/ft<sup>2</sup> /  $6.707$  ft<sup>2</sup> = 5.1 minutes ( $6.707$  ft<sup>2</sup> is the flow area for the seven filter tubes). This happens because during refilling the air-filled system takes more pressure to flow, reducing the TMP. After becoming liquid solid the filtrate system pressure goes down and the TMP increased to its original setting before the backpulse was made.

In the figure caption of Fig. 52 some average measurements, i.e.,  $V$ ,  $TMP$ , and Slurry Temperature,  $T$ , are given and are based on all the data points taken during the test run, excluding the first few minutes during the backpulse. For example, the data for Figure 52 can be found in Appendix E, Figs. E2-1 and E2-2. The averages were based on 119 data points from the 3<sup>rd</sup> minute until the 121<sup>st</sup> minute. The abscissa shows the filtrate flux at

25°C, which indicates that while the actual slurry temperature may have been different from 25°C (it was actually 25.3 ±0.3°C) it was adjusted for the effects of fluid viscosity and surface tension (Townson, 2002a) with the equation:

$$\text{Flux @ 25°C} = P/A \times C$$

where

Flux	= filtrate flux at 25°C (gpm/ft <sup>2</sup> )
P	= filtrate flow rate (gpm)
A	= filter surface area (ft <sup>2</sup> )
C	= temperature correction factor = $e^{(2500*((1/(273+T))-(1/298)))}$
T	= slurry/filtrate temperature in degrees Celsius

### 3.3.2.5.2 Filtering Batch 3C

No steady state tests were performed because the dewatering test was stopped after 46 hours because of low filterability and that the insoluble solids concentration only reached 8.5 wt%.

### 3.3.2.5.3 Filtering Batch 3B

The second Batch 3 test (called 3B) experienced good filterability and at the end of the dewatering, test run 1.16, it still was filtering at just above 0.01 gpm/ft<sup>2</sup> when the insoluble solids concentration reached its highest concentration, i.e., 22 wt%. The steady-state filter runs completed at 22 wt% insoluble solids were:

1.17, 1.18, 1.19, 1.20	done on 24 October 2002
1.21, 1.22, 1.23, 1.24	done on 28 October 2002
1.25, 1.26, 1.27, 1.28, 1.29	done on 29 October 2002

Figure 53 depicts the average filtrate flux results for all the Batch 3B test runs. As per the Task Plant (Duignan, 2002a) five of the runs (1.17, 1.18, 1.19, 1.24, and 1.29) were done for two hours and the remaining eight runs were done for one hour. However, the average filtrate flux values for all test runs are shown for one hour to make a better comparison. If the two-hour average were used it would only lower the average of those five test runs by 5 to 8%, or about to the lower part of the error bars shown, which are ±5.4%; this can be seen in Fig. 53. Also note that the temperature for two runs (1.26 and 1.27) exceeded the target of 25°C ±5°C. One had the highest slurry velocity, V=14.7 ft/s with a low TMP, i.e., 31 psid, and the other had the lowest TMP, i.e., 23 psid. At these pressures<sup>†</sup> the test rig cooling coil was unable to provide the necessary cooling.

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<sup>†</sup> The temperature control problem is an aspect of the pilot-scale test rig. Figure 2 shows the slurry cooling coil to be on either side of the pressure control valve, V11, which is in parallel with the main slurry flow. In order to obtain low filter pressures V11 is run almost wide open, which starves slurry flow to the cooling coil and thus cuts down on cooling. The coil could not be put in series with the main slurry flow because the pressure drop would have been too large for most of the test runs.

Figure 53 shows the Batch 3B test runs in chronological order and the total operational time the filter was active during these runs was about 18 hours. As time progressed the filtrate flux continually decreases. This is the result of depth fouling which is not removed by backpulsing. Fouling is actually increased because of backpulsing, which exposes the filter surface to the smallest particles in a slurry. For these tests the filter was backpulsed each time a new test began. Before a statement can be made about the dependence of filtrate flux on V and TMP, the effect of depth fouling needs addressing. Fortunately, the five 2-hour test runs were all done at the same V and TMP so a comparison can be made. By plotting only those five test runs the effect of fouling becomes more evident.

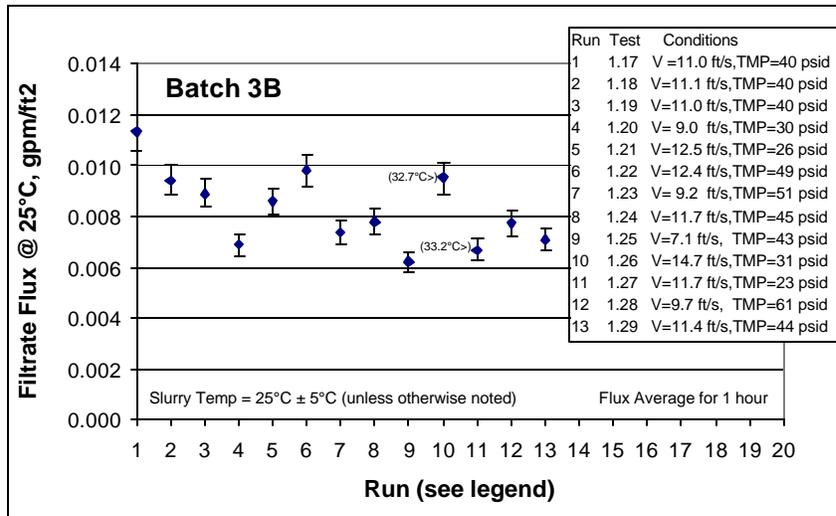


Figure 53. Batch 3B: Filtrate flux results averaged over the first hour of testing, including the five 2-hour test, i.e., 1.17, 1.18, 1.19, 1.24, and 1.29.

The tests were done from 10/24 to 10/29/2002 and at a constant insoluble solids concentration of 22 wt%.

Figure 54 shows just the five test runs with the same V and TMP. There was a small variation in these parameters, which are shown on the figure.

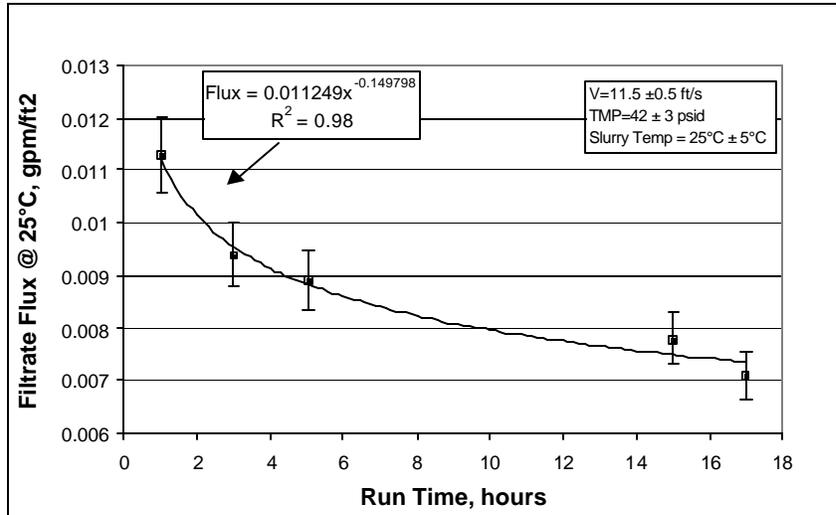


Figure 54. Batch 3B: Filtrate flux results averaged over the first hour of testing for the five 2-hour test runs, i.e., 1.17, 1.18, 1.19, 1.24, and 1.29. These runs are unique in that they all have the same flow parameters  $V \sim 11$  ft/s and  $TMP \sim 40$  psid.

The data indicate a decreasing average filtrate flux with time. Now this decrease could also indicate a slurry that is changing with time becoming more difficult to filter. It may be that the solid particles in the slurry were changing and making the filter cake less permeable. However, particle analyses do not support this theory<sup>†</sup>. As shown on Fig. 54, the data were correlated to the power relation indicated and each point includes the measurement uncertainty. This relation can then be used to adjust the steady-state data to remove the effect of fouling.

Figure 55 repeats Fig. 53, but with the data adjusted with the relation shown in Fig. 54. A comparison between the data in Figs. 53 and 55 indicate a difference as to which are the most appropriate parameters to obtain the best filtrate flux. As expected, from past tests (e.g., Duignan, 2000a and b) the key factor was the slurry axial velocity. Figure 55 shows that for run 10, test 1.26, with  $V = 14.7$  ft/s, the best filtrate flux occurred, despite the fact it had a very low TMP (31 psid). The next highest, but statistically the same filtrate flux, was run 6, test 1.22, where both the slurry velocity,  $V = 12.4$  ft/s, and TMP (49 psid) were moderately high.

<sup>†</sup> From the particle size analysis results on the slurry done before the steady state test runs (Appendix G, sample 300188110) and after (Appendix G, sample 300189271): Before - the population distribution particle average diameter was  $0.8 \pm 0.2$  and the volume distribution particle average diameter was  $0.9 \pm 0.5$  micron. After - the population distribution particle average diameter was  $1.2 \pm 0.4$  and the volume distribution particle average diameter was  $1.3 \pm 0.5$  micron. The uncertainty given is twice the standard deviation representing the 95% confidence level. Statistically the particle did not change in size.

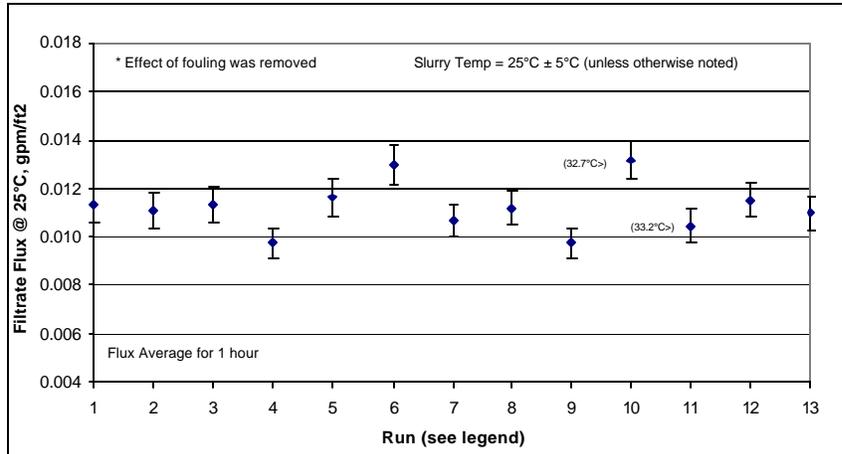


Figure 55. Batch 3B: This figure repeats the data shown in Fig. 53 with depth fouling effect removed. [The legend indicated in the abscissa title is that of Fig. 53.]

To more easily see the individual effects of V and TMP on the filtrate flux the data are shown for both. Figure 56 shows the effect of TMP and statistically there is none. The data were correlated with a linear least-squares fit and the correlation coefficient is near zero. Considering measurement uncertainty a coefficient of zero cannot be ruled out. Therefore, a decision of which operating TMP to use should be based on other consideration and not improvement of filtrate flux.

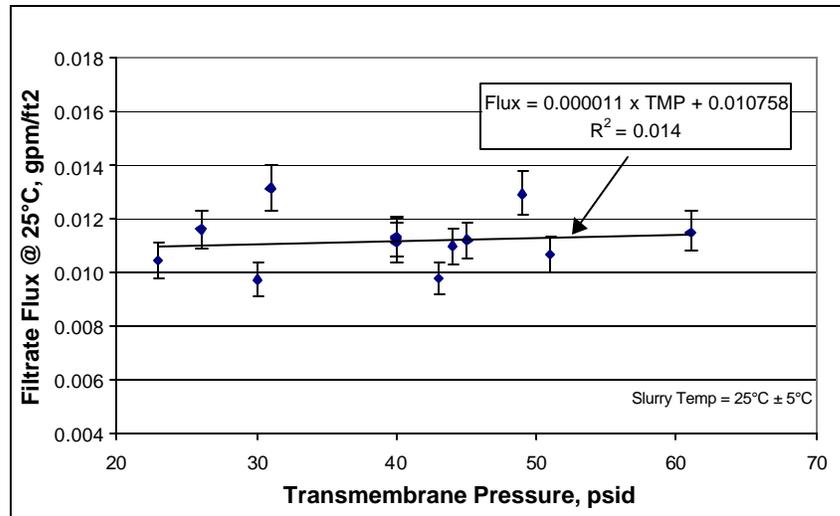


Figure 56. Batch 3B: All the steady-state data that were adjusted for depth fouling effect removed (Fig. 55) as a function of transmembrane pressure, TMP.

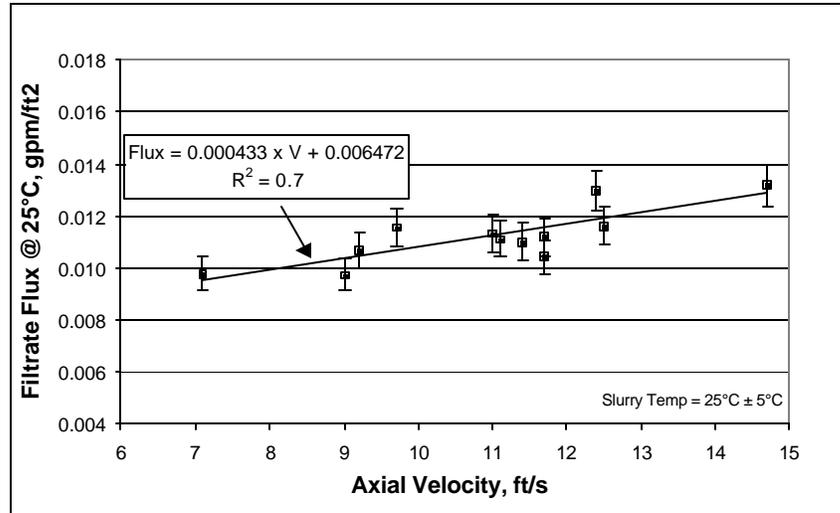


Figure 57. Batch 3B: All the steady-state data that were adjusted for depth fouling effect removed (Fig. 55) as a function of slurry axial velocity, V.

Figure 57 shows the Batch 3B data as a function of the slurry axial velocity, V. The figure includes a linear least-squares fit of the data with a correlation coefficient of 0.7 and therefore the filtrate flux is clearly dependent upon V, even when considering the measurement uncertainty as shown on the figure. The conclusion that can be made from this analysis is that to increase filtrate flux, V must increase.

#### 3.3.2.5.4 Filtering Batch 3A

The third Batch 3 test (called 3A) experienced better filterability than Batch 3C, but not as good as Batch 3B. Because of the length of the Batch 3A dewatering test, i.e., around 30 hours, and good Batch 3B results, the RPP customer did not require the full series of steady state test runs. However, due to the available time, slurry, and the desire to make some inter-Batch 3 comparisons, a limited number of steady-state runs were performed. Once the high insoluble solids concentration was attained (it ended up being 25 wt%) the steady-state runs began. The runs completed were:

1.17, 1.20	done on 11 November 2002
1.23, 1.25, 1.28, 1.29	done on 12 November 2002

The choice of test runs to perform depended on the ability to keep the slurry within the temperature limit of 25°C ±5°C. For instance, two attempts were made to do test run 1.27, which had the lowest TMP of 20 psid (see the first footnote in section 1.3.2.5.3). Unfortunately, within minutes of test initiation the temperature climbed above 30°C and reach 40°C before it could be controlled.

Figure 58 depicts the average filtrate flux results for all the Batch 3A test runs. The six tests done were limited to one hour of filtering. The RPP customer did not required the extra hour because these tests were only to confirm filtrate fluxes and not to be used to optimize flow

parameters. That is, all of the average filtrate flux values shown in Fig. 58 are over the entire run time for each test of one hour.

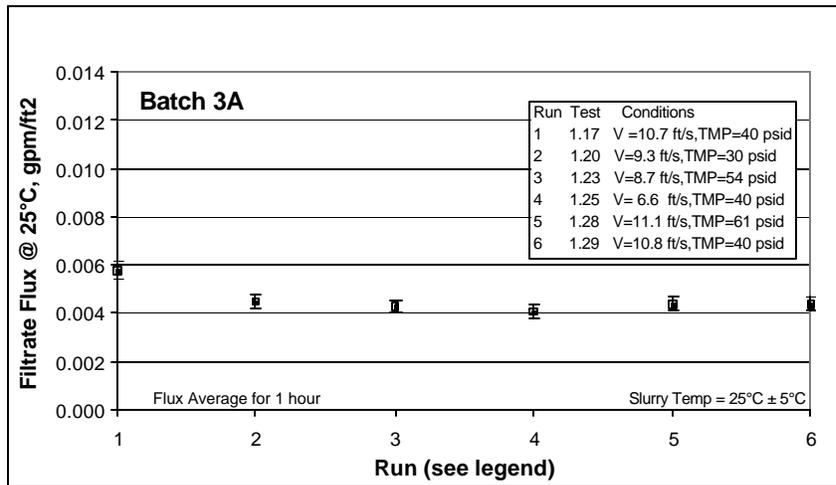


Figure 58. Batch 3A: Filtrate flux results averaged over the one hour of each test. The tests were done from 11/11 to 11/12/2002 and at a constant insoluble solids concentration of 25 wt%. The same filtrate flux range as shown on Fig. 53 was used for comparison.

Because the Batch 3A filtrate flux data are approximately a factor of 2 lower than the Batch 3B data (see Fig. 53) it's a bit harder to perceive trends, but both batches are similar. In fact, the depth fouling characteristics were very similar. Run 1, test 1.17, and run 6, test 1.29 for Batch 3A have the same flow conditions as those shown in Fig. 54. Since the Batch 3B and 3A filtrate flux magnitudes are different, the data shown in Figure 59 were normalized by the first result (at the 1-hour mark) from each data.

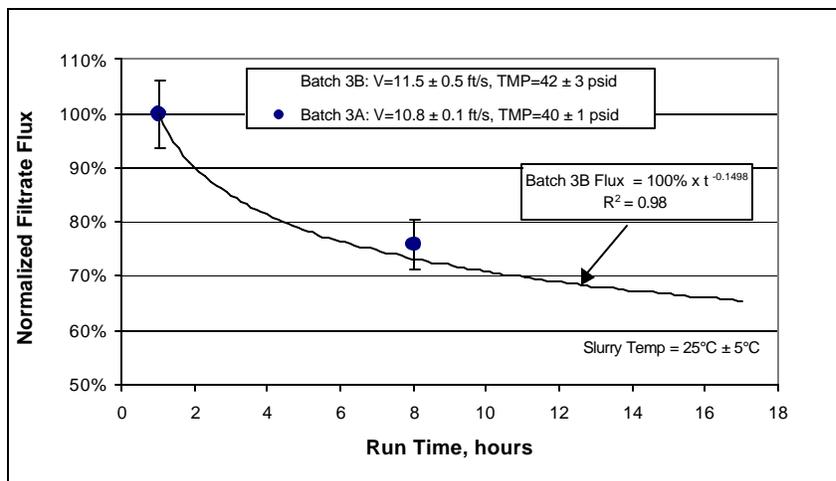


Figure 59. Batch 3A: Two filtrate flux data points shown are the average over the one hour test runs, i.e., 1.17 and 1.29. The Batch 3B curve fit is also shown for comparison. Both data sets were normalized by their respective first test run result (test run 1.17).

For example, the 1-hour average filtrate flux for Batch 3B was 0.0113 gpm/ft<sup>2</sup>, so each of the five points shown in Fig. 54 were divided by 0.0113; along with the fitted curve equation. The same was done for the two data points of Batch 3A using the 1-hour average filtrate flux of 0.0058 gpm/ft<sup>2</sup>. While the slurry solids were precipitated in a slightly different way, making Batch 3A not as filterable as Batch 3B, the filter depth fouling mechanism seems to be the same. This similarity is seen in Fig. 59 by the closeness of the Batch 3A datum point at the 8<sup>th</sup> hour to the Batch 3B data curve fit. Of course, because of the normalization the first point of Batches 3B and 3A were forced to be 100% and thus that degree of freedom was lost.

Using the same process to adjust the Batch 3B data to minimize the effects of depth fouling the Batch 3A data are shown in Figure 60. Note that the ordinate range has been reduced to better display the data because of the low magnitude and small differences.

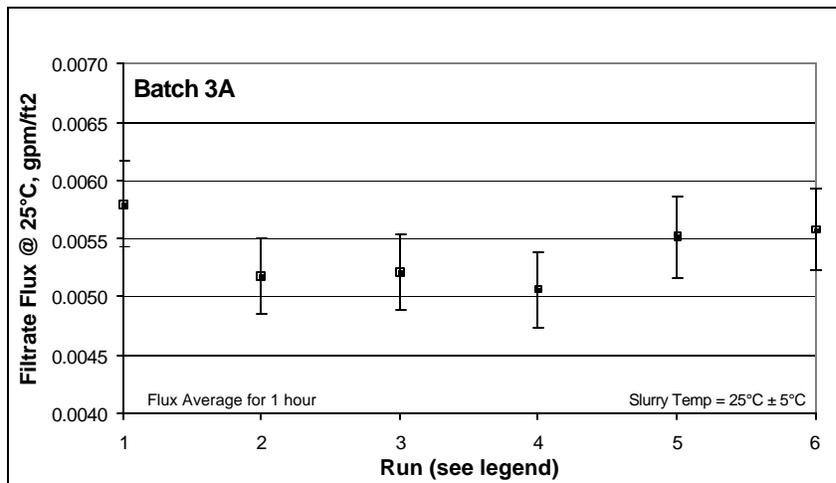


Figure 60. Batch 3A: This figure repeats of the data shown in Fig. 58 with depth fouling effect removed. [The legend indicated on the abscissa title is that of Fig. 58.]

As with Batch 3B data, if the Batch 3A results are shown as a function of TMP and V then filtrate flux dependence becomes evident. Figure 61 has TMP as the independent variable and Fig. 62 the axial velocity, V.

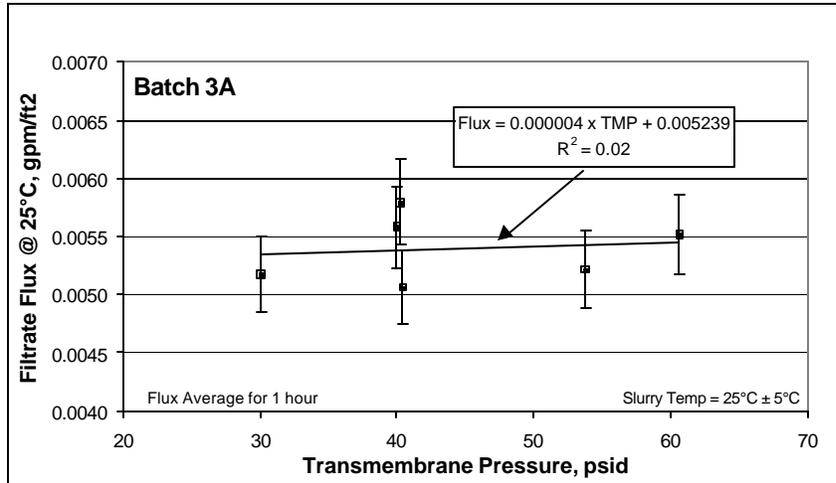


Figure 61. Batch 3A: All the steady-state data that were adjusted for depth fouling effect removed (Fig. 60) as a function of transmembrane pressure, TMP.

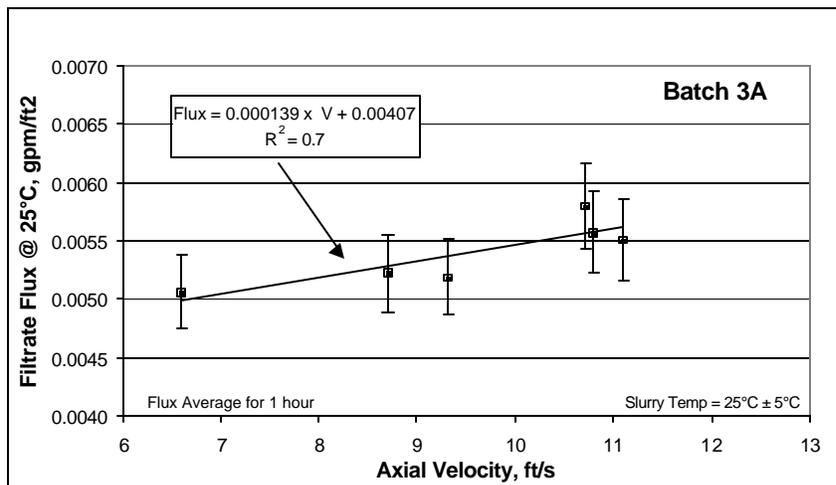


Figure 62. Batch 3A: All the steady-state data that were adjusted for depth fouling effect removed (Fig. 60) as a function of slurry axial velocity, V.

Once again, it appears that filtrate flux is not (or only very weakly) dependent upon the transmembrane pressure, while there is strong correlation with the slurry axial velocity in the filter tubes.

### 3.3.2.6 Washing and Concentration of Washed<sup>†</sup> AN-102R2 Slurry Simulant

To reduce the concentration of sodium of the waste slurry after being dewatered to some high concentration, e.g., between 15 wt% and 20 wt%, WTP will wash the slurry. The current

<sup>†</sup> All Steady State Filtering data can be found in Appendix F.

WTP plan is to have a concentrated slurry volume of approximately 18,000 gallons. To this volume will be added 21,000 gallons of inhibited water to perform the washing. This wash water will be added in 21 mini-batches of 1,000 gallons. After the addition of each mini-batch, the slurry will be dewatered to remove 1,000 gallons of diluted filtrate. This process will be repeated 21 times to complete the washing cycle.

The pilot-scale cross-flow test performed a similar washing cycle, but of course at a reduced scale. While this report deals with four different batches of AN-102R2 simulant, only after the first successful dewatering test could the steady state runs be done, and therefore, the washing test run. This occurred after the second batch, i.e., 3B. For subsequent batches most steady-state runs were not required, as well as the washing. After the last steady-state run with AN-102R2, Batch 3B, i.e., run 1.29, the test rig was made ready to wash the slurry.

At the end of test run 1.29 there were approximately 67 liters of concentrated slurry. As required by the test specification (Townson, 2002a), the slurry insoluble solids concentration was reduced from what was attained during the dewater test run 1.16 to 20 wt%, if it happened to be higher. The actual concentration for Batch 3B was approximately 22 wt%; therefore, before washing some of the previously removed filtrate was added back to the slurry to reduce the solids concentration. The added filtrate was 7.5 kg, or approximately 5.8 liters. The filtrate addition reduced the solids concentration of the simulant to 18.8 wt%. The slurry volume was approximately 73 liters, so 85 liters (i.e.,  $73 \times 21,000/18,000 = 73 \times 1.16 = 85$ ) of wash water were prepared. The 85 liters were added in 4.04-liter batches while 4.04 liters of washed filtrate were removed before adding the next batch. Of course this was done 21 times.

#### **3.3.2.6.1 Washing of AN-102R2, Batch 3B**

Figure 63 show the filtrate flux during the entire 3.7-hour process of washing the slurry. While the washing run was performed with a constant slurry velocity, 12 ft/s, and TMP, 40 psid, the test is not really a steady-state run. This is because the properties of the slurry are constantly changing with the wash-water additions. Figure 64 shows the properties before and after the entire washing process.

Note that in Fig. 64 there is a significant drop in total slurry solids, which is basically due to the loss of soluble solids because there was very little change to the insoluble solids concentration. The loss of solids caused the density to drop, but more importantly the slurry consistency reduce to more that half, which means that the solution presents less shear for the same motive force. Interestingly, the yield stress almost doubled. The increase in yield stress would have little effect for the slurry in motion, but it does indicate that from rest it would take about double the energy to put the slurry in motion again.

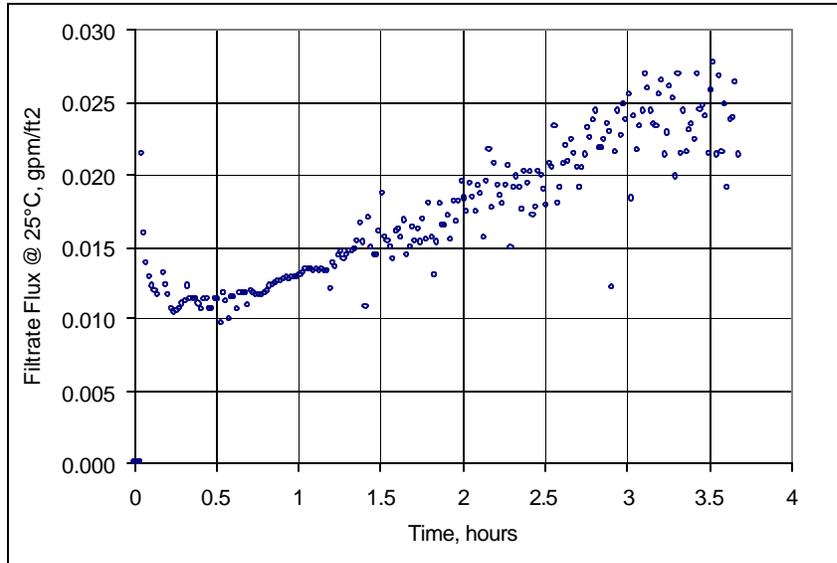


Figure 63. Washing of AN-102R2, Batch 3B after test run 1.29 and before concentration test run 1.30.

Over the filtering period the average slurry velocity was  $V = 12.1$  ft/s, the average transmembrane pressure was  $TMP = 40.2$  psid, and the average slurry temperature was  $T = 29^{\circ}C$  (the filtrate flux was adjusted to  $T = 25^{\circ}C$ ). The insoluble solids started at 19.0 wt% and ended at 18.8 wt%]

Vol. Wash Vol. Slurry	Total Solids Solids	Insoluble Solids	Slurry Density	Filtrate Density	Slurry Consistency	Slurry Yield Stress
	wt%	wt%	g/ml	g/ml	cP	Pa
0%	45.4	19.0	1.36	1.28	16	7.6
116%	28.5	18.8	1.15	1.09	7.1	14

Figure 64. Starting and ending slurry properties for the washing test run. The total amount of inhibited water added was  $21/18 X$  the initial slurry volume or approximately 116%.

These changes in slurry properties imply the scattering of filtrate flux data after about the first 60 minutes of washing. Figure 63 shows an increasing less stable flux as time (and added wash water) increased. The slurry velocity and TMP had to be continually trimmed to maintain that target values mentioned above. It is probable that as the slurry became successively more washed the filtrate cake was being affected and forcing the velocity and TMP to change. As the flux was trimmed to maintain it constant then the process repeated itself, leading to the shotgun scatter depicted in Fig. 63.

Of course, the reason for the washing was to remove some of the soluble salts, especially sodium. Figure 65 shows the result of the removal.

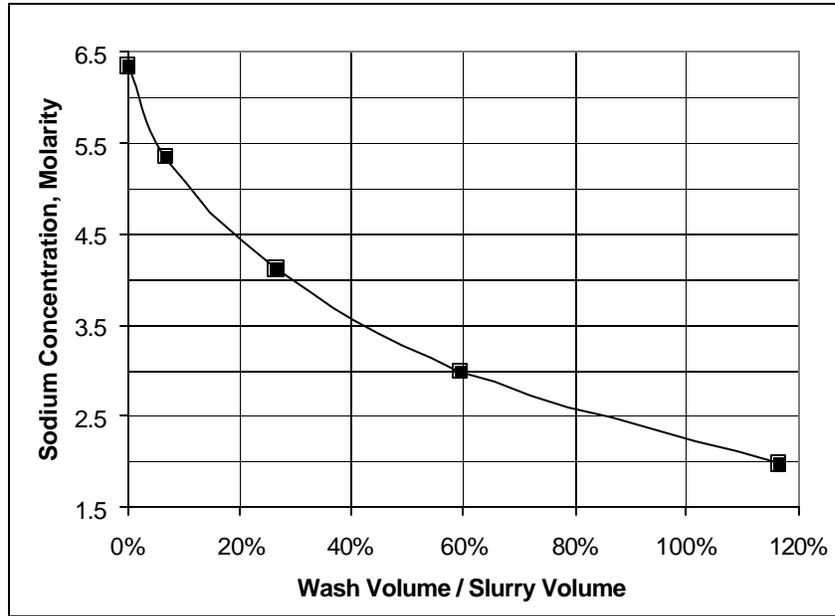


Figure 65. Reduction of Na<sup>+</sup> by washing with 21 mini-batches of inhibited water to AN-102R2, Batch 3B

**3.3.2.6.2 Concentration of Washed AN-102R2, Batch 3B**

Immediately following the washing test run the resulting slurry was concentrated under a constant slurry velocity of 12 ft/s and TMP = 40 psid. Figure 66 shows the results.

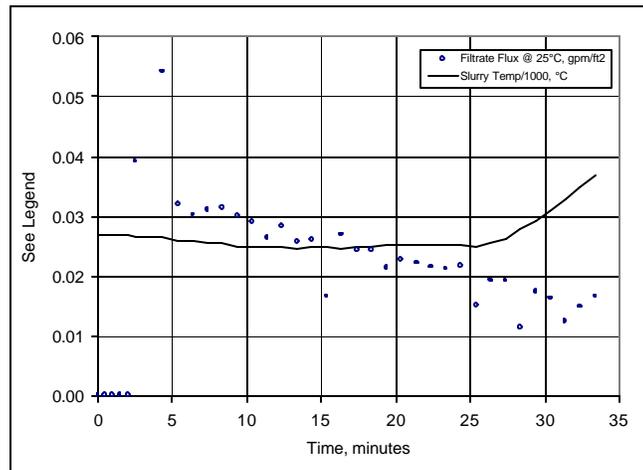


Figure 66. Dewatering of washed slurry (AN-102R2, Batch 3B): Test Run 1.30. The average slurry velocity was 11.9 ft/s and the average transmembrane pressure was TMP = 40.1 psid. The insoluble solids increased from 19 wt% to 25 wt%. The average slurry temperature was T = 27°C, but as is shown the temperature rose rapidly after 25 minutes. (The filtrate flux was adjusted to T = 25°C.)

The slurry began at approximately 19 wt% insoluble solids but the test was stopped when it reached 25 wt%. After about 25 minutes the slurry temperature began increasing rapidly and the test rig cooling system could no longer maintain the temperature stable. When the slurry temperature reached approximately 38°C the test was terminated. In fact, the thermal momentum caused the slurry temperature to continue rising until it reached 46°C. While the slurry was definitely thick in appearance it flowed freely and no plugging was observed.

### 3.3.3 Scaling: Differences between the PXU and Bench Top Cross-flow Test Facilities

#### 3.3.3.1 Comparison Challenges

The goal of the task at hand was to test several RPP WTP Envelope-C-type slurry simulants in a pilot-scale cross-flow ultrafiltration (PXU) facility. In many ways the pilot test rig is prototypic of the planned plant cross-flow ultrafiltration system. Figure 67 shows a comparison among the planned WTP filter bundle with that of the PXU facility and to the bench top test facility referred to as Cells Unit Filtration (CUF) facility.

Filter Tube Comparison	Planned WTP	Pilot Scale	Small Scale
Material	316 stainless steel	same	same
Pore Size	0.1 micron	same	same
Length	90 inches	same	24 inches
Tube Inside Diameter	1/2 inch	same	3/8 inch
Tube Outside Diameter	5/8 inch	same	1/2 inch
Arrangement	multiple	same	single
Number	241 per bundle	7	1
Grid Pattern	60° Triangular	same	not applicable
Center-to-Center Distance	7/8 inch	same	not applicable
Orientation <sup>†</sup>	Horizontal	Vertical	Horizontal
Other Features			
Slurry Pump	centrifugal	same	low shear

Figure 67. Comparison of full-scale to scaled<sup>†</sup> test facilities

Details of the CUF work are not given here, but can be found in Zamecnik et al. (2003). Only salient features of the CUF results are discussed in an attempt to see the effect of scale on experimental results. The purpose of the CUF test was two-fold: 1. Test actual waste, which is radioactively hot, and 2. compare the real waste filterability to simulants of that waste. To test actual radioactive wastes at pilot or plant scales would have been impractical. The handling of radioactively hot waste is very time consuming and costly and as scale increases so do the costs and risks. The CUF facility can operate with only 3 liters of slurry

<sup>†</sup> Orientation is included in the scaled criteria for completeness, however, it is not considered a significant difference. During an Oct 17, 2001 meeting, Prof. Joseph L. Gaddis of the Dept. of Mechanical Engineering of Clemson University, an expert on cross-flow filtration, stated that at the high velocities, i.e., high turbulence, that will be used for the cross-flow filtration facilities, orientation will not affect operation. He further stated that it is only important during shut down when gravity can assist emptying vertical tubes.

and has a small enough footprint that it can fit into most shielded cells to protect workers. Unfortunately, due to the complexities of the waste and the filter flow fields, extrapolating the small scale CUF data to the full-scale plant facility is not simple and at the very least would contain large uncertainties. The PXU facility was designed to be close to prototypic to minimize scaling issues so that confident full-scale data could be obtained. Of course, the drawback of the larger pilot scale is the amount of waste it needs and that it has to operate radioactively cold. This means a simulant must be used. For each waste a simulant, or simulants, is developed for large-scale testing. These simulants were made to match the real waste with respect to chemical and physical properties, while not being radioactive.

Because of the major differences between the PXU and CUF facilities filterability results were not expected to match. However, by showing statistically similar filter results for the actual waste and a simulant at the same scale, the CUF, then confidence was established for that simulated waste. A simulant verified with the CUF could then be used for testing at the pilot-scale to obtain results that would more closely match actual waste filterability at that large scale. The PXU results for the many conditions under which they were obtain, e.g., steady state, dewater, cleaning, rinsing, etc. have been previously discussed in this report. This section will be limited to discussing only comparable small-scale and pilot-scale results where possible. Even if results do not match between the scales, it is hoped that insight is obtained by making such a comparison.

Besides differences in scale of the CUF and PXU facilities, the other confounding feature is dissimilar simulants. This report deals with an organic based waste, classified as an Envelope C type waste. There are others, e.g., Envelopes A and B, which are non-organic and Envelope D, which is basically sludge based, containing most of the solids. All of these wastes are chemically complex and simulants are equally complex being comprised of dozens of compounds. Further, the Envelope C wastes are pre-treated to remove strontium and transuranics by precipitation before filtration occurs. This level of complexity makes one-to-one comparisons very difficult because no one simulant is the same. Even when two groups make the same simulant, following the same recipe, the resulting slurry may not be the same due to differences of how the recipe was applied and subsequent aging before filtration begins.

Because of differences in equipment of the CUF and PXU facilities and in formulations of waste simulants, there do not exist, to date, any data to make a quantitative side-by-side comparison of scale. However, there are some data that can be utilized to make some qualitative estimations of the effect of scaling.

Going back to 1997 (Nash and Siler, 1997) RPP-WTP work began with Envelope C simulated slurries. [In 1997 the waste types were just being defined and Envelope-C-type wastes were referred to as Envelope A. The important feature to remember is that this type of waste contained organic complexants, which necessitated precipitation to remove strontium and transuranic components. An explanation of the different types of Hanford wastes and simulant slurries developed for the project can be found in Eibling and Nash (2001).] This early version of the benchtop filter unit contained a single porous tube that had a 0.5-inch inside diameter, it was 4 feet long, and the 0.1-micron porous tube was of a

different design altogether. Besides the different filter structure, that 1997 test resulted in very poor filterability. After a little over a year of development SRTC recommended precipitation of Envelope C wastes with the additions of strontium nitrate and sodium permanganate. By the end of 1998 and into the early part of 1999 tests with the CUF showed that the new precipitation process with strontium and permanganate increased filterability (Nash, et al., 2000). Unfortunately, the CUF porous tube had been changed to a 0.2 micron tube and a 0.5-inch inside diameter, which made comparisons with to 0.1 micron porous tube filtration difficult.

### **3.3.3.2 A First PXU-to-CUF Comparison with an Envelope C Simulant (AN-107)**

After making some modifications to the SRTC CUF design, to conform to RPP-WTP needs, and refining the strontium and permanganate quantities, this new precipitation process was verified by PNNL by the end of 1999 with simulated Envelope C waste (AN-107) (Hallen, et al., 2000). The PNNL modified CUF had a two-foot long, 0.375-inch inside diameter filter tube with 0.1-micron porosity. That filter's initial filter flux was 0.03 gpm/ft<sup>2</sup> (averaged over 1 hour) at filter slurry velocity of 12.2 ft/s and a TMP = 50 psid. PXU (Duignan, 2000b) testing for Envelope C simulated waste (AN-107) began in October 1999 and it too had a 0.375-inch inside diameter filter tube with 0.1-micron porosity, but it was 3.3-feet long. That filter's initial filter flux was 0.08 gpm/ft<sup>2</sup> ±0.01 gpm/ft<sup>2</sup> (averaged over 1 hour). Why was the PXU (AN-107) result higher than the CUF (AN-107)? The reason is not known. For the PXU 2000 test the Envelope C simulant was based on an SRTC recipe (Eibling and Nash, 2001). After precipitation steps and then mixing for 4 hours at 50°C the simulant had a density of 1.29 g/mL, a viscosity of 4 cP, insoluble solids of approximately 1.9 wt%, sodium of 5.9 M, strontium of 0.075 M, and permanganate of 0.05 M. The CUF, used at PNNL (Hallen, et al., 2000) used the same recipe, that is, after precipitation it was mixed for 4 hours at 50°C. The PNNL simulant had a density of 1.26 g/mL, a viscosity of 7 to 18 cP, insoluble solids of approximately 1.9 wt%, sodium of 6 M, strontium of 0.075 M, and the permanganate of 0.05 M. It appears that both simulants were similar but for some reason the SRTC simulant did not start out as viscous. Now the differing viscosities could be attributed to measurement of rheological properties, but since the simulants were made from 3 dozen different compounds it would take significant analyses to understand the subtle differences and how those difference affect filtration.

### **3.3.3.3 A Second PXU-to-CUF Comparison with an Envelope C Simulant (AN-102R2)**

The reason data exist for the first comparison was simply a coincidence. That is, those data are available due to simultaneous programs being done in the DOE Complex to meet RPP-WTP requirements. In both cases, the only driver was to have a simulant as close as possible to actual waste. No attempt was made to have exactly the same slurries so that such

a comparison could be made. The only subsequent situation that occurred, which allowed<sup>†</sup> a conscious effort to be made to make a better comparison was during the precipitation and dewatering tests at SRTC of another Envelope-C-type simulant (AN-102R2). The first dewatering test of an AN-102R2 simulant (called Batch 3C and previously discussed in this report) resulted in very low filter fluxes for both the CUF (< 0.02 gpm/ft<sup>2</sup> at 8 wt% insoluble solids: Zamecnik, et al., 2003) and the PXU facility (= 0.005 gpm/ft<sup>2</sup> at 8 wt% insoluble solids: this report). For this first AN-102R2 test both the CUF and the PXU personnel made their own slurry simulants. To increase the filterability another dewatering test was done with some changes to the simulant. However, this time, after making the PXU 1000-liter batch, then precipitating and mixing for 4 hours at 50°C, 75 liters of simulant were removed and sent for use in a CUF facility. The hope was that differences in scale could be measured if the slurry were exactly the same in both facilities and operated under the same flow conditions. Unfortunately, while the CUF facility was the same as mentioned above, i.e., it had a two-foot long, 0.375-inch inside diameter filter tube with 0.1-micron porosity, the PXU facility had been changed to meet new RPP-WTP requirements of a 0.5-inch inside diameter and a 90-inch long porous tube. Figure 68 shows the comparison of the PXU and CUF tests which dewatered the AN-102R2 slurry from 1.2 wt% to 22 wt% (for the PXU) and 1.6 wt% to 19 wt% (for the CUF)<sup>‡</sup> over a 12-hour period.

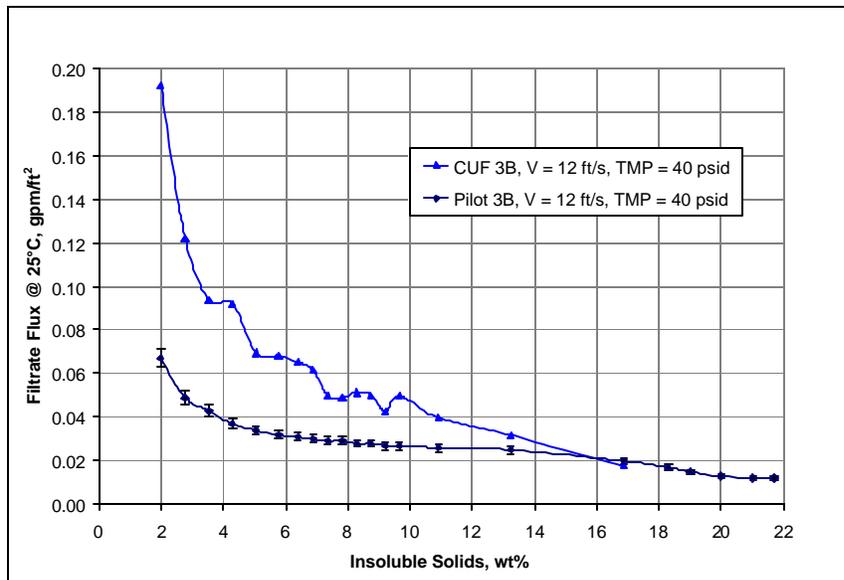


Figure 68. PXU to CUF filtrate flux comparison using an AN-102R2 simulant

It is important to note that the data in Figure 68 were obtained differently for each facility. For the CUF, each datum point was an average of a 3 liter batch of slurry. That is, filtrate flux is measured by the time it took for 3 liters to be filtered. The CUF test dewatered until

<sup>†</sup> The RPP-WTP research and technology project did not plan for dedicated one-to-one comparison testing; therefore, any such work had to be done in conjunction with other planned and funded tasks and at the initiative of the principal investigators.

<sup>‡</sup> The difference in the initial PXU and CUF insoluble solids concentrations may be due to analytical measurements or sampling techniques

the slurry solids concentration reached approximately 19 wt% but the last average flux value was at approximately 17 wt%. The PXU facility measured filtrate flux instantaneously and data were taken every minute. To make the Fig. 68 comparison the values of the PXU flux were taken at each of the averaged CUF insoluble solids points. This is the reason why all the abscissa points seem to line up. However, since the PXU dewatered up to 22 wt% insoluble solids, those points were also included. At about 16 wt% insoluble solids the two curve cross. At this point the CUF facility was close to its operational limit.

In general, it looks like the CUF filtrate flux is about a factor of 2 larger than the PXU facility up to approximately 10 wt% insoluble solids, after which the curves merge. At that point the thickness of the filter cake and increased slurry consistency minimize any scale differences. The data obtained from both tests do not give a clear indication as to why the curves are significantly different. Figure 69 includes some of the pertinent information of the facilities and the slurry used in both.

The PXU data have been taken from this report and those for the CUF have been estimated from data displayed in Zamecnic, et al. (2003). As already stated above, the starting slurry was exactly the same. It was made at one time and then 75 liters were separated for use in the CUF. The only starting difference is time. The PXU began filtration immediately after the newly precipitated slurry was mixed at 50°C for 4 hours. The CUF test began the following day, approximately 16 hours after the PXU test beginning; therefore, further precipitations reactions could have occurred. In fact, the particle-size distributions (PSD) for the initial CFU slurry appears to be slightly, but significantly, larger. However, all other characteristics, i.e., solids concentration, rheology, and density, appear to be the same<sup>†</sup>. The PSD difference may have existed or it may have simply been how the PSD was performed. For instance, the PSD samples sit for a while before processing so they are given a mild amount of sonication to reduce the particles to their base size. The question is, “What is that base size?”

However, in both tests the particle-size distribution show three distinct changes:

1. The mean particle size was reduced to approximately one half.
2. The spread of particle sizes was reduce to approximately one half.
3. The bimodal volume distribution was reduced to predominately a single size.

In discussing the filtrate flux differences shown in Fig. 68 Zamecnic, et al. (2003); (on page 63 of that reference), hypothesized that the different pump types, i.e., PXU high shear centrifugal to CUF low shear progressive cavity, caused the particles in the PXU test to become smaller and therefore be harder to filter. Unfortunately, the data do not back this claim up. The mean particle size of the concentrated slurry for the PXU may be slightly smaller than the CUF, but the difference is minimally significant. Further, the same difference is apparent in the initial slurry, which was exactly the same before each facility began testing, therefore this size difference is questionable. However, even if the particle were significantly smaller the same report contradicts its hypothesis by stating, “Surprisingly, the most filterable slurries appear to have more smaller particles in the 1-4 micrometer range

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<sup>†</sup> See the preceding footnote.

and, in general, have a flatter distribution of particle size.” Indeed, Fig. 14 of that report shows that as the mean particle size became smaller the average filter flux increased. This counter-intuitive result makes sense when looking at the micrograph of that report, Fig. 17, which shows “sheet-like flat” particles in the 5 to 20 micron range for less filterable slurries.

Test Facility	Pilot-scale* (PXU)	Small-scale* (CUF)
Date of Test	22-23 Oct.2002	23-24 Oct. 2002
Approximate duration of test	12 hours	14 hours
Approximate starting slurry volume	1000 liters	75 liters
Slurry mixing during precipitation	well mixed	same batch
Cross-flow slurry reservoir capacity	120 liters	6 liters
Flow Loop volume (without reservoir)	~ 34 liters	< 0.2 liters
Slurry circulation rate	193 lpm (27.6 lpm/tube)	15 lpm
Longest residence time of slurry	~ 48 seconds	~ 25 seconds
Slurry circulation time in flow loop	~ 10 seconds	~ 1 second
Type of circulation pumps	2 centrifugal	1 progressive cavity
Constant axial slurry velocity	12.1 ft/s	12 ft/s
Constant transmembrane pressure	40.5 psid	40 psid
<i>Slurry at Low Solids Concentration</i>		
Insoluble Solids	1.2 wt%	1.6 wt%
Total Solids	33 wt%	33 wt%
Slurry Consistency	4.0 cP	4.2 cP
Yield Stress	0 Pa	0 Pa
Filtrate Viscosity	3.8 cP	
Slurry Density	1.3 g/ml	1.3 g/ml
PSD (by volume dist.): Mean	8.55 micron**(48%)	~ 15 micron**
PSD (by volume dist.): Mean	2.25 micron**(52%)	~ 3.5 micron**
PSD (by volume dist.): Std Dev	4.27 micron	
PSD (by volume dist.): spread	1.2 to 52 micron	0.5 to 75 micron
PSD (by number dist.): Mean	1.94 micron	2.5 micron
PSD (by number dist.): Std Dev	0.45 micron	
PSD (by number dist.): spread	1.2 to 19 micron	0.8 to 6 micron
<i>Slurry at High Solids Concentration</i>		
Insoluble Solids	21.7 wt%	18.8 wt%
Total Solids	47.2 wt%	45.4 wt%
Slurry Consistency	20 cP	14.8 cP
Yield Stress	8.6 Pa	11 Pa
Filtrate Viscosity	3.7 cP	
Slurry Density	1.4 g/ml	1.4 g/ml
Filtrate Density	1.3 g/ml	
PSD (by volume dist.): Mean	8.2 micron**(13%)	6 micron
PSD (by volume dist.): Mean	0.9 micron**(87%)	1.5 micron
PSD (by volume dist.): Std Dev	0.25 micron	
PSD (by volume dist.): spread	<0.7 to 44 micron	0.3 to 45 micron
PSD (by number dist.): Mean	0.8 micron	2 micron
PSD (by number dist.): Std Dev	0.1 micron	
PSD (by number dist.): spread	<0.7 to 2 micron	0.8 to 5 micron
* PXU data can be found in Appendix G samples: 300187815,816,857,858 and 300188109,110,150,152		
* CUF data can be found in Zamecnik, et al.(2003)		
**bimodal distribution		

Figure 69. PXU to CUF comparison AN-102R2, Batch 3B simulant

As the slurry is processed in the filter facilities some of the large flat particle break up through shear. This breakup can happen in both the CUF and the PXU. Moreover, the fact that the CUF used a low shear pump does not mean the slurry does not experience significant

shearing. By design the CUF was made to minimize the amount of slurry needed to filter because radioactive slurry samples are small; therefore, the circulation rate is high. Note that in Fig. 69 the slurry in the CUF takes under 1 second to traverse the loop. If the longest residence time, as shown in Fig. 69. is used, then for the first charge of 6 liters of slurry, of which 3 liters was dewatered over a 20.4-min period, the slurry was circulated  $20.4 \times 60 / 24 = 51$  times. By the end of the 14-hour test the initial batch of slurry had circulated  $14 \times 3600 / 24 = 2,100$  times. For the PXU, the first slurry batch circulated only  $12 \times 3600 / 48 = 900$  times. Considering the high turn over rate of the slurry, the speed of the slurry, i.e., 12 ft/s, and the pipe fittings and control valve in the CUF flow loop, the slurry does experience a considerable amount of shear. Many of the compounds that make up the slurry have strong oxide particles, which seem not to get any smaller than approximately  $\frac{1}{2}$  micron. In fact, it appears (Nash and Siler, 1997) the particle breakup occurs mostly in the first few minutes of circulation and then remains fairly constant. The conclusion here is that when large flat particles are broken down to smaller, less flat, particles the slurry filters better. Since the smaller particles seem to be 3 to 20 times larger than the nominal pore rating of 0.1 micron, then the slurry becomes more filterable. That is, the flat particles are broken down so that they do not blind the filter element.

Another possible reason for differences in CUF and PXU filter fluxes is the difference in wall shear. Figure 70 shows a cartoon of how a cross-flow filter works. As the slurry and most of its liquor travels through the inside of the porous tubes a filter cake builds up on the inside. The thickness of the cake is exaggerated in Fig. 70 for illustration, but it could eventually build up to only about the thickness of a piece of paper.

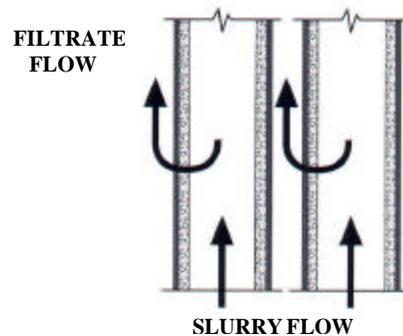


Figure 70. Operation of a multi-tube cross flow filter like the PXU

An advantage of the cross-flow filter over a dead-end filter is not needing periodic changing because the moving slurry constantly shears the cake, keeping it at reasonable thickness and a fairly constant filtering rate. Since the wall shear affects the cake formation on the porous wall, differing levels of wall shear may strongly influence that rate at which the slurry liquor can permeate through the porous wall, thus giving different filtration rates. As shown in Fig. 67 the CUF has a smaller diameter and shorter porous tube than the PXU, while Fig. 69 shows the axial slurry velocity was maintained the same at 12 ft/s.

To see the wall-shear effect more quantitatively a simple computational fluid dynamic model was made for two slurries that represent the initial slurry and the concentrated slurry.

Figure 71 shows the parameters assumed for the CUF and the PXU facilities. The slurry was assumed to be Newtonian and fully turbulent, i.e., Reynolds number greater than 2000. The slurry at low solids concentration does indeed behave as a Newtonian solution, however, as the solids concentration increased it become slightly thixotropic, i.e., shear thinning with a time dependent shear stress. This non-Newtonian effect is not strong and as long the slurry is flowing it still behaves like a Newtonian solution. While the turbulence in the larger diameter tube is 1/3<sup>rd</sup> more than the smaller tube for the same slurry velocity, i.e.,  $Re(\text{large}) / Re(\text{small}) = \text{large ID} / \text{small ID} = 0.5/0.375 = 1.333$ , they are both much larger than the turbulence threshold of  $Re = 2000$ . By using some rough parameters, Fig. 71, for the two situations a comparison can be made between the two flow situations.

Physical Parameters	1.5 wt% Slurry	25 wt% Slurry
Porous Tube I.D.	3/8 and 1/2 inch	3/8 and 1/2 inch
Axial Slurry Velocity	12 ft/s	12 ft/s
Slurry Density	1.3 g/ml	1.5 g/ml
Slurry Viscosity	4 cP	20 cP

Figure 71. Parameters used in a wall shear CFD model

Figure 72 shows the low solids concentration CFD results. Immediately obvious is the much higher wall shear for the small tube. At 24 inches (0.6 m) the steady state wall shear is 24% higher for the small tube. Further, it takes approximately 1/3<sup>rd</sup> of the 24-inch span for the wall shear to come to steady state because of entrance effects. There is approximately the same entrance effect on the larger tube, but since it is 90 inches long the effect is much less. When taking into account the entrance effects, the wall shear for the 3/8-inch tube is approximately 30% higher than the 1/2-inch tube.

As the slurry concentrates the wall shear difference decreases. Figure 73 shows the results. When taking into account the entrance effects, the wall shear for the 3/8-inch tube is approximately 20% higher than the 1/2-inch tube. However, since the filtrate cake built up when the slurry had a low concentration of insoluble solids, then the differences at the high concentrations may not be significant, as may be implied by the two filtrate flux curves coming together above approximately 16 wt% in Fig. 68.

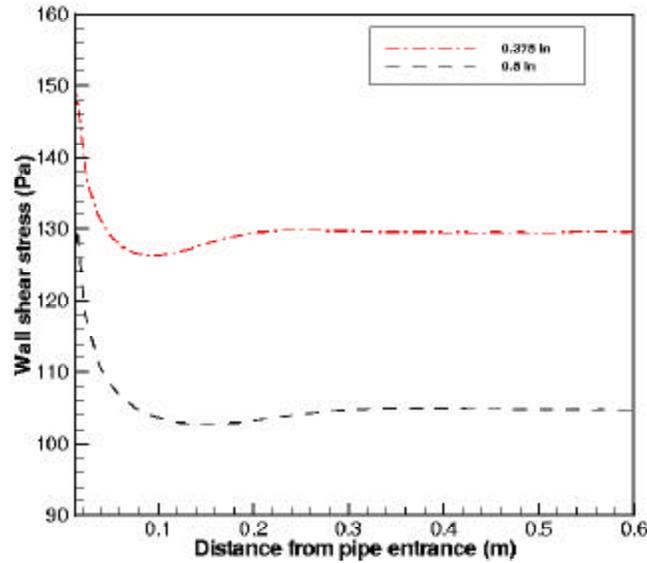


Figure 72. Wall shear comparison for two different tube IDs at 12 ft/s and a viscosity of 4 cP.

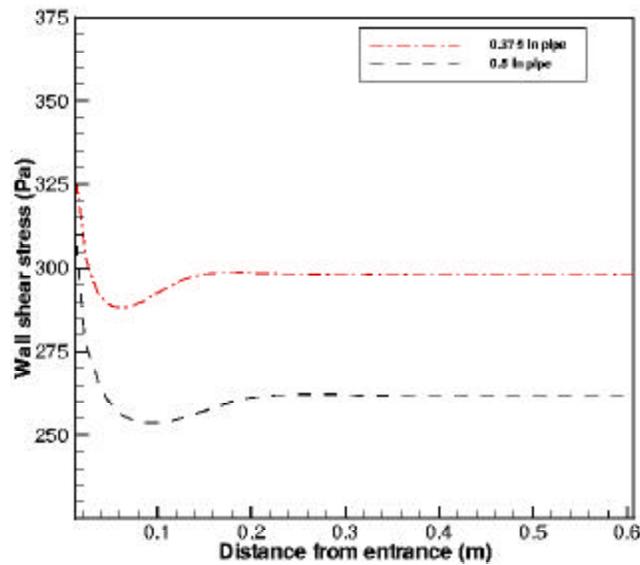


Figure 73. Wall shear comparison for two different tube IDs at 12 ft/s and a viscosity of 20 cP.

As stated by Murkes and Carlsson (1988) about crossflow filtration: “The method is basically a cake-free method (or intended to be such). Its purpose is to prevent the formation of the cake. Particles deposited on the filter medium are swept away by the feed flow. The clean-keeping efficiency of the flowing liquid increases with its velocity. Thus, the particle of the solute concentration polarization is controlled by the flow velocity.” In the comparison between the PXU and the CUF facilities the velocities were kept the same, however, due to differences in porous tube channel size, the larger the channel the lower the wall shear, which is the mechanism that shears away the particles deposited on the filter medium. Shear stress is directly related to fluid velocity through Newton’s law of viscosity, i.e.,

$$\tau = \mu \, dv/dy \quad \text{and at the wall} \quad \tau_{\text{wall}} = \mu \, [dv/dy]_{y=0}$$

where  $v$  is the local slurry velocity,  $y$  is the spatial coordinate perpendicular to the slurry flow,  $\mu$  is the slurry dynamic viscosity, and  $\tau$  is the local shear stress. Further Murkes and Carlsson show that the filtrate flux is related directly proportional to the filtrate cake permeability and inversely related to filtrate cake thickness. As the cake forms under the local wall shear both parameters will be affected. Figure 74 shows a schematic of slurry flow in a porous tube with an established filter cake. As the diameter,  $D$ , gets smaller so does the turbulence level, because it is directly proportional to the Reynolds number, which is directly proportional to this dimension. However, as  $D$  becomes smaller the boundary layer, where wall shear stress occurs, grows, and becomes a larger portion of the flow area, which is proportional to the square of the diameter. Therefore, wall shear stress is larger for smaller flow channels as long as the velocity remains constant.

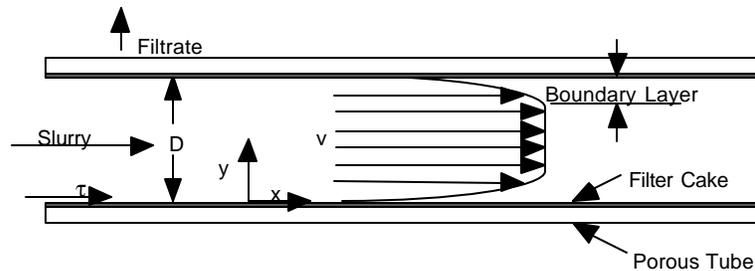


Figure 74. Slurry flow through a cross-flow ultrafiltration tube

Does the higher wall shear stress, and thus the higher “clean-keeping efficiency” of the CUF shown in Fig. 72 cause it to have a higher filtrate flux? The evidence seems to imply the affirmative. Is the initial 30% higher wall shear stress in the CUF enough to make its filtrate flux approximately double that of the PXU? It is possible, but there is not enough quantitative data to show this fact. These organic-based waste slurries appear to be very sticky, that is, there seems to be sufficient inter-particle forces to make the solids cling to each other more than, for example, sand in water. These solids probably form some kind of a gel-like cake on the filter surface, which does not lend itself to available analyses. However, the changing wall shear stress with scale must have an effect and possibly an effect large enough to cause the differing results obtained with the CUF and the PXU facilities.

### 3.3.3.4 Other PXU-to-CUF Differences

Even if the wall shear differences could be accurately taken into account it may not be enough to show the differences between these two filter facilities. Other differences must exist and have not been quantified. Consider the differences in the hardware like the two porous tubes used and the pumps that circulate the slurries, or in the slurry simulants, etc.

### 3.3.3.4.1 Differences in filter hardware

- Porosity - Both the CUF and the PXU facilities used 0.1 micron nominal porous tubes. However, each batch sintered-metal tubes is different. The 0.1 micron is an average value. At this ultrafiltration pore size small differences in porosity may have significant permeability effects. Besides, through the years a manufacturer like the Mott Corporation has changed, perfected, and enhanced their porous materials which sometimes has caused confusion of ordered products. For instance, the size 0.1 micron porosity sometimes means several difference things as described in Duignan (2001), and only with a closely monitored post-manufactured test can the porosity of any two tubes be equated.
- Tube Wall Thickness – While the inside diameter of tubes should be close to purchased size due to the process of forming sintered metal around a very accurately ground mandrel, the outside diameter depends on the force of a flexible surface to maintain the metal particle under pressure. This is evidenced by the measurements made on the seven-tube PXU tube assembly when it arrived from the manufacturer. Each of the seven tubes was made of four subsections (see Figs. 3 and 4) and a total of 100 measurements were made on the tubes to determine the dimensions. The manufacturer's stated inside diameter was 0.5 inch and the received tubes had an average diameter of 0.488 inch, with a maximum of 0.490 inch and a minimum of 0.485 inch. This 0.005-inch variation is considered very good. . However, the manufacturer's stated outside diameter was 0.625 inch and the received tubes had an average diameter of 0.654 inch, with a maximum of 0.674 inch and a minimum of 0.640 inch. This 0.034-inch variation is large but expected. While the 7-tube bundle of the PXU had 28 subsections, the CUF was comprised of a single 24-inch tube. The CUF would represent the PXU dimensionally only by coincidence, but more likely it was dimensionally different, which may have had some significant flux differences. The PXU will be more representative of the full-size plant filter unit because of the large variations in dimensions.

As the filter cake builds up on the inside of the porous tube the differences in porosity and wall thickness should become less evident because then the cake becomes the filtering medium and the largest source of pressure drop. However, it is probably very important how the filter cake is initially formed, which may persist for a significant amount of time until the cake is thick enough to make the two filters act the same. This seems to have happened as seen in Fig. 68.

- Feed Pumps – As mentioned in the section 3.3.3.3, the pumps for the two facilities were different. The CUF facility used a single air-driven progressive-cavity pump made by Oberdorfer. This pump had a stainless steel rotor, which was covered with a layer of hardened chrome. The rotor operated in a Buta-N stator, which has good resistance to caustic service but limited resistance to acid service, and moved the slurry in a piston-like fashion, through a helix-shaped cavity. Up to a threshold pressure this type of pump acts like a positive displacement pump, however, when the maximum pressure is reached (in this case it was approximately 90 psig) the elastomer liner gives. At a steady-state operation of a slurry velocity of 12 ft/s, the CUF pump flow was 4 gpm. As mentioned in section 3.2.1.1, the PXU facility used two centrifugal pumps in series and were made by

Galigher. The impellers and housings were made of EPDM, which has good resistance to both acid and caustic services. At a steady-state operation of a single filter tube slurry velocity of 12 ft/s, the PXU pumps flow was 51 gpm. With respect to shear, the progressive-cavity pump imparted less than the centrifugal pumps, however, as seen in Fig. 69, the CUF circulated the slurry at a much higher rate due to the very small flow loop. Unfortunately, the high shear at the CUF control valve may have negated any benefit to the lower shear present by the pump.

#### **3.3.3.4.2 Differences in slurry simulant**

- **Time** – The simulant used in the AN-102R2 comparison for both the CUF and the PXU facilities was made at one time and when it was ready for filtration some of the large batch was removed and transported to the CUF location. However, the filtration of the separated sub-batch of simulant for the CUF only began about 15 or 16 hours after the PXU began. Figure 69 shows some characteristics of the simulant at the beginning filtration for the respective facility, like slightly larger particles for the CUF simulant, however, it does not show the complex number of reactions that occurred in making the simulant, nor the changes due to the reactions with time. The precipitation report (Steeper and Williams, 2003) shows that while most of the simulant was predominantly stable after 4 hours of mixing, just before feeding to the PXU facility, there are still some reactions occurring. For instance, about 10% of the aluminum available as a solid, when the PXU began filtering, is incorporated into the aqueous after about 20 hours. The presence of solid aluminum is known to inhibit filtration and being present for the PXU testing and not for the CUF testing may have had an effect. The point here is that chemically the simulants were slightly different due to aging, which could have contributed to the differing results.

### **3.4 CONCLUSIONS**

#### **3.4.1 Water**

1. In general, inhibited water (0.01 M NaOH) tests before and after each slurry test indicate a return to “clean” filter fluxes (Fig. 19).
2. However, when water was used without the addition of caustic the filtrate flux was significantly higher (Fig. 21), which is assumed to be the result of having fewer precipitating solids left in the test rig.

#### **3.4.2 Standard Slurry (SrCO<sub>3</sub>)**

1. The use of a standard slurry to show a filter’s return to cleanliness was confounded by the level of cleanliness of not just the filter but of the entire filter system (Fig. 29). That is, unless the entire filtration loop was clean then determining the cleanliness of just the in-line filter may not be possible.
2. The heavy solids of the 5 wt% SrCO<sub>3</sub> standard slurry required transmembrane pressure above 20 psid for a filter to be challenged (Fig. 27).

- The standard slurry could only be effectively removed from the filter system with the used of acid because it dissolves carbonate. A concentration of 0.05 M HNO<sub>3</sub> was used.

### 3.4.3 Acid Cleaning

- The method used, two 90-minutes circulations of 2 M nitric acid, cleaned most of the solids away from the filter, but there were always some remaining solids, which reduced the acid filtrate fluxes from that of a clean filter. (Fig. 35). That is, the complex wastes may need more targeted cleaning to remove all waste remnants.
- Cleaning periods of more than three hours with the 2 M nitric acid may not improve effectiveness. (Fig. 33).

### 3.4.4 Dewatering

Batch Number	Precipitation Conditions*	Precipitation Mixing	Precipitation Temp, °C	Final Conc of Free OH <sup>-</sup>	Final Conc of SrNO <sub>3</sub>	Final Conc of NaMnO <sub>4</sub>	Filter Flux (gpm/ft <sup>2</sup> )			Location
							at 2 wt%	at 15 wt%	Avg to 15 wt%	
3C	NOC =	well	25	0.3 M	0.03 M	0.03 M	0.019	0.005**	0.010***	(Fig. 38)
3B	BC =	well	50	1.0 M	0.075 M	0.050 M	0.066	0.024	0.049	(Fig. 40)
3A	BC @ 25°C =	well	25	1.0 M	0.075 M	0.050 M	0.052	0.019	0.020	(Fig. 42)
4A	BC w/PJM =	PJM	50 > 25	1.0 M	0.075 M	0.050 M	0.021	0.014	0.020	(Fig. 44)

\* These are the dewatering results and the precipitation conditions nomenclature can be found in Fig. 17  
 \*\* Batch 3C only went to 8.3 wt% but flux was constant from 5 to 8.3 wt%  
 \*\*\* Batch 3C average assumes the filtrate flux continues at 0.005 gpm/ft<sup>2</sup> to 15 wt%

Figure 75. Overall dewatering results

- Filtering to above 15 wt% insoluble was attainable. (Fig. 36), with results in the 18 wt% to 25 wt% range.
- Precipitation with Newly Optimized Conditions left the wastes poorly filterable. (Figs. 37, 38, and the 1<sup>st</sup> line in Fig. 75)
- AN-102R2 had the best filterability when prepared at precipitation baseline conditions which included being well mixed and prepared at 50°C. (Figs. 39, 40, and the 2<sup>nd</sup> line in Fig. 75.)
- AN-102R2 was more filterable when solid particles were broken down to near the micron size. (Compare Fig. 50 to the penultimate column in Fig. 75 and see section 3.3.3.3, which discusses how larger sheet-like particles may reduce filtration.)
- Rheological properties of simulants underwent large changes as the slurry increases above 14 wt% insoluble solids. (Fig. 46)
- Backpulsing the filter with this Envelope C-type slurry was not very effective and after reaching an insoluble solids concentration of approximately 5 wt% backpulsing became ineffective. (Figs. 38, 42, and 44)
- Excellent solids separation was obtained with turbidities on the order of 0.2 NTU, possibly indicating that the separated filtrates had had less than 0.2 ppm of insoluble solids (see section 3.3.1).

### 3.4.5 Steady State

1. Increasing the slurry axial velocity by a factor of 2 increased the filtrate flux by approximately 20%. (Figs. 57 and 62)
2. Filtrate flux was not significantly dependent upon transmembrane pressure. (Figs. 56 and 61)
3. Slurry axial velocity should not go below 11 ft/s or the transmembrane pressure below 30 psid. Doing so will cause a significant loss of filtrate flux. (Fig. 55, Batch 3B runs: 4, 7, 9, 11, and 12) (Fig. 60, Batch 3A runs: 2, 3, and 4)
4. With backpulsing at a frequency of one to two hours, a 0.1-micron filter will depth foul with the result of the filtrate flux loss of approximately 60% ( $24^{-0.15}$ ) after 24 hours of continuous operation. (Figs. 54 and 59)
5. Excellent solids separation was obtained with turbidities on the order of 0.2 NTU, possibly indicating that the separated filtrates had had less than 0.2 ppm of insoluble solids (see section 3.3.1).

### 3.4.6 Washing

1. While washing a volume of AN-102R2 with an equal volume of inhibited water cuts its consistency in approximately one half, its yield stress approximately doubles. (Fig. 64)
2. Washing a volume of AN-102R2 with an equal volume of inhibited water removes approximately 65% of soluble sodium. (Fig. 65)

### 3.4.7 Scaling

1. Not enough data are available to make quantitative comparison between the benchtop (CUF) data and the pilot-scale (PXF) data. Qualitatively the limited data sets are not comparable and caution is recommended when relating small-scale results to full-scale operation. A detailed discussion can be found in section 3.3.3.

## 4.0 RECOMMENDATIONS

SRTC recommends that:

1. Axial slurry velocity be greater than 11 ft/s and the transmembrane pressure more than 30 psid. Higher velocities will filter slurries faster, but higher transmembrane pressures will not increase filter fluxes significantly.
2. Baseline conditions (BC in Fig. 75) be used when precipitating Envelope C-type wastes like AN-102 to obtain the best filterability.
3. Backpulsing be minimized because increasing backpulsing increases depth fouling of the filter and thus reduces time between acid cleanings.
4. A more effective cleaning method be determined than the use of 2 M nitric acid, alone.

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## Appendix A: Water

As required by the RPP-WTP Test Specification each time the cross-flow filter experienced a slurry run the filter was to be tested with inhibited water. The water was distilled and filtered (to 0.1 micron absolute) and then made inhibited by adding caustic to a concentration of 0.01 M NaOH. Those tests were noted in the test matrix as runs 1.00 before a slurry test and 1.34 after a slurry. Along with these tests there were other water rinses included that came after using the standard slurry (1.02), after the final slurry concentration test (1.31A) and after cleaning the filter with acid (1.32).

Run 1.02 was generally not done because initial tests with the slurry (during the preconditioning test with AN-107 and slurry AN-102R2 batch 3C) determined that only with considerable number of water rinses and acid cleaning could the baseline slurry be removed from the filter, costing time and money, therefore starting the AN-102R2 batch 3B test the RPP-WTP customer allowed baselining the filter only after each slurry test (run 1.33). Without the initial baseline slurry tests, then the rinse run, 1.02 was no longer necessary. This report deal with the testing of five separate batches of slurry (preconditioning with AN-107, AN-102R2:3C, AN-102R2:3B, AN-102R2:3A, and AN-102R2:4) therefore the water runs were:

### Water test runs related to the Simulant Slurry AN-107 (Filter Preconditioning):

1A, 1B, 1C	Pre-Standard Slurry Test and Before Preconditioning the filter with AN-107; pre-test rig modification
3A, 3B, 3C, 3D	Post-Standard Slurry Test Rinse and Before Preconditioning the filter with AN-107; with <b>INHIBITED</b> water
3a, 3b, 3c, 3(TMP=5 psid)	Post-Standard Slurry Test Rinse and Before Preconditioning the filter with AN-107; with <b>NON-INHIBITED</b> water
5A	After Preconditioning the filter with AN-107, but <b>BEFORE</b> acid cleaning
6	After Preconditioning the filter with AN-107. But <b>AFTER</b> acid cleaning
8A, 8B, 8C	After Preconditioning the filter with AN-107, and after both acid cleaning and final standard slurry testing

### Water test runs related to the Simulant Slurry AN-102R2 Batch 3C:

1.00A, 1.00B, 1.00C	Before standard slurry test
1.02	After initial standard slurry test
1.31A	After batch 3C test and before acid cleaning
<del>1.32</del>	After acid cleaning, not included do to pump liner change
<del>1.34A, 1.34B, 1.34C</del>	Not done since 1.00A, 1.00B, 1.00C following tests give the same information

### Water test runs related to the Simulant Slurry AN-102R2 Batch 3B:

1.00A, 1.00B, 1.00C	Before standard slurry test
<del>1.02</del>	Not done since initial standard slurry test was no longer done
1.31A	After batch 3B test and before acid cleaning
1.32	After acid cleaning, but before final standard slurry test
1.34A, 1.34B, 1.34C, 1.34D	After final standard slurry test (extra test, TMP=40 psid was done in error)

### Water test runs related to the Simulant Slurry AN-102R2 Batch 3A:

<del>1.00A, 1.00B, 1.00C</del>	Not done because preceding tests 1.34a, 1.34b, 1.34c give the same information
<del>1.02</del>	Not done since initial standard slurry test was no longer done
1.31A	After batch 3A test and before acid cleaning
1.32	After acid cleaning, but before final standard slurry test
1.34A, 1.34B, 1.34C	After final standard slurry test

Water test runs related to the Simulant Slurry AN-102R2 Batch 4:

1.00A, 1.00B, 1.00C Before batch 4 test  
1.00r1 Because the preceding tests 1.00A, 1.00B, 1.00C had a low filtrate flux the filter was soaked for 4 days in 2 M nitric acid and this revision 1 (r1) water test at TMP=20 psid was done with NO caustic, to compare to the following repeat test with caustic.

1.00Ar1, 1.00Br1, 1.00Cr1 The preceding tests were repeated after an extra acid cleaning

~~1.02~~ Not done since initial standard slurry test was no longer done  
1.31A After batch 4 test and before acid cleaning  
1.32 After acid cleaning, but before final standard slurry test  
1.34A, 1.34B, 1.34C After final standard slurry test

The letter A, B, C indicate different constant transmembrane pressure (TMP), generally, but not always: A=10 psid, B=20 psid, C=30 ; psid.

For each water test this appendix contains a graph of the filtrate flux with time and tables of the data taken and calculated. To better understand the presented information important aspects of the graphs and tables are explained below:

Graphs – Each graph contains time averages of some of the important parameters taken during the run at the top of the figures, i.e. Water velocity in the filter tube, V; transmembrane pressure, TMP; water pressure at the entrance of the filter tube, Filter Pres; and the water temperature, T.

Tables – Each table is divided into raw data (the first 17 columns) and calculations (the last 10 columns) which are based on the raw data. The raw data section is divided into three parts:

Individual Entries – Raw Data (Note: Slurry = Water for these tests)

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid which has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.

Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.707 ft<sup>2</sup>)<sup>†</sup>  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T))-(1/298)]$  as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)

Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing

Permiability – Same as Permiability but in metric units, meter/day/bar

#### Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 x Std Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not include the points taken during the backpulse sequence of each test. This is explained below.

#### Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is where the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

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<sup>†</sup> For the water tests during preconditioning it will be noticed that 6.87 ft<sup>2</sup> was used. This was based on a tube inside diameter of 0.5 inch, which was based on the manufacturer’s specification. After the tubes were measured the i.d. was changed to 0.488 inch and the area to 6.707 ft<sup>2</sup>. This means that absolute axial velocity and filtrate flux are low by 2.5% for the preconditioning runs.

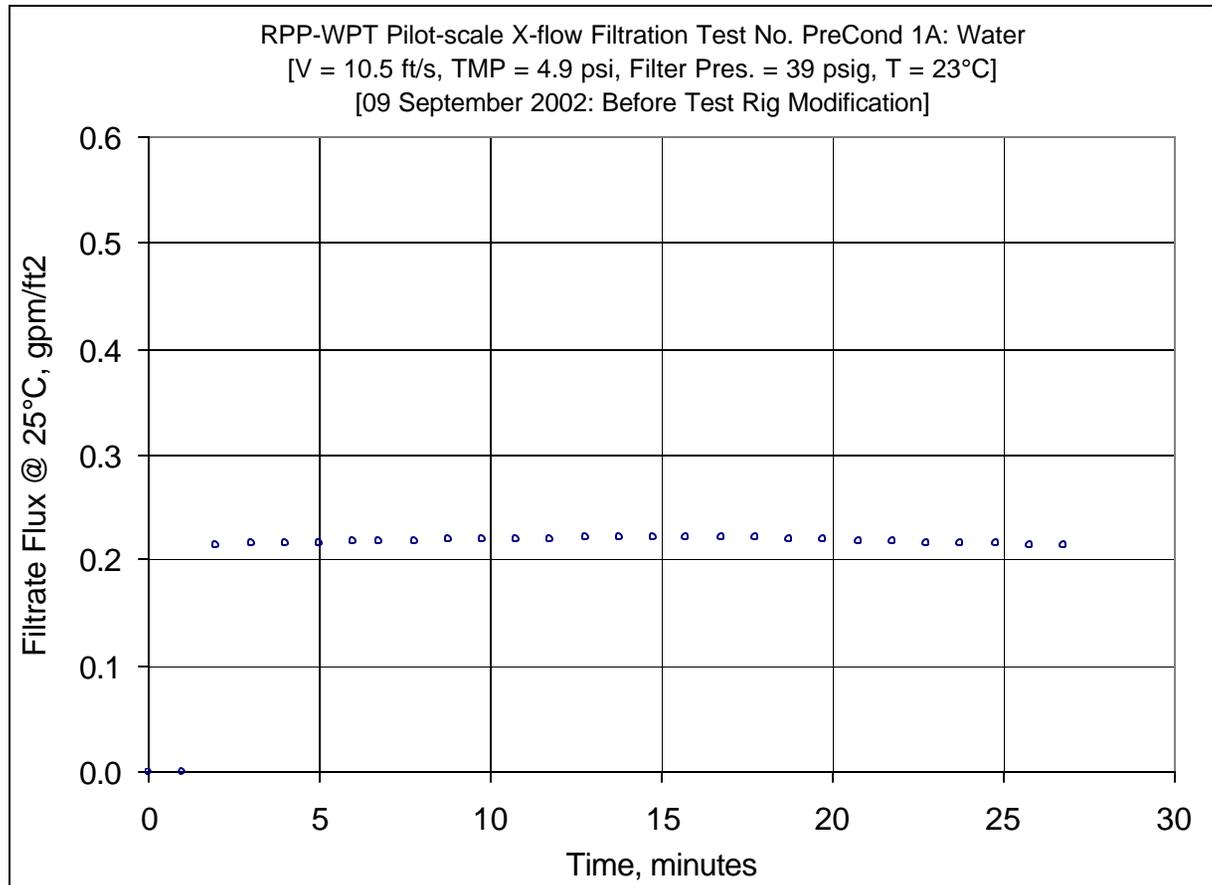


Figure A1: PreConditioning 1A – Inhibited Deionized & Filtered Water – Before Test Rig Modification



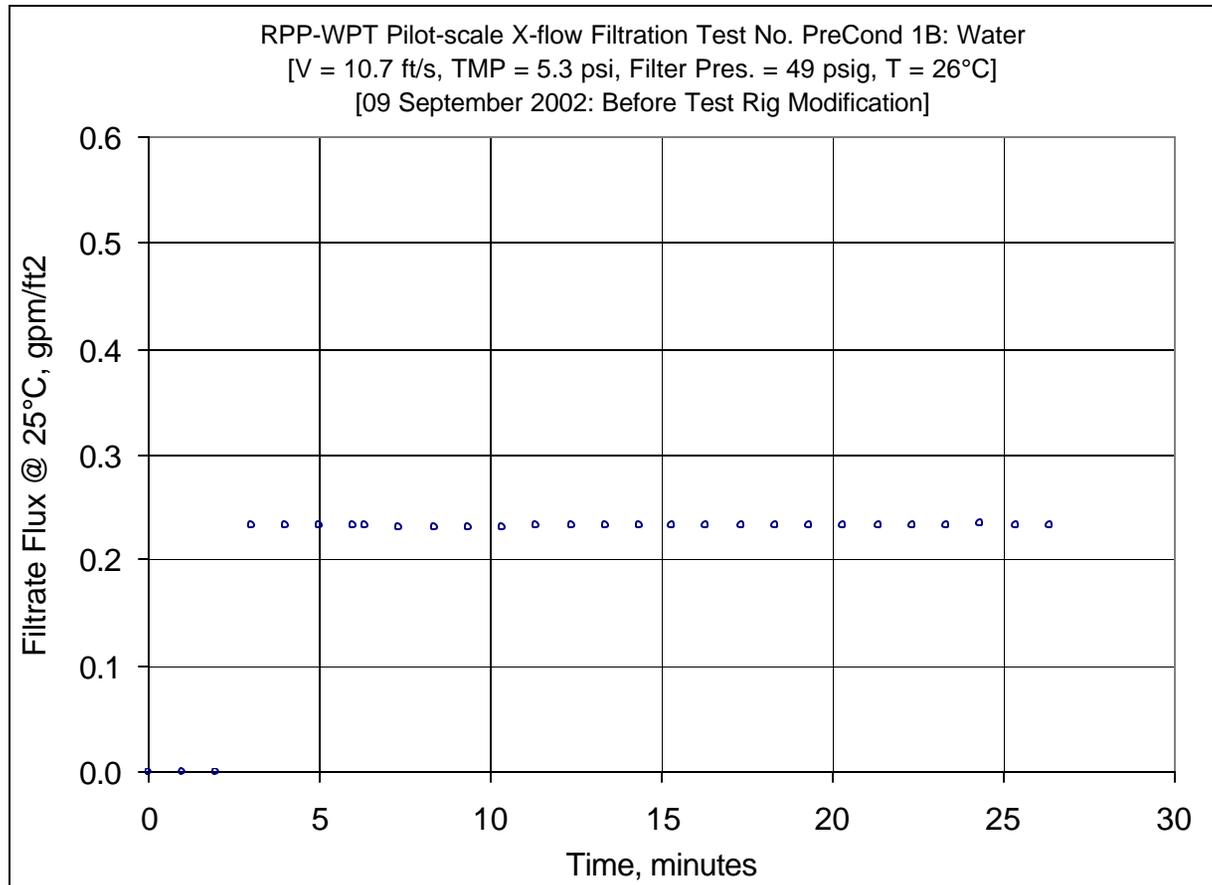


Figure A3: PreConditioning 1B – Inhibited Deionized & Filtered Water – Before Test Rig Modification



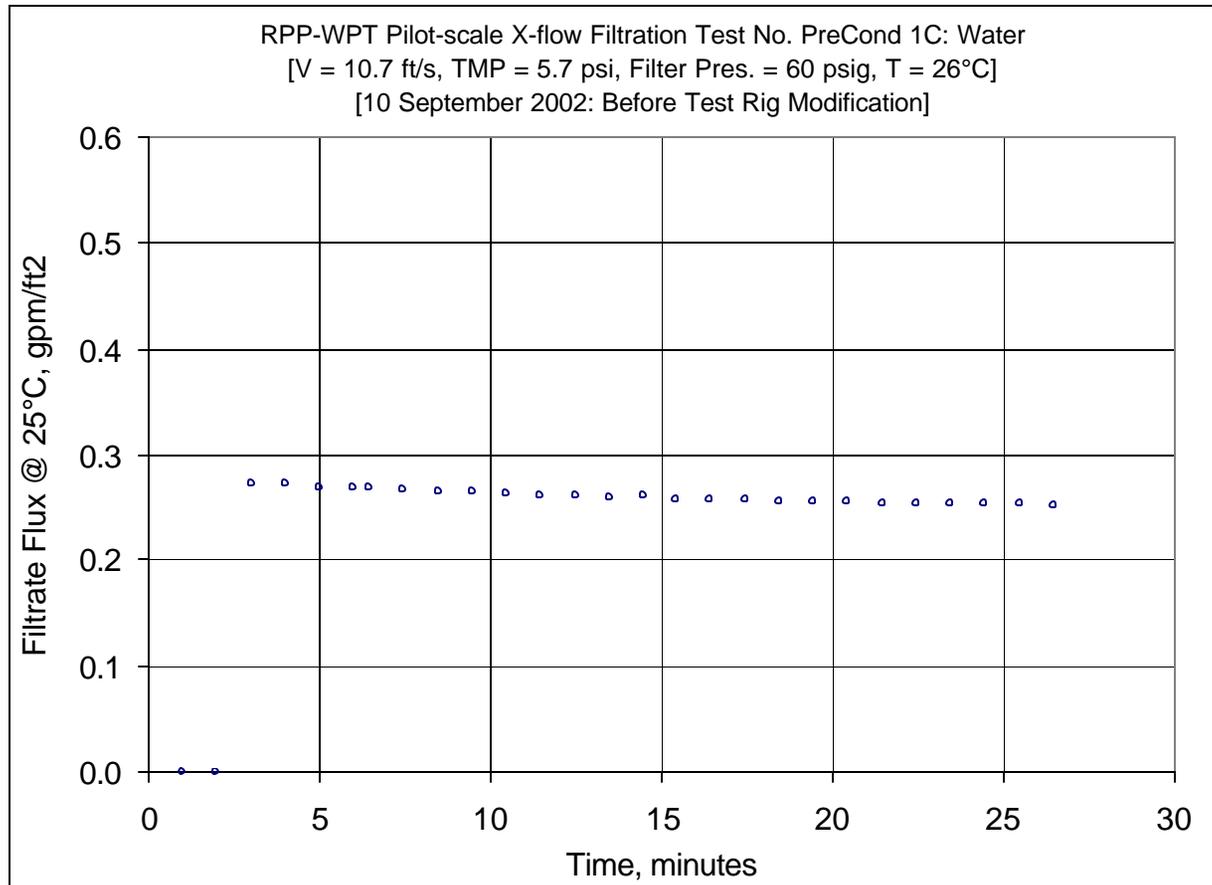


Figure A5: PreConditioning 1C – Inhibited Deionized & Filtered Water – Before Test Rig Modification



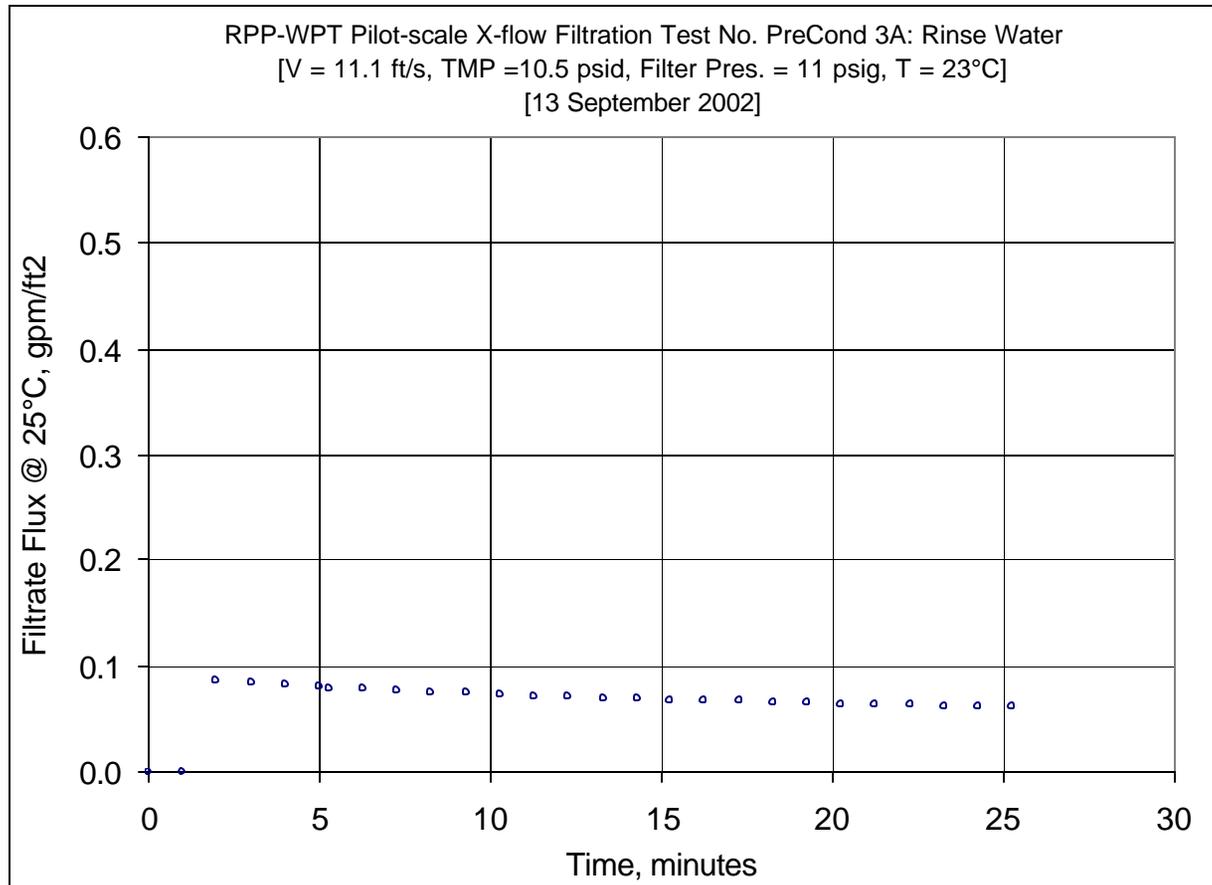


Figure A7: PreConditioning 3A – Inhibited Deionized & Filtered Water – Post Standard Slurry Tests



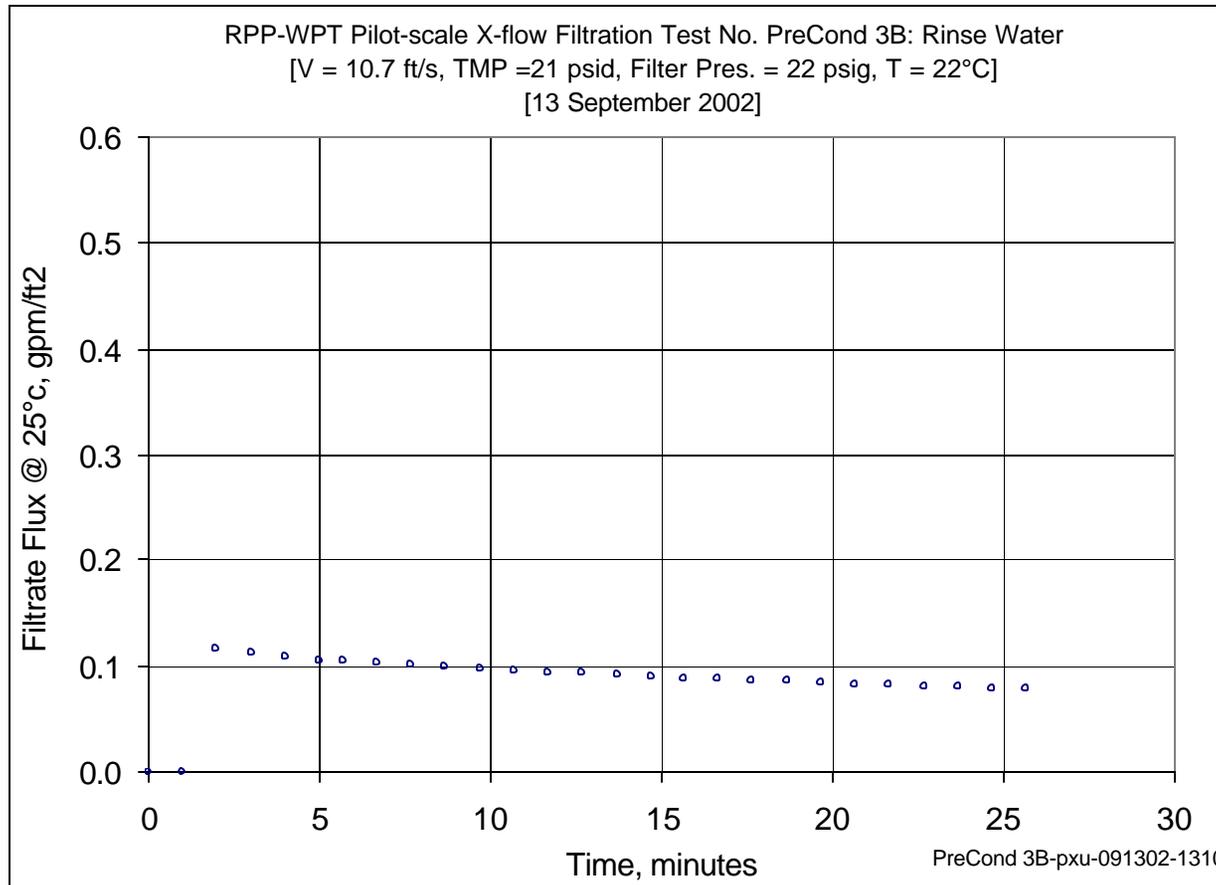


Figure A9: PreConditioning 3B – Inhibited Deionized & Filtered Water – Post Standard Slurry Tests



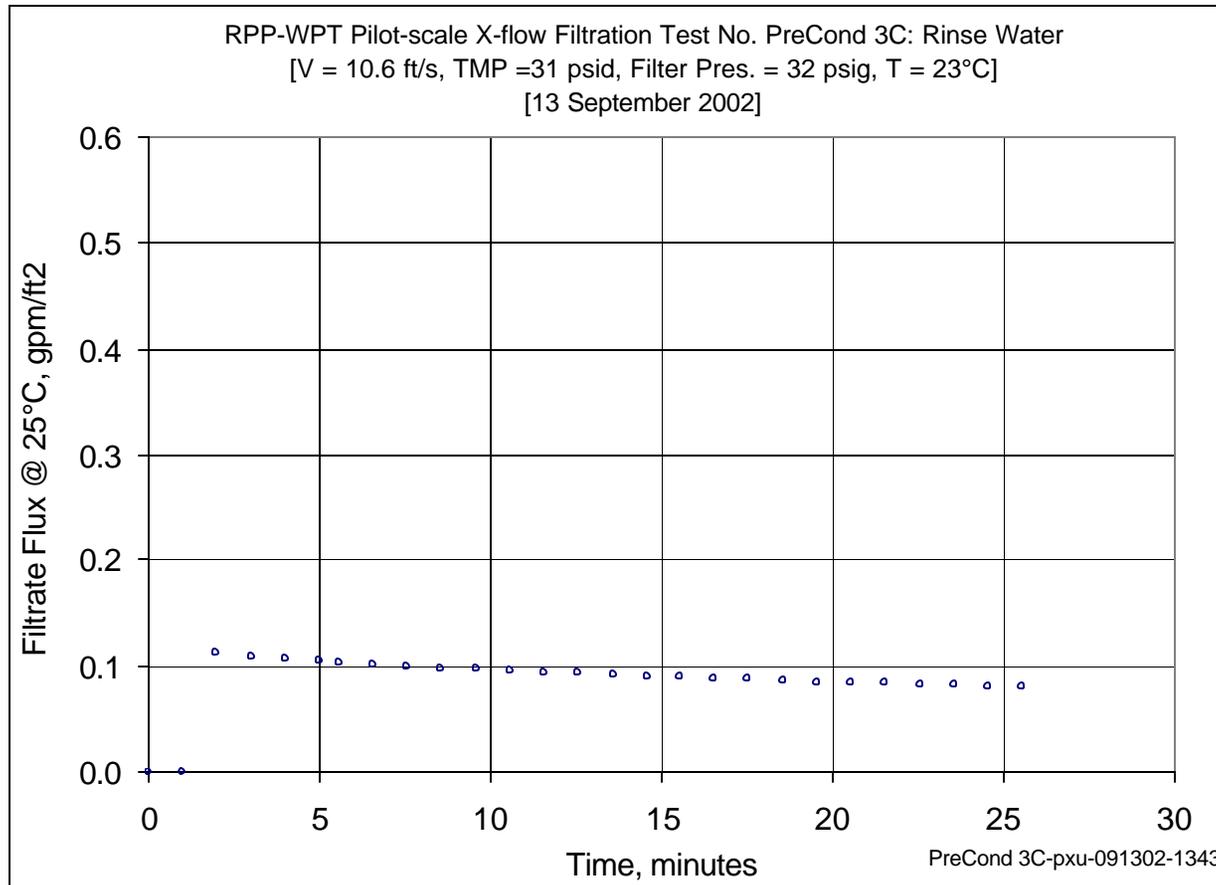


Figure A11: PreConditioning 3C – Inhibited Deionized & Filtered Water – Post Standard Slurry Tests



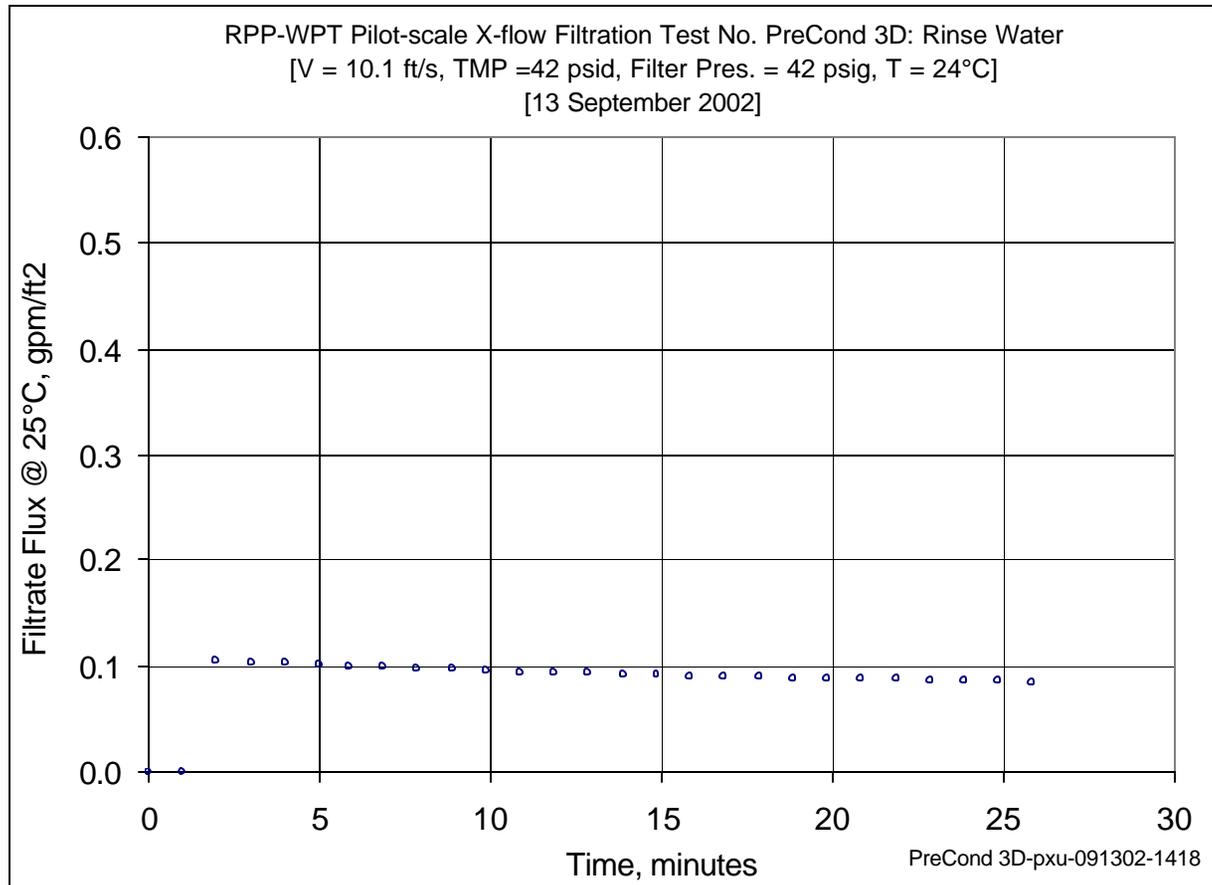


Figure A13: PreConditioning 3D – Inhibited Deionized & Filtered Water – Post Standard Slurry Tests



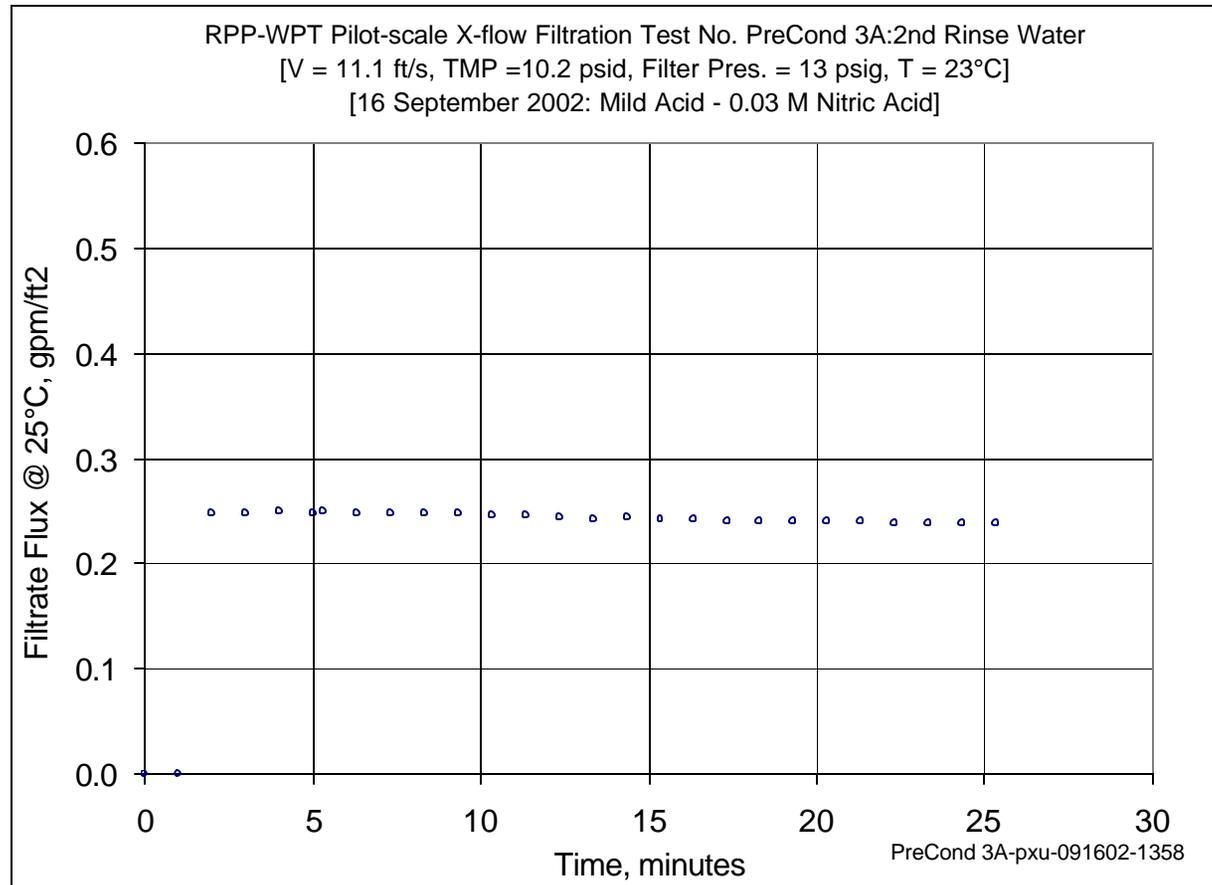


Figure A15: PreConditioning 3A – Deionized & Filtered Water with 0.03 M Nitric Acid – Post Standard Slurry Tests



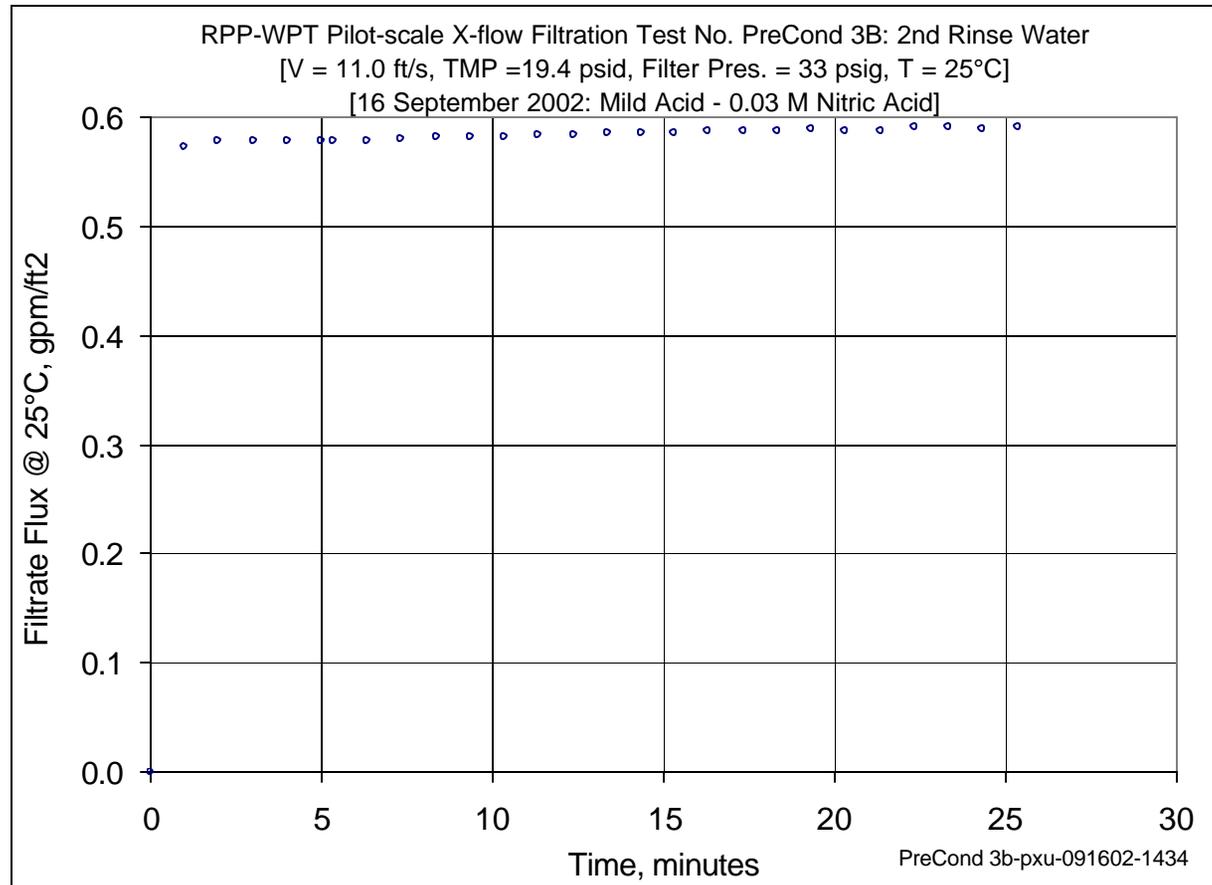


Figure A17: PreConditioning 3B – Deionized & Filtered Water with 0.03 M Nitric Acid – Post Standard Slurry Tests



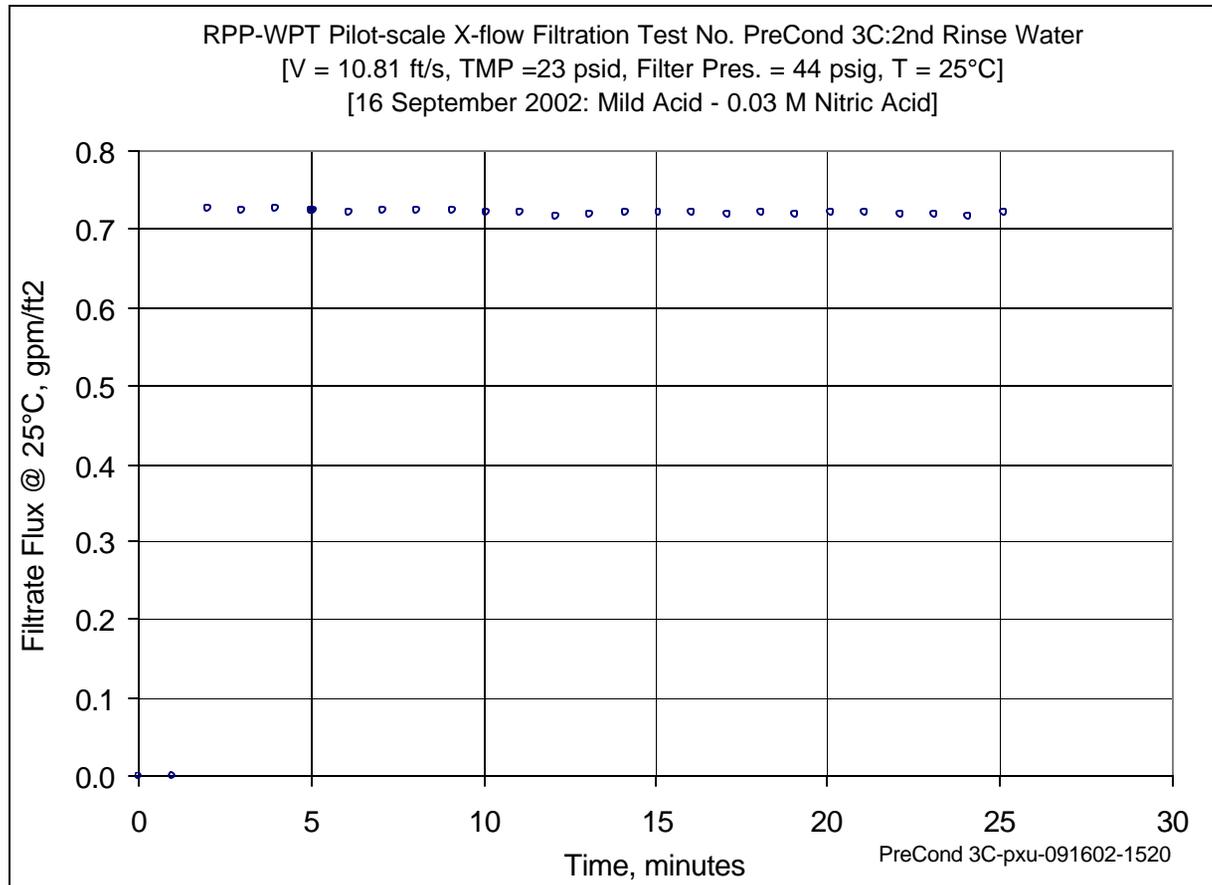


Figure A19: PreConditioning 3C – Deionized & Filtered Water with 0.03 M Nitric Acid – Post Standard Slurry Tests



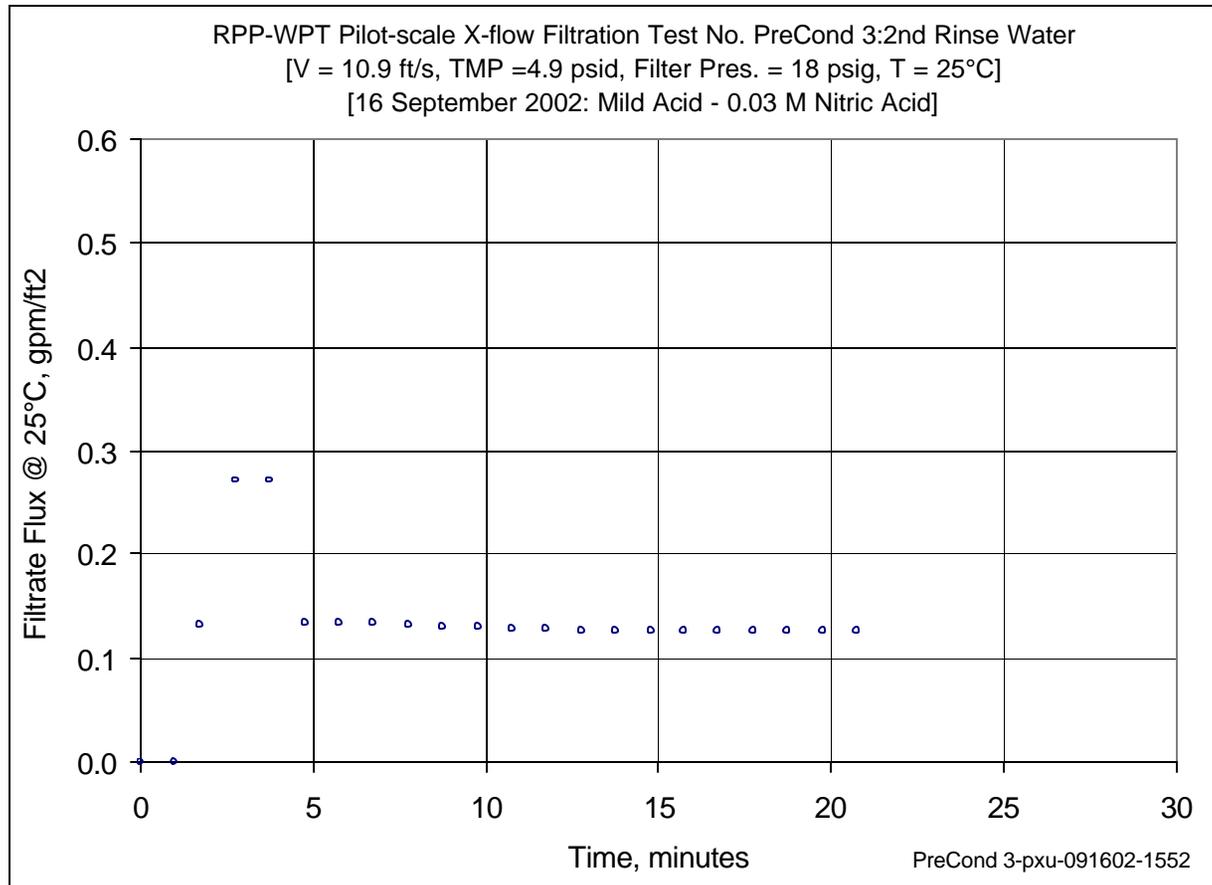


Figure A21: PreConditioning 3 – Deionized & Filtered Water with 0.03 M Nitric Acid – Post Standard Slurry Tests



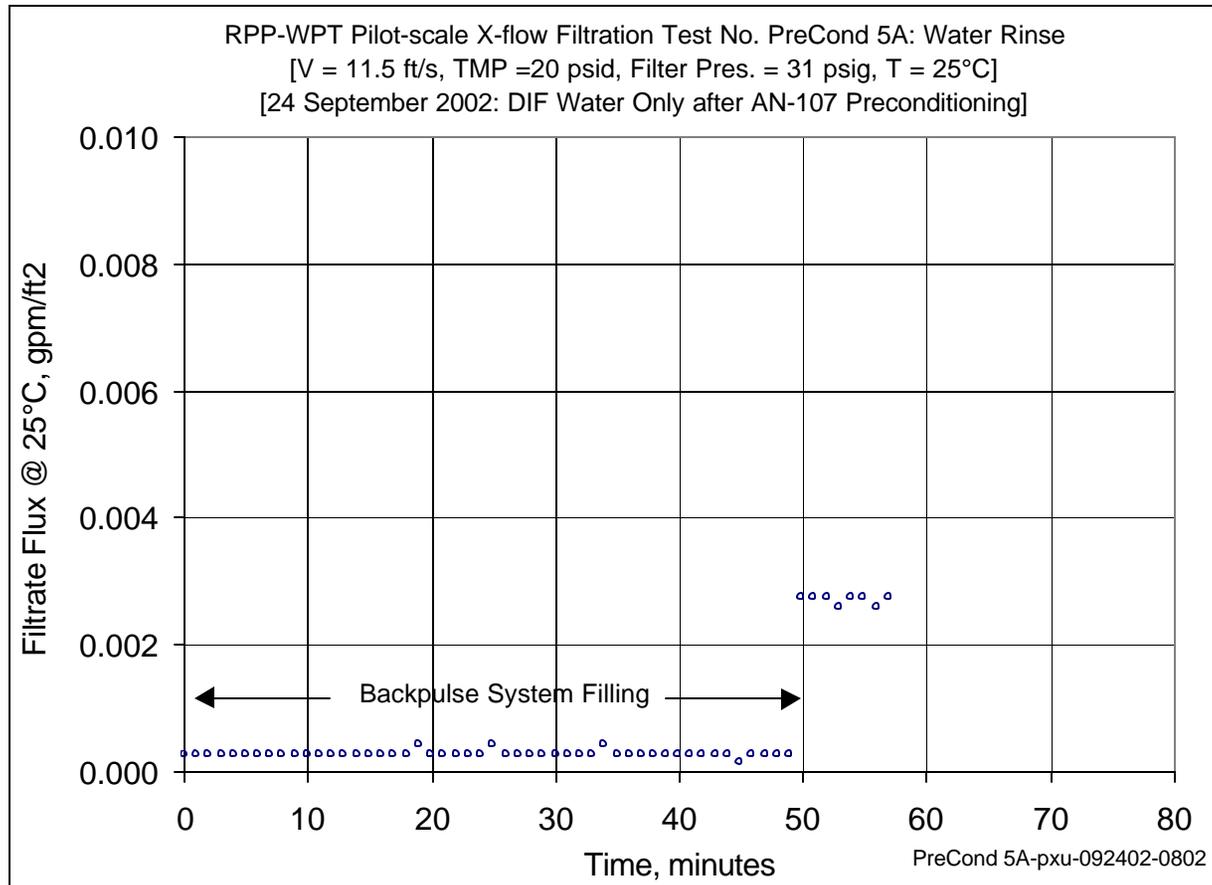


Figure A23: PreConditioning 5A – Deionized & Filtered Water – Post AN-107 Preconditioning Slurry Test



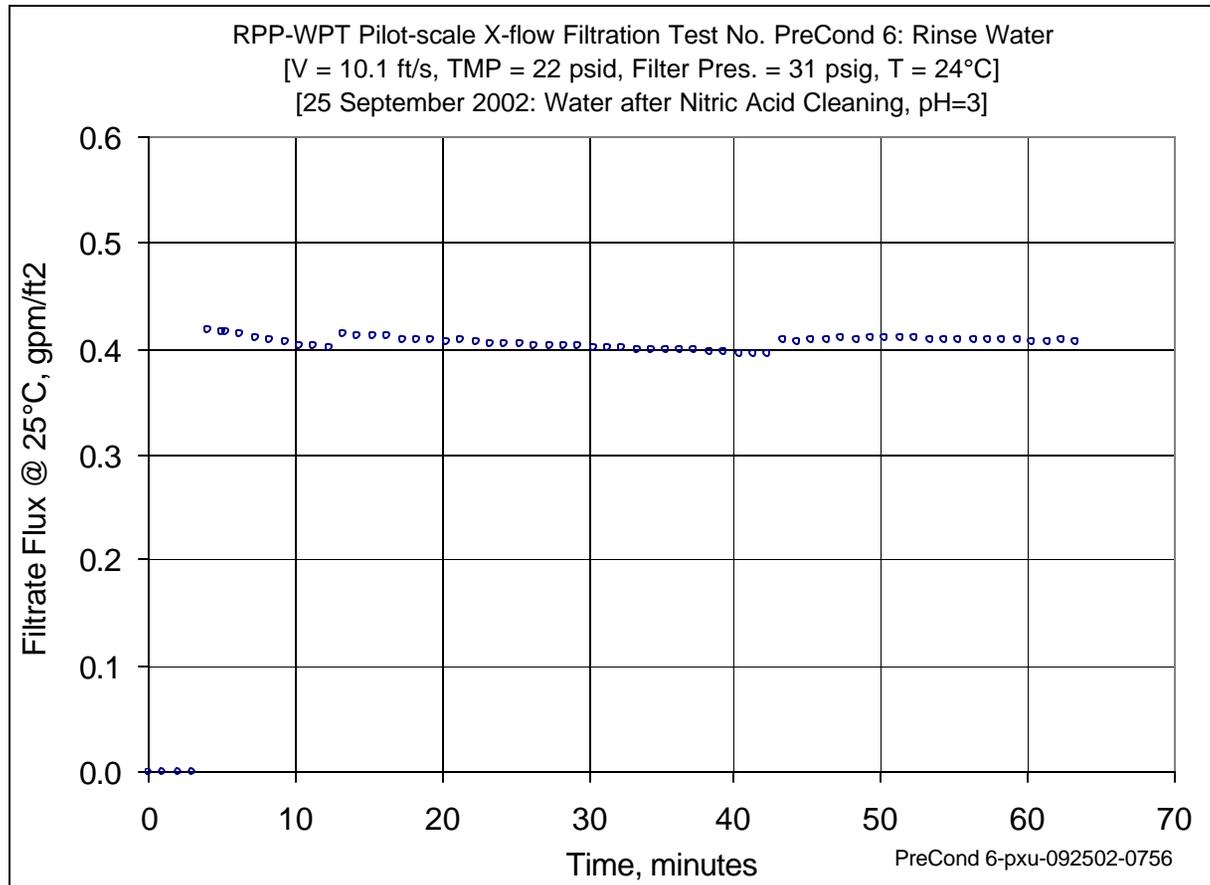


Figure A25: PreConditioning 6 – Deionized & Filtered Water – Post Nitric Acid Cleaning



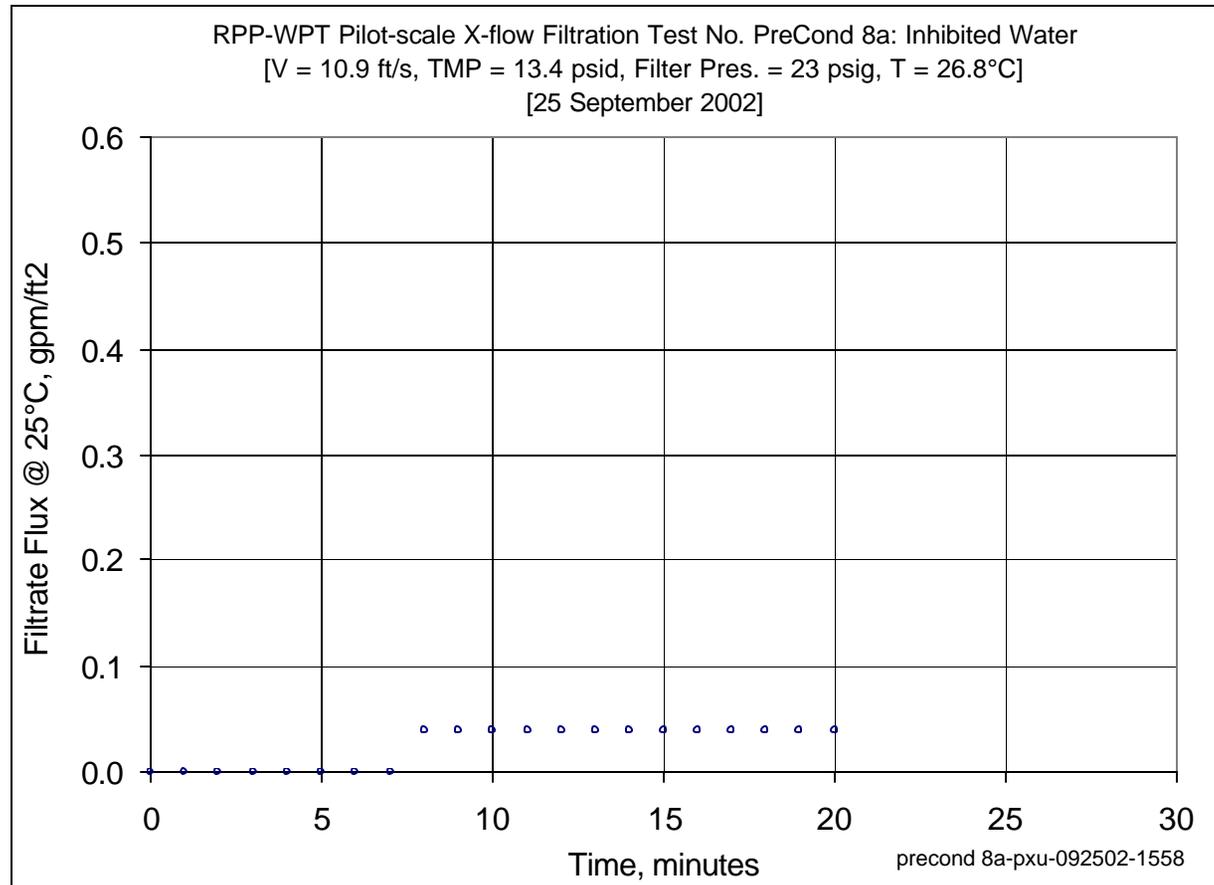


Figure A27: PreConditioning 8A – Deionized & Filtered Water – Post Standard Slurry Tests



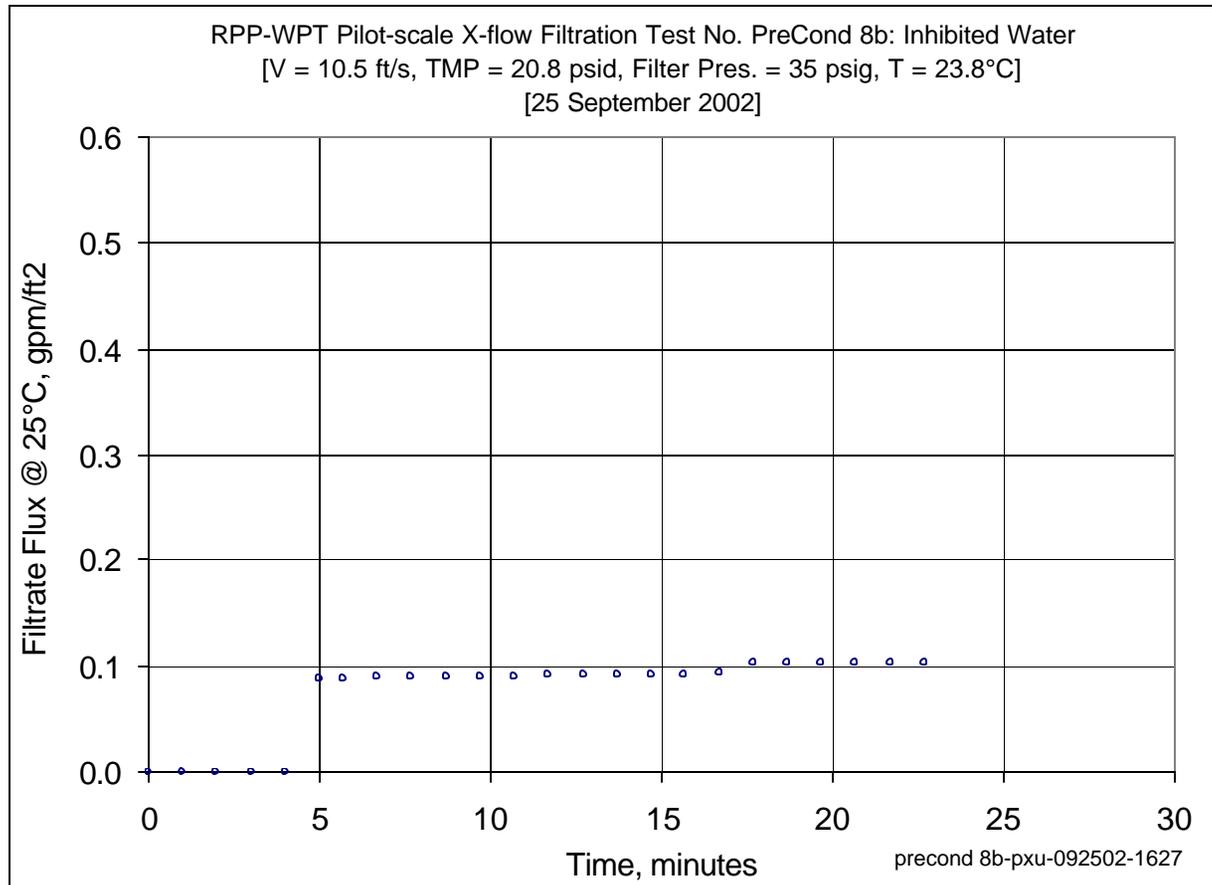


Figure A29: PreConditioning 8B – Deionized & Filtered Water – Post Standard Slurry Tests



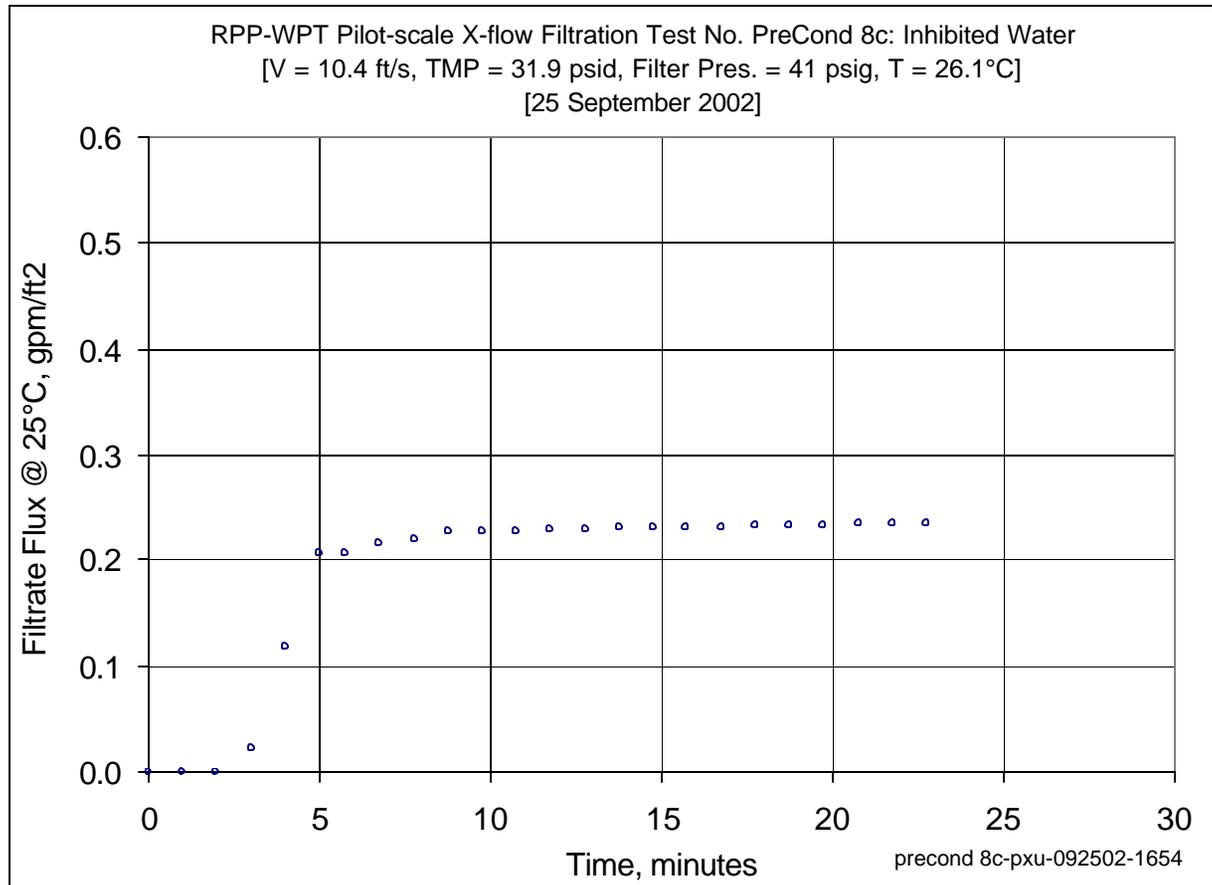


Figure A31: PreConditioning 8C – Deionized & Filtered Water – Post Standard Slurry Tests



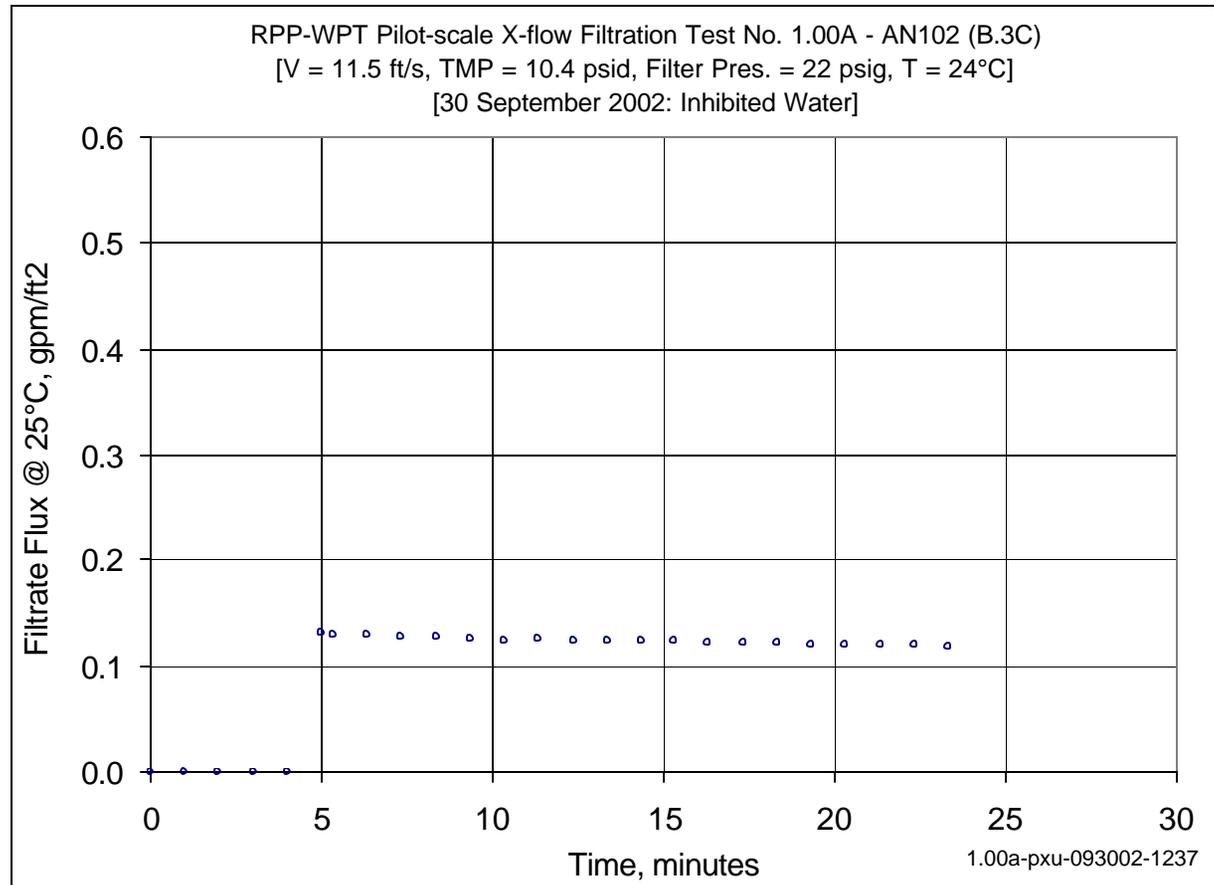


Figure A33: AN-102R2, Batch 3C Slurry Test 1.00A – Inhibited Deionized & Filtered Water



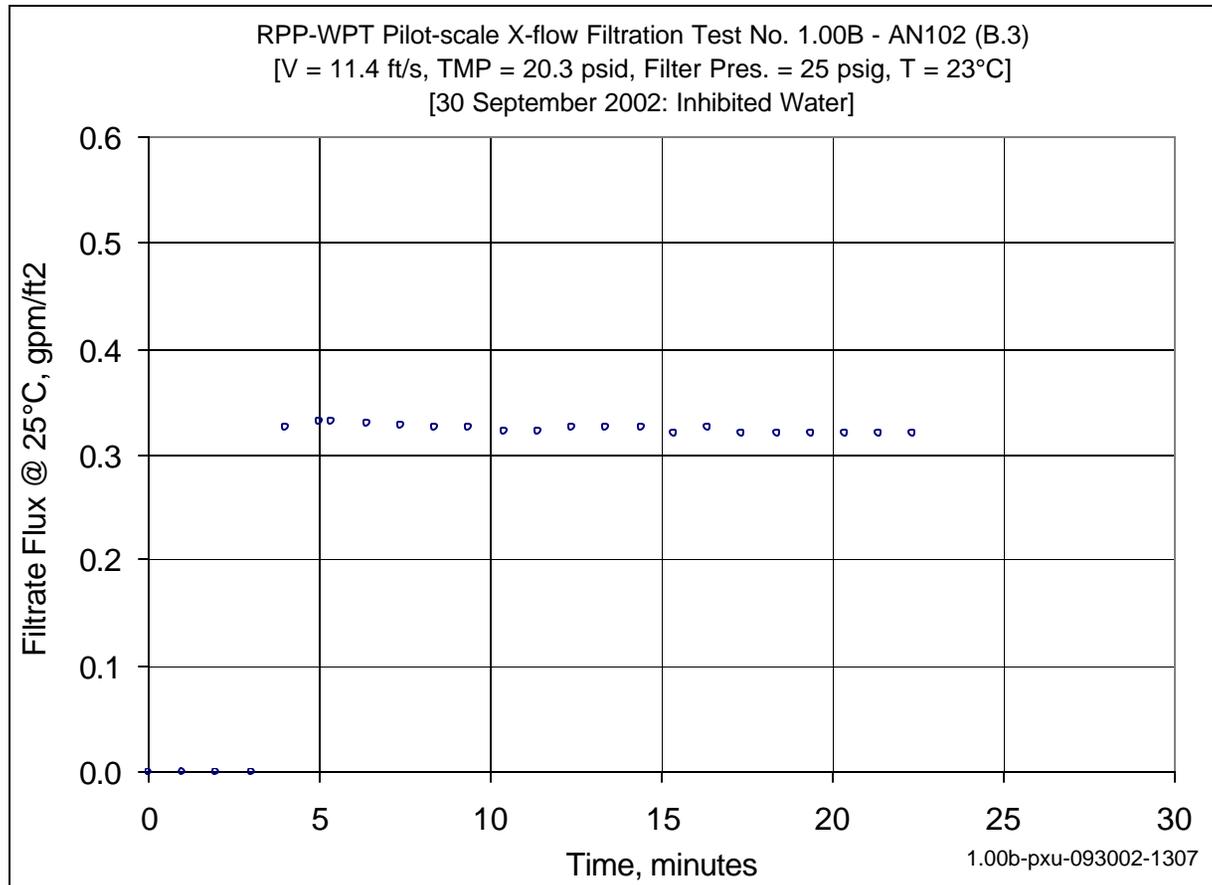


Figure A35: AN-102R2, Batch 3C Slurry Test 1.00B – Inhibited Deionized & Filtered Water



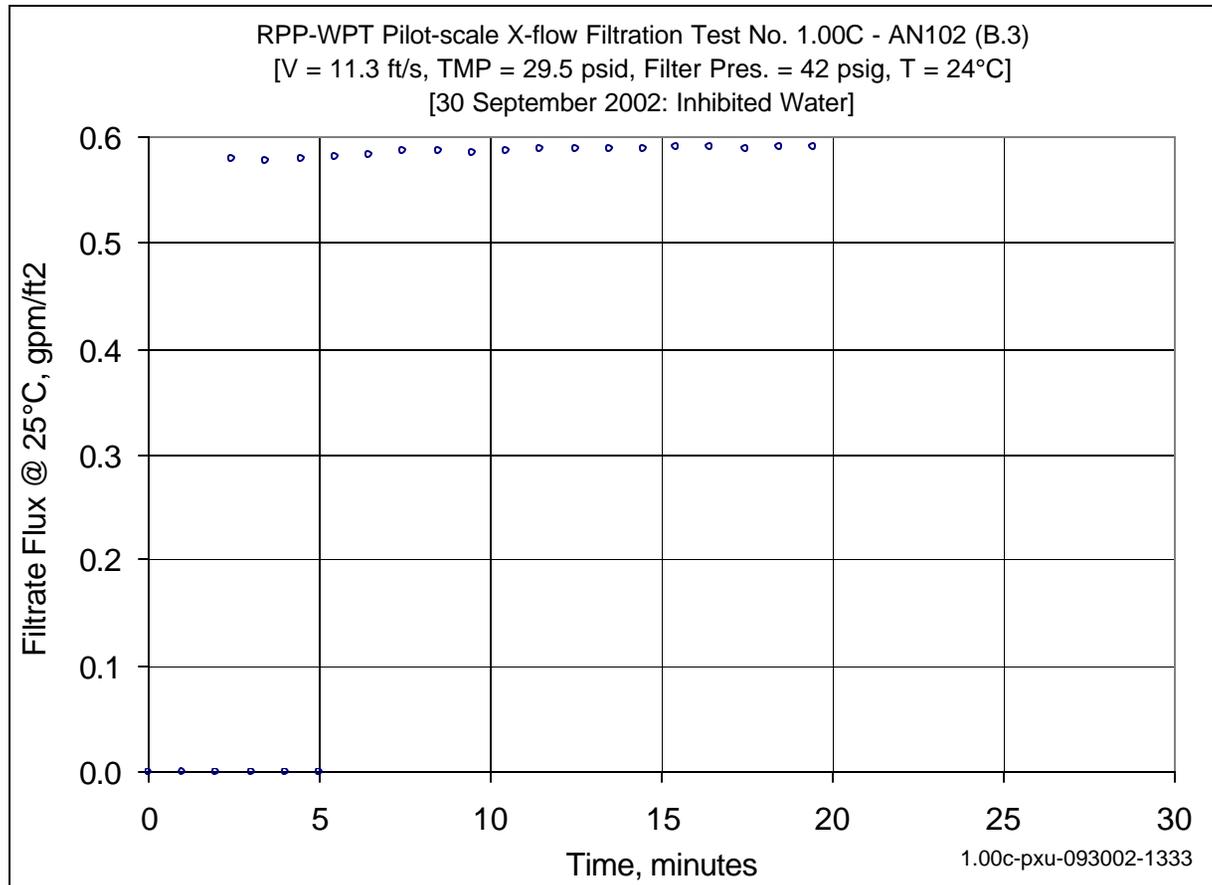


Figure A37: AN-102R2, Batch 3C Slurry Test 1.00C – Inhibited Deionized & Filtered Water



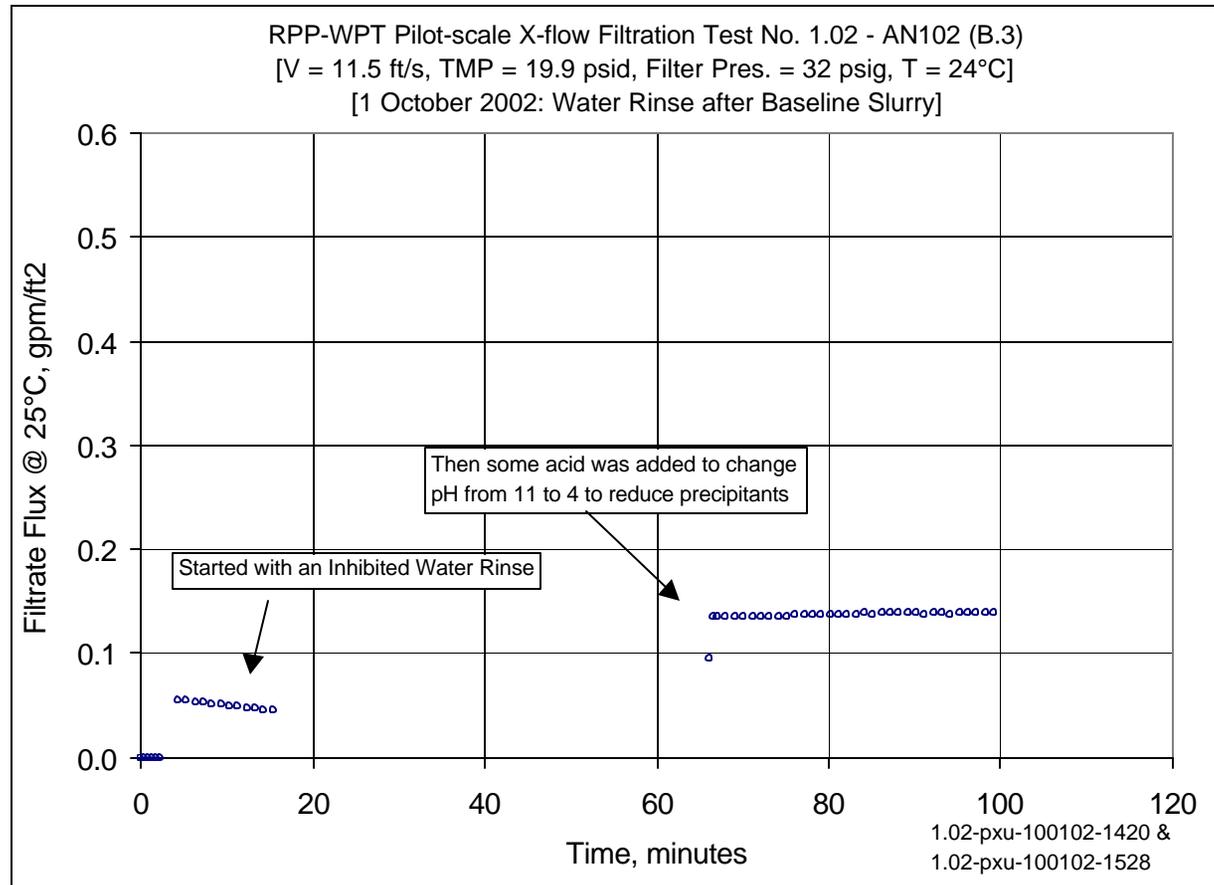


Figure A39: AN-102R2, Batch 3C Slurry Test 1.02 – Inhibited Deionized & Filtered Water, Then a Mild Acid was Added



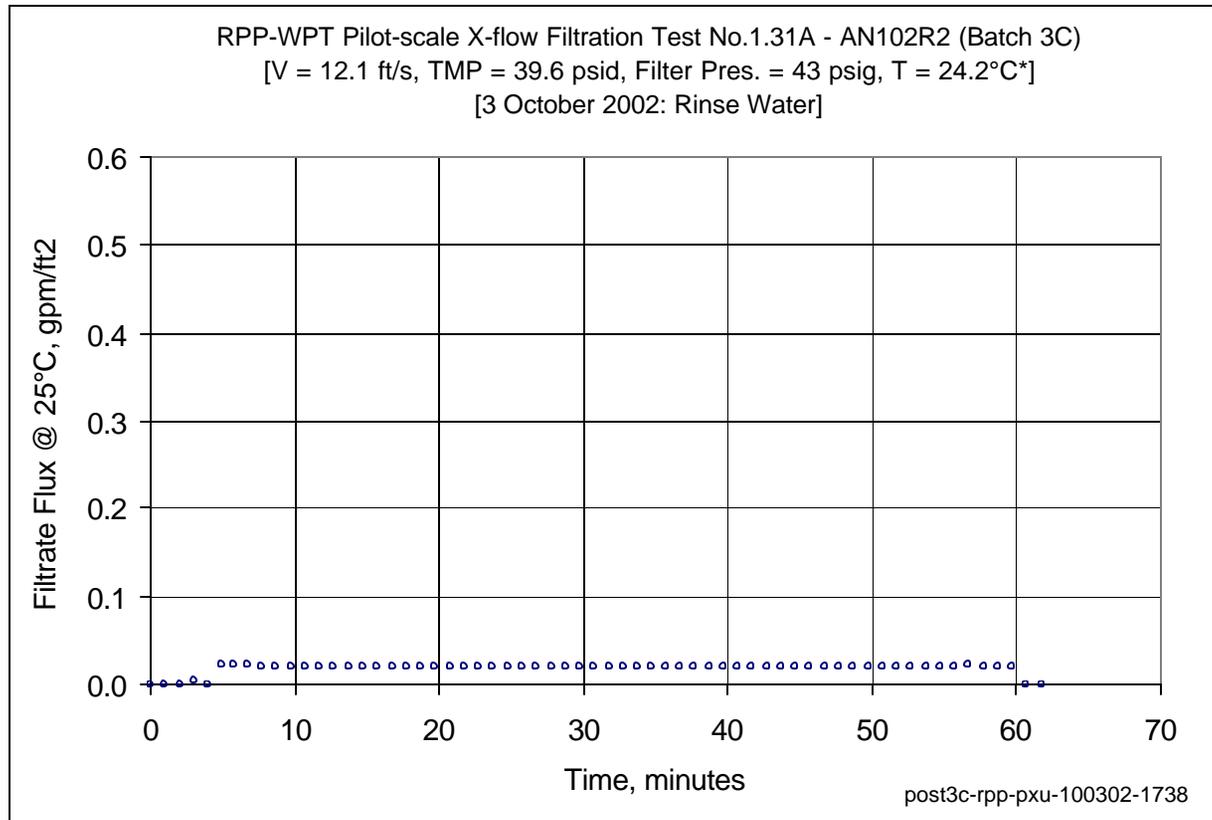


Figure A41: AN-102R2, Batch 3C Slurry Test 1.31A – Deionized & Filtered Water Rinse after Dewatering Slurry



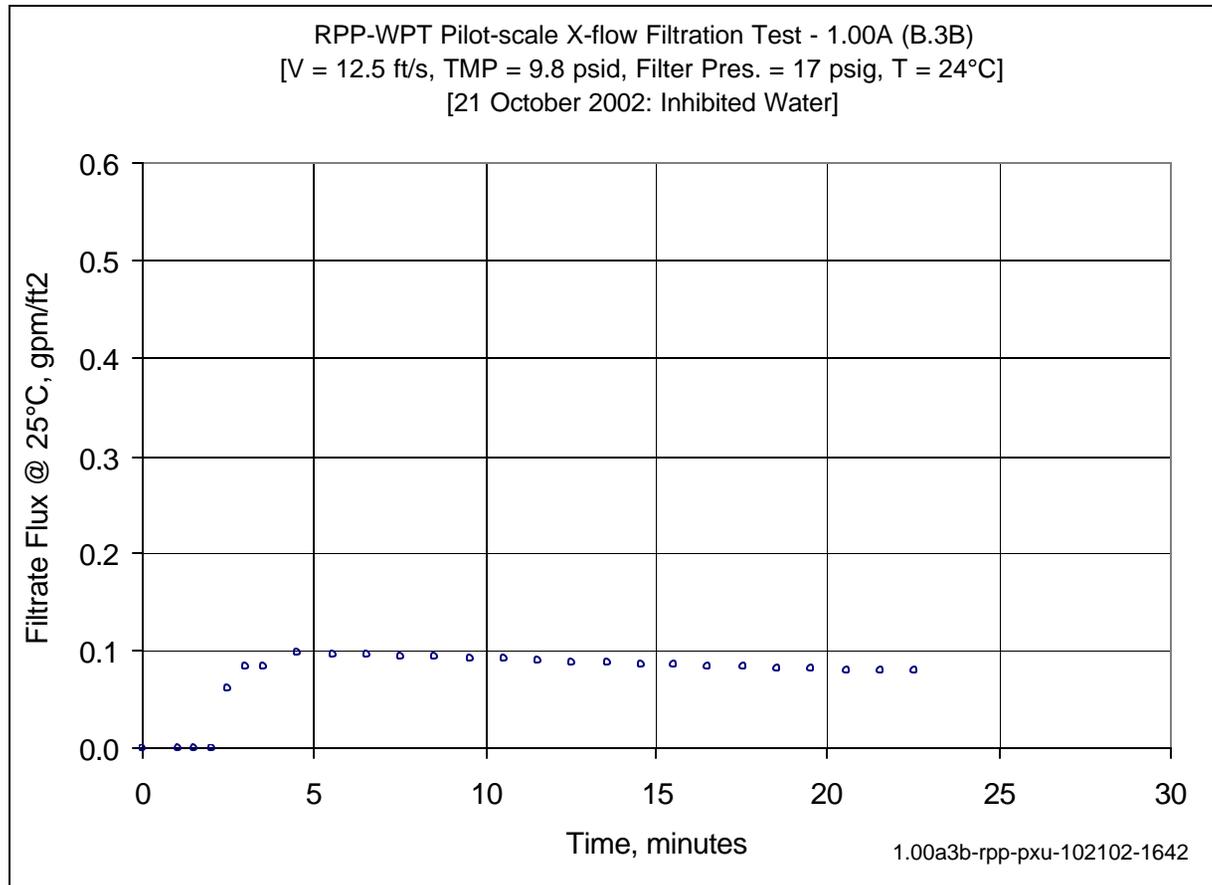


Figure A43: AN-102R2, Batch 3B Slurry Test 1.00A – Inhibited Deionized & Filtered Water



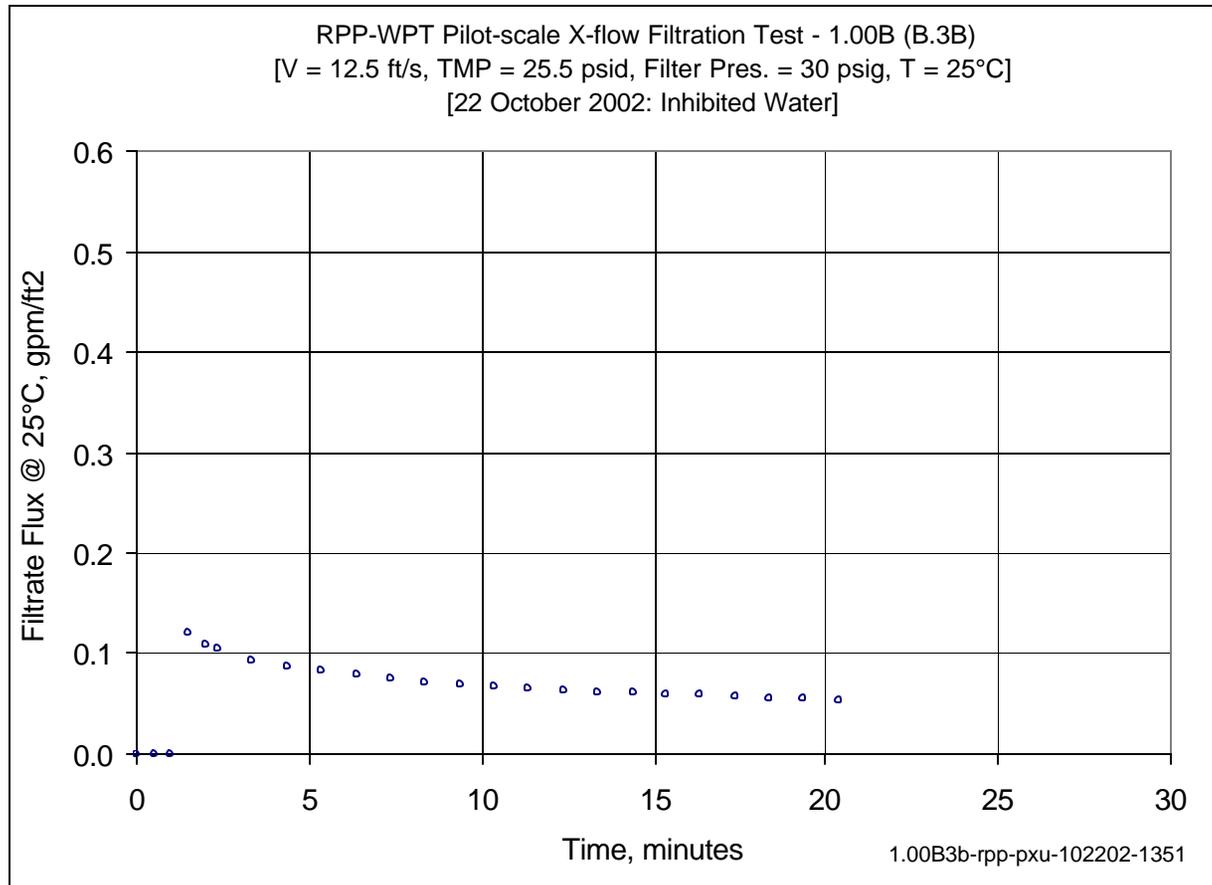


Figure A43: AN-102R2, Batch 3B Slurry Test 1.00B – Inhibited Deionized & Filtered Water



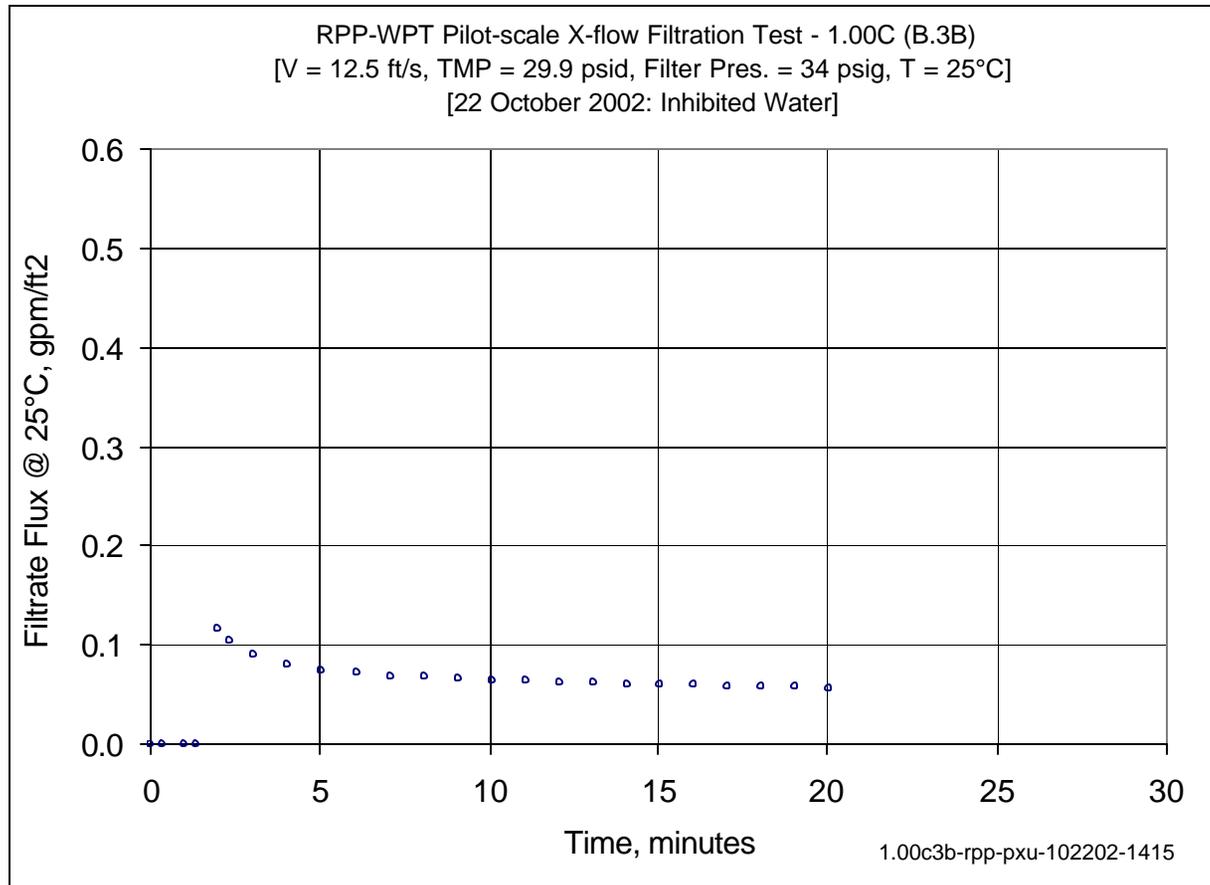


Figure A45: AN-102R2, Batch 3B Slurry Test 1.00C – Inhibited Deionized & Filtered Water



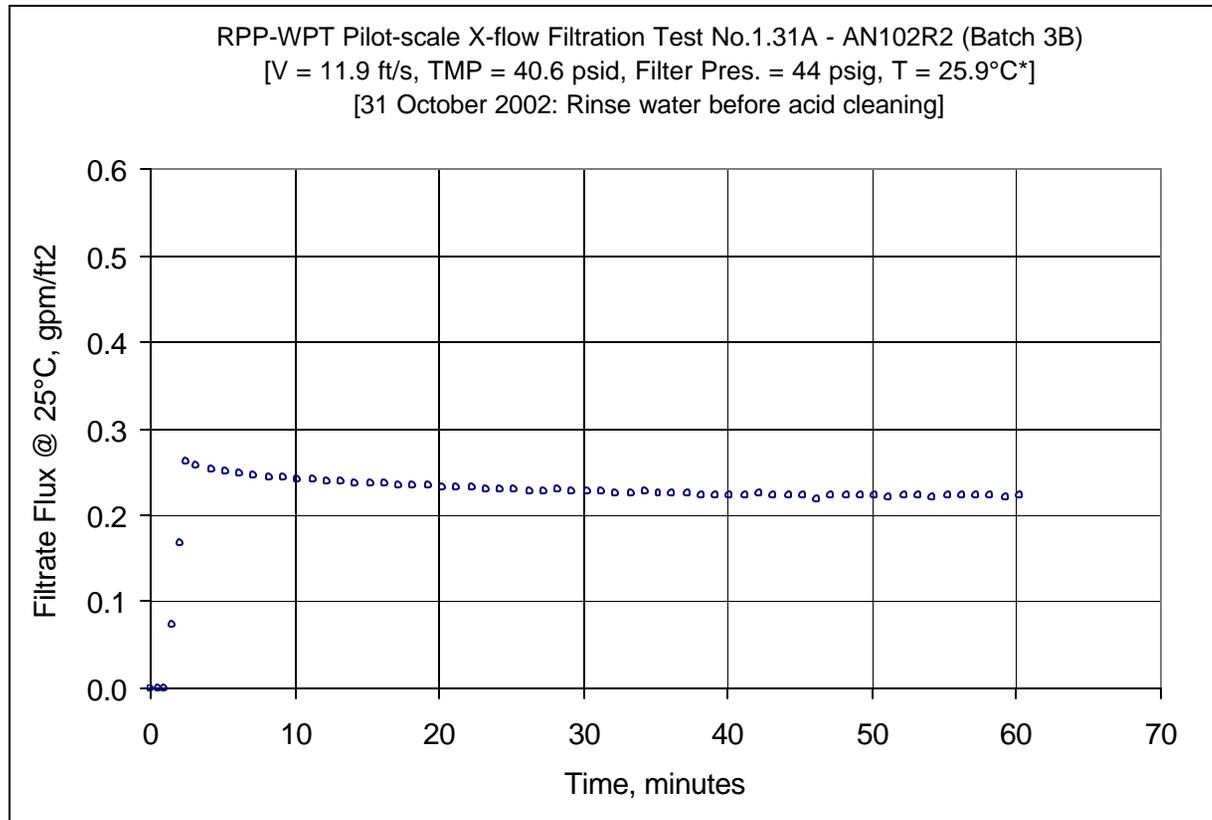


Figure A49: AN-102R2, Batch 3B Slurry Test 1.31A – Deionized & Filtered Water Rinse after Dewatering Slurry



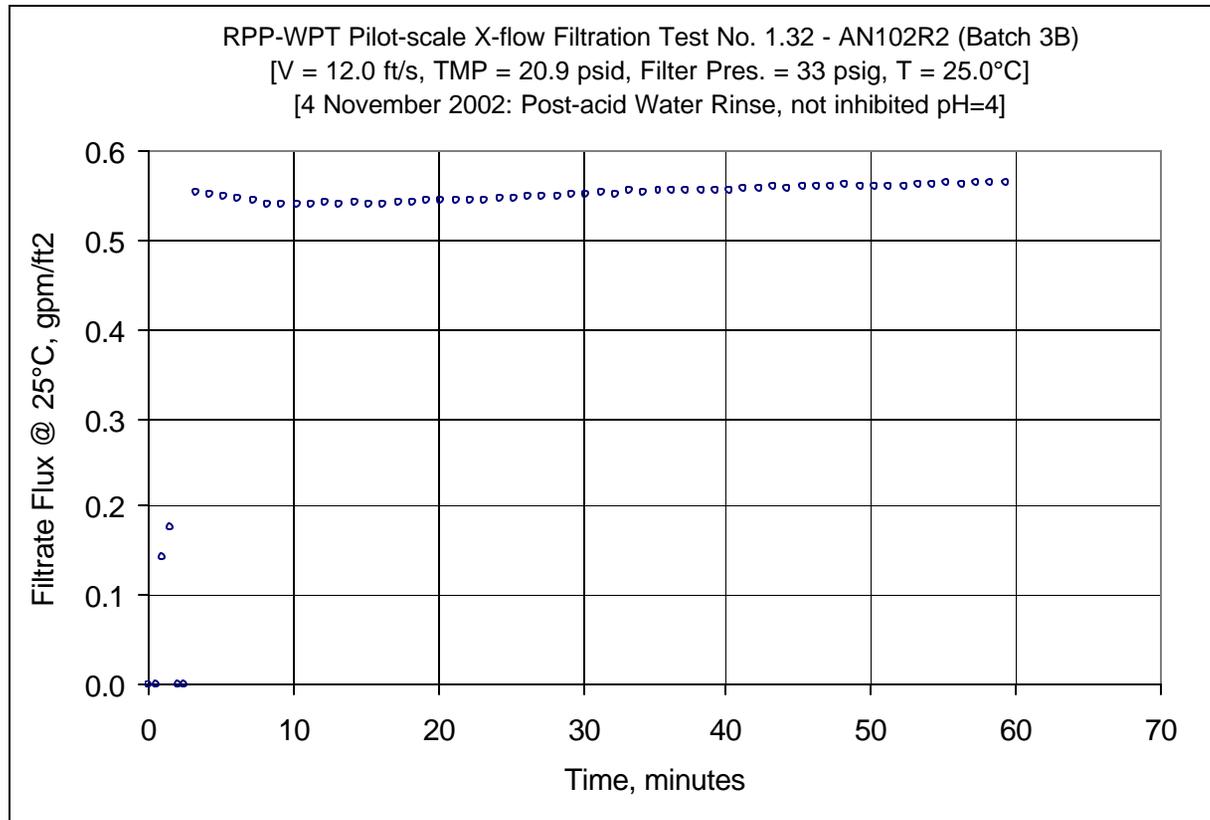


Figure A51: AN-102R2, Batch 3B Slurry Test 1.32 – Deionized & Filtered Water (pH=4) Rinse after Acid Cleaning



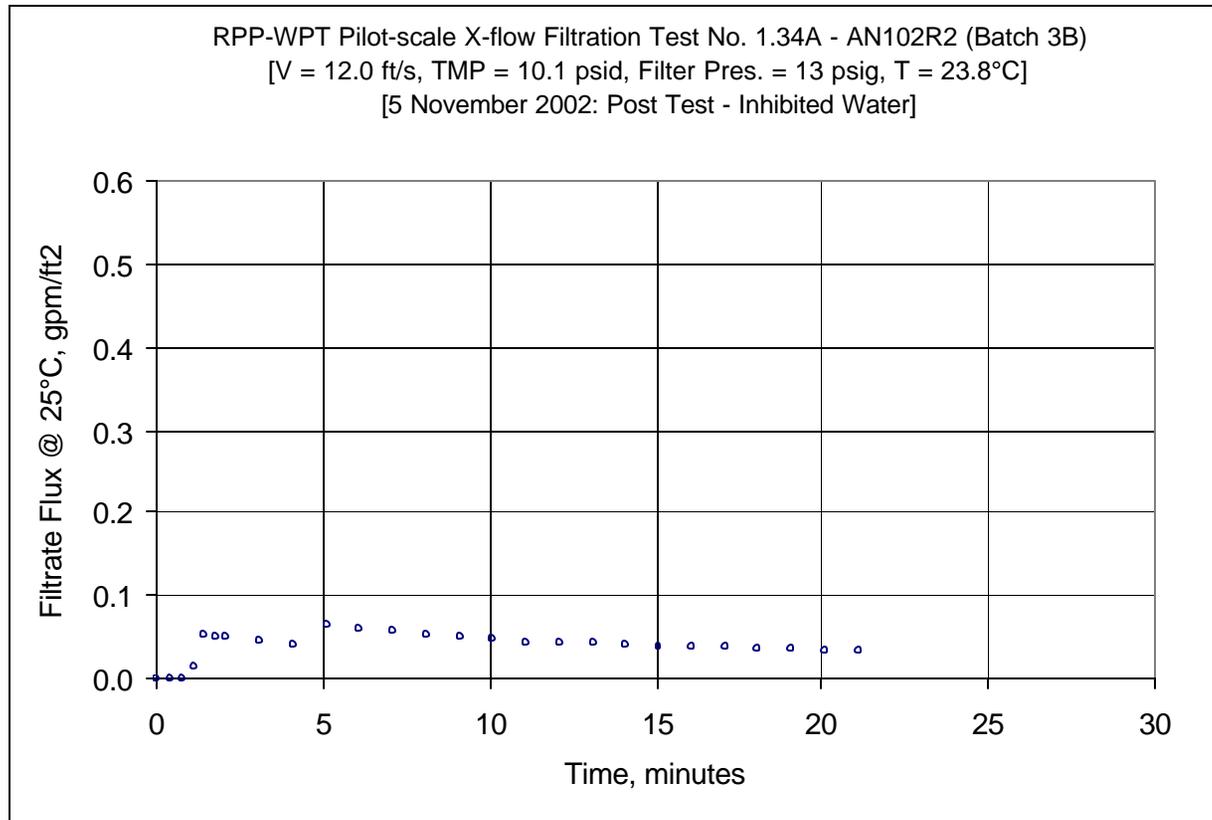


Figure A53: AN-102R2, Batch 3B Slurry Test 1.34A – Inhibited Deionized & Filtered Water Test after Standard Slurry



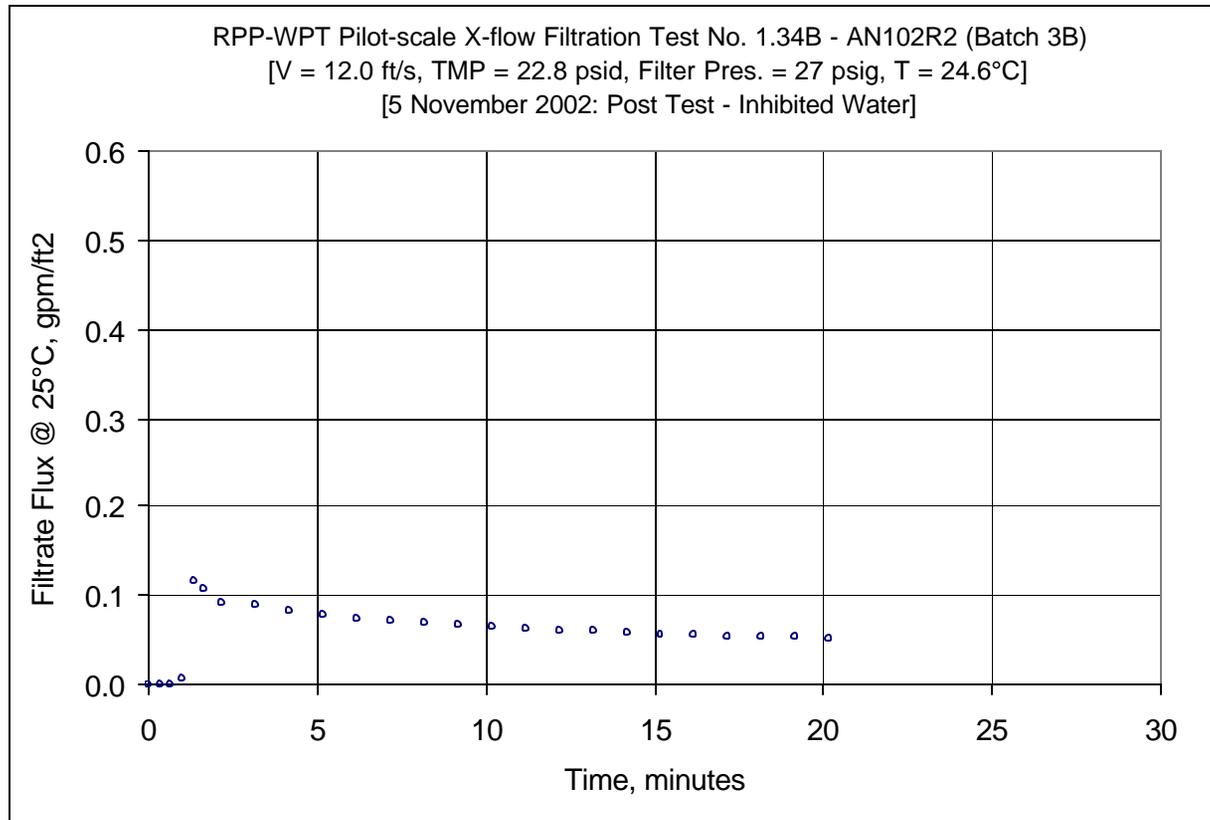


Figure A55: AN-102R2, Batch 3B Slurry Test 1.34B – Inhibited Deionized & Filtered Water Test after Standard Slurry



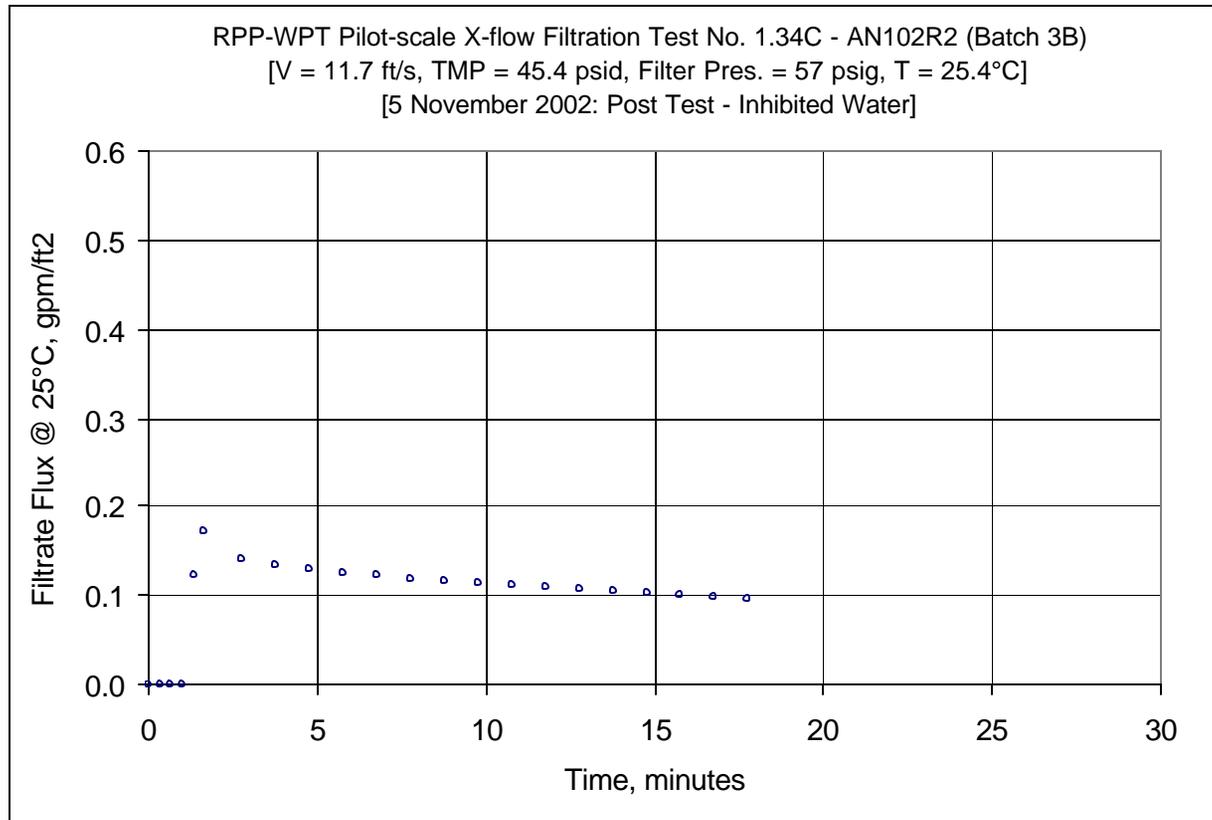


Figure A57: AN-102R2, Batch 3B Slurry Test 1.34C – Inhibited Deionized & Filtered Water Test after Standard Slurry



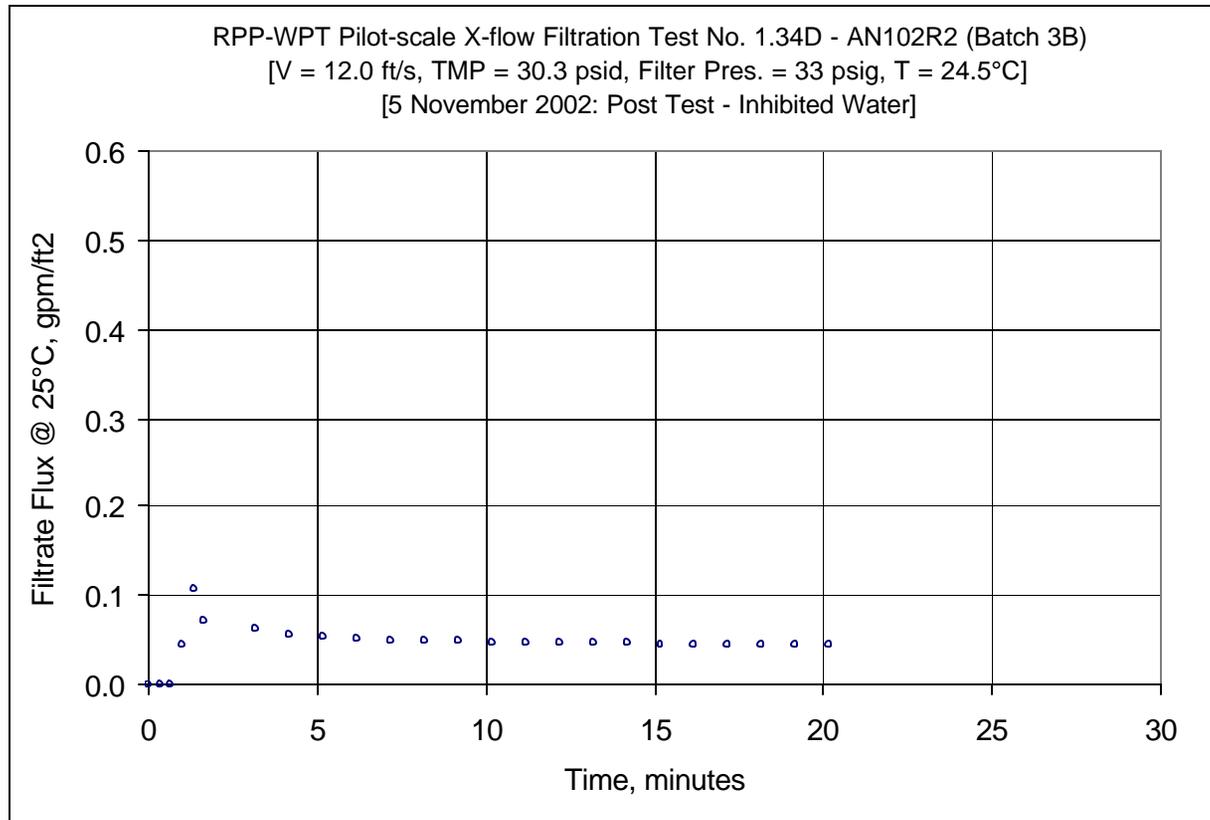


Figure A59: AN-102R2, Batch 3B Slurry Test 1.34D – Inhibited Deionized & Filtered Water Test after Standard Slurry



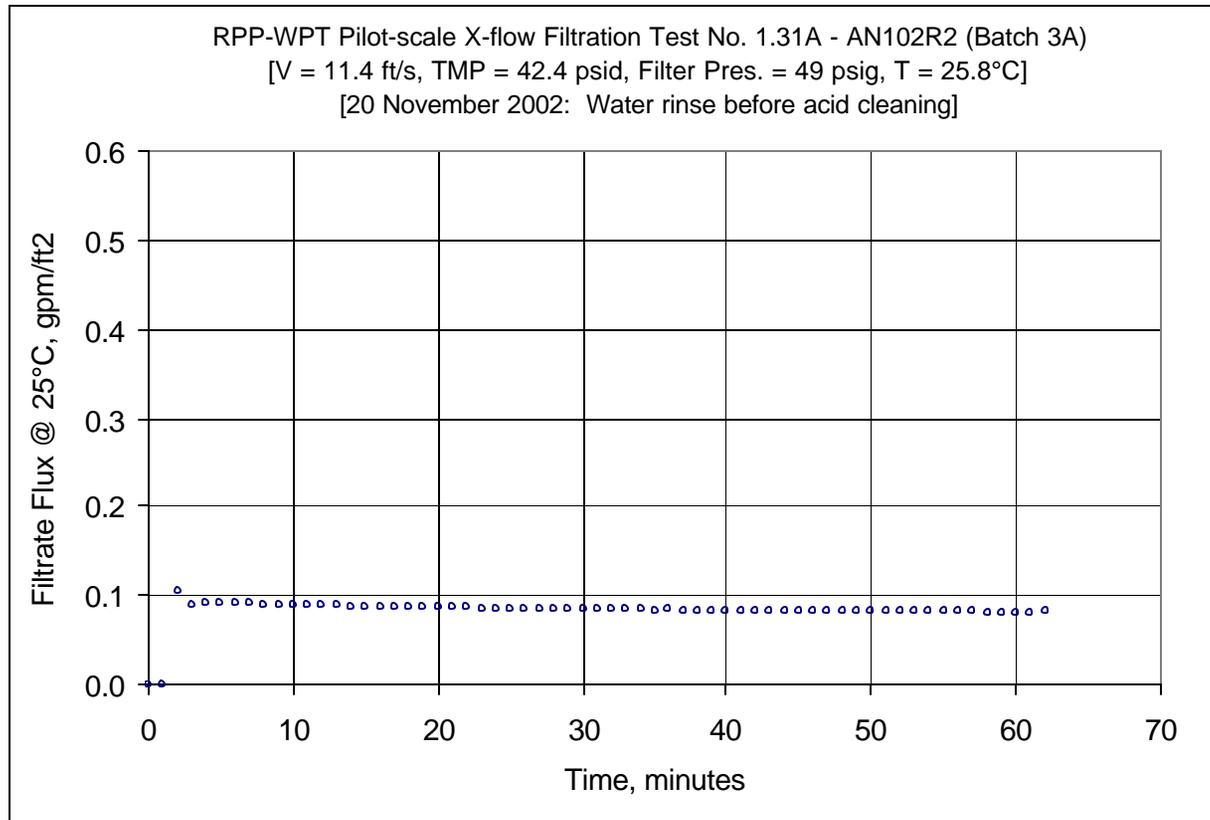


Figure A61: AN-102R2, Batch 3A Slurry Test 1.31A – Deionized & Filtered Water Rinse after Dewatering Slurry



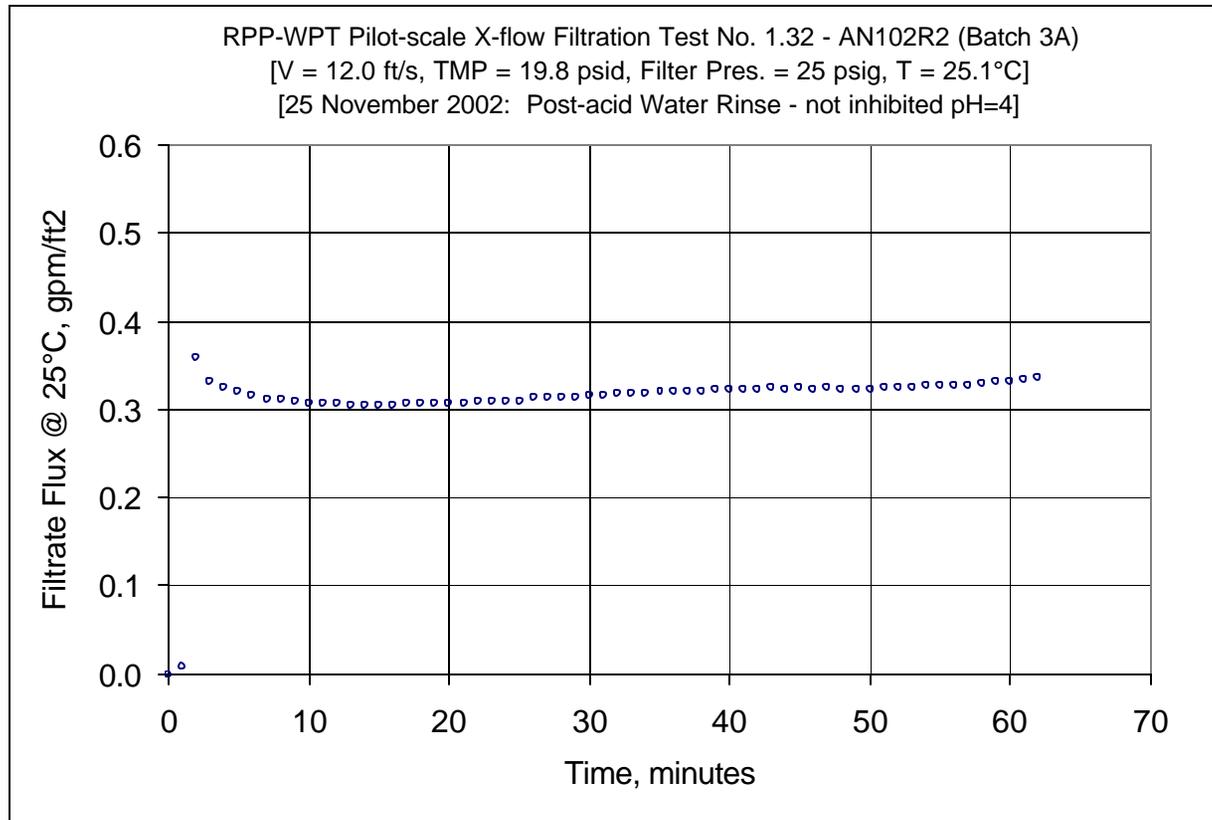


Figure A63: AN-102R2, Batch 3A Slurry Test 1.32 – Deionized & Filtered Water (pH=4) Rinse after Acid Cleaning



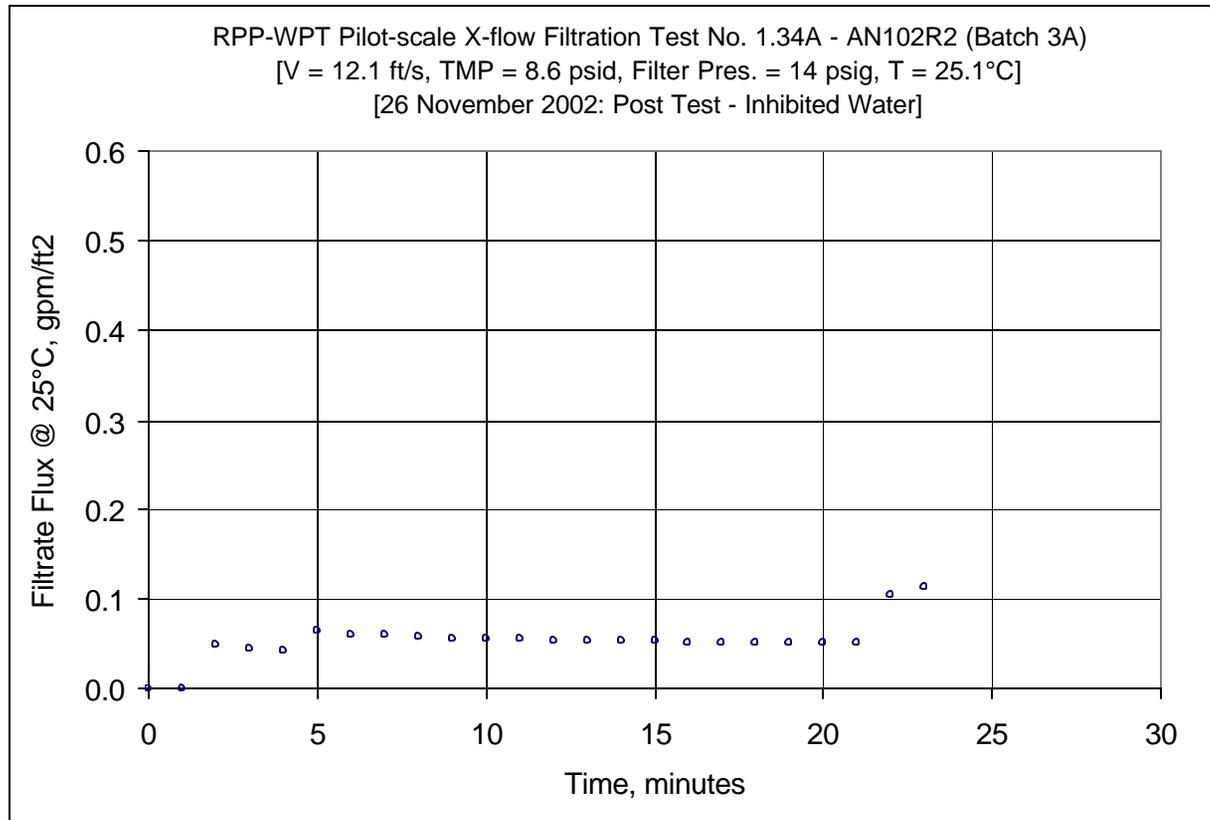


Figure A65: AN-102R2, Batch 3A Slurry Test 1.34A – Inhibited Deionized & Filtered Water Test after Standard Slurry



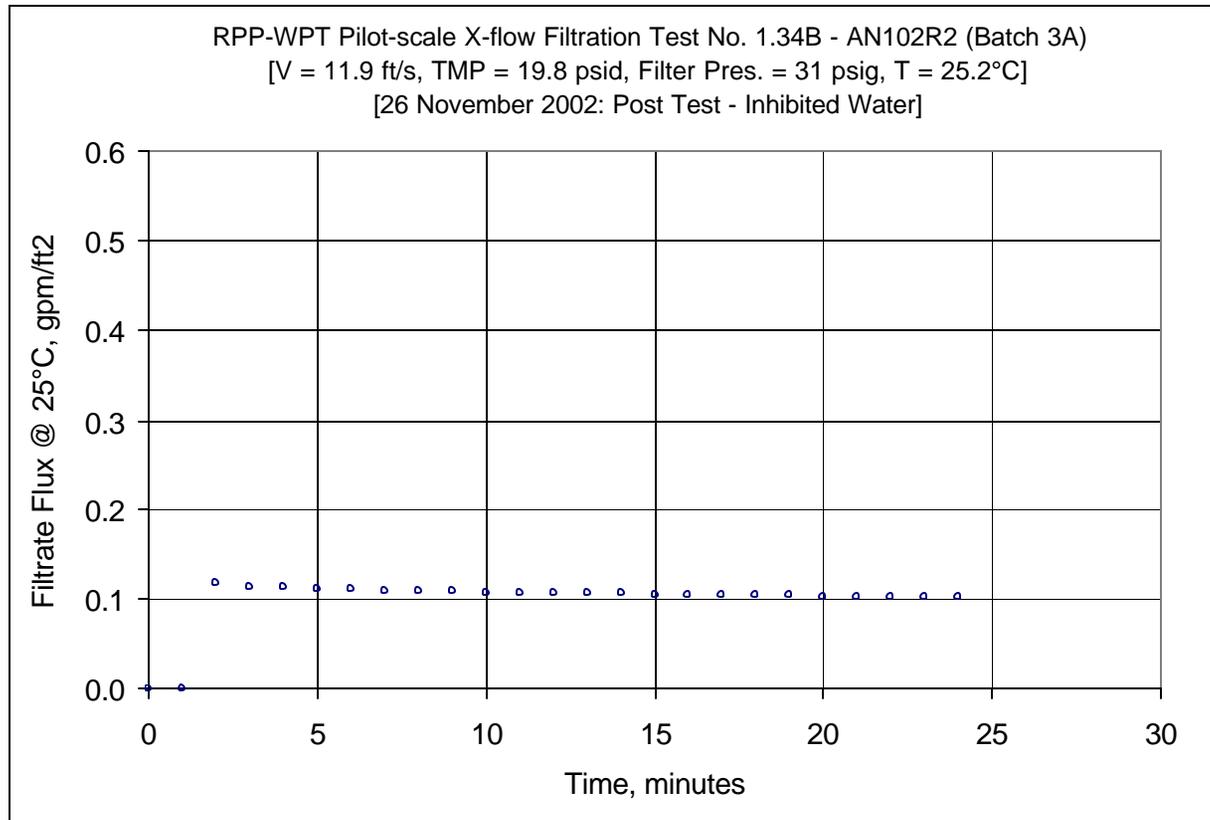


Figure A67: AN-102R2, Batch 3A Slurry Test 1.34B – Inhibited Deionized & Filtered Water Test after Standard Slurry



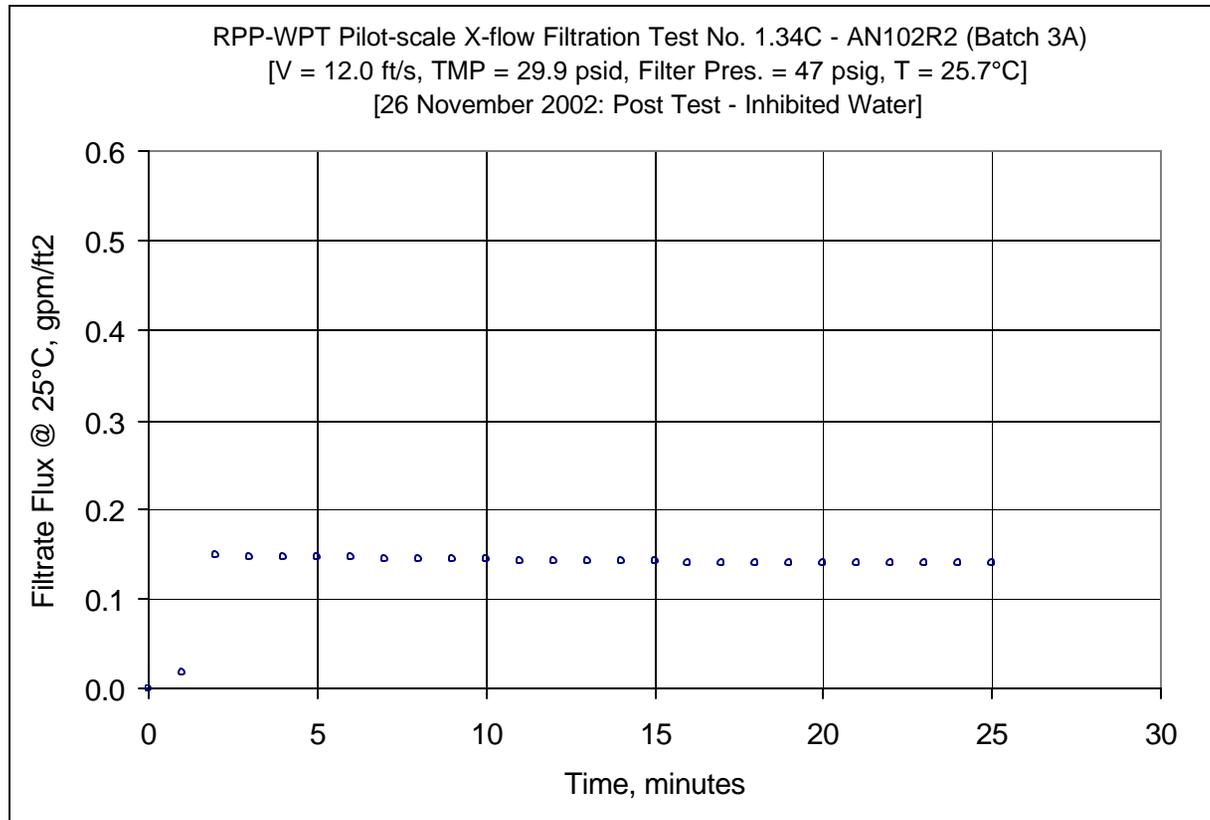


Figure A69: AN-102R2, Batch 3A Slurry Test 1.34C – Inhibited Deionized & Filtered Water Test after Standard Slurry



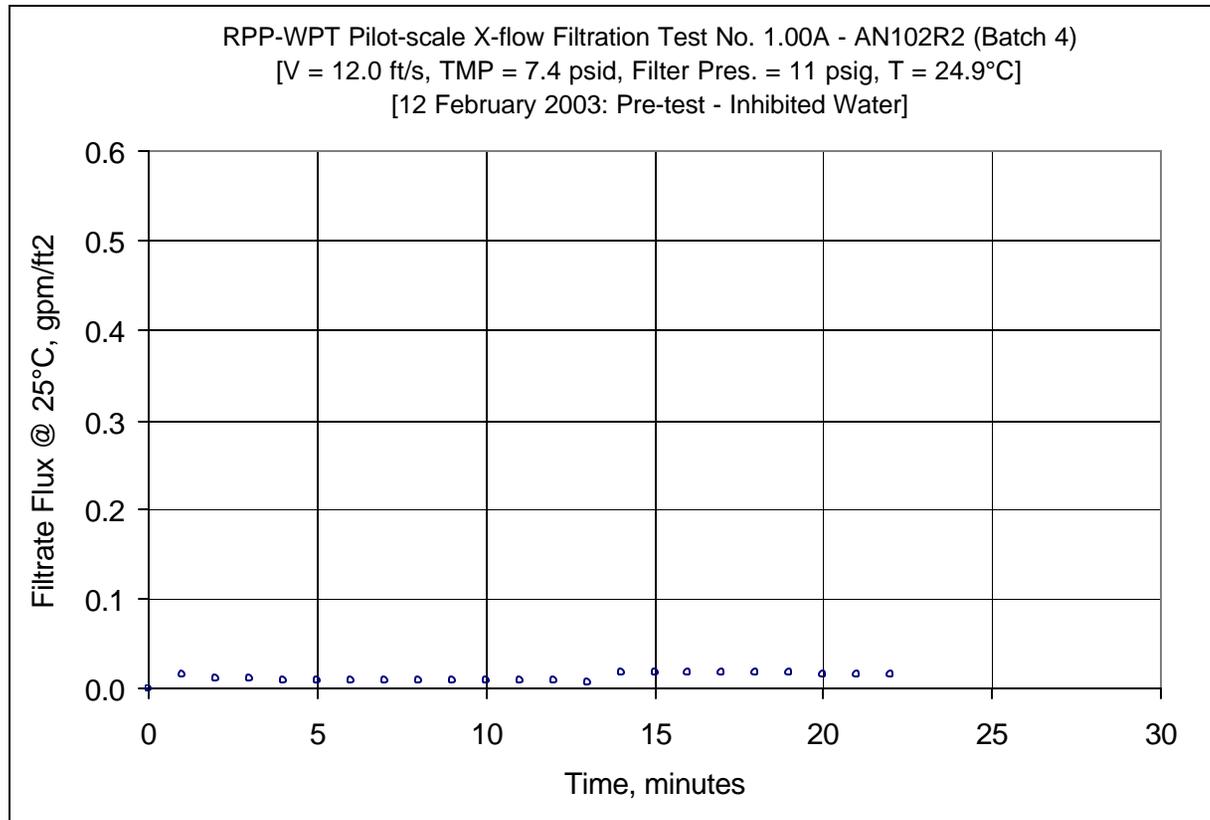


Figure A71: AN-102R2, Batch 4 Slurry Test 1.00A – Inhibited Deionized & Filtered Water (Compare to 1.34A on 11/26/02)



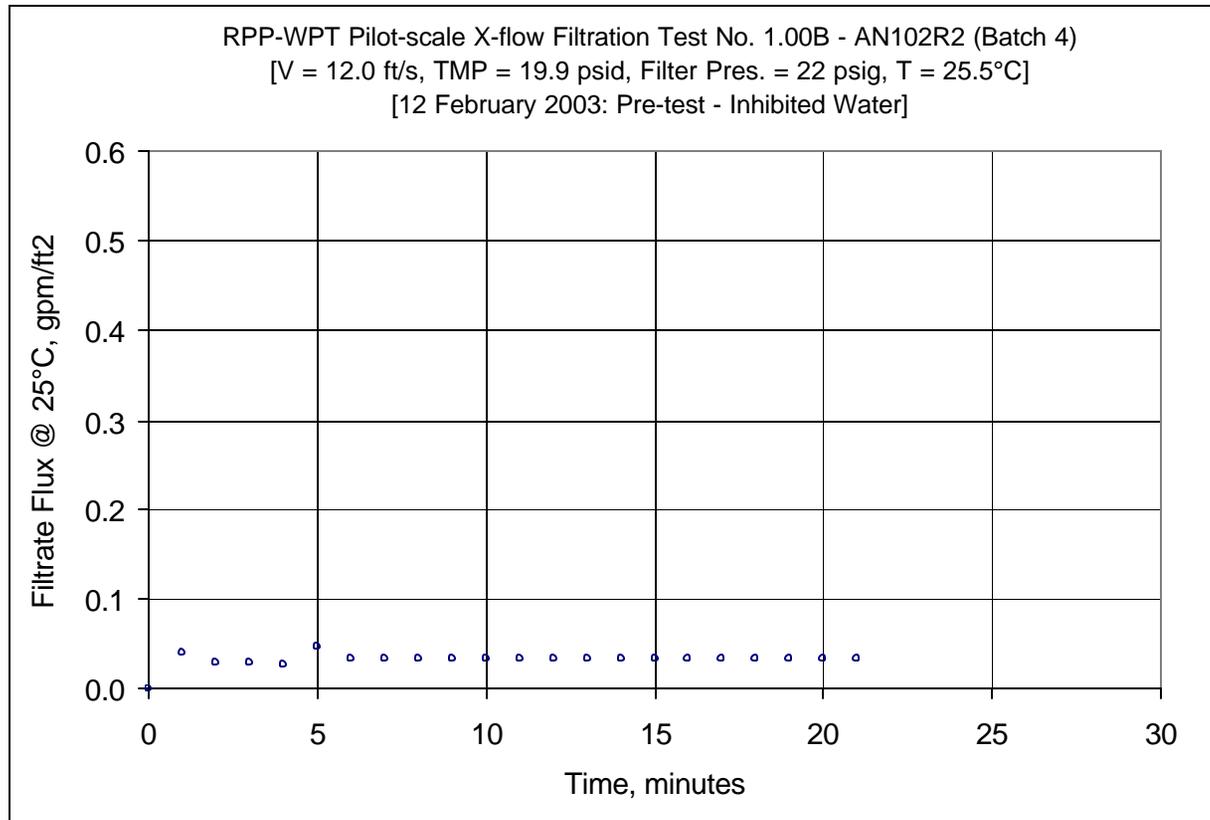


Figure A73: AN-102R2, Batch 4 Slurry Test 1.00B – Inhibited Deionized & Filtered Water (Compare to 1.34B on 11/26/02)



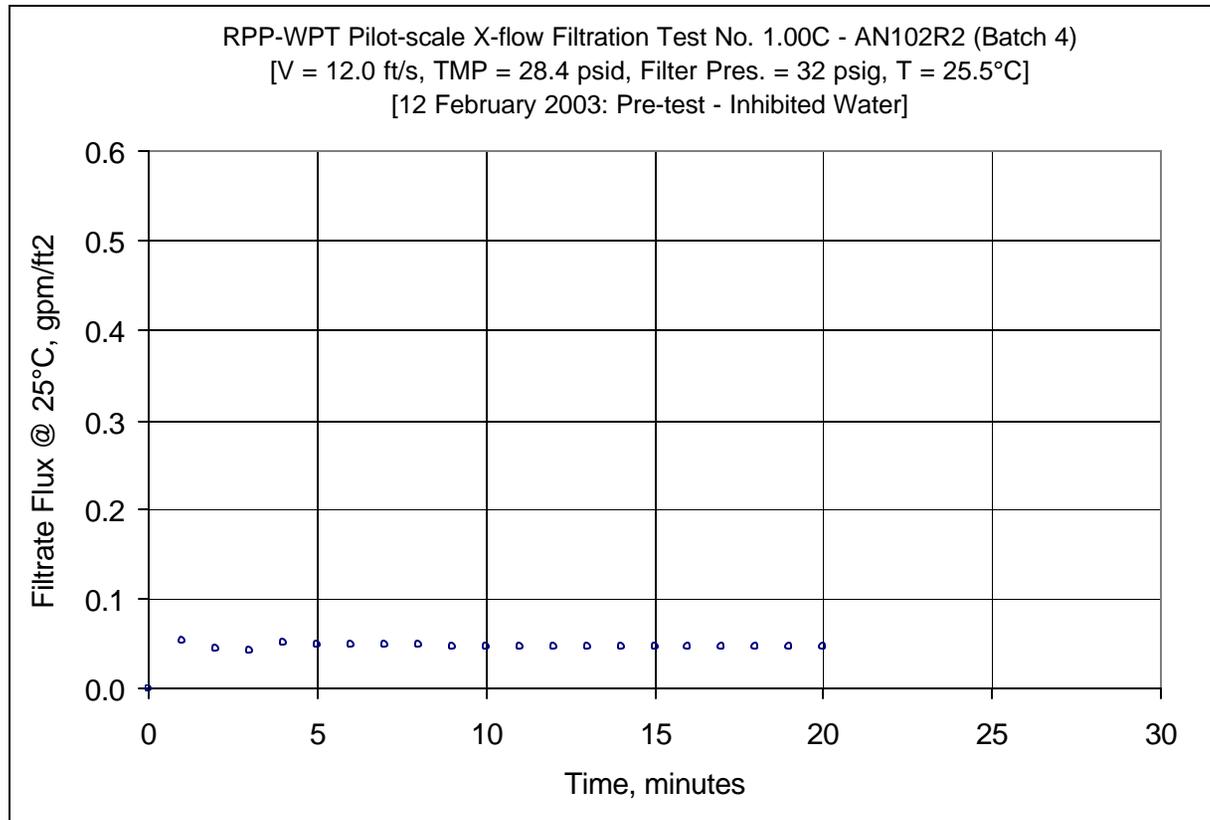


Figure A75: AN-102R2, Batch 4 Slurry Test 1.00C – Inhibited Deionized & Filtered Water (Compare to 1.34C on 11/26/02)



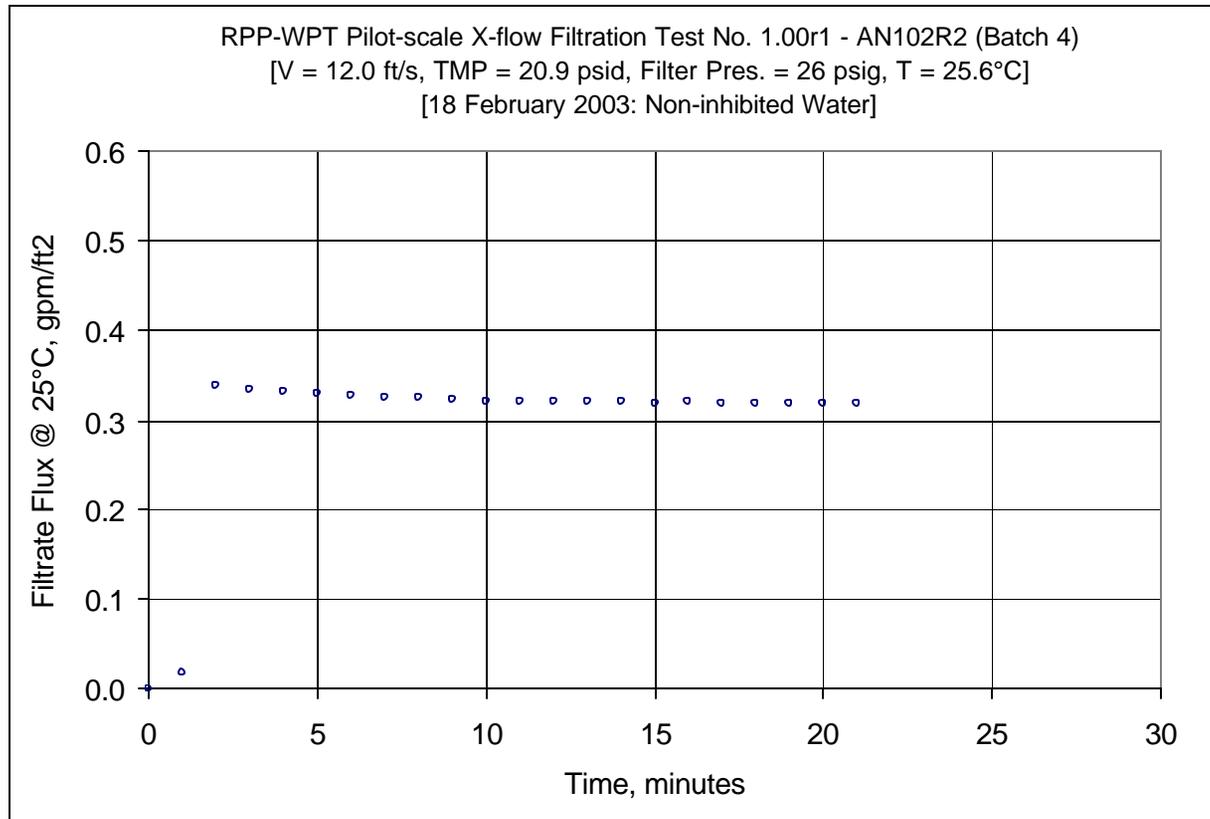


Figure A77: AN-102R2, Batch 4 Slurry Test 1.00r1 – Non-Inhibited Deionized & Filtered Water



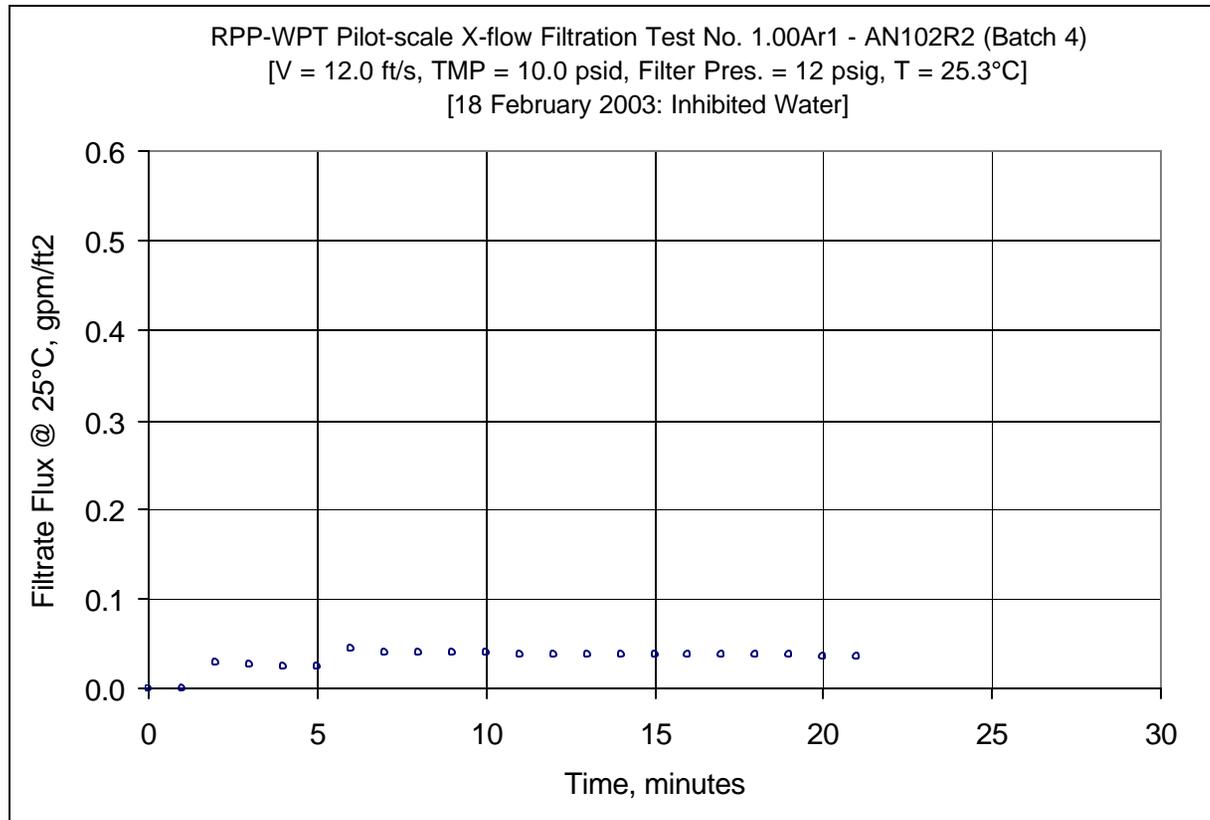


Figure A79: AN-102R2, Batch 4 Slurry Test 1.00Ar1 – Inhibited Deionized & Filtered Water (compare to Test 1.00A done on 2/12/03)



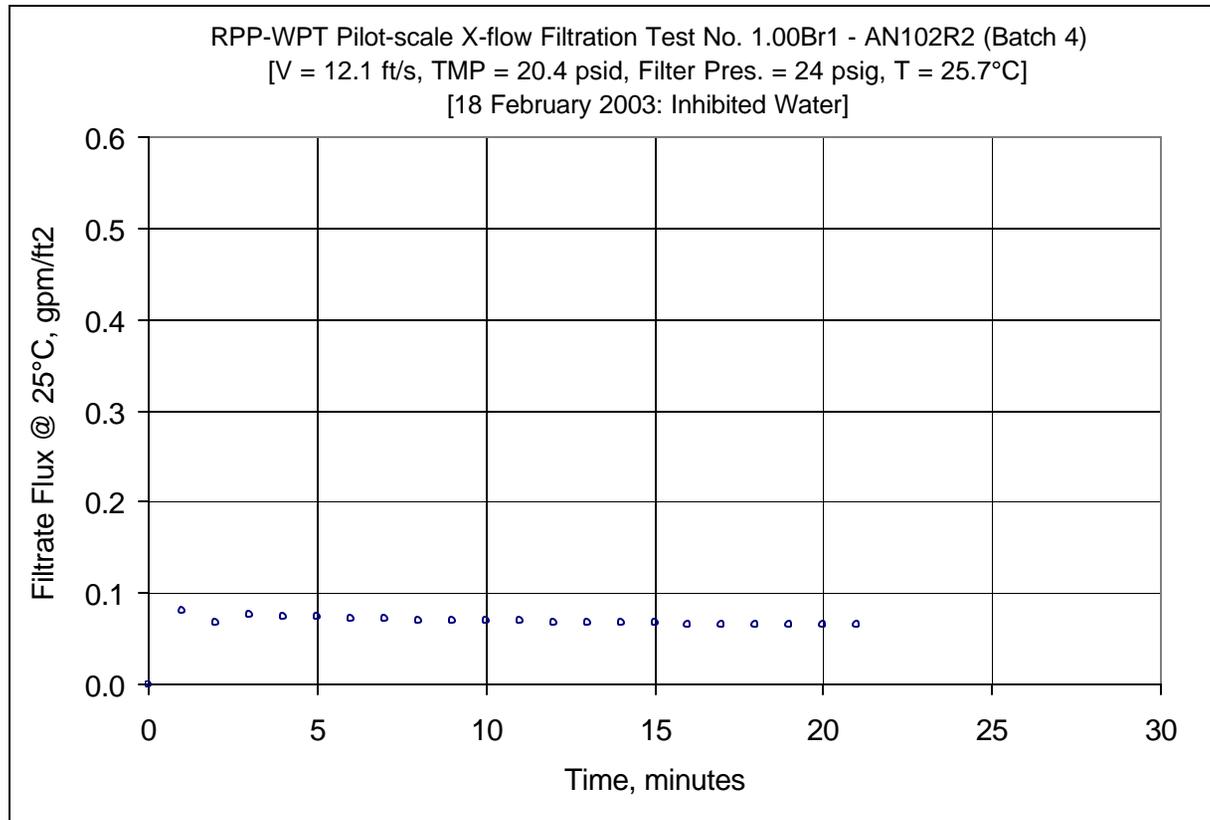


Figure A81: AN-102R2, Batch 4 Slurry Test 1.00Br1 – Inhibited Deionized & Filtered Water (compare to Test 1.00B done on 2/12/03)



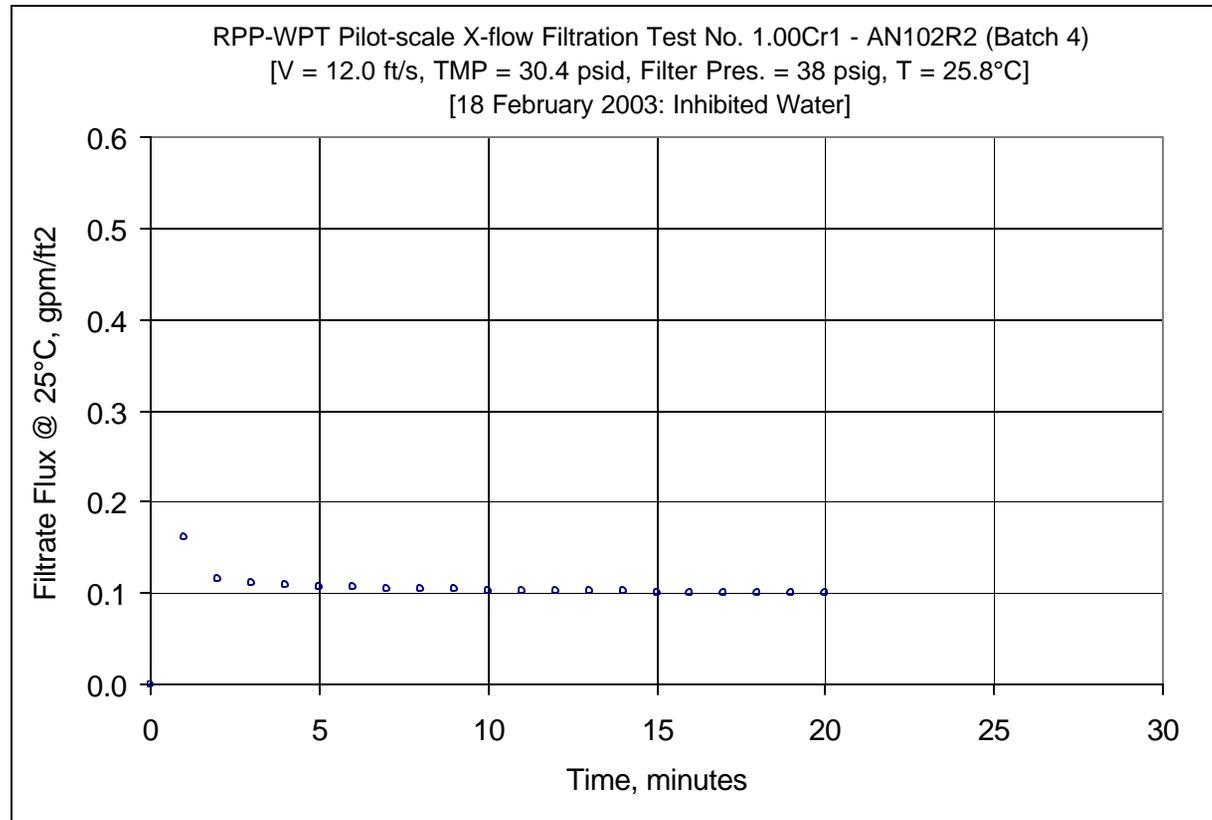


Figure A83: AN-102R2, Batch 4 Slurry Test 1.00Cr1 – Inhibited Deionized & Filtered Water (compare to Test 1.00C done on 2/12/03)



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## Appendix B: Baseline Slurry

As required by the RPP-WTP Test Specification each time the cross-flow filter experienced a slurry run the filter was to be tested with a standard slurry, called here the Baseline Slurry, of 5 wt% of SrCo<sub>3</sub> in distilled and filtered (to 0.1 micron absolute) water. Those tests were noted in the test matrix as runs 1.01 before a slurry test and 1.33 after a slurry. Initial tests with the slurry (during the preconditioning test with AN-107 and slurry AN-102R2 batch 3C) determined that only with considerable number of water rinses and acid cleaning could the baseline slurry be removed from the filter, costing time and money, therefore starting the AN-102R2 batch 3B test the RPP-WTP customer allowed baselining the filter only after each slurry test (run 1.33). As such, the baseline slurry run 1.33 after any slurry test could be used as the initial baseline run (1.01) for the next sequential slurry test. This report deals with the testing of five separate batches of slurry (peconditioning with AN-107, AN-102R2:3C, AN-102R2:3B, AN-102R2:3A, and AN-102R2:4) therefore the baseline slurry runs were:

2A, 2B	Before Preconditioning the filter with AN-107; pre-test rig modification
2A, 2B, 2C, 2D	After Preconditioning the filter with AN-107, post-test rig modification
7A, 7B, 7C	After Preconditioning the filter with AN-107
1.01A, 1.01B, 1.01C	Before AN-102R2, batch 3C
1.33A, 1.33B, 1.33C	After AN-102R2, batch 3C
1.33A, 1.33B, 1.33C	After AN-102R2, batch 3B
1.33A, 1.33B, 1.33C	After AN-102R2, batch 3A
1.33A, 1.33B, 1.33C	After AN-102R2, batch 4A

The letter a, b, c indicate different constant transmembrane pressure (TMP), generally, but not always: A=10 psid, B=20 psid, C=30 ; psid. Test runs that do not hold to this are 2A, 2B, (pre-test rig modification) because the high filtration pressure drop did not allow TMPs above 7 psid; 2D was done at above 40 psid to determine the limit the modified test rig could attain.

For each baseline slurry test this appendix contains a graph of the filtrate flux with time and tables of the data taken and calculated. To better understand the presented information important aspects of the graphs and tables are explained below:

Graphs – Each graph contains time averages of some of the imporant parameters taken during the run at the top of the figures, i.e. Slurry velocity in the filter tube, V; transmembrane pressure, TMP; slurry pressure at the entrance of the filter tube, Filter Pres; and the slurry temperature, T.

Tables – Each table is divided into raw data (the first 17 columns) and calculations (the last 10 columns) which are based on the raw data. The raw data section is divided into three parts:

### Individual Entries – Raw Data

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid which has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column and corrected for a 40.9-inch water column that exists from the transducer to the point where P1 is measured.)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.  
Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.707 ft<sup>2</sup>)<sup>†</sup>  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T)-(1/298))]$  as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)  
Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing  
Permiability – Same as Permiability but in metric units, meter/day/bar

Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 x Std Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not included the points taken during the backpulse sequence of each test. This is explained below.

Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is were the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests (see Figs. B36, B38, and B40) do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

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<sup>†</sup> For the baseline slurry tests during preconditioning it will be noticed that 6.87 ft<sup>2</sup> was used. This was based on a tube inside diameter of 0.5 inch, which was based on the manufacturer’s specification. After the tubes were measured the i.d. was changed to 0.488 inch and the area to 6.707 ft<sup>2</sup>. This means that absolute axial velocity and filtrate flux are low by 2.5% for the preconditioning runs.

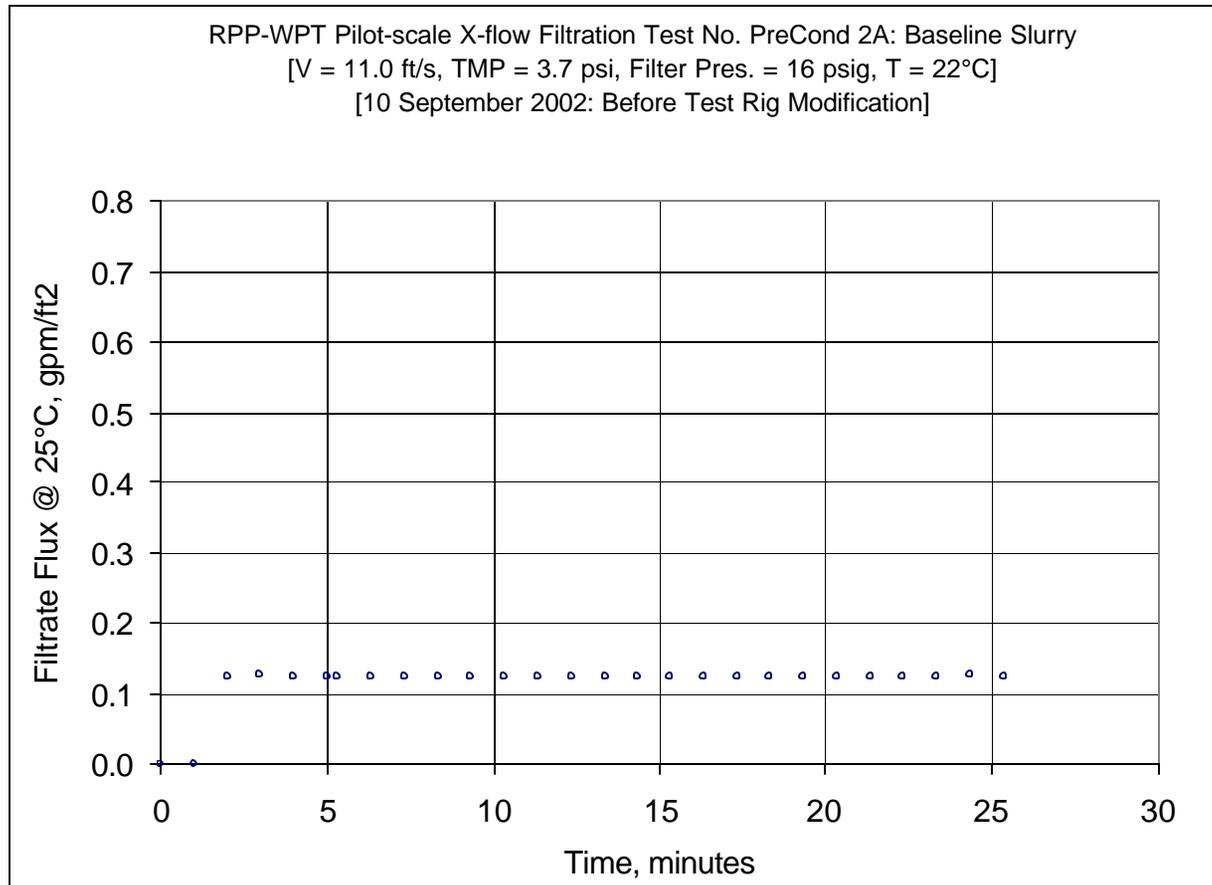


Figure B1: PreConditioning 2A – Baseline Slurry – Before Test Rig Modification



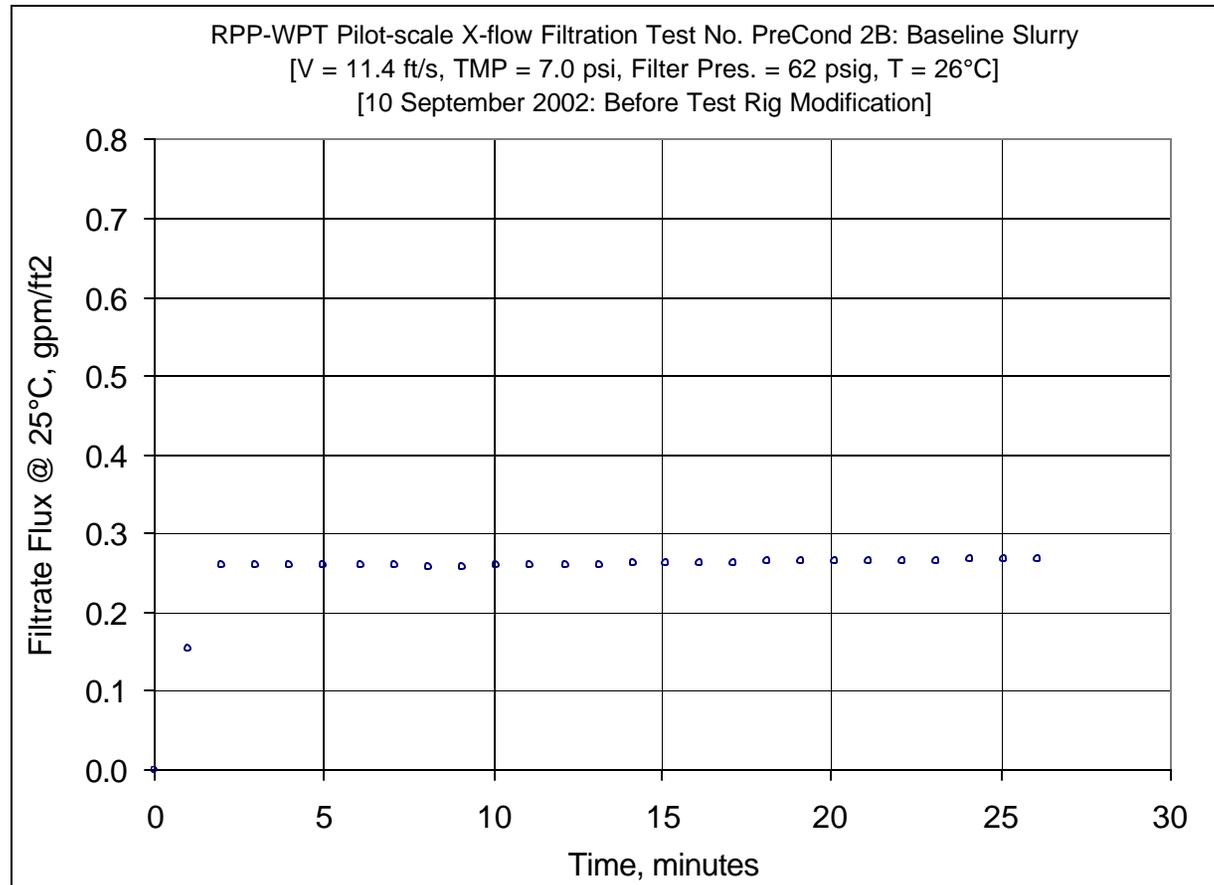


Figure B3: PreConditioning 2B – Baseline Slurry – Before Test Rig Modification



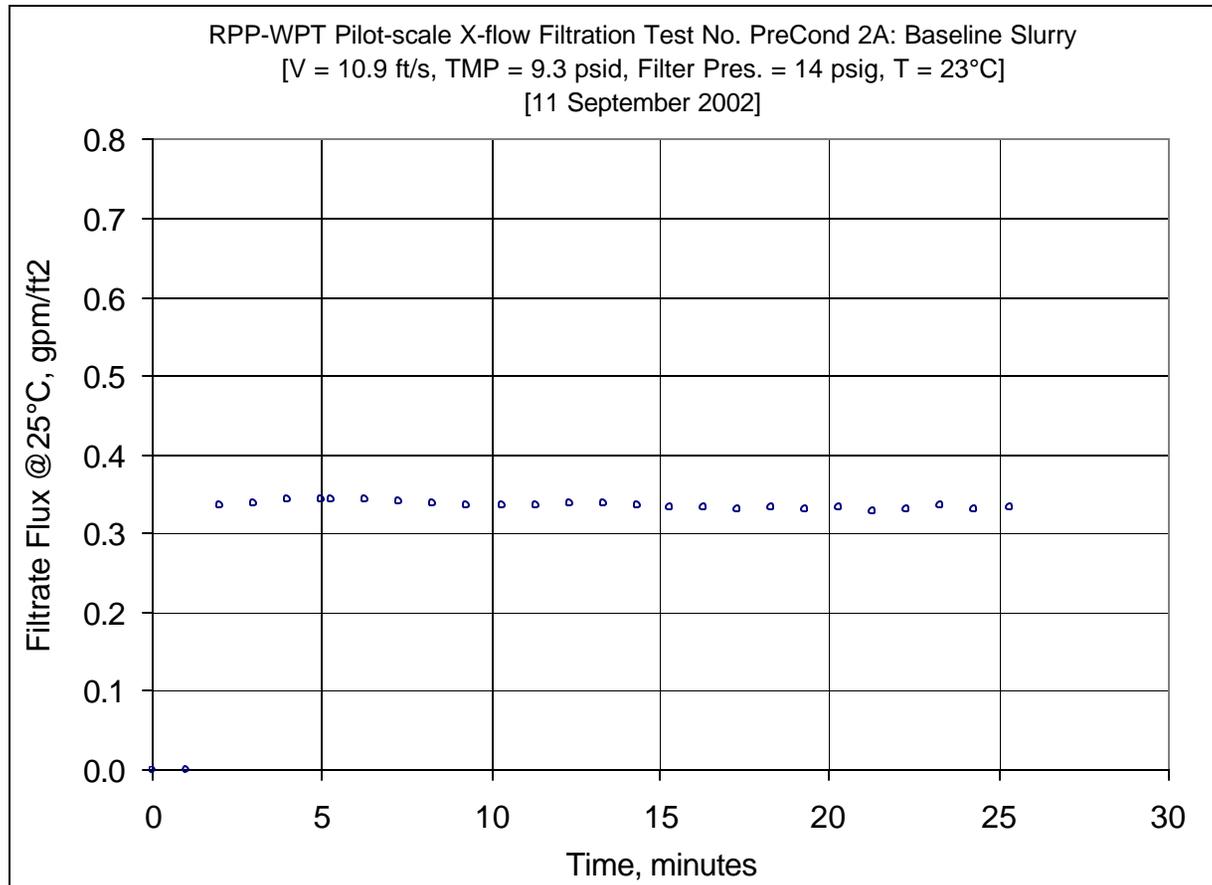


Figure B5: PreConditioning 2A – Baseline Slurry – After Test Rig Modification



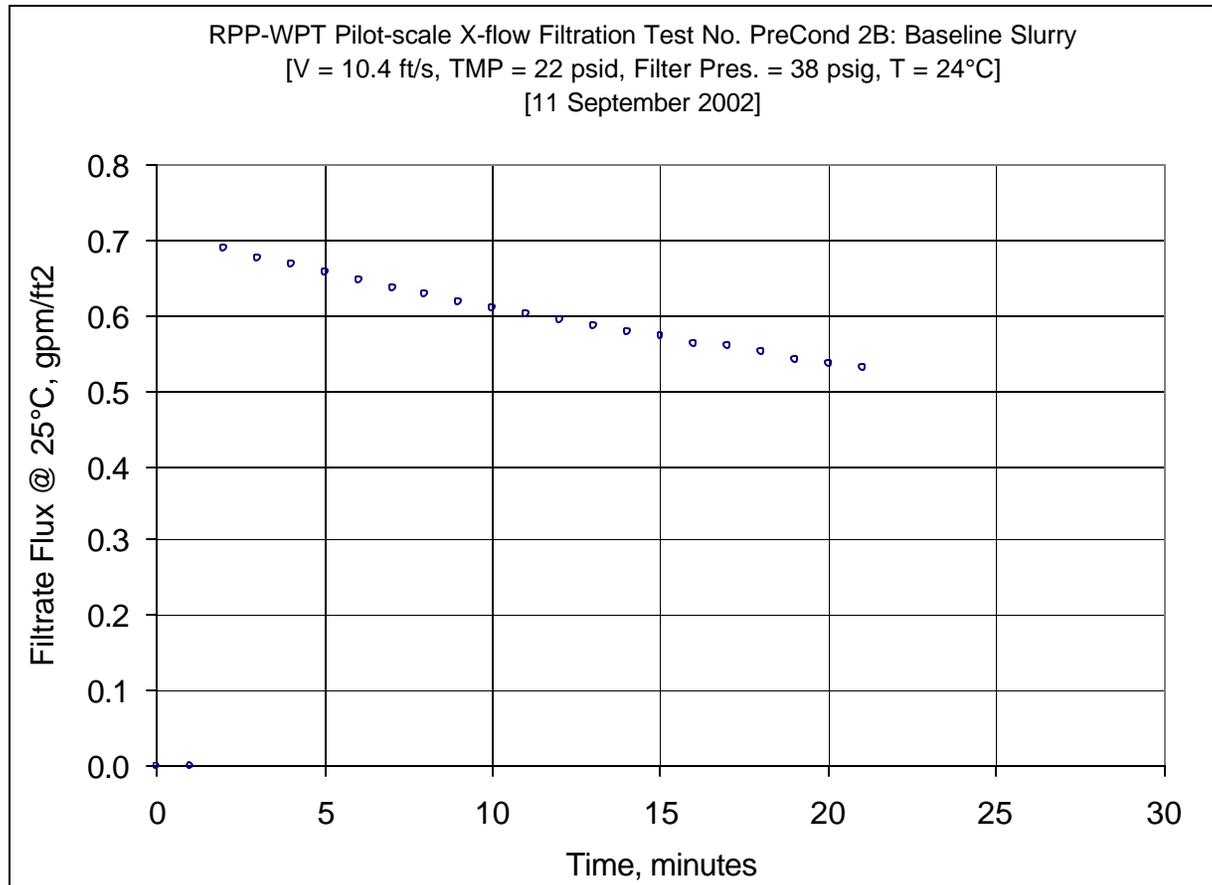


Figure B7: PreConditioning 2B – Baseline Slurry – After Test Rig Modification



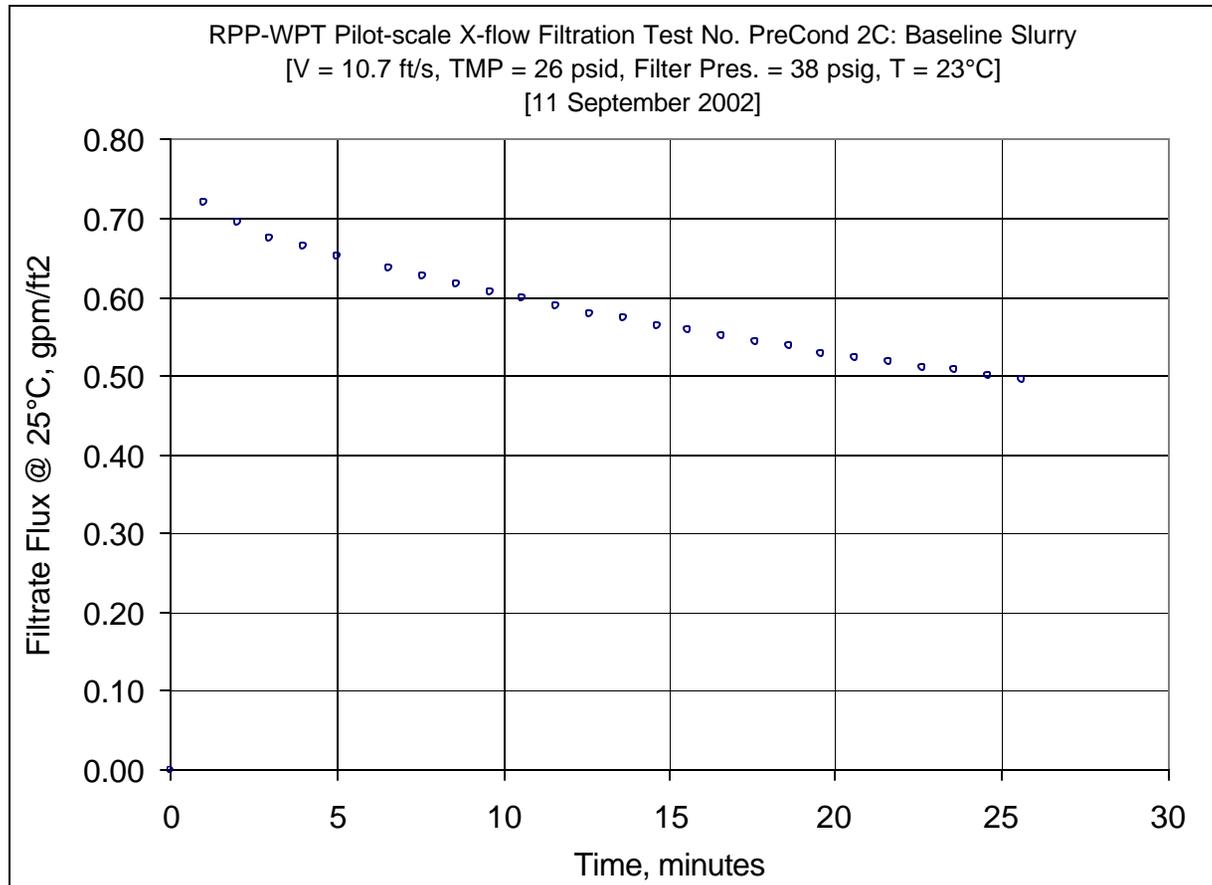


Figure B9: PreConditioning 2C – Baseline Slurry – After Test Rig Modification



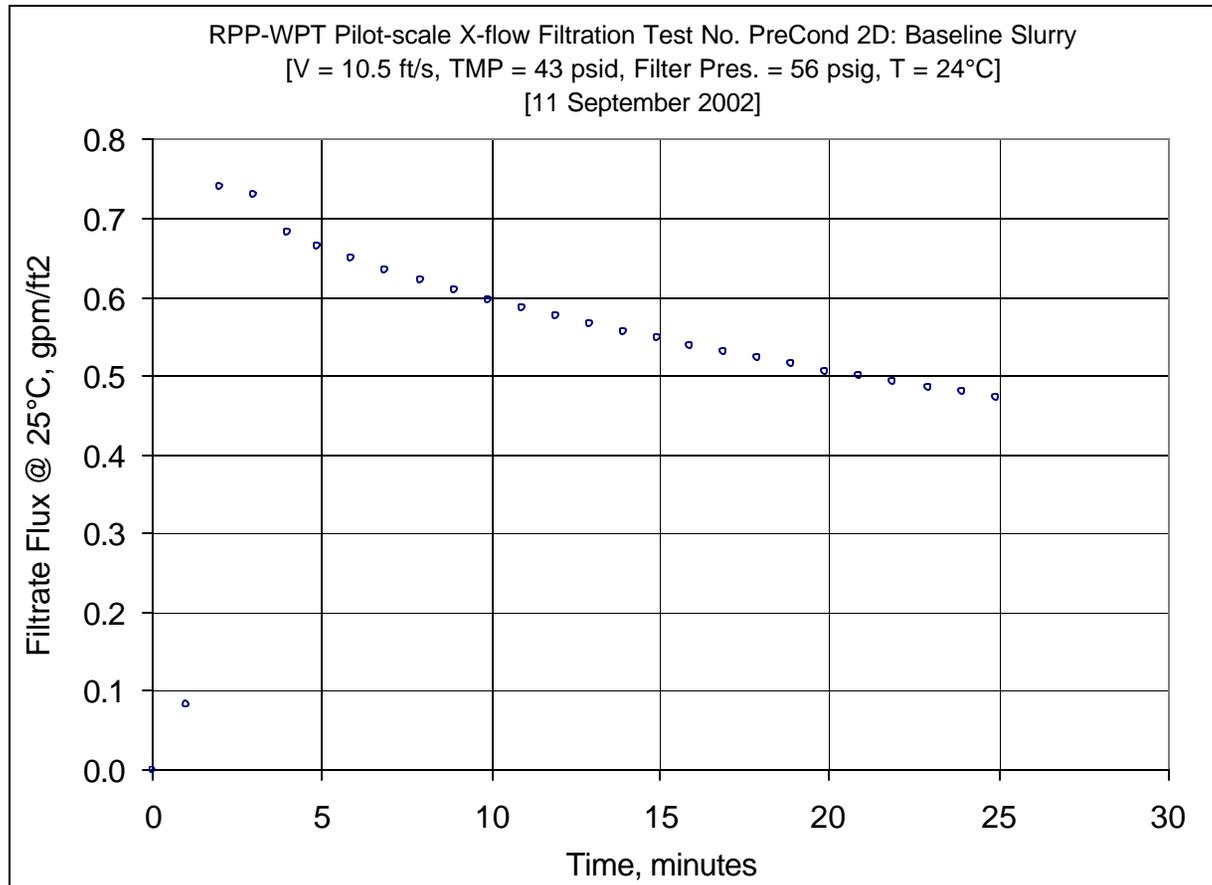


Figure B11: PreConditioning 2D – Baseline Slurry – After Test Rig Modification



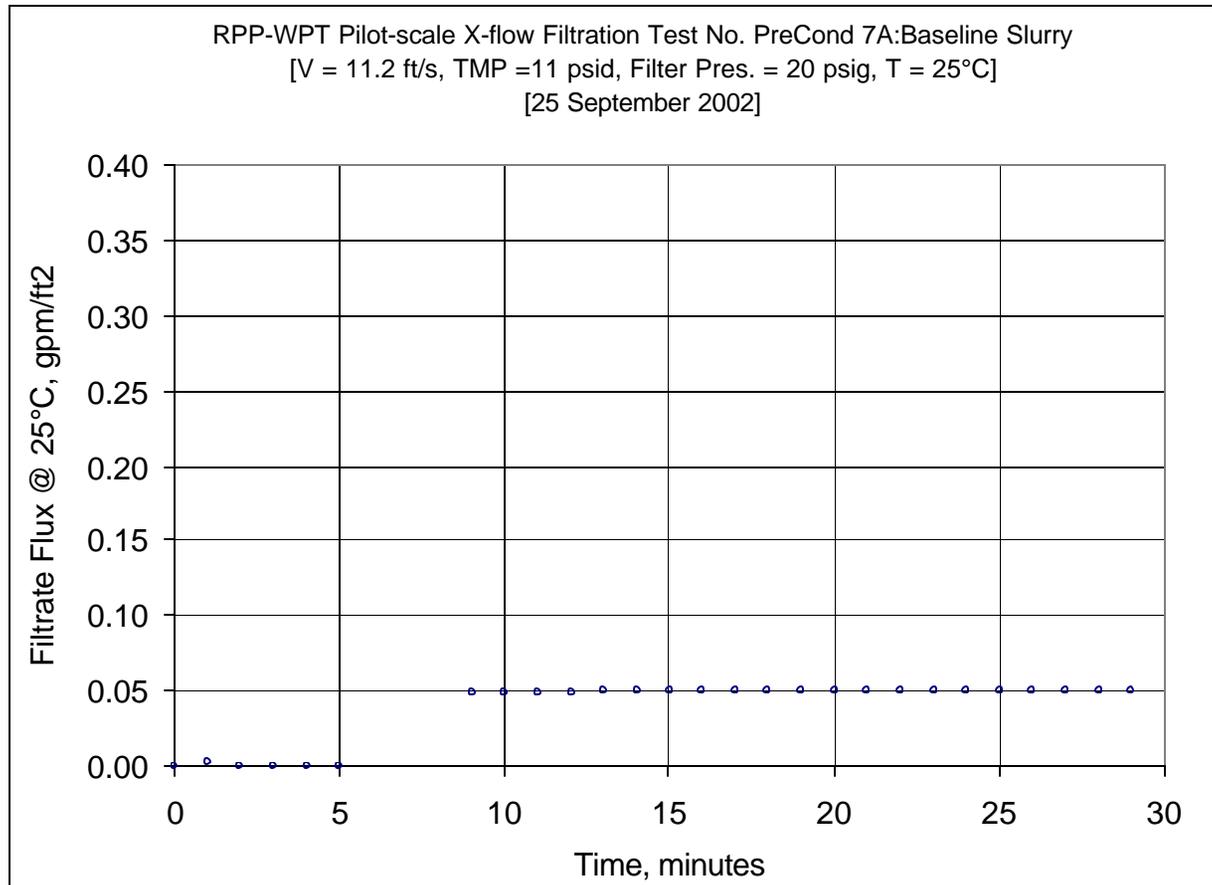


Figure B13: PreConditioning 7A – Baseline Slurry – After Preconditioning Filter with AN-107



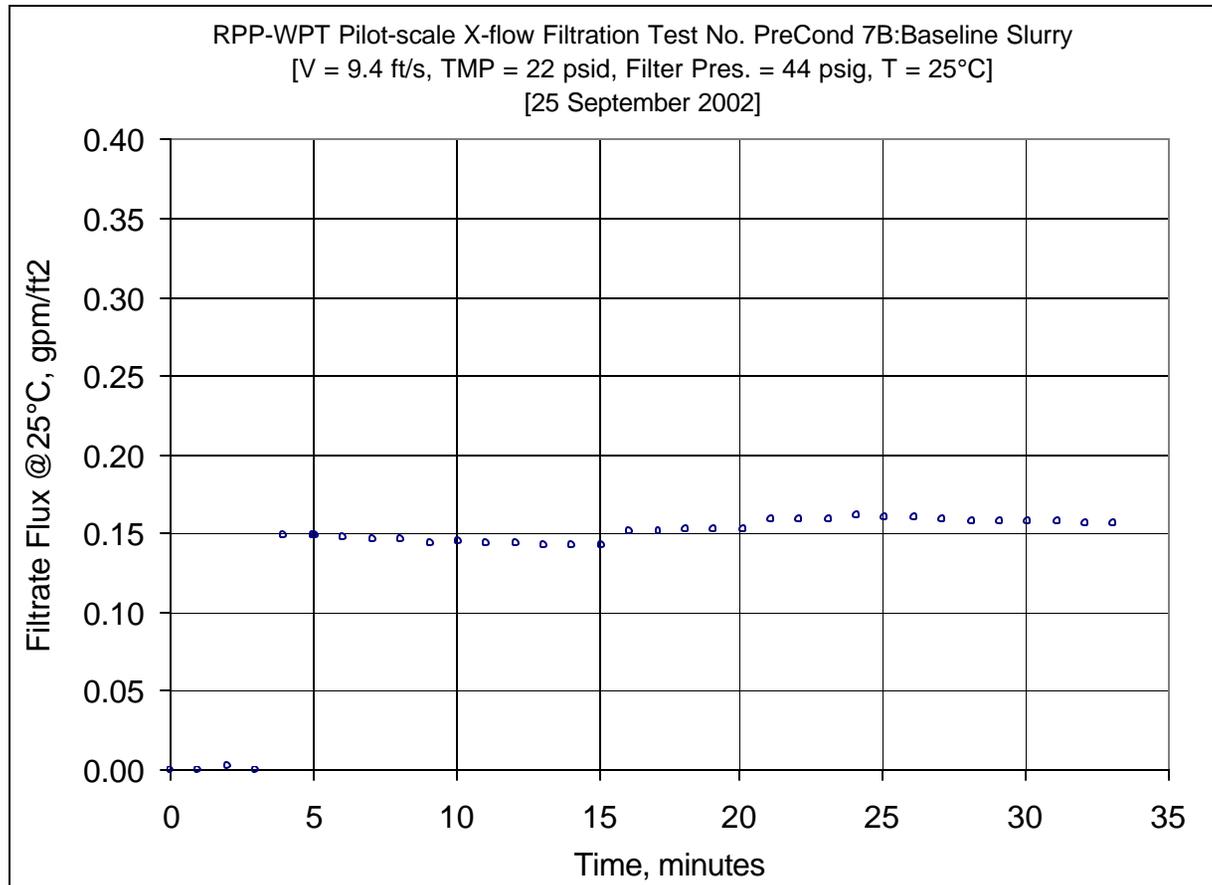


Figure B15: PreConditioning 7B – Baseline Slurry – After Preconditioning Filter with AN-107



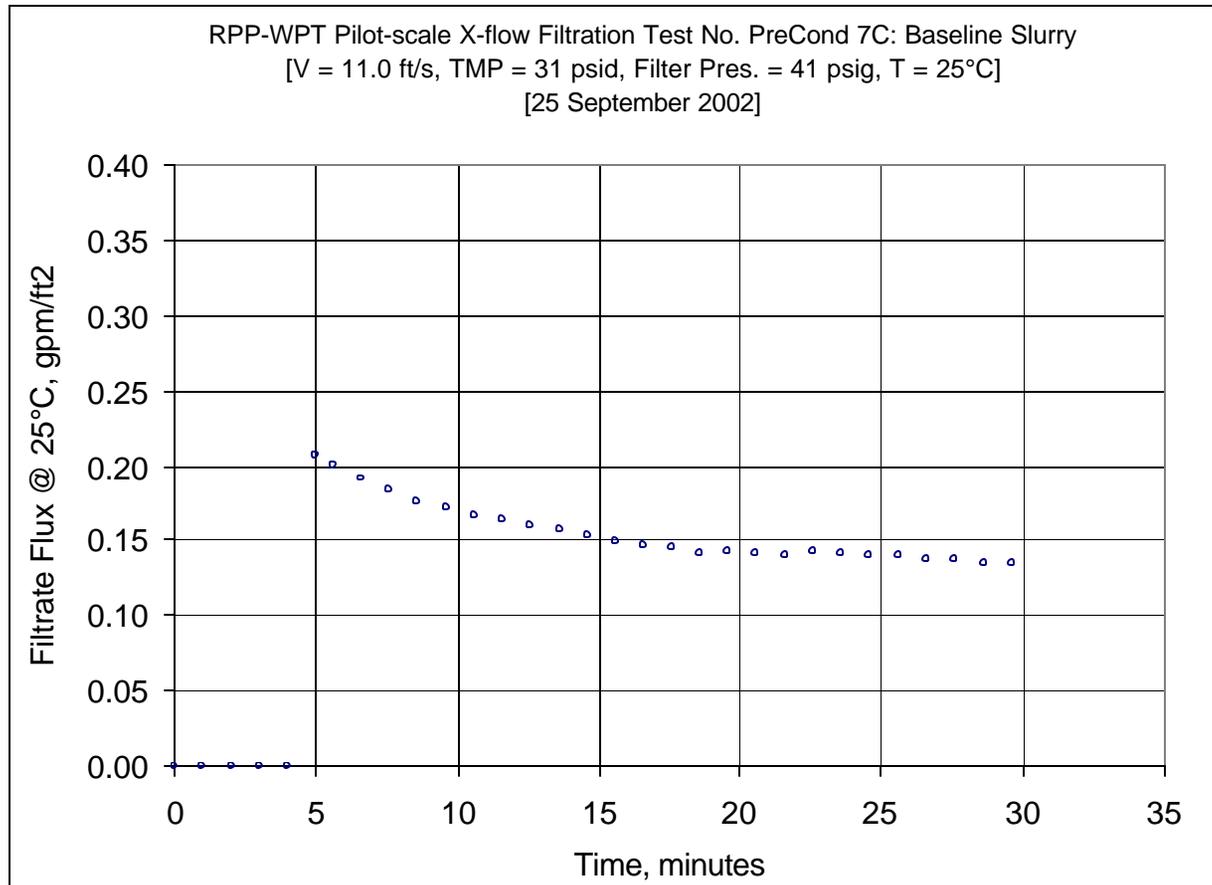


Figure B15: PreConditioning 7C – Baseline Slurry – After Preconditioning Filter with AN-107



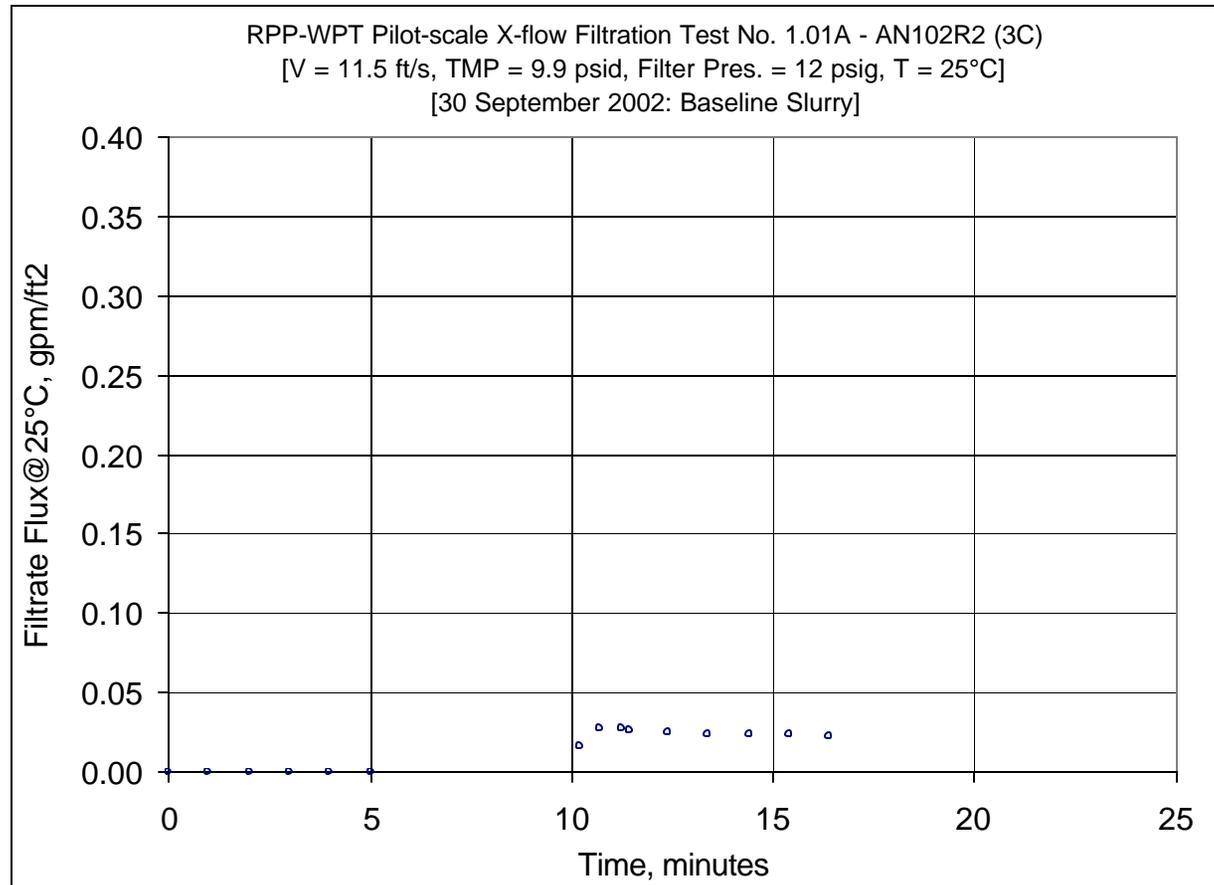


Figure B17: Run 1.01A – Baseline Slurry – Before Using Slurry AN-102R2 Batch 3C



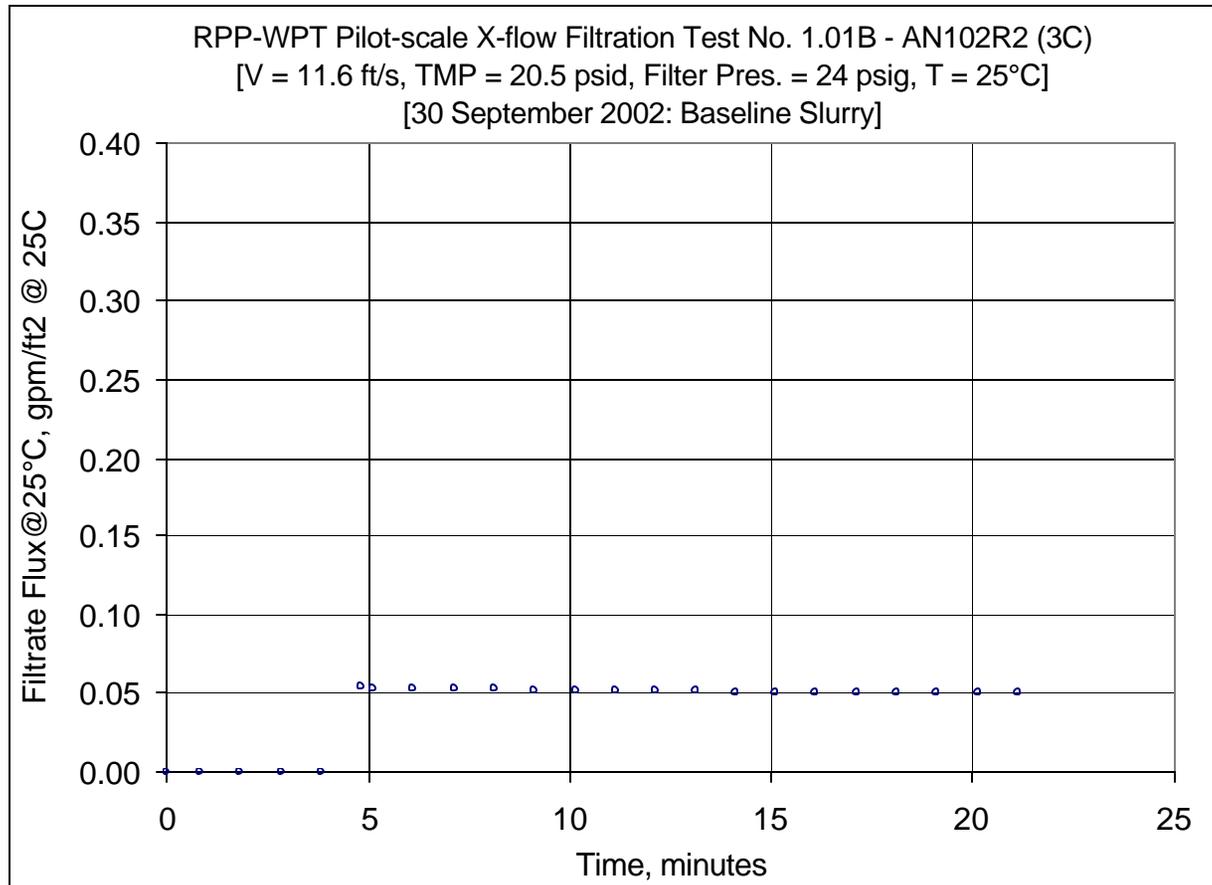


Figure B19: Run 1.01B – Baseline Slurry – Before Using Slurry AN-102R2 Batch 3C



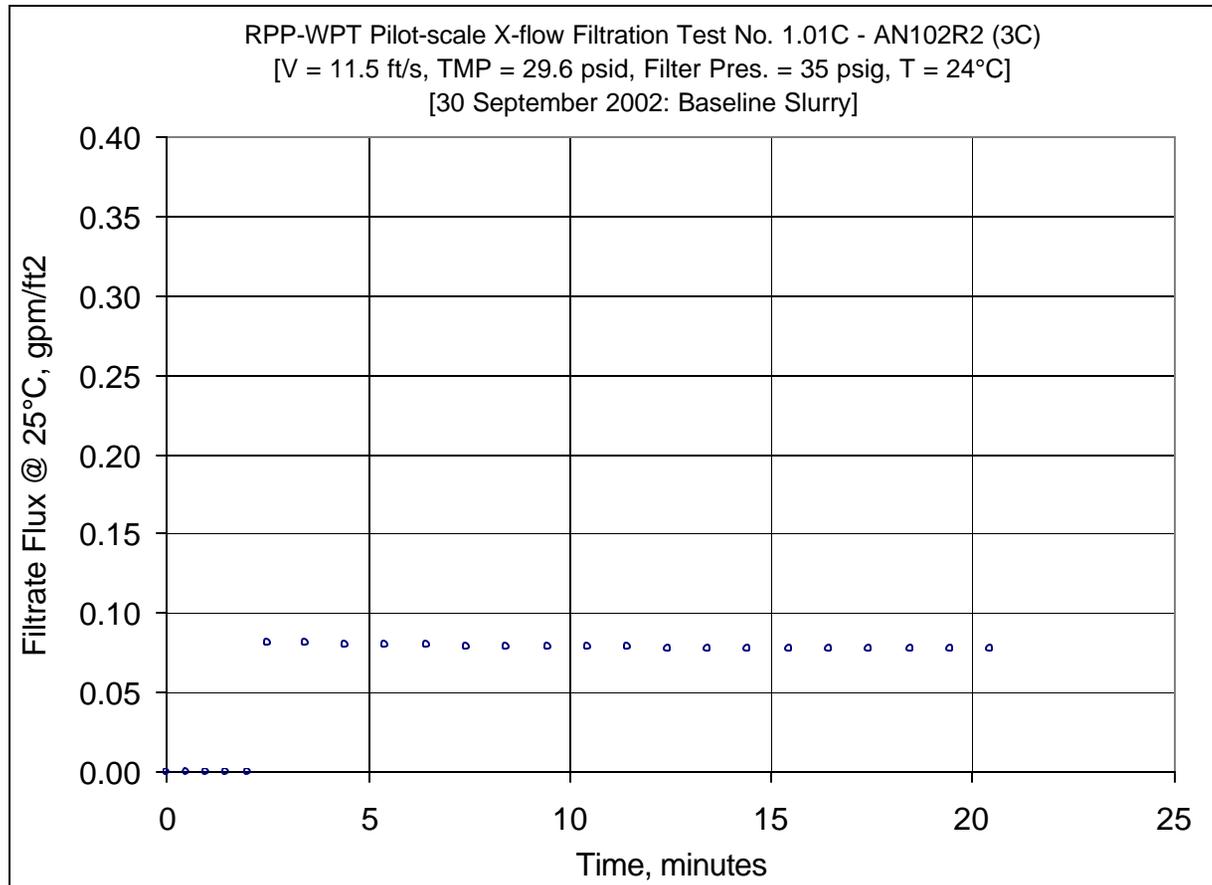


Figure B21: Run 1.01C – Baseline Slurry – Before Using Slurry AN-102R2 Batch 3C



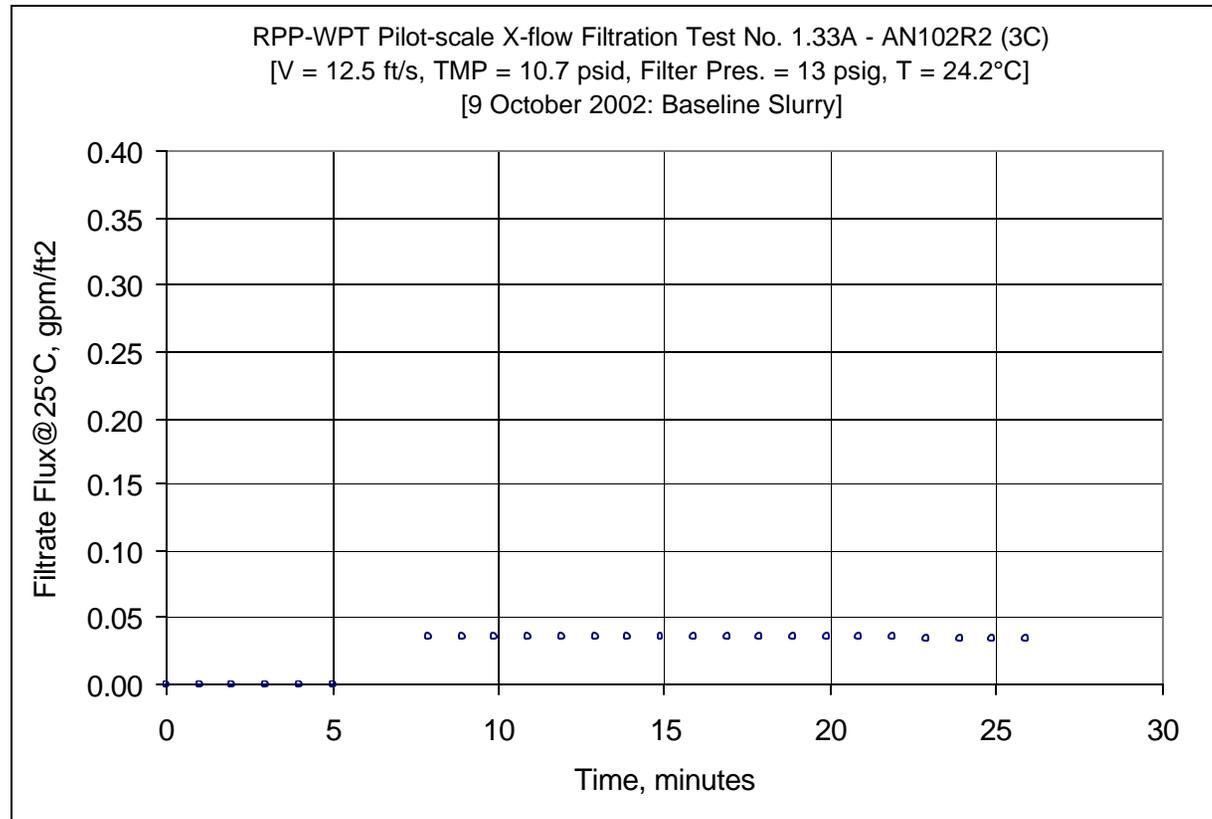


Figure B23: Run 1.33A – Baseline Slurry – After AN-102R2 Batch 3C and Before Batch 3B



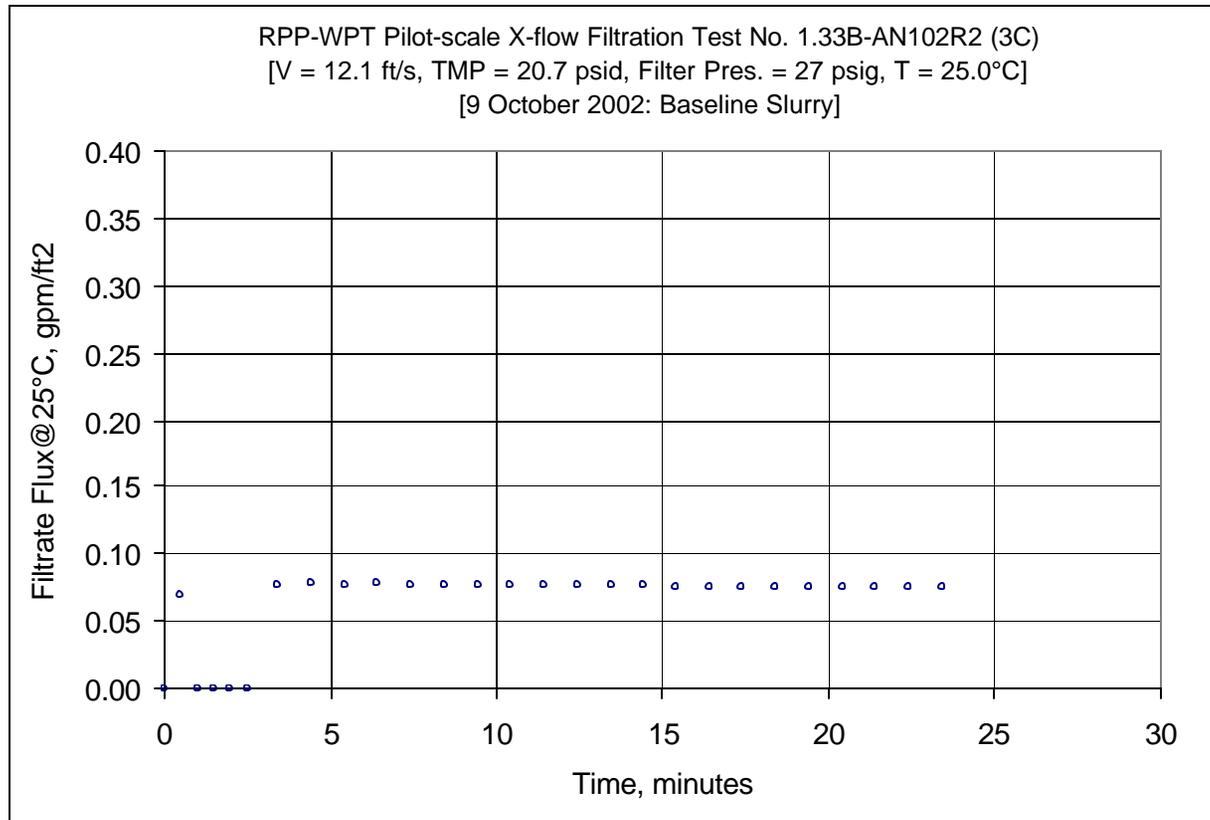


Figure B25: Run 1.33B – Baseline Slurry – After AN-102R2 Batch 3C and Before Batch 3B



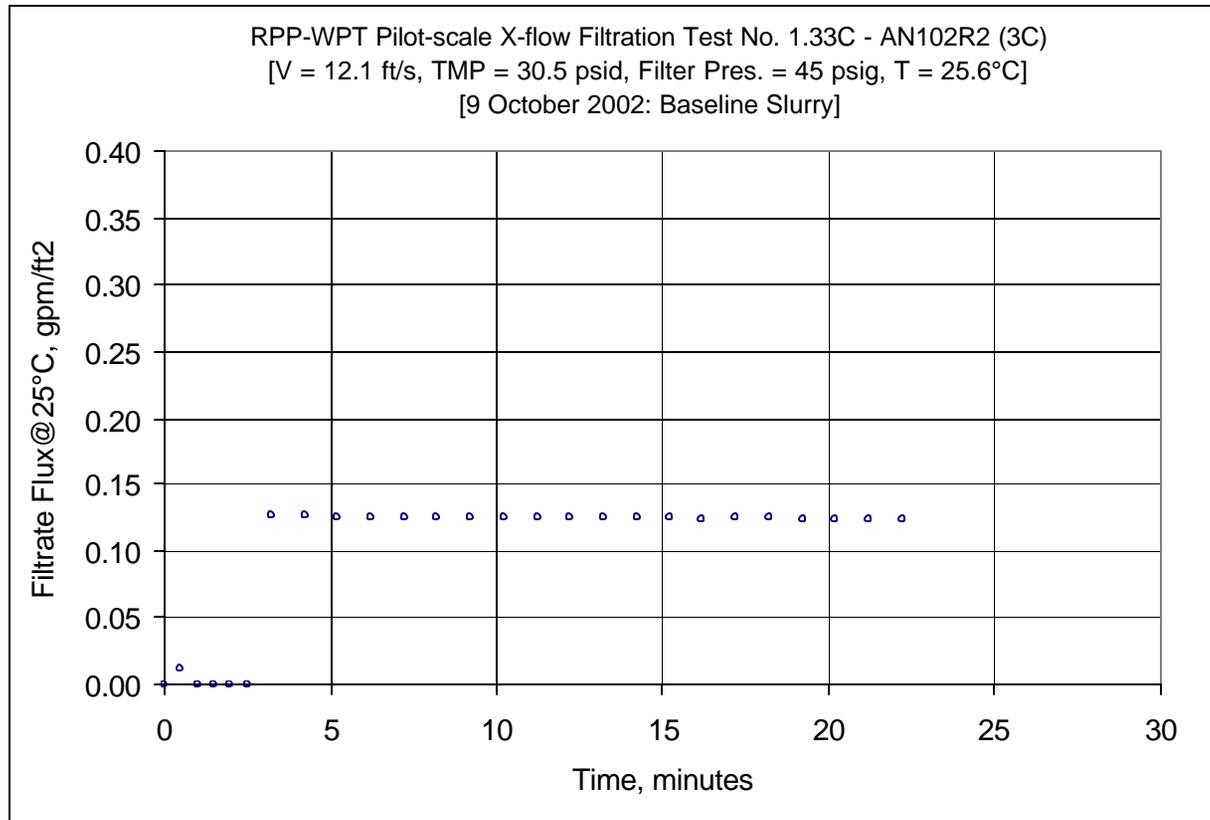


Figure B27: Run 1.33C – Baseline Slurry – After AN-102R2 Batch 3C and Before Batch 3B



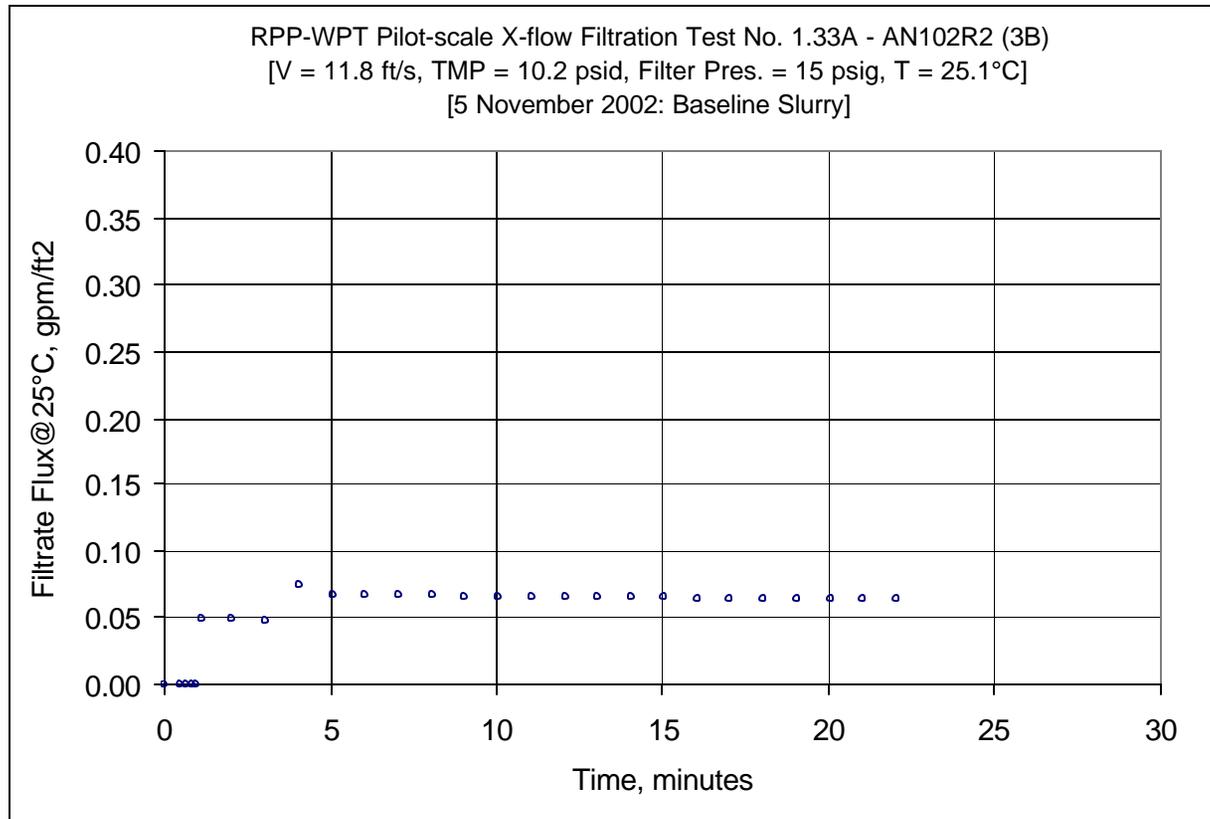


Figure B29: Run 1.33A – Baseline Slurry – After AN-102R2 Batch 3B and Before Batch 3A



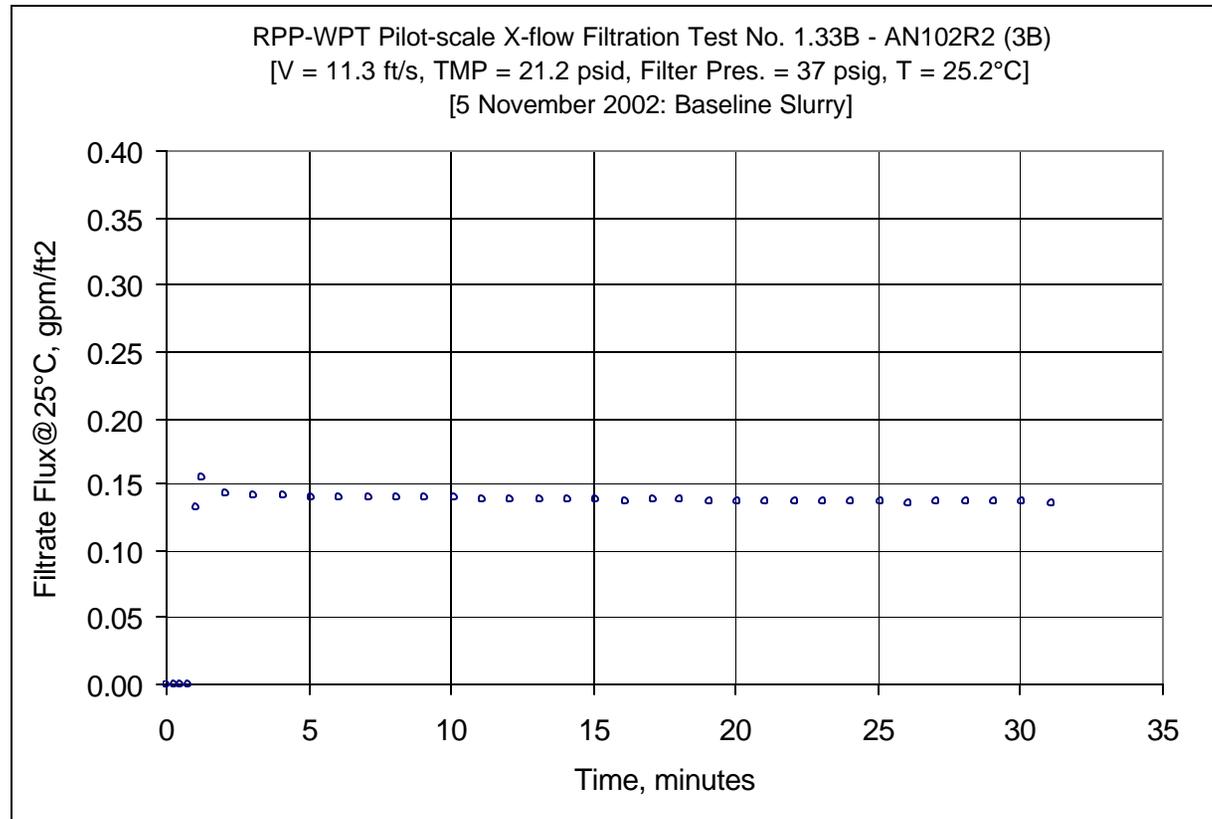


Figure B31: Run 1.33B – Baseline Slurry – After AN-102R2 Batch 3B and Before Batch 3A



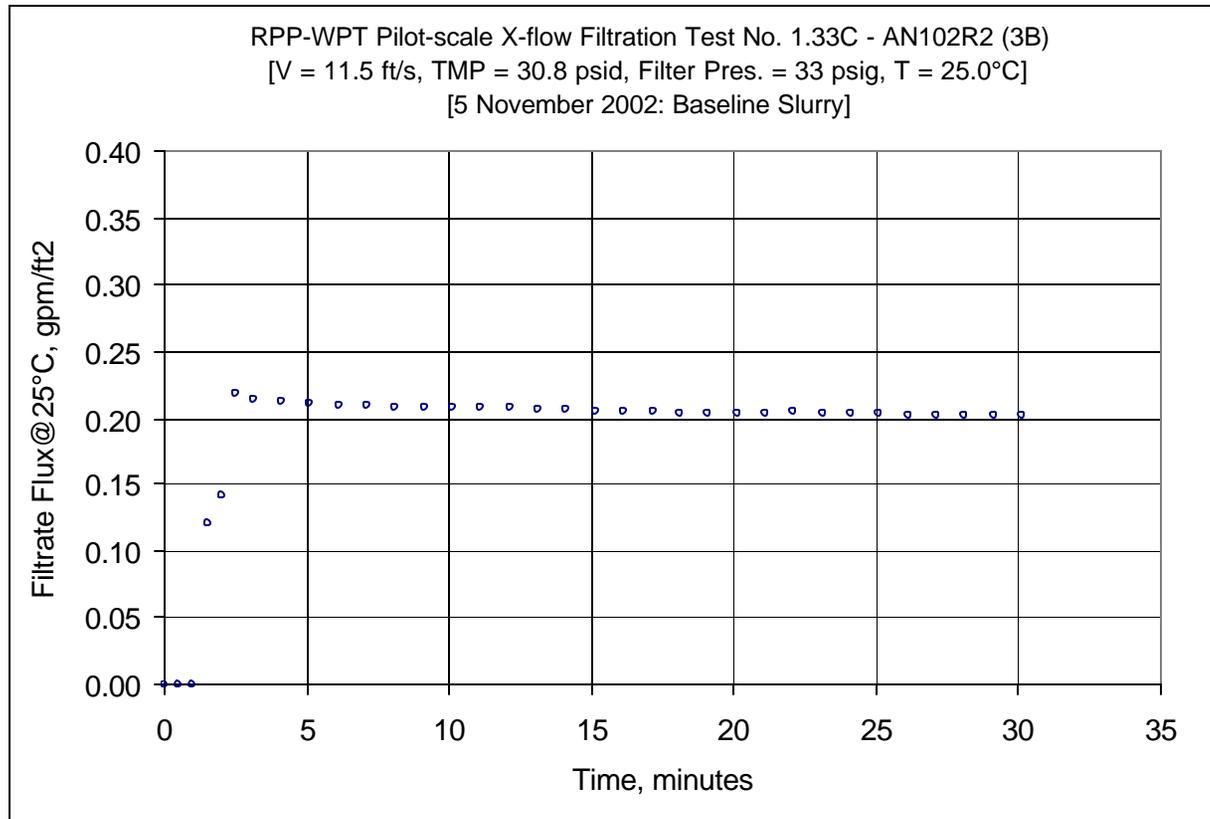


Figure B33: Run 1.33C – Baseline Slurry – After AN-102R2 Batch 3B and Before Batch 3A



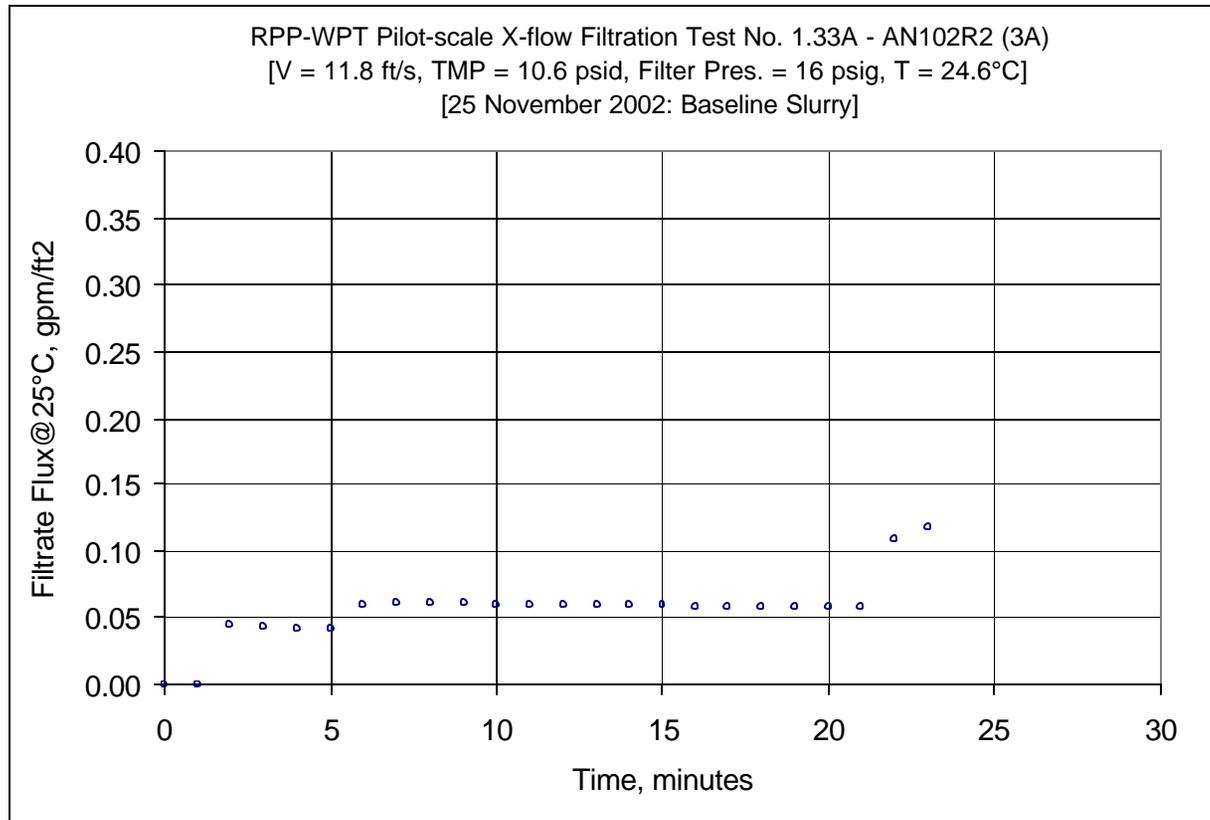


Figure B35: Run 1.33A – Baseline Slurry – After AN-102R2 Batch 3A and Before Batch 4A



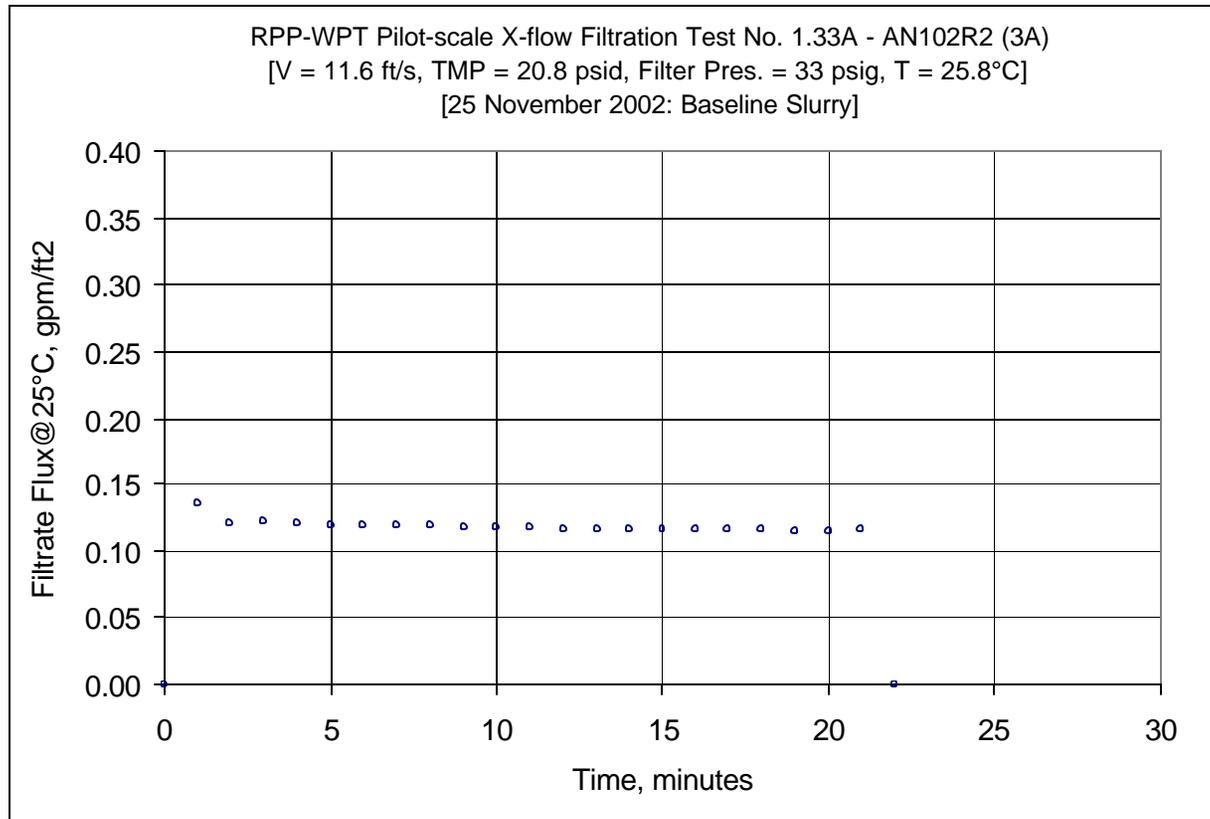


Figure B37: Run 1.33B – Baseline Slurry – After AN-102R2 Batch 3A and Before Batch 4A



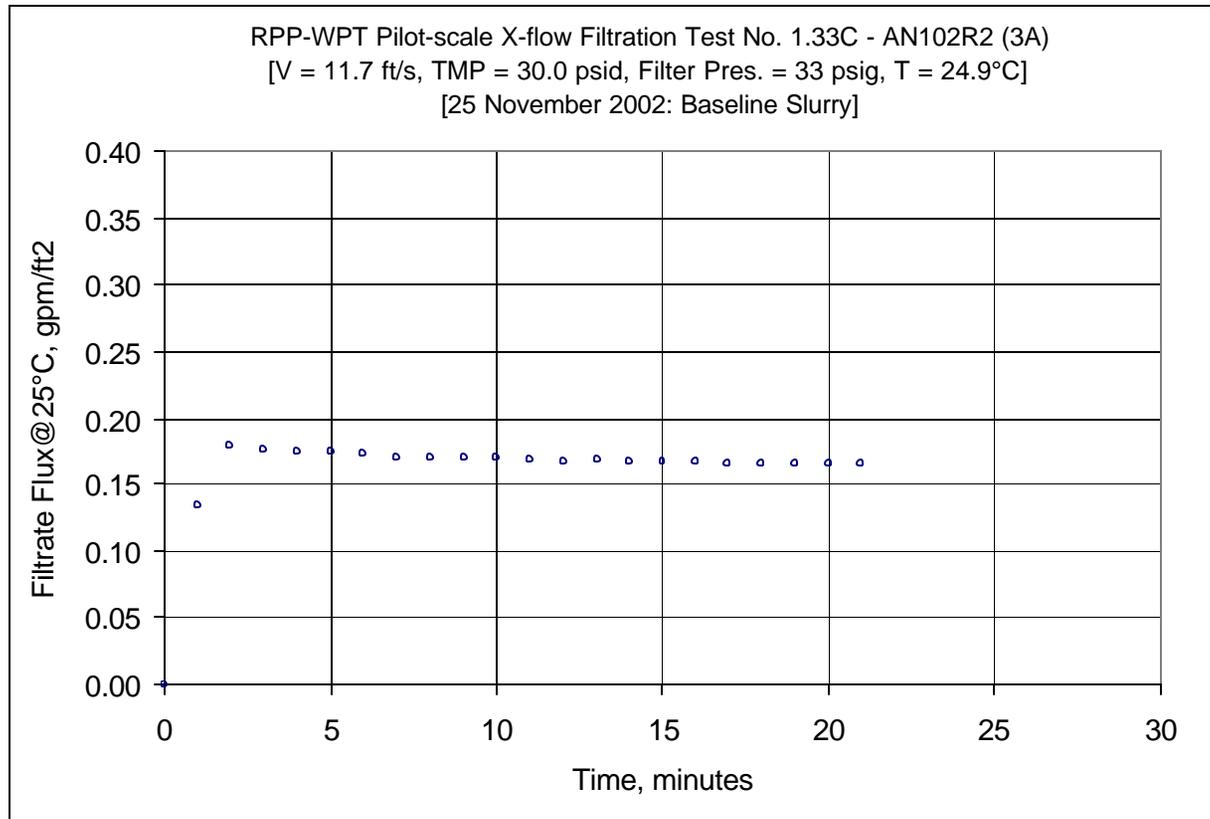


Figure B39: Run 1.33C – Baseline Slurry – After AN-102R2 Batch 3A and Before Batch 4A



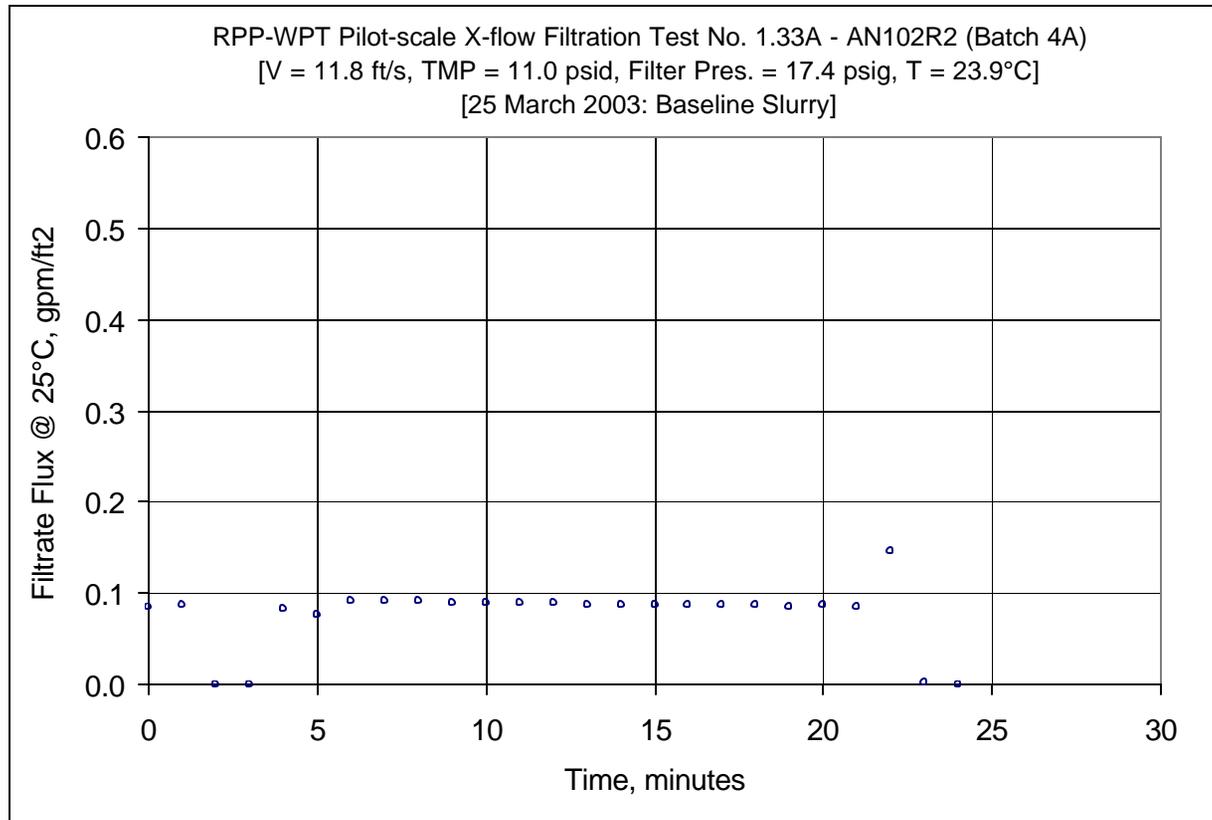


Figure B41: Run 1.33A – Baseline Slurry – After AN-102R2 Batch 4A



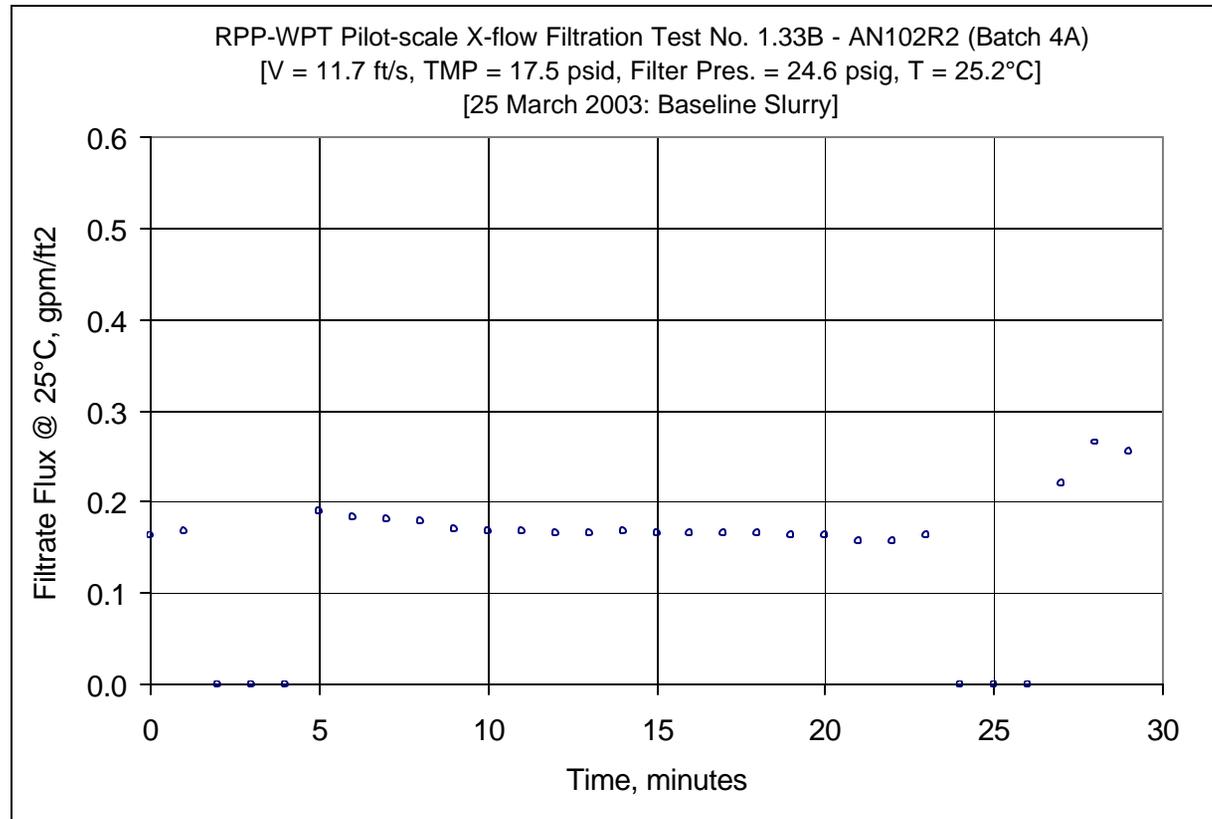


Figure B43: Run 1.33B – Baseline Slurry – After AN-102R2 Batch 4A



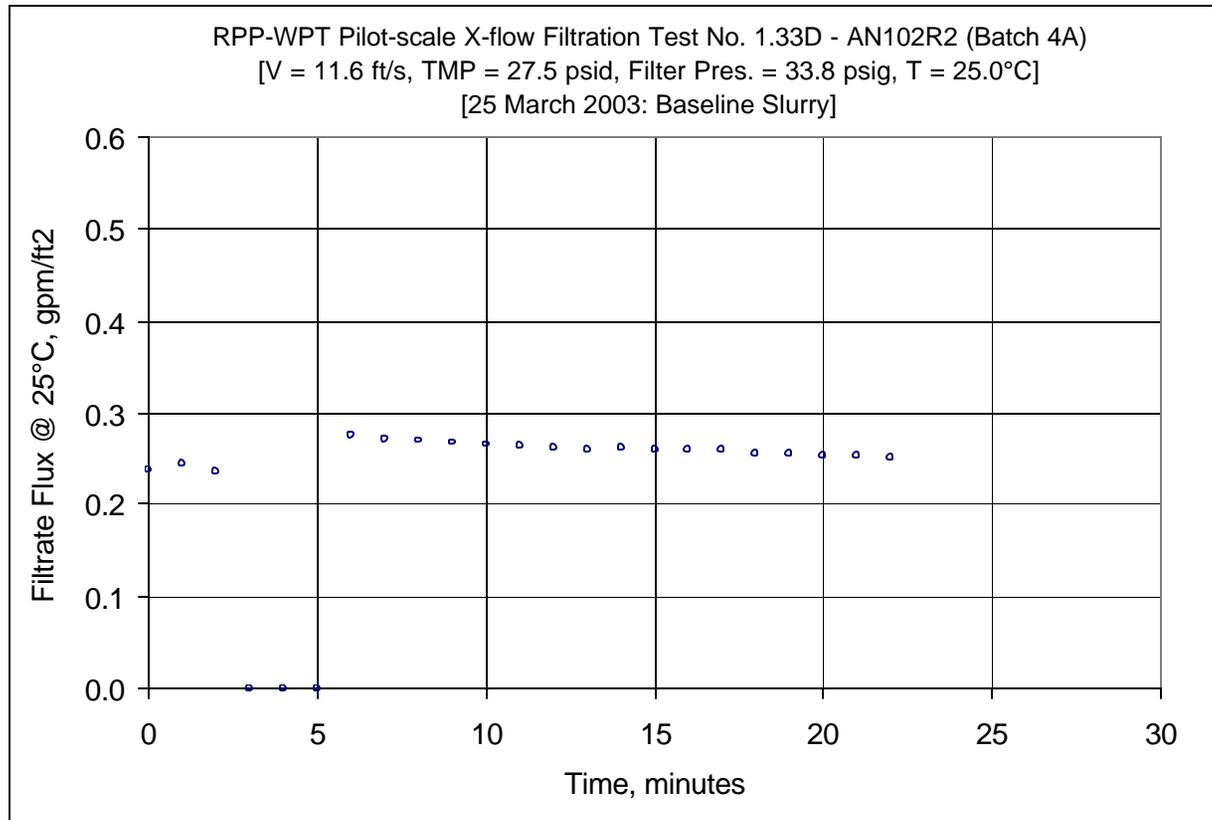


Figure B45: Run 1.33D – Baseline Slurry – After AN-102R2 Batch 4A (replaced 1.33C which had control problems)



## Appendix C: 2 M Nitric Acid Cleaning

As required by the RPP-WTP Test Specification each time the cross-flow filter experienced a slurry run the filter was to be cleaned with 2 M Nitric Acid. Those tests were noted in the test matrix as runs 1.31B and 1.31C, 1.31A was a water rinse that began the process of cleaning. (Note that prior to slurry testing the filter was preconditioned with an AN-107 simulant slurry during which the acid cleaning steps were referred to as 5B and 5C.) Since the slurries tested for this task were (in chronological order): an AN-107 simulant slurry (to precondition the filter) and AN-102R2 simulant slurries, Batches 3C, 3B, 3C, and 4, the filter was cleaned with acid at least 5 times. This Appendix includes the following cleaning test runs

5B, 5C	After Preconditioning the filter with AN-107
Clean 1, Clean 2 <sup>†</sup>	After AN-102R2, batch 3C (using the cleaning loop)
1.31B, 1.31C	After AN-102R2, batch 3B
1.31B, 1.31C	After AN-102R2, batch 3A
ACIDA & ACIDB <sup>‡</sup>	Before AN-102R2, batch 4A (4-day acid soak)
1.31B, 1.31C	After AN-102R2, batch 4A

The letter B and C (or numbers 1 and 2) simply indicate different cleaning cycle. When this task was done there was no set protocol for cleaning. The only requirement was to use a nitric acid with a concentration of 2 molar. While there were some exceptions, as shown in the data in this Appendix, in general, the filter was cleaned by the following method:

1. Rinse the filter once with water (test 1.31A).
2. Circulate 100 liters of 2 M HNO<sub>3</sub> for 90 minutes at a circulation axial velocity of 11 to 12 ft/s and a transmembrane pressure of 20 psid, then discard the 100 liters.
3. Repeat step 2 once.
4. Rinse with water (test 1.32)

These cleaning steps were basically arbitrarily chosen. At the time of this task some bench top tests used two 90-minute steps, however, there seemed to be no set rule. For instance, some bench-top tests allowed the filter to soak for several days in acid to bring it to a very clean condition. For this test it was thought more important to clean the filter similar to how the actual plant may operate. To spend several days cleaning the filter did not seem practical. The exception is between slurry test AN-102R2, batch 3A and 4 during which the filter sat idle for almost 3 months. Just before batch 4 the filter was given a much more thorough cleaning by letting it soak over a 4-day period before use.

Each acid-cleaning test in this Appendix contains a graph of the filtrate flux with time and tables of the data taken and calculated. To better understand the presented information important aspects of the graphs and tables are explained below:

Graphs – Each graph contains time averages of some of the important parameters taken during the run at the top of the figures, i.e. Slurry velocity in the filter tube, V; transmembrane pressure, TMP; slurry pressure at the entrance of the filter tube, Filter Pres; and the slurry temperature, T.

Tables – Each table is divided into raw data (the first 17 columns) and calculations (the last 10 columns) which are based on the raw data. The raw data section is divided into three parts:

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<sup>†</sup> Clean 1 and Clean 2 would have been called 1.31B and 1.31C, like the other test run cleaning, but a different nomenclature was given to those cleaning because there were pump lining problems, which forced the use of the Test Rig cleaning loop. The cleaning loop had a much smaller pump than the Test Rig, therefore the nitric acid solution circulation velocity and transmembrane pressure could not meet the test specification requirements of 12 ft/s and 20 psid, respectively. The actual values used are listed in this Appendix.

<sup>‡</sup> Because the filter sat idle, submerged in inhibited water, for 3 months between test 3A and 4A it was more extensively cleaned.

Individual Entries – Raw Data

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used, except for tests Clean 1 & 2) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid which has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column and corrected for a 40.9-inch water column that exists from the transducer to the point where P1 is measured.)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.  
Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.707 ft<sup>2</sup>)<sup>†</sup>  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T))-(1/298)] \text{ as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0}$$

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)  
Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing  
Permiability – Same as Permiability but in metric units, meter/day/bar

Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 xStd Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not included the points taken during the backpulse sequence of each test. This is explained below.

Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is were the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation

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<sup>†</sup> For the acid-cleaning tests during preconditioning it will be noticed that 6.87 ft<sup>2</sup> was used. This was based on a tube inside diameter of 0.5 inch, which was based on the manufacturer’s specification. After the tubes were measured the i.d. was changed to 0.488 inch and the area to 6.707 ft<sup>2</sup>. This means that absolute axial velocity and filtrate flux are low by 2.5% % for the preconditioning runs.

were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

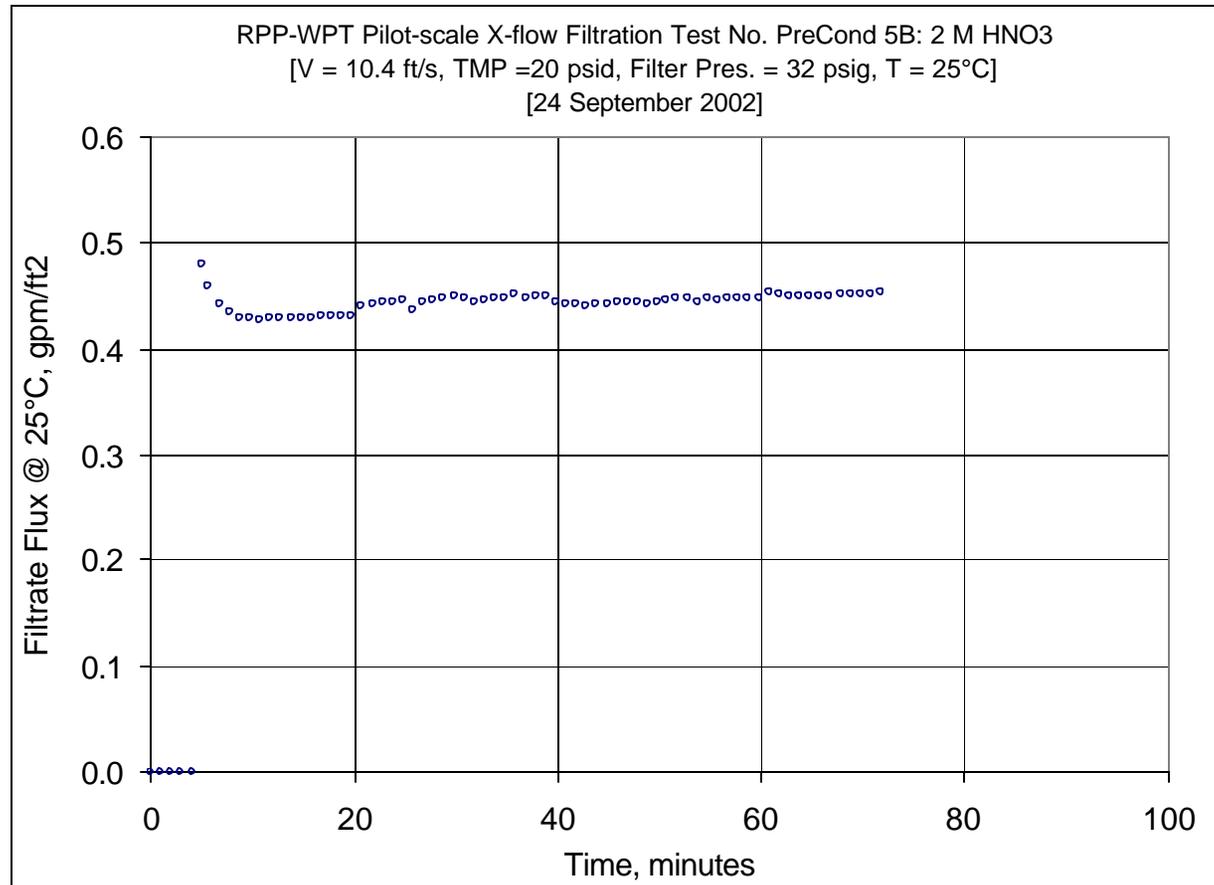


Figure C1: PreConditioning 5B – 2 M Nitric Acid Cleaning – FirstCleaning



9/24/2002	11:04:41 AM	25.3	22.741	24.742	23.649	23.019	24.878	33.616	11.02	15.227	2.636	-3.032	44.372	0.002	3.026	0.002	45.8	32.1	10.4	20.1	1.383	0.440	0.444	0.022	22.119	18.82
9/24/2002	11:05:41 AM	25.334	22.755	24.701	23.727	23.063	25.052	33.698	11.041	15.401	2.575	-3.032	44.216	0.002	3.024	0.002	46.8	32.2	10.3	20.2	1.395	0.440	0.444	0.022	21.939	18.67
9/24/2002	11:06:41 AM	25.348	22.769	24.77	23.752	23.112	25.168	33.878	11.177	15.612	2.65	-3.029	44.401	0.001	3.028	0	47.8	32.4	10.4	20.4	1.406	0.441	0.443	0.022	21.750	18.51
9/24/2002	11:07:41 AM	25.363	22.794	24.8	23.852	23.167	25.118	33.829	11.117	15.539	2.627	-3.018	44.195	0.002	3.025	0.004	48.8	32.4	10.3	20.3	1.402	0.440	0.443	0.022	21.776	18.53
9/24/2002	11:08:41 AM	25.388	22.789	24.76	23.907	23.212	25.046	33.794	11.008	15.485	2.65	-3.018	44.183	0.002	3.03	0.002	49.8	32.3	10.3	20.3	1.397	0.441	0.444	0.022	21.904	18.64
9/24/2002	11:09:41 AM	25.409	22.82	24.861	23.948	23.279	25.052	34.023	11.12	15.428	2.775	-3.018	44.489	0.002	3.052	0.002	50.8	32.6	10.4	20.2	1.395	0.444	0.446	0.022	22.028	18.75
9/24/2002	11:10:41 AM	25.429	22.835	24.826	24.059	23.319	25.042	34.12	11.146	15.189	2.798	-3.015	44.63	0.002	3.06	0.002	51.8	32.6	10.4	20.1	1.387	0.445	0.447	0.022	22.244	18.93
9/24/2002	11:11:41 AM	25.444	22.82	24.811	24.023	23.328	25.006	33.876	11.058	15.428	2.815	-3.015	44.47	0.002	3.06	0	52.8	32.4	10.4	20.2	1.394	0.445	0.448	0.022	22.142	18.84
9/24/2002	11:12:41 AM	25.467	22.853	24.914	24.081	23.337	24.708	33.49	11.04	15.103	2.737	-3.012	44.583	0.002	3.05	0.002	53.8	32.0	10.4	19.9	1.372	0.444	0.445	0.022	22.350	19.02
9/24/2002	11:13:41 AM	25.485	22.856	24.837	24.039	23.345	25.104	34.048	11.098	15.496	2.827	-3.012	44.38	0.002	3.065	0.001	54.8	32.6	10.4	20.3	1.400	0.446	0.448	0.022	22.071	18.78
9/24/2002	11:14:41 AM	25.512	22.868	24.904	24.066	23.336	24.654	33.5	10.989	15.113	2.902	-3.012	44.351	0.002	3.064	0.003	55.8	32.0	10.4	19.9	1.371	0.446	0.447	0.022	22.484	19.13
9/24/2002	11:15:41 AM	25.508	22.864	24.91	24.032	23.343	24.853	33.814	11.087	15.207	2.91	-3.006	44.497	0.002	3.071	0.001	56.8	32.3	10.4	20.0	1.381	0.447	0.448	0.022	22.367	19.03
9/24/2002	11:16:41 AM	25.544	22.885	24.881	24.043	23.339	25.075	34.172	11.015	15.608	2.916	-3	44.468	0.002	3.071	0.003	57.8	32.7	10.4	20.3	1.402	0.447	0.448	0.022	22.042	18.76
9/24/2002	11:17:41 AM	25.545	22.871	24.928	23.995	23.35	25.357	34.211	11.095	15.897	2.957	-3.006	44.466	0.001	3.077	0.001	58.8	32.7	10.4	20.6	1.422	0.448	0.449	0.022	21.751	18.51
9/24/2002	11:18:41 AM	25.551	22.891	24.928	24.005	23.335	25	34.013	11.091	15.465	2.91	-3.003	44.388	0.002	3.076	0	59.8	32.5	10.4	20.2	1.395	0.448	0.449	0.022	22.168	18.86
9/24/2002	11:19:41 AM	25.581	22.902	24.938	24.02	23.345	25.06	34.241	11.024	15.446	3.026	-3.003	44.153	0.002	3.107	0	60.8	32.8	10.3	20.3	1.396	0.452	0.453	0.022	22.362	19.03
9/24/2002	11:20:41 AM	25.611	22.907	25.033	23.99	23.341	24.962	34.094	11.199	15.244	3.017	-3.006	44.286	0.001	3.102	0.001	61.8	32.6	10.3	20.1	1.387	0.451	0.451	0.022	22.421	19.08
9/24/2002	11:21:41 AM	25.641	22.922	24.988	24.02	23.321	25.031	34.214	11.173	15.344	2.983	-2.997	44.372	0.002	3.087	0.001	62.8	32.7	10.4	20.2	1.392	0.449	0.449	0.022	22.259	18.94
9/24/2002	11:22:41 AM	25.666	22.922	25.003	24.02	23.336	24.934	33.978	10.958	15.563	2.983	-2.997	44.651	0.002	3.088	0.001	63.8	32.5	10.4	20.2	1.396	0.449	0.449	0.022	22.190	18.88
9/24/2002	11:23:41 AM	25.646	22.927	25.048	24.03	23.301	24.888	34	11.13	15.287	3.069	-3	44.464	0.002	3.096	0.001	64.8	32.5	10.4	20.1	1.385	0.451	0.450	0.022	22.397	19.06
9/24/2002	11:24:41 AM	25.651	22.922	24.968	24.015	23.315	24.969	34.166	11.235	15.082	3.02	-2.997	44.573	0.002	3.095	0.001	65.8	32.7	10.4	20.0	1.381	0.450	0.451	0.023	22.510	19.16
9/24/2002	11:25:41 AM	25.665	22.926	25.027	23.989	23.309	24.613	33.715	11.074	14.971	3.023	-2.997	44.518	0.002	3.101	0	66.8	32.2	10.4	19.8	1.365	0.451	0.451	0.023	22.782	19.39
9/24/2002	11:26:41 AM	25.654	22.93	25.021	24.008	23.314	24.65	33.843	11.053	15.17	3.104	-2.997	44.535	0.002	3.11	0	67.8	32.4	10.4	19.9	1.373	0.453	0.452	0.023	22.716	19.33
9/24/2002	11:27:41 AM	25.669	22.935	24.976	23.998	23.299	24.758	33.821	11.028	15.299	3.066	-2.995	44.422	0.002	3.109	0.001	68.8	32.3	10.4	20.0	1.381	0.452	0.453	0.023	22.603	19.24
9/24/2002	11:28:41 AM	25.668	22.934	25.05	23.972	23.272	24.698	33.94	11.01	14.949	3.081	-2.995	44.42	0.002	3.113	0.001	69.8	32.5	10.4	19.8	1.367	0.453	0.452	0.023	22.819	19.42
9/24/2002	11:29:41 AM	25.663	22.934	25.015	23.991	23.277	24.862	34.18	11.07	15.346	3.092	-2.995	44.445	0.002	3.112	0.002	70.8	32.7	10.4	20.1	1.387	0.453	0.453	0.023	22.504	19.15
9/24/2002	11:30:41 AM	25.673	22.924	24.985	23.961	23.267	24.864	34.04	11.286	15.111	3.081	-2.995	44.386	0.001	3.118	0	71.8	32.6	10.4	20.0	1.378	0.454	0.454	0.023	22.709	19.33
	Averages	25.1	22.8	24.5	23.7	23.0	25.0	33.7	11.2	15.3	2.6	-3.0	44.5	0.0	3.0	0.0		32.2	10.4	20.2	1.4	0.438	0.444	0.022	22.0	18.7
	Maximum	25.7	22.9	25.1	24.1	23.4	25.4	34.2	11.8	15.9	3.1	-3.0	46.5	0.0	3.1	0.0		32.8	10.9	20.6	1.4	0.454	0.460	0.024	24.3	20.6
	Median	25.2	22.7	24.6	23.6	22.9	25.1	33.7	11.1	15.3	2.6	-3.0	44.4	0.0	3.0	0.0		32.2	10.4	20.2	1.4	0.439	0.445	0.022	21.9	18.7
	Minimum	24.4	22.7	23.7	23.4	22.8	24.1	33.1	10.7	13.9	1.9	-3.1	43.3	0.0	2.9	0.0		31.6	10.1	19.0	1.3	0.421	0.428	0.021	21.0	17.9
	2 x Std Dev	0.771	0.198	0.782	0.468	0.422	0.462	0.654	0.458	0.643	0.734	0.074	1.181	0.001	0.138	0.005		0.655	0.276	0.489	0.034	0.020	0.015	0.001	1.001	0.852
	Number of Points Used*	67	67	67	67	67	67	67	67	67	67	67	67	67	67	67		67	67	67	67	67	67	67	67	67

\* Backpulse points in box are not included

Figure C2b: PreConditioning 5B – 2 M Nitric Acid Cleaning – FirstCleaning (remaining 22 minutes) – Raw & Calculated Data

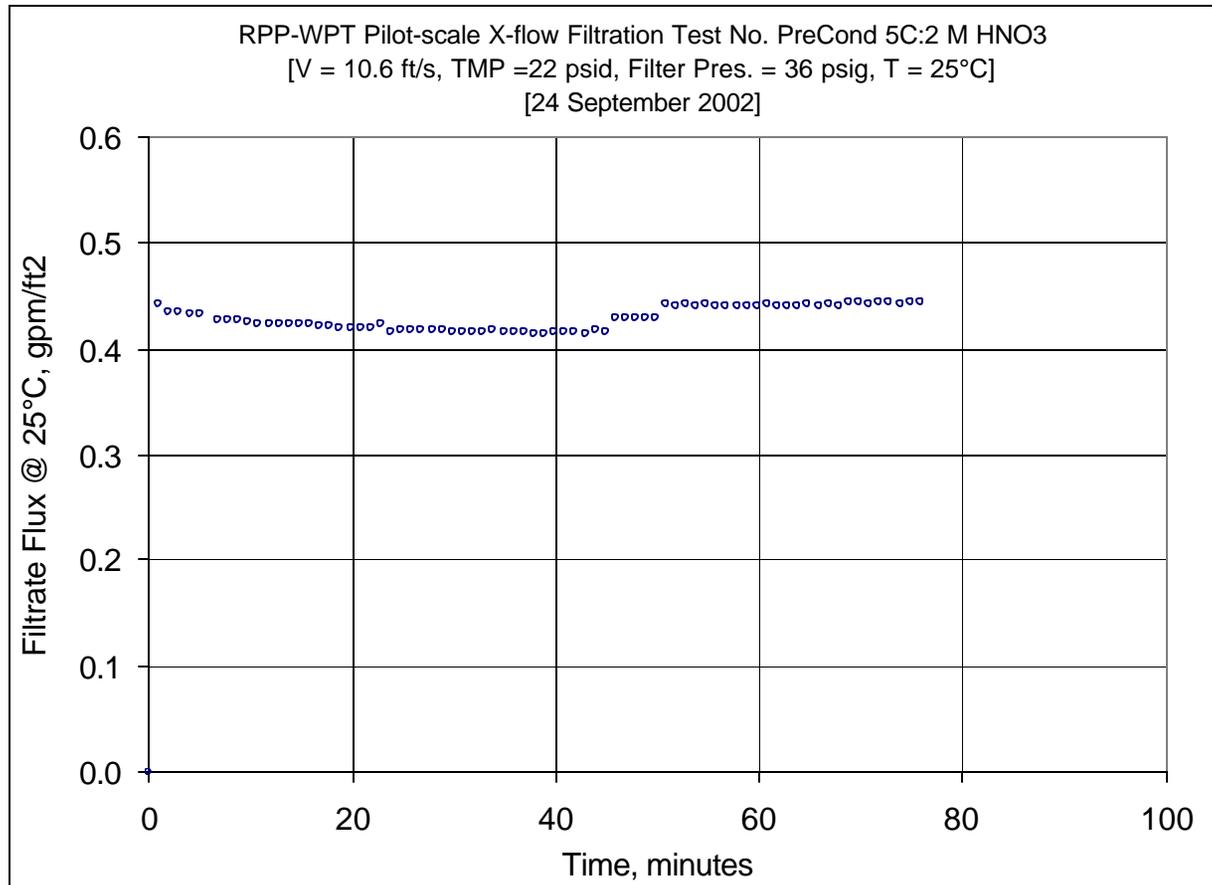


Figure C3: PreConditioning 5C – 2 M Nitric Acid Cleaning – Second Cleaning



9/24/2002	1:05:00 PM	25.607	23.149	24.919	24.462	23.306	29.617	37.884	16.816	14.108	2.22	36.118	45.143	0.002	2.943	0.002	46.8	36.4	10.5	21.9	1.507	0.428	0.429	0.020	19.633	16.71
9/24/2002	1:06:00 PM	25.652	23.149	24.934	24.502	23.296	29.582	37.97	16.722	13.942	2.217	36.121	45.125	0.002	2.943	0.002	47.8	36.5	10.5	21.8	1.500	0.428	0.429	0.020	19.715	16.78
9/24/2002	1:07:00 PM	25.673	23.155	25.04	24.539	23.328	30.021	38.279	17.068	14.169	2.225	36.118	45.192	0.002	2.95	0.002	48.8	36.8	10.5	22.1	1.523	0.429	0.429	0.019	19.406	16.51
9/24/2002	1:08:00 PM	25.708	23.155	25.005	24.549	23.318	29.513	37.836	16.667	14.034	2.222	36.118	45.167	0.002	2.951	0.003	49.8	36.4	10.5	21.8	1.501	0.429	0.429	0.020	19.719	16.78
9/24/2002	1:09:00 PM	25.749	23.151	25.041	24.504	23.333	30.039	38.922	16.016	15.322	2.67	36.112	44.109	0.001	3.04	0.002	50.8	37.4	10.3	22.7	1.564	0.442	0.442	0.019	19.481	16.58
9/24/2002	1:10:00 PM	25.775	23.152	25.112	24.46	23.339	29.911	38.601	16.183	15.029	2.595	36.115	43.982	0.002	3.035	0.002	51.8	37.1	10.3	22.5	1.549	0.442	0.440	0.020	19.592	16.67
9/24/2002	1:11:00 PM	25.81	23.162	25.057	24.485	23.334	29.712	38.461	16.081	15.039	2.688	36.115	44.122	0.002	3.041	0.001	52.8	37.0	10.3	22.4	1.543	0.443	0.442	0.020	19.745	16.80
9/24/2002	1:12:00 PM	25.815	23.152	25.117	24.455	23.32	29.665	38.452	15.941	15.088	2.673	36.112	44.147	0.002	3.038	0.002	53.8	37.0	10.3	22.4	1.543	0.442	0.441	0.020	19.691	16.76
9/24/2002	1:13:00 PM	25.825	23.162	25.127	24.445	23.335	29.505	38.378	16.173	14.703	2.757	36.109	44.044	0.001	3.048	0.003	54.8	36.9	10.3	22.1	1.524	0.444	0.442	0.020	19.994	17.01
9/24/2002	1:14:00 PM	25.856	23.163	25.108	24.531	23.325	29.604	38.477	16.081	14.64	2.679	36.115	44.067	0.002	3.04	0.002	55.8	37.0	10.3	22.1	1.525	0.442	0.441	0.020	19.936	16.97
9/24/2002	1:15:00 PM	25.866	23.169	25.179	24.577	23.346	29.342	38.235	16.105	14.533	2.734	36.112	44.047	0.002	3.047	0.002	56.8	36.8	10.3	21.9	1.513	0.443	0.441	0.020	20.109	17.11
9/24/2002	1:16:00 PM	25.856	23.174	25.133	24.592	23.336	29.482	38.45	16.297	14.243	2.754	36.118	44.074	0.002	3.043	0.004	57.8	37.0	10.3	21.9	1.507	0.443	0.441	0.020	20.178	17.17
9/24/2002	1:17:00 PM	25.883	23.185	25.13	24.598	23.347	29.87	38.75	16.231	14.961	2.679	36.115	44.191	0.002	3.043	0.002	58.8	37.3	10.3	22.4	1.545	0.443	0.441	0.020	19.682	16.75
9/24/2002	1:18:00 PM	25.868	23.175	25.19	24.598	23.332	29.304	37.89	16.013	14.66	2.728	36.109	44.131	0.001	3.049	0.002	59.8	36.4	10.3	22.0	1.516	0.444	0.441	0.020	20.076	17.08
9/24/2002	1:19:00 PM	25.883	23.191	25.15	24.629	23.343	29.342	38.061	15.954	14.818	2.746	36.118	44.208	0.002	3.051	0.002	60.8	36.6	10.3	22.1	1.522	0.444	0.442	0.020	20.022	17.04
9/24/2002	1:20:00 PM	25.894	23.186	25.171	24.614	23.358	29.731	38.726	16.155	14.853	2.728	36.112	44.122	0.002	3.046	0.004	61.8	37.3	10.3	22.3	1.537	0.443	0.441	0.020	19.788	16.84
9/24/2002	1:21:00 PM	25.884	23.186	25.206	24.589	23.378	29.337	38.183	15.905	14.775	2.772	36.112	44.023	0.002	3.05	0.002	62.8	36.7	10.3	22.1	1.521	0.444	0.441	0.020	20.006	17.03
9/24/2002	1:22:00 PM	25.895	23.187	25.137	24.65	23.354	29.354	38.221	15.946	14.599	2.682	36.109	44.21	0.002	3.045	0.002	63.8	36.7	10.3	22.0	1.515	0.443	0.441	0.020	20.084	17.09
9/24/2002	1:23:00 PM	25.905	23.192	25.202	24.6	23.349	29.358	38.252	16.079	14.572	2.746	36.109	44.091	0.002	3.054	0.002	64.8	36.8	10.3	22.0	1.514	0.444	0.442	0.020	20.117	17.12
9/24/2002	1:24:00 PM	25.895	23.192	25.192	24.585	23.359	29.449	38.368	15.98	14.681	2.734	36.106	44.059	0.001	3.045	0.003	65.8	36.9	10.3	22.1	1.521	0.443	0.441	0.020	19.973	17.00
9/24/2002	1:25:00 PM	25.92	23.197	25.157	24.54	23.364	29.192	38.124	16.075	14.509	2.786	36.112	43.971	0.002	3.051	0.002	66.8	36.7	10.3	21.9	1.507	0.443	0.442	0.020	20.229	17.21
9/24/2002	1:26:00 PM	25.925	23.202	25.237	24.53	23.384	29.17	37.888	16.01	14.556	2.743	36.109	43.969	0.002	3.043	0.003	67.8	36.4	10.3	21.9	1.507	0.443	0.440	0.020	20.119	17.12
9/24/2002	1:27:00 PM	25.93	23.207	25.197	24.585	23.374	29.435	38.531	15.718	14.974	2.893	36.109	43.885	0.002	3.067	0.002	68.8	37.1	10.2	22.2	1.531	0.446	0.444	0.020	19.988	17.01
9/24/2002	1:28:00 PM	25.95	23.212	25.217	24.586	23.37	29.518	38.496	16.005	14.802	2.861	36.109	43.824	0.002	3.071	0.002	69.8	37.0	10.2	22.2	1.528	0.447	0.444	0.020	20.043	17.06
9/24/2002	1:29:00 PM	25.966	23.218	25.303	24.556	23.395	29.188	38.074	15.915	14.378	2.91	36.109	43.893	0.002	3.072	0.003	70.8	36.6	10.2	21.8	1.502	0.447	0.443	0.020	20.347	17.32
9/24/2002	1:30:00 PM	25.981	23.214	25.254	24.617	23.411	29.143	38.022	15.863	14.566	2.922	36.109	43.709	0.002	3.079	0.003	71.8	36.5	10.2	21.8	1.506	0.448	0.445	0.020	20.360	17.33
9/24/2002	1:31:00 PM	26.031	23.224	25.304	24.657	23.416	29.257	38.246	15.921	14.701	2.936	36.109	43.717	0.002	3.08	0.003	72.8	36.8	10.2	22.0	1.515	0.448	0.444	0.020	20.218	17.21
9/24/2002	1:32:00 PM	26.052	23.239	25.399	24.572	23.407	29.327	38.301	15.744	14.922	2.977	36.106	43.789	0.002	3.08	0.002	73.8	36.8	10.2	22.1	1.525	0.448	0.443	0.020	20.031	17.05
9/24/2002	1:33:00 PM	26.077	23.234	25.334	24.532	23.417	29.238	38.268	15.446	15.234	2.983	36.103	43.751	0.002	3.083	0.003	74.8	36.8	10.2	22.2	1.533	0.449	0.444	0.020	19.987	17.01
9/24/2002	1:34:00 PM	26.113	23.245	25.395	24.558	23.412	29.186	38.113	15.775	14.924	2.968	36.103	43.537	0.001	3.088	0.002	75.8	36.6	10.2	22.1	1.521	0.449	0.444	0.020	20.149	17.15
	Averages	25.6	23.2	24.9	24.4	23.3	29.7	37.9	17.0	13.9	2.2	36.1	45.5	0.0	2.9	0.0	36.4	10.6	21.8	1.5	0.428	0.429	0.020	19.7	16.7	
	Maximum	26.1	23.2	25.4	24.7	23.4	30.3	38.9	18.1	15.3	3.0	36.2	47.4	0.0	3.1	0.0	37.4	11.1	22.7	1.6	0.449	0.445	0.020	20.4	17.3	
	Median	25.6	23.1	24.9	24.4	23.3	29.7	37.8	17.6	13.7	1.9	36.1	46.3	0.0	2.9	0.0	36.4	10.8	21.8	1.5	0.420	0.425	0.020	19.7	16.8	
	Minimum	25.2	23.1	24.4	24.2	23.2	29.1	37.2	15.4	12.6	1.6	36.1	43.5	0.0	2.8	0.0	35.7	10.2	21.0	1.5	0.413	0.414	0.019	18.9	16.0	
	2 x Std Dev	0.513	0.065	0.516	0.275	0.125	0.570	0.813	1.687	1.520	0.992	0.031	2.376	0.001	0.187	0.001	0.813	0.555	0.681	0.047	0.027	0.022	0.001	0.769	0.654	
	Number of Points Used*	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70

\* Backpulse points in box are not included

Figure C4b: PreConditioning 5C – 2 M Nitric Acid Cleaning – Second Cleaning (remaining 36 minutes) – Raw & Calculated Data

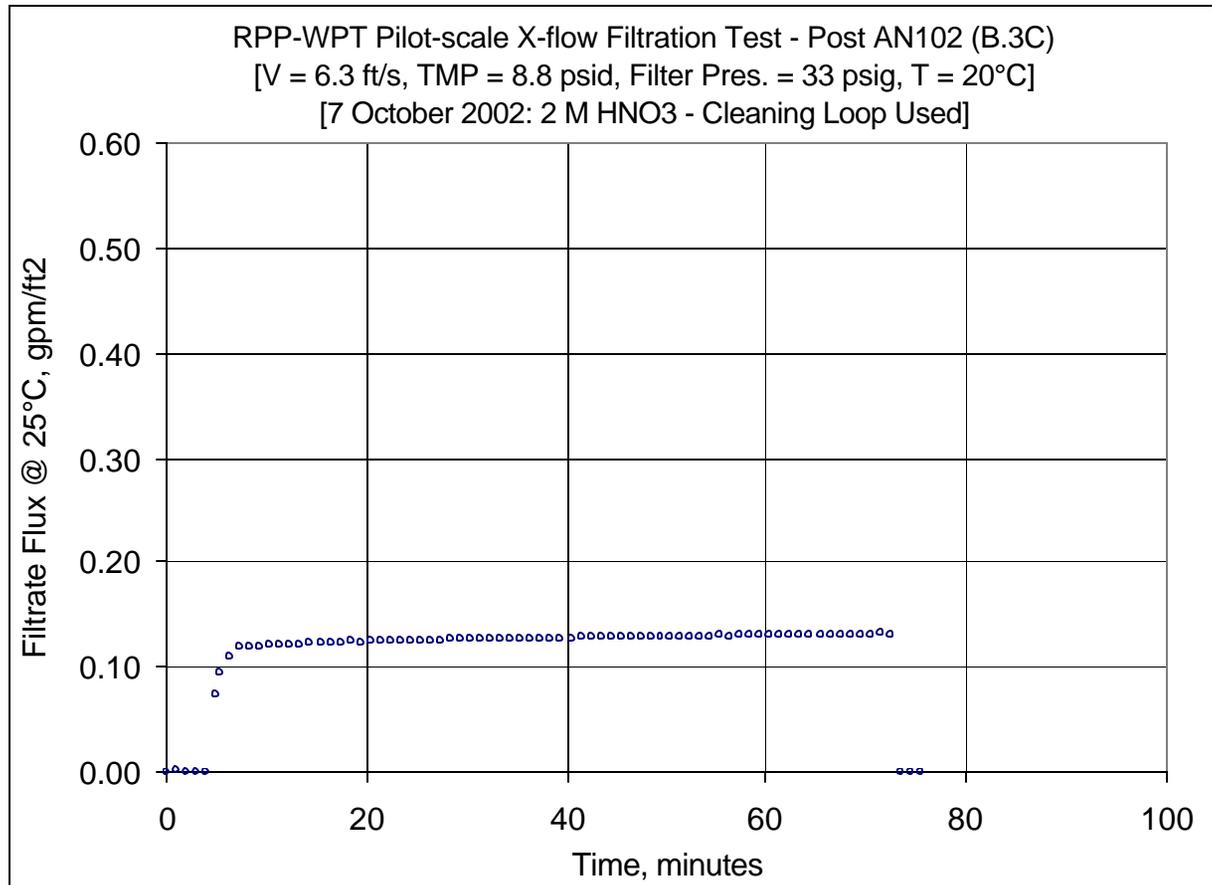


Figure C5: Clean 1: After AN-102R2, Batch 3C – 2 M Nitric Acid Cleaning – First Cleaning



10/7/2002	3:50:35 PM	25.736	25.4	19.779	23.904	20.411	9.425	34.383	1.613	8.066	19.724	19.24	26.049	0.741	0.001	0	46.38	32.9	6.4	8.7	0.603	0.110	0.128	0.015	14.671	12.49
10/7/2002	3:51:35 PM	25.465	25.549	19.743	23.959	20.395	9.017	34.079	1.756	7.379	19.808	19.336	26.164	0.743	0.001	0	47.38	32.6	6.4	8.2	0.565	0.111	0.129	0.016	15.709	13.37
10/7/2002	3:52:35 PM	25.471	25.941	19.749	23.91	20.412	9.172	34.288	1.708	7.624	19.92	19.472	26.16	0.745	0.001	0	48.38	32.8	6.4	8.4	0.579	0.111	0.129	0.015	15.374	13.08
10/7/2002	3:53:35 PM	25.662	26.257	19.74	23.886	20.433	8.945	34.135	1.674	7.389	20.004	19.503	26.2	0.746	0.001	0	49.38	32.7	6.4	8.2	0.563	0.111	0.129	0.016	15.834	13.48
10/7/2002	3:54:35 PM	25.632	25.406	19.735	24.001	20.422	8.884	34.127	1.786	7.137	19.932	19.466	26.139	0.744	0.001	0	50.38	32.7	6.4	8.0	0.552	0.111	0.129	0.016	16.103	13.70
10/7/2002	3:55:35 PM	25.491	25.776	19.724	24.156	20.422	9.032	34.185	1.69	7.555	19.923	19.472	26.101	0.745	0.001	0	51.38	32.7	6.4	8.3	0.572	0.111	0.129	0.016	15.579	13.26
10/7/2002	3:56:35 PM	25.622	26.207	19.73	24.207	20.448	9.125	34.414	1.839	7.385	19.958	19.448	26.141	0.745	0.001	0	52.38	32.9	6.4	8.3	0.569	0.111	0.129	0.016	15.649	13.32
10/7/2002	3:57:35 PM	25.812	25.416	19.75	24.252	20.448	9.172	34.452	1.724	7.653	20.042	19.538	26.213	0.748	0.001	0	53.38	33.0	6.4	8.4	0.580	0.112	0.130	0.015	15.409	13.11
10/7/2002	3:58:35 PM	25.592	25.681	19.75	24.462	20.442	8.891	34.141	1.67	7.454	20.036	19.59	26.171	0.746	0.001	0	54.38	32.7	6.4	8.2	0.563	0.111	0.129	0.016	15.819	13.46
10/7/2002	3:59:35 PM	25.585	26.085	19.764	24.456	20.451	8.963	34.441	1.717	7.481	20.169	19.706	26.252	0.75	0.001	0	55.38	33.0	6.4	8.2	0.567	0.112	0.130	0.016	15.801	13.45
10/7/2002	4:00:35 PM	25.8	25.839	19.763	24.46	20.45	9.139	34.551	1.785	7.555	20.103	19.64	26.099	0.748	0.001	0	56.38	33.1	6.4	8.3	0.575	0.112	0.130	0.016	15.524	13.21
10/7/2002	4:01:35 PM	25.639	25.568	19.757	24.354	20.455	8.646	33.974	1.652	7.188	20.16	19.645	26.217	0.751	0.001	0	57.38	32.5	6.4	7.9	0.546	0.112	0.130	0.016	16.435	13.99
10/7/2002	4:02:35 PM	25.558	25.948	19.746	24.429	20.459	8.837	34.228	1.707	7.473	20.204	19.706	26.192	0.75	0.001	0	58.38	32.8	6.4	8.2	0.562	0.112	0.130	0.016	15.940	13.56
10/7/2002	4:03:35 PM	25.728	26.323	19.736	24.499	20.459	8.561	34.011	1.646	7.131	20.204	19.75	26.166	0.752	0.001	0	59.38	32.5	6.4	7.8	0.541	0.112	0.130	0.017	16.616	14.14
10/7/2002	4:04:35 PM	25.703	25.447	19.736	24.433	20.464	9.204	34.582	1.718	7.774	20.131	19.628	26.06	0.75	0.001	0	60.38	33.1	6.4	8.5	0.585	0.112	0.130	0.015	15.317	13.03
10/7/2002	4:05:35 PM	25.567	25.832	19.75	24.598	20.463	8.715	34.044	1.588	7.418	20.207	19.695	26.236	0.75	0.001	0	61.38	32.6	6.4	8.1	0.556	0.112	0.130	0.016	16.113	13.71
10/7/2002	4:06:35 PM	25.682	26.252	19.75	24.623	20.473	8.965	34.596	1.725	7.516	20.348	19.79	26.206	0.754	0.001	0	62.38	33.1	6.4	8.2	0.568	0.112	0.131	0.016	15.857	13.49
10/7/2002	4:07:35 PM	25.826	25.411	19.744	24.567	20.467	8.646	34.129	1.784	6.953	20.204	19.732	26.12	0.752	0.001	0	63.38	32.7	6.4	7.8	0.538	0.112	0.130	0.017	16.712	14.22
10/7/2002	4:08:35 PM	25.617	25.717	19.75	24.527	20.473	8.541	34.123	1.669	7.182	20.418	19.865	26.232	0.755	0.001	0	64.38	32.6	6.4	7.9	0.542	0.113	0.131	0.017	16.643	14.16
10/7/2002	4:09:35 PM	25.617	26.122	19.745	24.387	20.458	8.549	34.139	1.7	7.084	20.432	19.819	26.232	0.755	0.001	0	65.38	32.7	6.4	7.8	0.539	0.113	0.131	0.017	16.741	14.25
10/7/2002	4:10:35 PM	25.823	25.853	19.746	24.373	20.479	8.52	34.06	1.661	7.135	20.374	19.828	26.124	0.754	0.001	0	66.38	32.6	6.4	7.8	0.540	0.112	0.131	0.017	16.695	14.21
10/7/2002	4:11:35 PM	25.668	25.597	19.731	24.428	20.484	8.831	34.371	1.643	7.547	20.345	19.79	26.164	0.755	0.001	0	67.38	32.9	6.4	8.2	0.565	0.113	0.131	0.016	15.986	13.60
10/7/2002	4:12:35 PM	25.608	25.998	19.751	24.644	20.484	8.468	34.029	1.666	7.135	20.403	19.906	26.227	0.755	0.001	0	68.38	32.6	6.4	7.8	0.538	0.113	0.131	0.017	16.771	14.27
10/7/2002	4:13:35 PM	25.748	26.383	19.721	24.739	20.479	8.719	34.48	1.717	7.284	20.435	19.891	26.167	0.756	0.001	0	69.38	33.0	6.4	8.0	0.552	0.113	0.131	0.016	16.387	13.95
10/7/2002	4:14:35 PM	25.748	25.497	19.731	24.619	20.484	8.63	34.257	1.718	7.194	20.38	19.86	26.164	0.756	0.001	0	70.38	32.8	6.4	7.9	0.546	0.113	0.131	0.017	16.568	14.10
10/7/2002	4:15:35 PM	25.602	25.882	19.745	24.718	20.473	8.418	34.019	1.657	7.094	20.484	19.92	26.154	0.759	0.001	0	71.38	32.5	6.4	7.8	0.535	0.113	0.132	0.017	16.961	14.43
10/7/2002	4:16:35 PM	25.702	26.297	19.735	24.758	20.478	8.483	34.172	1.727	6.998	20.449	19.964	26.101	0.757	0.001	0	72.38	32.7	6.4	7.7	0.534	0.113	0.131	0.017	16.955	14.43
10/7/2002	4:17:35 PM	25.883	25.487	19.74	24.678	20.478	11.022	34.172	1.668	9.665	17.845	17.045	26.114	0.002	1.032	0	73.38	32.7	6.4	10.3	0.713	0.000	0.000	0.000	0.034	0.03
10/7/2002	4:18:35 PM	25.627	25.767	19.735	24.673	20.483	10.9	34.135	1.656	9.581	17.912	17.039	26.085	0.002	1.035	0	74.38	32.7	6.4	10.2	0.706	0.000	0.000	0.000	0.034	0.03
10/7/2002	4:19:35 PM	25.667	26.162	19.735	24.588	20.489	10.579	33.76	1.618	9.295	17.961	17.071	26.041	0.002	1.035	0	75.38	32.3	6.4	9.9	0.685	0.000	0.000	0.000	0.035	0.03
	Averages	25.3	25.4	19.8	24.2	20.4	9.5	34.1	1.7	8.0	19.3	18.9	25.9	0.7	0.0	0.0		32.6	6.3	8.8	0.605	0.104	0.121	0.0140	14.0	11.9
	Maximum	25.9	26.4	19.9	24.8	20.5	11.0	34.8	1.8	9.7	20.5	20.0	26.3	0.8	1.0	0.0		33.3	6.4	10.3	0.713	0.113	0.132	0.0174	17.4	14.8
	Median	25.4	25.5	19.8	24.2	20.4	9.5	34.3	1.7	8.0	19.6	19.1	26.1	0.7	0.0	0.0		32.8	6.4	8.7	0.603	0.110	0.127	0.0146	14.6	12.5
	Minimum	24.5	24.1	19.7	23.5	20.4	5.9	23.9	1.1	4.9	12.8	12.6	19.6	0.0	0.0	0.0		22.4	4.8	5.4	0.374	0.000	0.000	0.0000	0.0	0.0
	2 x Std Dev	0.760	1.127	0.109	0.576	0.074	1.710	2.570	0.175	1.647	2.253	2.199	1.718	0.299	0.416	0.000		2.570	0.421	1.7	0.115	0.045	0.052	0.0066	6.602	5.619
	Number of Points Used*	71	71	71	71	71	71	71	71	71	71	71	71	71	71	71		71	71	71	71	71	71	71	71	71
	* Backpulse points in box are not included																									

Figure C6b: Clean 1: After AN-102R2, Batch 3C – 2 M Nitric Acid Cleaning – First Cleaning (remaining 30 minutes) – Raw & Calculated Data

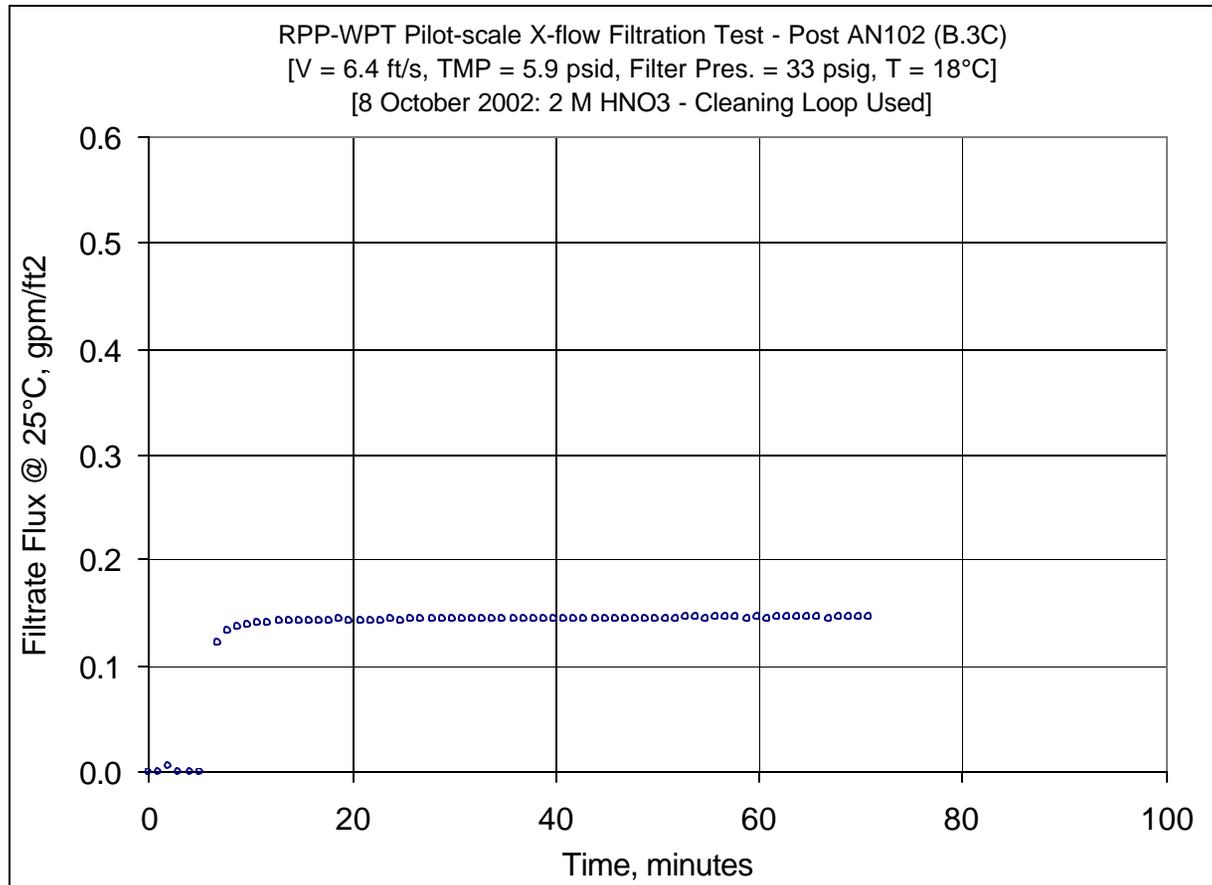


Figure C7: Clean 2: After AN-102R2, Batch 3C – 2 M Nitric Acid Cleaning – Second Cleaning



10/8/2002	10:50:02 AM	25.256	25.966	18.288	19.515	18.957	6.411	34.627	1.683	5.024	23.21	22.538	26.16	0.801	0.001	0	45.78	33.2	6.4	5.7	0.394	0.119	0.145	0.025	25.341	21.57		
10/8/2002	10:51:02 AM	25.496	25.511	18.293	19.484	18.952	6.496	34.7	1.695	5.031	23.065	22.434	26.171	0.8	0.001	0	46.78	33.2	6.4	5.8	0.397	0.119	0.145	0.025	25.104	21.36		
10/8/2002	10:52:02 AM	25.235	25.394	18.272	19.569	18.936	6.171	34.404	1.674	4.732	23.135	22.495	26.177	0.801	0.001	0	47.78	32.9	6.4	5.5	0.376	0.119	0.145	0.027	26.591	22.63		
10/8/2002	10:53:02 AM	25.159	25.76	18.282	19.574	18.921	6.246	34.435	1.671	4.787	23.094	22.495	26.215	0.801	0.001	0	48.78	33.0	6.4	5.5	0.380	0.119	0.145	0.026	26.269	22.36		
10/8/2002	10:54:02 AM	25.31	26.125	18.257	19.504	18.926	6.235	34.555	1.693	4.865	23.204	22.683	26.219	0.802	0.001	0	49.78	33.1	6.4	5.6	0.383	0.120	0.145	0.026	26.163	22.26		
10/8/2002	10:55:02 AM	25.505	25.334	18.277	19.549	18.936	6.368	34.708	1.754	4.875	23.172	22.538	26.242	0.803	0.001	0	50.78	33.2	6.4	5.6	0.388	0.120	0.145	0.026	25.847	22.00		
10/8/2002	10:56:02 AM	25.199	25.619	18.272	19.609	18.925	6.457	34.745	1.689	5.18	23.1	22.555	26.152	0.8	0.001	0	51.78	33.3	6.4	5.8	0.401	0.119	0.145	0.025	24.882	21.18		
10/8/2002	10:57:02 AM	25.205	26.005	18.262	19.559	18.936	6.184	34.35	1.64	4.799	23.103	22.521	26.217	0.803	0.001	0	52.78	32.9	6.4	5.5	0.379	0.120	0.145	0.026	26.471	22.53		
10/8/2002	10:58:02 AM	25.395	26.38	18.282	19.529	18.936	6.509	34.975	1.736	5.026	23.256	22.654	26.263	0.804	0.001	0	53.78	33.5	6.4	5.8	0.398	0.120	0.145	0.025	25.220	21.46		
10/8/2002	10:59:02 AM	25.449	25.419	18.256	19.564	18.92	6.484	34.849	1.715	5.082	23.1	22.509	26.206	0.801	0.001	0	54.78	33.4	6.4	5.8	0.399	0.119	0.145	0.025	25.078	21.34		
10/8/2002	11:00:02 AM	25.199	25.724	18.241	19.553	18.915	6.412	34.772	1.761	4.902	23.27	22.555	26.25	0.804	0.001	0	55.78	33.3	6.4	5.7	0.390	0.120	0.146	0.026	25.744	21.91		
10/8/2002	11:01:02 AM	25.254	26.099	18.266	19.558	18.91	6.302	34.648	1.638	5.022	23.346	22.668	26.32	0.806	0.001	0	56.78	33.2	6.5	5.7	0.390	0.120	0.146	0.026	25.766	21.93		
10/8/2002	11:02:02 AM	25.443	26.309	18.266	19.492	18.909	6.42	34.878	1.751	4.861	23.233	22.581	26.146	0.805	0.001	0	57.78	33.4	6.4	5.6	0.389	0.120	0.146	0.026	25.832	21.98		
10/8/2002	11:03:02 AM	25.393	25.488	18.285	19.562	18.894	6.32	34.547	1.62	5.041	23.221	22.59	26.179	0.802	0.001	0	58.78	33.1	6.4	5.7	0.392	0.120	0.145	0.026	25.541	21.74		
10/8/2002	11:04:02 AM	25.217	25.822	18.26	19.526	18.888	6.258	34.532	1.654	4.803	23.181	22.59	26.133	0.803	0.001	0	59.78	33.1	6.4	5.5	0.381	0.120	0.145	0.026	26.285	22.37		
10/8/2002	11:05:02 AM	25.327	26.183	18.254	19.466	18.898	6.283	34.536	1.647	4.986	23.181	22.561	26.2	0.802	0.001	0	60.78	33.1	6.4	5.6	0.388	0.120	0.145	0.026	25.773	21.93		
10/8/2002	11:06:02 AM	25.532	25.918	18.265	19.451	18.898	5.991	34.383	1.639	4.691	23.363	22.709	26.24	0.805	0.001	0	61.78	32.9	6.4	5.3	0.368	0.120	0.146	0.027	27.282	23.22		
10/8/2002	11:07:02 AM	25.331	25.556	18.253	19.53	18.877	6.097	34.408	1.665	4.715	23.221	22.605	26.179	0.804	0.001	0	62.78	32.9	6.4	5.4	0.373	0.120	0.146	0.027	26.930	22.92		
10/8/2002	11:08:02 AM	25.252	25.902	18.279	19.556	18.903	6.167	34.561	1.719	4.711	23.296	22.648	26.267	0.806	0.001	0	63.78	33.1	6.4	5.4	0.375	0.120	0.146	0.027	26.812	22.82		
10/8/2002	11:09:02 AM	25.367	26.267	18.249	19.485	18.923	6.31	34.636	1.639	5.076	23.285	22.668	26.208	0.805	0.001	0	64.78	33.2	6.4	5.7	0.393	0.120	0.146	0.026	25.607	21.79		
10/8/2002	11:10:02 AM	25.583	25.577	18.265	19.491	18.944	6.242	34.652	1.693	4.871	23.325	22.683	26.286	0.806	0.001	0	65.78	33.2	6.4	5.6	0.383	0.120	0.146	0.026	26.256	22.34		
10/8/2002	11:11:02 AM	25.338	25.653	18.275	19.638	18.974	6.209	34.503	1.585	4.949	23.221	22.668	26.141	0.803	0.001	0	66.78	33.0	6.4	5.6	0.385	0.120	0.145	0.026	26.045	22.17		
10/8/2002	11:12:02 AM	25.288	26.014	18.271	19.674	19	6.221	34.623	1.648	4.857	23.296	22.694	26.21	0.806	0.001	0	67.78	33.1	6.4	5.5	0.382	0.120	0.146	0.026	26.335	22.41		
10/8/2002	11:13:02 AM	25.449	26.364	18.251	19.624	19.031	6.03	34.507	1.676	4.683	23.357	22.796	26.278	0.805	0.001	0	68.78	33.0	6.4	5.4	0.369	0.120	0.146	0.027	27.214	23.16		
10/8/2002	11:14:02 AM	25.529	25.429	18.272	19.725	19.072	6.246	34.687	1.683	4.779	23.285	22.689	26.227	0.805	0.001	0	69.78	33.2	6.4	5.5	0.380	0.120	0.146	0.026	26.428	22.49		
10/8/2002	11:15:02 AM	25.301	25.771	18.283	19.818	19.119	6.405	35.039	1.658	5.09	23.464	22.842	26.303	0.807	0.001	0	70.78	33.6	6.4	5.7	0.396	0.120	0.146	0.025	25.402	21.62		
	Averages	25.2	25.6	18.2	19.6	18.9	6.6	34.5	1.7	5.2	22.8	22.2	26.1	0.8	0.0	0.0		33.0	6.4	5.9	0.409	0.118	0.144	0.0243	24.343	20.716		
	Maximum	25.6	26.4	18.3	19.8	19.1	8.0	35.0	1.8	6.6	23.5	22.8	26.3	0.8	0.0	0.0		33.6	6.5	7.2	0.497	0.120	0.146	0.0273	27.282	23.217		
	Median	25.2	25.6	18.3	19.6	19.0	6.5	34.6	1.7	5.1	23.0	22.4	26.2	0.8	0.0	0.0		33.1	6.4	5.8	0.400	0.119	0.145	0.0249	24.882	21.175		
	Minimum	24.7	24.8	18.1	19.2	18.6	6.0	30.1	1.4	4.7	17.4	17.1	23.3	0.7	0.0	0.0		28.6	5.7	5.3	0.368	0.100	0.122	0.0171	17.080	14.535		
	2 x Std Dev	0.359	0.791	0.103	0.271	0.251	0.860	1.234	0.117	0.882	1.764	1.661	0.822	0.040	0.000	0.000		1.234	0.202	0.865	0.060	0.006	0.007	0.0042	4.151	3.533		
	Number of Points Used*	65	65	65	65	65	65	65	65	65	65	65	65	65	65	65		65	65	65	65	65	65	65	65	65		
	* Backpulse points in box are not included																											

Figure C8b: Clean 2: After AN-102R2, Batch 3C – 2 M Nitric Acid Cleaning – Second Cleaning (remaining 25 minutes) – Raw & Calculated Data

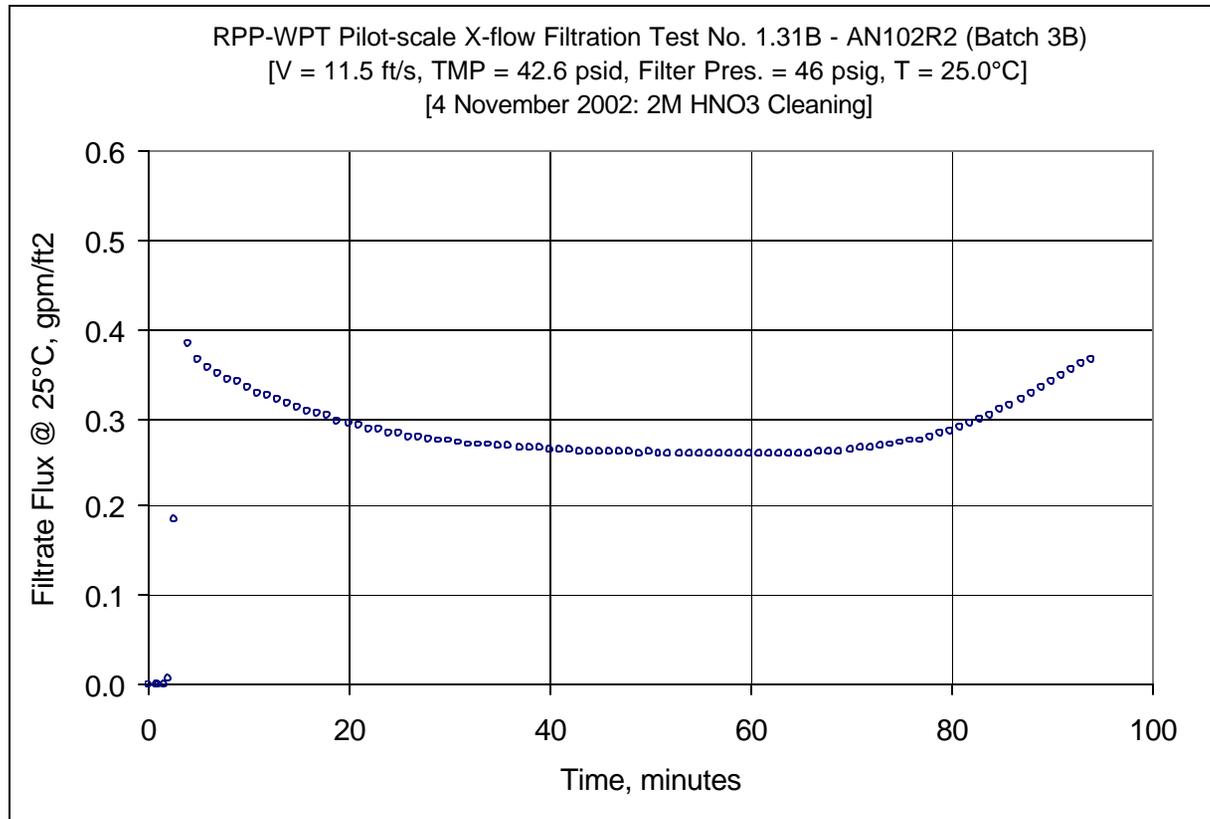


Figure C9: 1.31B: After AN-102R2, Batch 3B – 2 M Nitric Acid Cleaning – First Cleaning



11/4/2002	11:12:40 AM	26.013	19.91	25.481	21.085	21.324	44.859	47.626	4.421	41.014	-1.285	-5.098	46.721	0.001	1.77	0.001	45.87	0.76444	46.2	11.4	42.9	2.960	0.264	0.260	0.0061	6.064	5.16
11/4/2002	11:13:40 AM	26.065	19.932	25.368	21.147	21.356	45.207	48.038	4.443	41.411	-1.285	-5.092	49.289	0.001	1.768	0.002	46.87	0.78111	46.6	12.1	43.3	2.986	0.264	0.261	0.0060	6.024	5.13
11/4/2002	11:14:40 AM	26.057	19.944	25.485	21.113	21.357	45.128	47.843	4.397	41.34	-1.285	-5.096	46.791	0.001	1.771	0	47.87	0.79778	46.4	11.5	43.2	2.981	0.264	0.260	0.0060	6.025	5.13
11/4/2002	11:15:40 AM	26.044	19.961	25.477	21.146	21.395	45.168	47.709	4.366	41.54	-1.285	-5.086	46.61	0.001	1.765	0.001	48.87	0.81444	46.2	11.4	43.4	2.989	0.263	0.260	0.0060	5.989	5.10
11/4/2002	11:16:40 AM	26.086	19.983	25.394	21.188	21.417	45.174	47.913	4.376	41.514	-1.285	-5.083	46.726	0.001	1.763	0	49.87	0.83111	46.4	11.5	43.3	2.988	0.263	0.260	0.0060	5.997	5.10
11/4/2002	11:17:40 AM	26.087	20.005	25.535	21.074	21.433	45.412	48.224	4.456	41.522	-1.285	-5.078	46.828	0.001	1.765	0.001	50.87	0.84778	46.8	11.5	43.5	2.997	0.263	0.259	0.0060	5.964	5.08
11/4/2002	11:18:40 AM	26.075	20.018	25.463	21.122	21.451	45.282	47.909	4.396	41.579	-1.288	-5.078	46.696	0.001	1.76	0	51.87	0.86444	46.4	11.4	43.4	2.994	0.262	0.259	0.0060	5.964	5.08
11/4/2002	11:19:40 AM	26.106	20.034	25.409	21.173	21.483	45.199	47.986	4.399	41.456	-1.285	-5.069	46.77	0.001	1.759	0.001	52.87	0.88111	46.5	11.5	43.3	2.987	0.262	0.259	0.0060	5.984	5.09
11/4/2002	11:20:40 AM	26.097	20.055	25.565	21.144	21.504	45.097	47.783	4.442	41.28	-1.288	-5.063	46.789	0.001	1.761	0.002	53.87	0.89778	46.3	11.5	43.2	2.978	0.263	0.258	0.0060	5.983	5.09
11/4/2002	11:21:40 AM	26.105	20.073	25.458	21.131	21.536	45.164	47.847	4.407	41.393	-1.291	-5.063	46.629	0.001	1.755	0	54.87	0.91444	46.4	11.4	43.3	2.984	0.262	0.258	0.0060	5.989	5.08
11/4/2002	11:22:40 AM	26.146	20.104	25.459	21.137	21.568	45.149	48.048	4.498	41.147	-1.285	-5.054	46.757	0.001	1.758	0	55.87	0.93111	46.6	11.5	43.1	2.975	0.262	0.259	0.0060	5.997	5.10
11/4/2002	11:23:40 AM	26.117	20.111	25.58	21.089	21.579	45.166	47.611	4.4	41.365	-1.288	-5.052	46.803	0.001	1.757	0.001	56.87	0.94778	46.1	11.5	43.3	2.984	0.262	0.258	0.0060	5.955	5.07
11/4/2002	11:24:40 AM	26.128	20.132	25.466	21.226	21.606	45.042	47.642	4.394	41.293	-1.291	-5.052	46.738	0.001	1.755	0.001	57.87	0.96444	46.2	11.5	43.2	2.976	0.262	0.258	0.0060	5.983	5.09
11/4/2002	11:25:40 AM	26.16	20.158	25.503	21.227	21.632	45.263	47.92	4.438	41.395	-1.282	-5.043	46.698	0.001	1.756	0.001	58.87	0.98111	46.4	11.4	43.3	2.987	0.262	0.258	0.0060	5.957	5.07
11/4/2002	11:26:40 AM	26.136	20.17	25.604	21.294	21.654	45.474	48.495	4.476	41.546	-1.285	-5.037	46.77	0.001	1.759	0.001	59.87	0.99778	47.0	11.5	43.5	3.000	0.262	0.258	0.0059	5.926	5.04
11/4/2002	11:27:40 AM	26.162	20.197	25.48	21.376	21.665	45.325	48.218	4.424	41.46	-1.285	-5.037	46.822	0.001	1.755	0.001	60.87	1.01444	46.7	11.5	43.4	2.992	0.262	0.258	0.0059	5.949	5.06
11/4/2002	11:28:40 AM	26.184	20.213	25.547	21.352	21.692	45.168	47.841	4.41	41.391	-1.285	-5.028	46.726	0.001	1.761	0	61.87	1.03111	46.4	11.5	43.3	2.984	0.263	0.259	0.0060	5.974	5.08
11/4/2002	11:29:40 AM	26.17	20.235	25.608	21.353	21.713	45.087	47.814	4.364	41.411	-1.285	-5.026	46.703	0.001	1.762	0.001	62.87	1.04778	46.3	11.4	43.2	2.982	0.263	0.258	0.0060	5.971	5.08
11/4/2002	11:30:40 AM	26.192	20.252	25.495	21.451	21.745	45.122	47.965	4.406	41.28	-1.285	-5.023	46.759	0.001	1.764	0.001	63.87	1.06444	46.5	11.5	43.2	2.979	0.263	0.259	0.0060	6.004	5.11
11/4/2002	11:31:40 AM	26.214	20.273	25.597	21.443	21.767	45.193	47.907	4.405	41.44	-1.285	-5.017	46.78	0.001	1.772	0.001	64.87	1.08111	46.4	11.5	43.3	2.987	0.264	0.260	0.0060	5.998	5.10
11/4/2002	11:32:40 AM	26.195	20.3	25.603	21.414	21.794	45.147	47.876	4.382	41.419	-1.285	-5.014	46.675	0.001	1.77	0	65.87	1.09778	46.4	11.4	43.3	2.984	0.264	0.259	0.0060	5.994	5.10
11/4/2002	11:33:40 AM	26.222	20.327	25.51	21.486	21.81	45.004	48.004	4.434	41.08	-1.288	-5.005	46.594	0.001	1.775	0.001	66.87	1.11444	46.5	11.4	43.0	2.968	0.265	0.261	0.0061	6.061	5.16
11/4/2002	11:34:40 AM	26.214	20.334	25.627	21.432	21.827	45.385	48.112	4.394	41.657	-1.285	-5.002	46.715	0.001	1.786	0.001	67.87	1.13111	46.6	11.4	43.5	3.001	0.266	0.262	0.0060	6.012	5.12
11/4/2002	11:35:40 AM	26.205	20.371	25.613	21.424	21.849	45.017	47.839	4.366	41.395	-1.282	-4.994	46.684	0.001	1.786	0.001	68.87	1.14778	46.4	11.4	43.2	2.979	0.266	0.262	0.0061	6.058	5.16
11/4/2002	11:36:40 AM	26.242	20.383	25.525	21.446	21.871	45.042	47.961	4.368	41.233	-1.285	-4.991	46.721	0.001	1.795	0.002	69.87	1.16444	46.5	11.4	43.1	2.974	0.268	0.264	0.0061	6.113	5.20
11/4/2002	11:37:40 AM	26.219	20.395	25.662	21.412	21.888	45.01	47.969	4.433	41.121	-1.288	-4.988	46.682	0.001	1.808	0.002	70.87	1.18111	46.5	11.4	43.1	2.969	0.270	0.265	0.0061	6.144	5.23
11/4/2002	11:38:40 AM	26.21	20.421	25.583	21.519	21.899	45.12	48.025	4.419	41.348	-1.285	-4.979	46.77	0.001	1.814	0.002	71.87	1.19778	46.6	11.5	43.2	2.981	0.270	0.266	0.0062	6.154	5.24
11/4/2002	11:39:40 AM	26.241	20.433	25.53	21.546	21.936	44.998	48.067	4.407	41.164	-1.285	-4.973	46.661	0.001	1.823	0.001	72.87	1.21444	46.6	11.4	43.1	2.970	0.272	0.268	0.0062	6.216	5.29
11/4/2002	11:40:40 AM	26.233	20.465	25.686	21.503	21.943	44.963	47.994	4.338	41.286	-1.282	-4.968	46.453	0.001	1.838	0.001	73.87	1.23111	46.5	11.4	43.1	2.973	0.274	0.269	0.0062	6.233	5.30
11/4/2002	11:41:40 AM	26.234	20.476	25.568	21.539	21.964	44.733	47.808	4.417	41.016	-1.282	-4.968	46.912	0.001	1.848	0	74.87	1.24778	46.3	11.5	42.9	2.956	0.276	0.271	0.0063	6.324	5.38
11/4/2002	11:42:40 AM	26.26	20.492	25.663	21.53	21.97	44.72	47.752	4.443	40.94	-1.285	-4.956	46.721	0.001	1.865	0.001	75.87	1.26444	46.3	11.4	42.8	2.953	0.278	0.274	0.0064	6.390	5.44
11/4/2002	11:43:40 AM	26.232	20.509	25.68	21.657	22.006	44.716	48.005	4.416	40.881	-1.285	-4.953	46.69	0.001	1.883	0	76.87	1.28111	46.5	11.4	42.8	2.951	0.281	0.275	0.0064	6.435	5.48
11/4/2002	11:44:40 AM	26.237	20.529	25.535	21.587	22.012	44.756	48.16	4.438	40.969	-1.285	-4.944	46.795	0.001	1.901	0.001	77.87	1.29778	46.7	11.5	42.9	2.955	0.283	0.279	0.0065	6.514	5.54
11/4/2002	11:45:40 AM	26.259	20.541	25.572	21.539	22.024	44.213	47.568	4.356	40.525	-1.291	-4.942	46.745	0.001	1.925	0.001	78.87	1.31444	46.1	11.5	42.4	2.921	0.287	0.282	0.0067	6.666	5.67
11/4/2002	11:46:40 AM	26.235	20.568	25.663	21.504	22.07	44.443	48.019	4.443	40.65	-1.291	-4.93	46.843	0.001	1.951	0	79.87	1.33111	46.5	11.5	42.5	2.933	0.291	0.286	0.0067	6.711	5.71
11/4/2002	11:47:40 AM	26.251	20.579	25.534	21.677	22.092	44.368	47.903	4.352	40.756	-1.288	-4.918	46.732	0.001	1.974	0	80.87	1.34778	46.4	11.5	42.6	2.935	0.294	0.290	0.0068	6.812	5.80
11/4/2002	11:48:40 AM	26.272	20.605	25.636	21.658	22.103	44.109	47.86	4.363	40.484	-1.285	-4.907	46.866	0.001	2.012	0	81.87	1.36444	46.4	11.5	42.3	2.916	0.300	0.295	0.0070	6.967	5.93
11/4/2002	11:49:40 AM	26.264	20.632	25.672	21.69	22.145	44.163	48.013	4.411	40.429	-1.282	-4.895	46.791	0.001	2.039	0.002	82.87	1.38111	46.5	11.5	42.3	2.916	0.304	0.298	0.0071	7.053	6.00
11/4/2002	11:50:40 AM	26.274	20.637	25.542	21.7	22.16	44.025	47.876	4.336	40.414	-1.285	-4.892	46.914	0.001	2.068	0.001	83.87	1.39778	46.4	11.5	42.2	2.911	0.308	0.304	0.0072	7.192	6.12
11/4/2002	11:51:40 AM	26.291	20.665	25.665	21.556	22.172	44.039	48.137	4.411	40.421	-1.288	-4.887	46.872	0.001	2.115	0.001	84.87	1.41444	46.7	11.5	42.2	2.912	0.315	0.309	0.0073	7.329	6.24
11/4/2002	11:52:40 AM	26.267	20.686	25.646	21.708	22.183	43.927	48.276	4.453	40.169	-1.285	-4.872	46.862	0.001	2.148	0	85.87	1.43111	46.8	11.5	42.0	2.899	0.320	0.314	0.0075	7.479	6.36
11/4/2002	11:53:																										

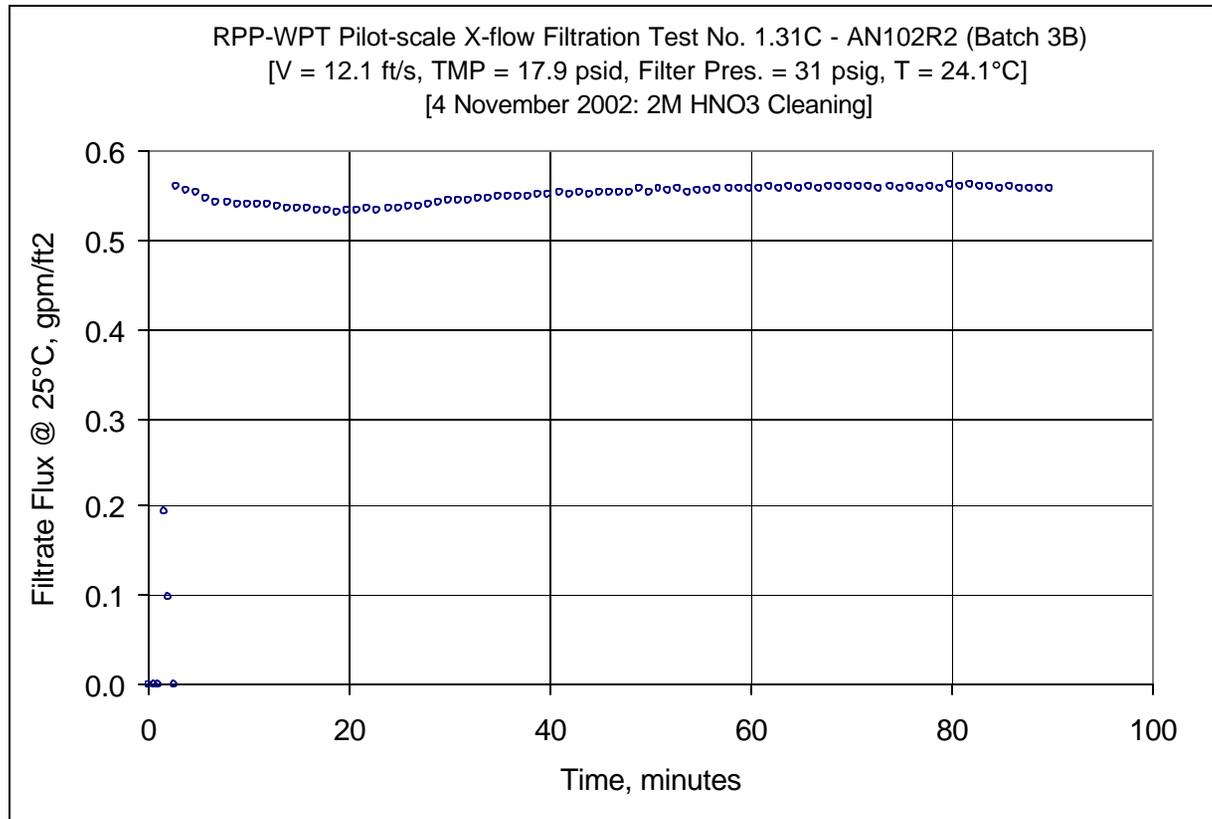


Figure C11: 1.31C: After AN-102R2, Batch 3B – 2 M Nitric Acid Cleaning – Second Cleaning



WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

11/4/2002	1:58:18 PM	25.124	19.613	24.565	20.541	17.455	19.168	31.941	4.605	16.135	6.429	-4.406	49.308	0.001	3.665	0	45.82	0.76361	30.5	12.1	17.7	1.217	0.546	0.553	0.0313	31.338	26.67
11/4/2002	1:59:18 PM	25.157	19.531	24.429	20.515	17.342	19.129	32.013	4.66	15.875	6.424	-4.409	49.253	0.002	3.658	0	46.82	0.78028	30.5	12.1	17.5	1.207	0.545	0.554	0.0317	31.667	26.95
11/4/2002	2:00:18 PM	25.116	19.423	24.577	20.483	17.214	19.067	31.864	4.637	15.906	6.49	-4.403	49.073	0.001	3.664	0	47.82	0.79694	30.4	12.0	17.5	1.206	0.546	0.553	0.0316	31.614	26.90
11/4/2002	2:01:18 PM	25.116	19.298	24.387	20.463	17.103	19.336	32.087	4.665	16.264	6.461	-4.397	49.163	0.001	3.67	0	48.82	0.81361	30.6	12.0	17.8	1.227	0.547	0.557	0.0313	31.276	26.62
11/4/2002	2:02:18 PM	25.12	19.241	24.587	20.472	17.061	19.144	31.996	4.71	15.92	6.505	-4.391	49.391	0.002	3.672	0	49.82	0.83028	30.5	12.1	17.5	1.209	0.547	0.554	0.0316	31.592	26.89
11/4/2002	2:03:18 PM	25.111	19.151	24.403	20.438	16.961	19.197	32.092	4.641	16.041	6.507	-4.391	49.253	0.001	3.673	0	50.82	0.84694	30.6	12.1	17.6	1.215	0.548	0.557	0.0316	31.609	26.90
11/4/2002	2:04:18 PM	25.131	19.096	24.603	20.398	16.946	19.113	32.04	4.633	16.01	6.548	-4.388	49.324	0.001	3.68	0	51.82	0.86361	30.6	12.1	17.6	1.211	0.549	0.555	0.0316	31.594	26.89
11/4/2002	2:05:18 PM	25.111	19.04	24.452	20.377	16.89	19.21	32.131	4.638	16.164	6.531	-4.38	49.278	0.001	3.678	0	52.82	0.88028	30.7	12.1	17.7	1.219	0.548	0.557	0.0315	31.486	26.80
11/4/2002	2:06:18 PM	25.164	19.023	24.641	20.391	17.015	19.057	31.941	4.611	15.986	6.574	-4.386	49.312	0.001	3.677	0	53.82	0.89694	30.5	12.1	17.5	1.208	0.548	0.554	0.0316	31.606	26.90
11/4/2002	2:07:18 PM	25.126	19.019	24.537	20.427	17.168	18.858	31.725	4.624	15.767	6.536	-4.374	49.236	0.001	3.682	0	54.82	0.91361	30.3	12.1	17.3	1.194	0.549	0.556	0.0321	32.125	27.34
11/4/2002	2:08:18 PM	25.145	18.953	24.596	20.411	17.076	18.939	31.889	4.591	15.865	6.536	-4.38	49.213	0.001	3.679	0	55.82	0.93028	30.4	12.1	17.4	1.201	0.549	0.555	0.0319	31.855	27.11
11/4/2002	2:09:18 PM	25.098	18.91	24.519	20.455	17.044	18.833	31.713	4.657	15.609	6.536	-4.365	49.694	0.001	3.683	0	56.82	0.94694	30.2	12.2	17.2	1.187	0.549	0.557	0.0323	32.321	27.51
11/4/2002	2:10:18 PM	25.166	18.873	24.562	20.448	16.981	19.009	32.058	4.597	15.9	6.577	-4.36	49.278	0.002	3.687	0	57.82	0.96361	30.6	12.1	17.5	1.203	0.550	0.557	0.0319	31.885	27.13
11/4/2002	2:11:18 PM	25.076	18.787	24.513	20.458	16.844	18.984	31.988	4.674	15.771	6.554	-4.36	49.287	0.002	3.683	0	58.82	0.98028	30.5	12.1	17.4	1.198	0.549	0.557	0.0320	32.035	27.26
11/4/2002	2:12:18 PM	25.146	18.711	24.467	20.438	16.697	19.094	32.123	4.689	15.927	6.583	-4.36	49.234	0.001	3.688	0	59.82	0.99694	30.7	12.1	17.5	1.207	0.550	0.558	0.0319	31.877	27.13
11/4/2002	2:13:18 PM	25.066	18.645	24.497	20.387	16.605	19.075	32.201	4.653	15.894	6.591	-4.351	49.268	0.001	3.69	0	60.82	1.01361	30.7	12.1	17.5	1.205	0.550	0.558	0.0319	31.914	27.16
11/4/2002	2:14:18 PM	25.12	18.578	24.416	20.336	16.503	19.119	32.025	4.646	16.064	6.542	-4.354	49.22	0.001	3.688	0	61.82	1.03028	30.6	12.1	17.6	1.213	0.550	0.559	0.0318	31.776	27.04
11/4/2002	2:15:18 PM	25.043	18.506	24.474	20.284	16.415	19.073	32.098	4.662	15.929	6.586	-4.354	49.234	0.001	3.688	0	62.82	1.04694	30.6	12.1	17.5	1.207	0.550	0.558	0.0319	31.888	27.14
11/4/2002	2:16:18 PM	25.138	18.46	24.409	20.273	16.369	18.967	31.885	4.61	15.935	6.597	-4.348	49.182	0.002	3.688	0	63.82	1.06361	30.4	12.1	17.5	1.203	0.550	0.559	0.0320	32.038	27.26
11/4/2002	2:17:18 PM	25.041	18.388	24.482	20.201	16.291	19.119	32.145	4.63	16.056	6.612	-4.345	49.303	0.001	3.69	0	64.82	1.08028	30.7	12.1	17.6	1.213	0.550	0.558	0.0317	31.741	27.01
11/4/2002	2:18:18 PM	25.126	18.341	24.401	20.185	16.24	18.939	31.883	4.665	15.791	6.554	-4.336	49.148	0.001	3.69	0	65.82	1.09694	30.4	12.0	17.4	1.197	0.550	0.560	0.0322	32.221	27.42
11/4/2002	2:19:18 PM	25.055	18.275	24.506	20.175	16.123	18.897	31.866	4.611	15.861	6.597	-4.336	49.289	0.001	3.691	0	66.82	1.11361	30.4	12.1	17.4	1.198	0.550	0.558	0.0321	32.109	27.32
11/4/2002	2:20:18 PM	25.11	18.204	24.381	20.155	16.052	18.901	31.878	4.578	15.81	6.588	-4.331	49.23	0.001	3.689	0	67.82	1.13028	30.4	12.1	17.4	1.197	0.550	0.560	0.0322	32.248	27.44
11/4/2002	2:21:18 PM	25.051	18.144	24.522	20.125	16.016	18.912	31.974	4.649	15.726	6.724	-4.331	49.194	0.001	3.702	0	68.82	1.14694	30.5	12.1	17.3	1.194	0.552	0.559	0.0323	32.301	27.49
11/4/2002	2:22:18 PM	25.098	18.05	24.384	20.122	15.938	18.81	31.792	4.673	15.548	6.646	-4.322	49.215	0.002	3.697	0	69.82	1.16361	30.3	12.1	17.2	1.184	0.551	0.561	0.0326	32.648	27.78
11/4/2002	2:23:18 PM	25.041	17.968	24.492	20.065	15.921	18.835	31.701	4.59	15.851	6.635	-4.319	49.014	0.001	3.701	0	70.82	1.18028	30.2	12.0	17.3	1.196	0.552	0.560	0.0323	32.275	27.47
11/4/2002	2:24:18 PM	25.104	17.945	24.379	20.027	16.009	18.833	31.891	4.57	15.738	6.666	-4.319	48.865	0.001	3.697	0	71.82	1.19694	30.4	12.0	17.3	1.192	0.551	0.561	0.0325	32.451	27.62
11/4/2002	2:25:18 PM	25.073	17.929	24.574	20.041	16.13	19.094	32.166	4.659	15.881	6.612	-4.316	49.05	0.001	3.699	0	72.82	1.21361	30.7	12.0	17.5	1.206	0.551	0.568	0.0319	31.917	27.16
11/4/2002	2:26:18 PM	25.109	17.92	24.46	20.053	16.259	18.916	31.992	4.588	15.816	6.62	-4.307	49.113	0.001	3.702	0	73.82	1.23028	30.5	12.0	17.4	1.197	0.552	0.560	0.0323	32.270	27.46
11/4/2002	2:27:18 PM	25.081	17.902	24.627	20.03	16.388	18.806	31.825	4.643	15.632	6.727	-4.307	49.177	0.001	3.704	0	74.82	1.24694	30.4	12.1	17.2	1.187	0.552	0.558	0.0324	32.410	27.58
11/4/2002	2:28:18 PM	25.082	17.877	24.458	20.036	16.358	18.909	31.976	4.624	15.798	6.718	-4.302	48.934	0.001	3.696	0	75.82	1.26361	30.5	12.0	17.4	1.196	0.551	0.560	0.0322	32.243	27.44
11/4/2002	2:29:18 PM	25.06	17.83	24.591	20.008	16.275	18.874	31.916	4.658	15.697	6.721	-4.299	49.066	0.001	3.703	0	76.82	1.28028	30.4	12.0	17.3	1.192	0.552	0.558	0.0323	32.310	27.50
11/4/2002	2:30:18 PM	25.077	17.771	24.428	19.995	16.211	18.994	32.096	4.621	15.881	6.727	-4.296	49.127	0.001	3.698	0	77.82	1.29694	30.6	12.0	17.4	1.202	0.551	0.560	0.0321	32.132	27.35
11/4/2002	2:31:18 PM	25.058	17.726	24.569	19.941	16.166	18.802	31.928	4.63	15.622	6.606	-4.299	49.146	0.001	3.701	0	78.82	1.31361	30.5	12.0	17.2	1.187	0.552	0.559	0.0325	32.450	27.62
11/4/2002	2:32:18 PM	25.076	17.698	24.421	19.953	16.138	18.854	31.908	4.566	15.812	6.695	-4.293	49.108	0.001	3.704	0	79.82	1.33028	30.4	12.0	17.3	1.195	0.552	0.561	0.0324	32.385	27.56
11/4/2002	2:33:18 PM	25.064	17.615	24.565	19.921	16.004	18.928	32.025	4.58	15.869	6.632	-4.284	49.121	0.001	3.705	0	80.82	1.34694	30.6	12.0	17.4	1.200	0.552	0.559	0.0321	32.141	27.35
11/4/2002	2:34:18 PM	25.074	17.585	24.404	19.901	16.02	18.794	31.908	4.6	15.728	6.727	-4.284	49.295	0.001	3.705	0	81.82	1.36361	30.4	12.1	17.3	1.190	0.552	0.562	0.0325	32.544	27.70
11/4/2002	2:35:18 PM	25.096	17.547	24.597	19.867	16.001	18.705	31.897	4.547	15.636	6.802	-4.284	49.117	0.001	3.707	0	82.82	1.38028	30.4	12.0	17.2	1.184	0.553	0.559	0.0326	32.566	27.71
11/4/2002	2:36:18 PM	25.079	17.524	24.43	19.876	16.025	18.876	31.881	4.605	15.812	6.646	-4.276	49.115	0.001	3.702	0	83.82	1.39694	30.4	12.0	17.3	1.196	0.552	0.561	0.0323	32.339	27.52
11/4/2002	2:37:18 PM	25.12	17.526	24.646	19.923	16.143	18.963	32.17	4.611	15.853	6.785	-4.273	49.1	0.001	3.709	0	84.82	1.41361	30.7	12.0	17.4	1.200	0.553	0.559	0.0321	32.084	27.30
11/4/2002	2:38:18 PM	25.098	17.528	24.508	19.94	16.308	18.957	31.938	4.654	15.808	6.658	-4.267	49.177	0.001	3.701	0	85.82	1.43028	30.5	12.1	17.4	1.198	0.552	0.559	0.0322	32.187	27.39
11/4/2002	2:39:18 PM	25.142	17.538	24.698	19.959	16.51	19.075	32.265																			

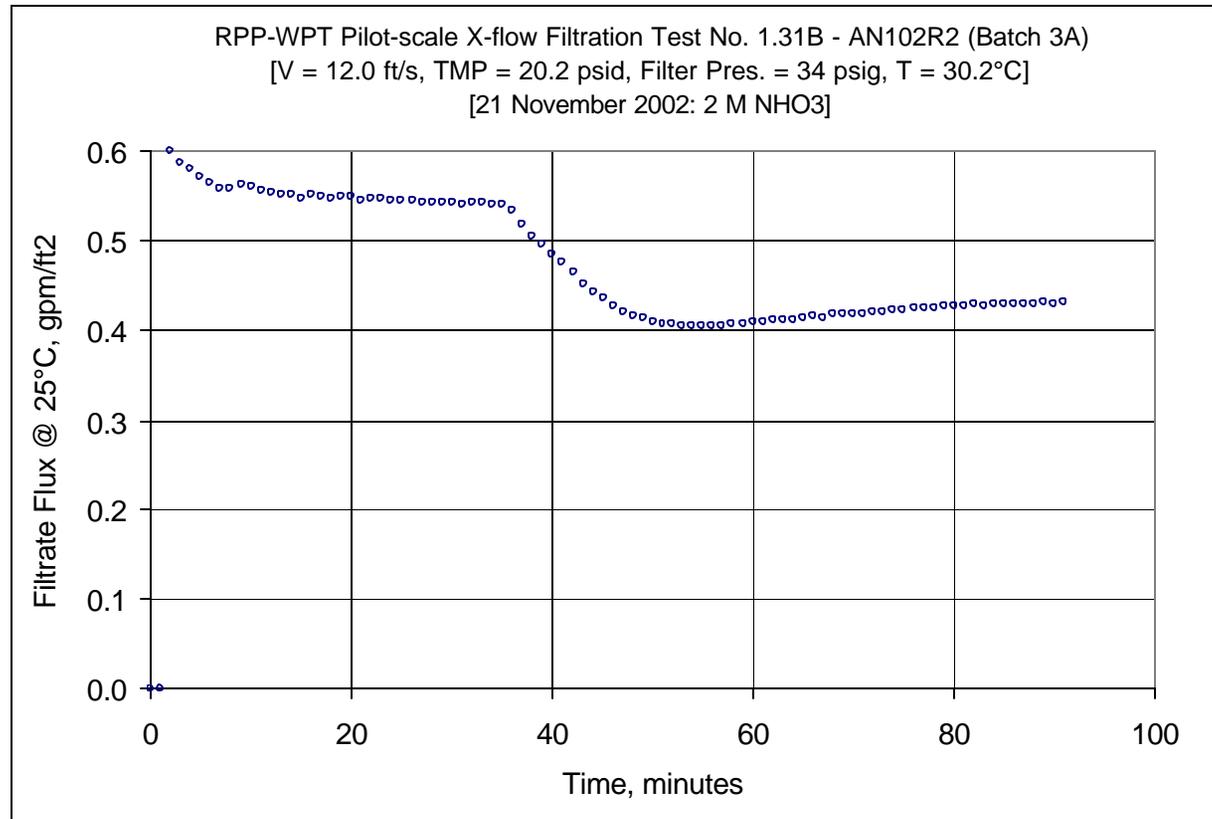


Figure C13: 1.31B: After AN-102R2, Batch 3A – 2 M Nitric Acid Cleaning – First Cleaning



11/21/2002	2:09:21 PM	30.757	22.511	30.375	23.329	23.307	24.845	35.523	4.633	21.819	4.127	1.158	48.923	0.001	3.32	0	46.00	0.76667	34.1	12.0	23.3	1.609	0.495	0.427	0.0183	18.285	15.56
11/21/2002	2:10:21 PM	30.719	22.533	30.491	23.296	23.294	25.021	35.48	4.561	21.907	3.968	1.155	48.866	0.001	3.268	0.001	47.00	0.78333	34.0	12.0	23.5	1.618	0.490	0.421	0.0179	17.950	15.28
11/21/2002	2:11:21 PM	30.708	22.562	30.415	23.289	23.312	25.102	35.453	4.622	21.913	3.679	1.152	48.923	0.001	3.243	0	48.00	0.8	34.0	12.0	23.5	1.621	0.484	0.416	0.0177	17.708	15.07
11/21/2002	2:12:21 PM	30.76	22.59	30.378	23.342	23.335	25.524	35.744	4.677	22.239	3.468	1.149	48.801	0.001	3.214	0	49.00	0.81667	34.3	12.0	23.9	1.647	0.479	0.413	0.0173	17.292	14.72
11/21/2002	2:13:21 PM	30.753	22.598	30.53	23.37	23.364	25.373	35.358	4.584	22.175	3.442	1.146	48.808	0.001	3.195	0	50.00	0.83333	33.9	12.0	23.8	1.639	0.476	0.409	0.0172	17.197	14.63
11/21/2002	2:14:21 PM	30.731	22.611	30.468	23.388	23.386	25.794	35.811	4.683	22.411	3.344	1.143	48.585	0.001	3.178	0	51.00	0.85	34.3	11.9	24.1	1.662	0.474	0.407	0.0169	16.900	14.38
11/21/2002	2:15:21 PM	30.789	22.644	30.432	23.507	23.425	25.932	35.747	4.694	22.581	3.303	1.146	48.701	0.001	3.171	0.001	52.00	0.86667	34.3	11.9	24.3	1.672	0.473	0.407	0.0168	16.772	14.27
11/21/2002	2:16:21 PM	30.821	22.667	30.534	23.51	23.448	25.864	35.682	4.668	22.652	3.249	1.14	48.791	0.001	3.168	0	53.00	0.88333	34.2	12.0	24.3	1.673	0.472	0.405	0.0167	16.709	14.22
11/21/2002	2:17:21 PM	30.8	22.69	30.567	23.528	23.496	25.665	35.411	4.661	22.439	3.202	1.146	48.77	0.001	3.165	0.001	54.00	0.9	33.9	12.0	24.1	1.658	0.472	0.405	0.0168	16.821	14.32
11/21/2002	2:18:21 PM	30.827	22.708	30.49	23.566	23.509	26.005	35.705	4.676	22.691	3.254	1.146	48.73	0.002	3.161	0.001	55.00	0.91667	34.2	11.9	24.3	1.679	0.471	0.405	0.0166	16.631	14.15
11/21/2002	2:19:21 PM	30.865	22.726	30.508	23.599	23.522	25.535	35.19	4.591	22.407	3.301	1.146	48.703	0.001	3.17	0.001	56.00	0.93333	33.7	11.9	24.0	1.653	0.473	0.406	0.0169	16.932	14.41
11/21/2002	2:20:21 PM	30.831	22.742	30.608	23.589	23.532	25.68	35.544	4.643	22.468	3.315	1.149	48.789	0.001	3.17	0	57.00	0.95	34.1	12.0	24.1	1.660	0.473	0.405	0.0168	16.814	14.31
11/21/2002	2:21:21 PM	30.836	22.747	30.509	23.56	23.513	25.711	35.455	4.625	22.564	3.37	1.143	48.732	0.001	3.178	0.001	58.00	0.96667	34.0	11.9	24.1	1.664	0.474	0.407	0.0169	16.857	14.35
11/21/2002	2:22:21 PM	30.875	22.756	30.473	23.443	23.482	25.663	35.432	4.623	22.581	3.341	1.146	48.768	0.001	3.184	0.001	59.00	0.98333	34.0	12.0	24.1	1.663	0.475	0.408	0.0169	16.916	14.40
11/21/2002	2:23:21 PM	30.86	22.771	30.617	23.338	23.471	25.514	35.676	4.63	22.269	3.445	1.149	48.663	0.001	3.2	0	60.00	1	34.2	11.9	23.9	1.647	0.477	0.409	0.0171	17.098	14.55
11/21/2002	2:24:21 PM	30.837	22.769	30.53	23.209	23.419	25.402	35.362	4.556	22.329	3.457	1.146	48.789	0.002	3.195	0	61.00	1.01667	33.9	12.0	23.9	1.645	0.476	0.409	0.0171	17.131	14.58
11/21/2002	2:25:21 PM	30.865	22.767	30.454	23.137	23.396	25.406	35.291	4.624	22.241	3.468	1.143	48.755	0.001	3.206	0.001	62.00	1.03333	33.8	11.9	23.8	1.643	0.478	0.411	0.0173	17.255	14.68
11/21/2002	2:26:21 PM	30.882	22.784	30.595	23.084	23.364	25.381	35.554	4.624	22.159	3.598	1.152	48.806	0.002	3.226	0	63.00	1.05	34.1	12.0	23.8	1.639	0.481	0.412	0.0173	17.336	14.75
11/21/2002	2:27:21 PM	30.85	22.781	30.562	23.041	23.326	25.359	35.535	4.716	22.018	3.506	1.149	48.776	0.001	3.224	0.001	64.00	1.06667	34.1	12.0	23.7	1.633	0.481	0.412	0.0174	17.400	14.81
11/21/2002	2:28:21 PM	30.876	22.778	30.47	23.018	23.327	25.294	35.411	4.617	22.118	3.645	1.146	48.715	0.001	3.23	0	65.00	1.08333	33.9	11.9	23.7	1.634	0.482	0.414	0.0175	17.463	14.86
11/21/2002	2:29:21 PM	30.884	22.781	30.522	23.016	23.33	25.236	35.449	4.569	22.108	3.751	1.149	48.692	0.001	3.246	0	66.00	1.1	34.0	11.9	23.7	1.632	0.484	0.415	0.0176	17.550	14.94
11/21/2002	2:30:21 PM	30.858	22.784	30.585	23.064	23.344	25.11	35.43	4.599	21.942	3.749	1.149	48.833	0.002	3.249	0	67.00	1.11667	34.0	12.0	23.5	1.622	0.484	0.415	0.0176	17.645	15.02
11/21/2002	2:31:21 PM	30.851	22.783	30.474	23.148	23.347	25.332	35.701	4.685	22.145	3.778	1.152	49.491	0.001	3.259	0.002	68.00	1.13333	34.2	12.1	23.7	1.637	0.486	0.418	0.0176	17.594	14.97
11/21/2002	2:32:21 PM	30.885	22.792	30.479	23.203	23.387	25.06	35.345	4.598	21.997	3.858	1.155	48.785	0.001	3.265	0.001	69.00	1.15	33.9	12.0	23.5	1.622	0.487	0.418	0.0178	17.781	15.13
11/21/2002	2:33:21 PM	30.861	22.808	30.618	23.218	23.397	25.317	35.823	4.637	22.102	3.83	1.155	48.921	0.001	3.271	0	70.00	1.16667	34.4	12.0	23.7	1.635	0.488	0.418	0.0176	17.611	14.99
11/21/2002	2:34:21 PM	30.866	22.828	30.539	23.289	23.412	24.893	35.335	4.61	21.809	3.879	1.155	49.095	0.002	3.276	0.001	71.00	1.18333	33.9	12.0	23.4	1.610	0.488	0.419	0.0179	17.948	15.27
11/21/2002	2:35:21 PM	30.887	22.818	30.47	23.299	23.448	25.114	35.769	4.664	21.932	4.003	1.155	48.74	0.002	3.289	0	72.00	1.2	34.3	11.9	23.5	1.622	0.490	0.422	0.0179	17.921	15.25
11/21/2002	2:36:21 PM	30.877	22.829	30.615	23.32	23.454	24.93	35.492	4.643	21.741	3.98	1.158	48.862	0.002	3.3	0	73.00	1.21667	34.0	12.0	23.3	1.609	0.492	0.421	0.0181	18.054	15.36
11/21/2002	2:37:21 PM	30.86	22.847	30.573	23.373	23.497	24.772	35.393	4.58	21.684	4.11	1.155	48.875	0.001	3.309	0	74.00	1.23333	33.9	12.0	23.2	1.601	0.493	0.423	0.0182	18.208	15.49
11/21/2002	2:38:21 PM	30.881	22.853	30.489	23.434	23.523	24.704	35.138	4.542	21.79	4.087	1.158	48.589	0.001	3.308	0	75.00	1.25	33.7	11.9	23.2	1.603	0.493	0.424	0.0182	18.229	15.51
11/21/2002	2:39:21 PM	30.882	22.844	30.54	23.455	23.554	24.959	35.713	4.682	21.809	4.121	1.158	48.948	0.001	3.319	0	76.00	1.26667	34.2	12.0	23.4	1.612	0.495	0.425	0.0182	18.157	15.45
11/21/2002	2:40:21 PM	30.859	22.876	30.602	23.588	23.601	24.799	35.544	4.706	21.52	4.119	1.163	48.948	0.001	3.328	0.002	77.00	1.28333	34.1	12.0	23.2	1.597	0.496	0.425	0.0184	18.352	15.62
11/21/2002	2:41:21 PM	30.87	22.877	30.514	23.589	23.638	24.543	35.223	4.65	21.383	4.185	1.161	48.889	0.001	3.324	0.001	78.00	1.3	33.8	12.0	23.0	1.583	0.496	0.426	0.0185	18.531	15.77
11/21/2002	2:42:21 PM	30.916	22.899	30.525	23.596	23.654	24.644	35.48	4.663	21.541	4.295	1.163	48.908	0.002	3.338	0.001	79.00	1.31667	34.0	12.0	23.1	1.592	0.498	0.427	0.0185	18.499	15.74
11/21/2002	2:43:21 PM	30.878	22.905	30.65	23.552	23.681	24.64	35.533	4.647	21.573	4.33	1.163	48.915	0.001	3.346	0	80.00	1.33333	34.1	12.0	23.1	1.593	0.499	0.427	0.0185	18.469	15.72
11/21/2002	2:44:21 PM	30.886	22.928	30.573	23.645	23.708	24.76	35.72	4.634	21.641	4.298	1.163	48.927	0.001	3.346	0.001	81.00	1.35	34.2	12.0	23.2	1.600	0.499	0.428	0.0184	18.433	15.69
11/21/2002	2:45:21 PM	30.902	22.934	30.5	23.611	23.72	24.439	35.269	4.608	21.379	4.338	1.163	48.906	0.001	3.348	0.002	82.00	1.36667	33.8	12.0	22.9	1.579	0.499	0.429	0.0187	18.716	15.93
11/21/2002	2:46:21 PM	30.905	22.952	30.642	23.609	23.742	24.81	35.747	4.649	21.653	4.358	1.166	48.843	0.001	3.358	0	83.00	1.38333	34.3	12.0	23.2	1.602	0.501	0.428	0.0184	18.440	15.69
11/21/2002	2:47:21 PM	30.882	22.979	30.629	23.606	23.77	24.582	35.488	4.653	21.5	4.361	1.169	48.915	0.002	3.359	0	84.00	1.4	34.0	12.0	23.0	1.589	0.501	0.429	0.0186	18.604	15.83
11/21/2002	2:48:21 PM	30.899	22.986	30.537	23.603	23.797	24.628	35.556	4.645	21.565	4.376	1.169	48.894	0.001	3.358	0	85.00	1.41667	34.1	12.0	23.1	1.592	0.501	0.430	0.0186	18.601	15.83
11/21/2002	2:49:21 PM	30.926	22.998	30.598	23.575	23.814	24.259	35.113	4.557	21.273	4.434	1.166	48.912	0.001	3.363	0	86.00	1.43333	33.6	12.0	22.8	1.570	0.501	0.430	0.0189	18.867	16.06
11/21/2002	2:50:21 PM	30.889	23.01																								

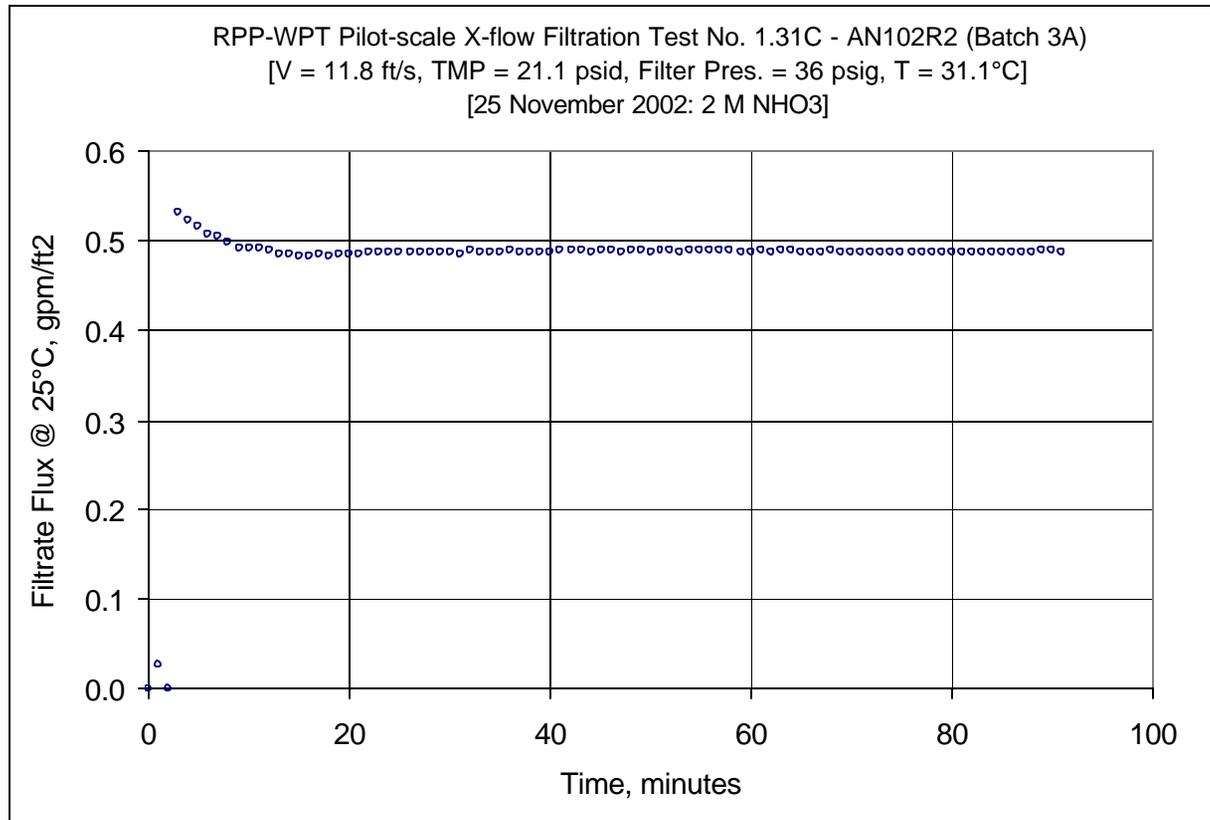


Figure C15: 1.31C: After AN-102R2, Batch 3A – 2 M Nitric Acid Cleaning – Second Cleaning



11/25/2002	9:25:33 AM	31.081	19.362	30.841	21.469	20.278	23.435	37.373	4.477	20.667	7.37	-2.966	48.048	0.001	3.853	0	46.00	0.76667	35.9	11.8	22.1	1.520	0.574	0.489	0.0222	22.171	18.87
11/25/2002	9:26:33 AM	31.05	19.401	30.92	21.463	20.307	23.497	37.422	4.473	20.642	7.292	-2.96	48.239	0.002	3.844	0	47.00	0.78333	36.0	11.8	22.1	1.522	0.573	0.487	0.0221	22.053	18.77
11/25/2002	9:27:33 AM	31.053	19.41	30.794	21.431	20.34	23.227	36.992	4.333	20.593	7.336	-2.963	48.214	0.002	3.85	0	48.00	0.8	35.5	11.8	21.9	1.511	0.574	0.489	0.0223	22.325	19.00
11/25/2002	9:28:33 AM	31.116	19.449	30.857	21.374	20.359	23.364	37.246	4.489	20.575	7.379	-2.957	48.277	0.002	3.852	0	49.00	0.81667	35.8	11.8	22.0	1.515	0.574	0.489	0.0222	22.238	18.92
11/25/2002	9:29:33 AM	31.06	19.457	30.934	21.322	20.383	23.2	37.102	4.411	20.488	7.445	-2.96	48.218	0.002	3.856	0	50.00	0.83333	35.6	11.8	21.8	1.506	0.575	0.488	0.0223	22.342	19.01
11/25/2002	9:30:33 AM	31.052	19.465	30.803	21.294	20.411	23.316	37.265	4.423	20.603	7.339	-2.957	48.122	0.002	3.853	0	51.00	0.85	35.8	11.8	22.0	1.514	0.574	0.489	0.0223	22.286	18.97
11/25/2002	9:31:33 AM	31.115	19.492	30.811	21.211	20.413	23.329	37.25	4.448	20.566	7.373	-2.957	48.224	0.001	3.851	0	52.00	0.86667	35.8	11.8	21.9	1.513	0.574	0.489	0.0223	22.282	18.96
11/25/2002	9:32:33 AM	31.053	19.495	30.927	21.229	20.431	23.151	37.151	4.387	20.484	7.48	-2.957	48.139	0.001	3.856	0	53.00	0.88333	35.7	11.8	21.8	1.504	0.575	0.488	0.0224	22.373	19.04
11/25/2002	9:33:33 AM	31.051	19.508	30.807	21.182	20.449	23.091	37.04	4.405	20.364	7.365	-2.954	48.189	0.001	3.856	0	54.00	0.9	35.6	11.8	21.7	1.498	0.575	0.490	0.0225	22.539	19.18
11/25/2002	9:34:33 AM	31.113	19.536	30.799	21.149	20.487	23.196	37.19	4.453	20.4	7.336	-2.954	48.214	0.002	3.85	0	55.00	0.91667	35.7	11.8	21.8	1.503	0.574	0.489	0.0224	22.436	19.09
11/25/2002	9:35:33 AM	31.097	19.559	30.96	21.131	20.499	23.178	37.1	4.335	20.531	7.431	-2.951	48.151	0.002	3.86	0	56.00	0.93333	35.6	11.8	21.9	1.507	0.575	0.488	0.0223	22.339	19.01
11/25/2002	9:36:33 AM	31.063	19.556	30.843	21.108	20.512	23.335	37.265	4.444	20.64	7.307	-2.951	48.195	0.002	3.853	0	57.00	0.95	35.8	11.8	22.0	1.516	0.574	0.489	0.0222	22.234	18.92
11/25/2002	9:37:33 AM	31.11	19.564	30.761	21.03	20.509	23.337	37.251	4.487	20.546	7.307	-2.951	48.386	0.001	3.843	0	58.00	0.96667	35.8	11.9	21.9	1.513	0.573	0.489	0.0223	22.272	18.95
11/25/2002	9:38:33 AM	31.097	19.586	30.952	21.058	20.542	23.124	36.998	4.433	20.417	7.341	-2.951	48.376	0.002	3.85	0	59.00	0.98333	35.5	11.9	21.8	1.501	0.574	0.487	0.0224	22.372	19.04
11/25/2002	9:39:33 AM	31.07	19.598	30.865	21.009	20.499	23.348	37.323	4.466	20.64	7.321	-2.951	48.245	0.001	3.847	0	60.00	1	35.9	11.8	22.0	1.516	0.574	0.489	0.0222	22.179	18.87
11/25/2002	9:40:33 AM	31.127	19.621	30.803	20.992	20.582	23.43	37.296	4.486	20.665	7.312	-2.951	48.373	0.001	3.847	0	61.00	1.01667	35.8	11.9	22.0	1.520	0.574	0.488	0.0222	22.186	18.88
11/25/2002	9:41:33 AM	31.104	19.623	30.934	20.988	20.578	23.341	37.18	4.445	20.638	7.281	-2.945	48.357	0.001	3.849	0	62.00	1.03333	35.7	11.9	22.0	1.516	0.574	0.487	0.0222	22.154	18.85
11/25/2002	9:42:33 AM	31.076	19.63	30.876	21.016	20.555	23.29	37.294	4.462	20.46	7.339	-2.948	48.222	0.002	3.852	0	63.00	1.05	35.8	11.8	21.9	1.508	0.574	0.488	0.0223	22.322	19.00
11/25/2002	9:43:33 AM	31.102	19.642	30.784	20.982	20.547	23.294	37.188	4.47	20.501	7.336	-2.945	48.166	0.001	3.845	0	64.00	1.06667	35.7	11.8	21.9	1.510	0.573	0.489	0.0223	22.314	18.99
11/25/2002	9:44:33 AM	31.129	19.664	30.915	21.005	20.569	23.095	36.762	4.413	20.433	7.26	-2.942	48.522	0.001	3.847	0	65.00	1.08333	35.3	11.9	21.8	1.501	0.574	0.487	0.0224	22.383	19.05
11/25/2002	9:45:33 AM	31.087	19.676	30.902	20.981	20.546	23.093	37.023	4.451	20.302	7.344	-2.942	48.527	0.002	3.847	0	66.00	1.1	35.6	11.9	21.7	1.496	0.574	0.487	0.0225	22.460	19.11
11/25/2002	9:46:33 AM	31.113	19.688	30.814	20.973	20.548	23.325	37.199	4.401	20.652	7.35	-2.942	48.388	0.002	3.843	0	67.00	1.11667	35.7	11.9	22.0	1.516	0.573	0.488	0.0222	22.192	18.89
11/25/2002	9:47:33 AM	31.13	19.695	30.886	20.985	20.58	23.209	37.18	4.482	20.319	7.333	-2.94	48.262	0.002	3.854	0	68.00	1.13333	35.7	11.8	21.8	1.501	0.575	0.488	0.0224	22.442	19.10
11/25/2002	9:48:33 AM	31.092	19.717	30.932	21.012	20.567	23.076	36.911	4.432	20.294	7.289	-2.94	48.525	0.002	3.841	0	69.00	1.15	35.4	11.9	21.7	1.495	0.573	0.486	0.0224	22.420	19.08
11/25/2002	9:49:33 AM	31.109	19.734	30.83	21.049	20.584	23.397	37.182	4.48	20.642	7.272	-2.94	48.355	0.002	3.842	0	70.00	1.16667	35.7	11.9	22.0	1.518	0.573	0.488	0.0221	22.146	18.85
11/25/2002	9:50:33 AM	31.145	19.751	30.876	21.015	20.57	23.221	37.097	4.455	20.421	7.304	-2.94	48.191	0.001	3.845	0	71.00	1.18333	35.6	11.8	21.8	1.504	0.573	0.487	0.0223	22.337	19.01
11/25/2002	9:51:33 AM	31.097	19.757	30.937	21.007	20.597	23.318	37.172	4.451	20.558	7.281	-2.94	48.273	0.001	3.846	0	72.00	1.2	35.7	11.8	21.9	1.513	0.573	0.487	0.0222	22.187	18.88
11/25/2002	9:52:33 AM	31.123	19.799	30.859	21.034	20.599	23.194	36.998	4.437	20.46	7.275	-2.94	48.535	0.001	3.838	0	73.00	1.21667	35.5	11.9	21.8	1.505	0.572	0.487	0.0223	22.300	18.98
11/25/2002	9:53:33 AM	31.145	19.806	30.846	21.005	20.631	23.401	37.147	4.47	20.705	7.272	-2.94	48.269	0.001	3.842	0	74.00	1.23333	35.7	11.8	22.1	1.520	0.573	0.487	0.0221	22.103	18.81
11/25/2002	9:54:33 AM	31.102	19.823	30.962	21.017	20.657	23.153	36.984	4.43	20.409	7.35	-2.94	48.413	0.001	3.849	0	75.00	1.25	35.5	11.9	21.8	1.502	0.574	0.487	0.0223	22.349	19.02
11/25/2002	9:55:33 AM	31.104	19.85	30.845	21.029	20.69	23.377	37.265	4.416	20.744	7.278	-2.942	48.275	0.001	3.845	0	76.00	1.26667	35.8	11.8	22.1	1.521	0.573	0.488	0.0221	22.113	18.82
11/25/2002	9:56:33 AM	31.161	19.888	30.857	21.062	20.712	23.134	37.075	4.437	20.4	7.321	-2.934	48.426	0.002	3.84	0	77.00	1.28333	35.6	11.9	21.8	1.501	0.573	0.487	0.0224	22.375	19.04
11/25/2002	9:57:33 AM	31.113	19.889	30.968	21.058	20.729	23.213	37.069	4.469	20.415	7.298	-2.94	48.17	0.002	3.85	0	78.00	1.3	35.6	11.8	21.8	1.504	0.574	0.487	0.0223	22.317	18.99
11/25/2002	9:58:33 AM	31.095	19.917	30.871	21.065	20.716	23.318	36.953	4.393	20.705	7.269	-2.937	48.311	0.002	3.842	0	79.00	1.31667	35.5	11.8	22.0	1.518	0.573	0.487	0.0221	22.129	18.83
11/25/2002	9:59:33 AM	31.146	19.934	30.803	21.057	20.738	23.416	37.22	4.461	20.667	7.203	-2.94	48.375	0.002	3.839	0	80.00	1.33333	35.7	11.9	22.0	1.520	0.572	0.488	0.0221	22.123	18.83
11/25/2002	10:00:33 AM	31.124	19.966	30.979	21.074	20.75	23.31	37.052	4.445	20.568	7.312	-2.934	48.334	0.002	3.846	0	81.00	1.35	35.6	11.8	21.9	1.513	0.573	0.486	0.0222	22.161	18.86
11/25/2002	10:01:33 AM	31.1	19.973	30.891	21.111	20.747	23.225	37.155	4.491	20.427	7.333	-2.937	48.229	0.001	3.847	0	82.00	1.36667	35.7	11.8	21.8	1.505	0.574	0.487	0.0223	22.334	19.01
11/25/2002	10:02:33 AM	31.142	19.985	30.818	21.138	20.769	23.159	36.948	4.445	20.39	7.249	-2.937	48.285	0.002	3.842	0	83.00	1.38333	35.5	11.8	21.8	1.501	0.573	0.488	0.0224	22.402	19.06
11/25/2002	10:03:33 AM	31.129	20.012	30.964	21.12	20.811	23.412	37.404	4.493	20.624	7.301	-2.937	48.327	0.001	3.847	0	84.00	1.4	35.9	11.8	22.0	1.518	0.574	0.487	0.0221	22.096	18.80
11/25/2002	10:04:33 AM	31.09	20.023	30.896	21.096	20.812	23.151	37.023	4.422	20.392	7.298	-2.931	48.355	0.002	3.843	0	85.00	1.41667	35.6	11.9	21.8	1.501	0.573	0.487	0.0224	22.364	19.03
11/25/2002	10:05:33 AM	31.131	20.044	30.812	21.087	20.823	23.327	37.267	4.498	20.488	7.234	-2.937	48.352	0.002	3.843	0	86.00	1.43333	35.8	11.8	21.9	1.510	0.573	0.488	0.0223	22.276	18.96
11/25/2002	10:06:33 AM	31.142	20.061	30.933	21.068	20.84	23.337	37.222	4.5	20																	

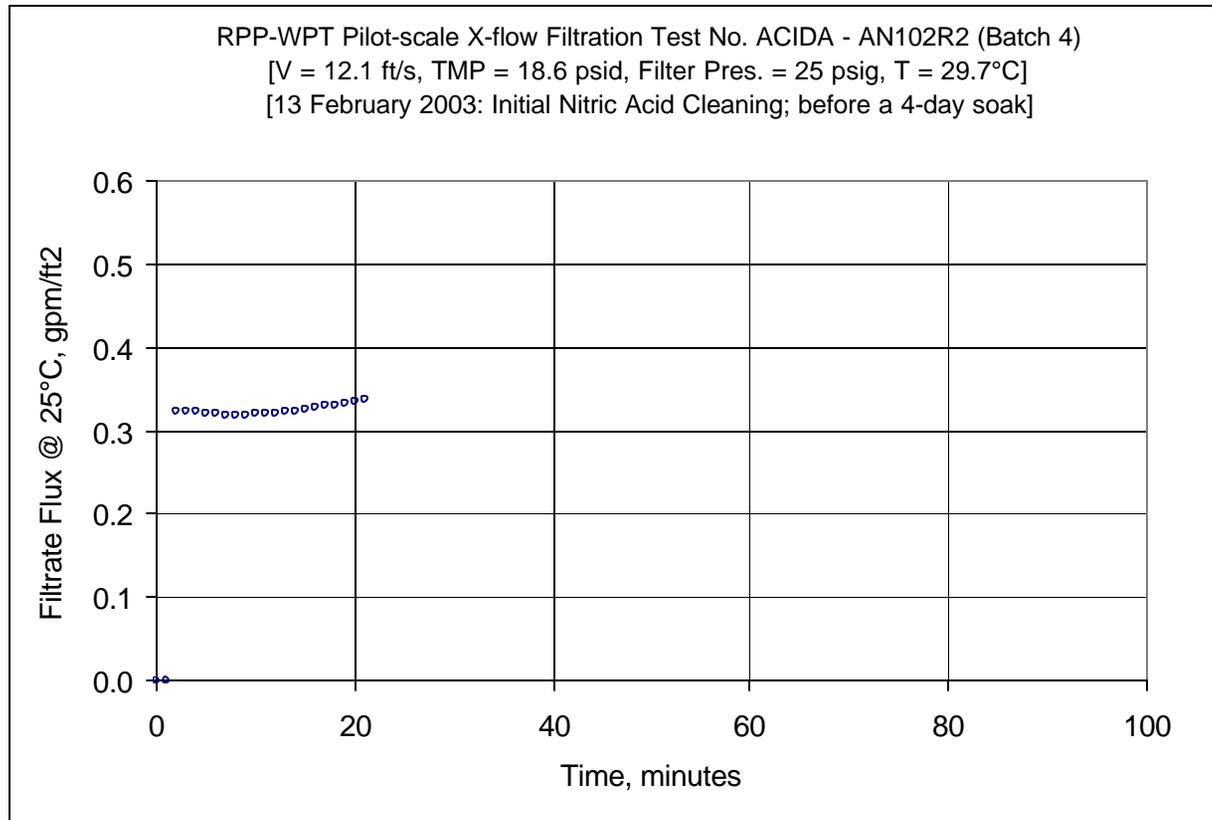


Figure C17: ACIDA: Before AN-102R2, Batch 4 – 2 M Nitric Acid Cleaning – First 20 minutes of a 4-day soak



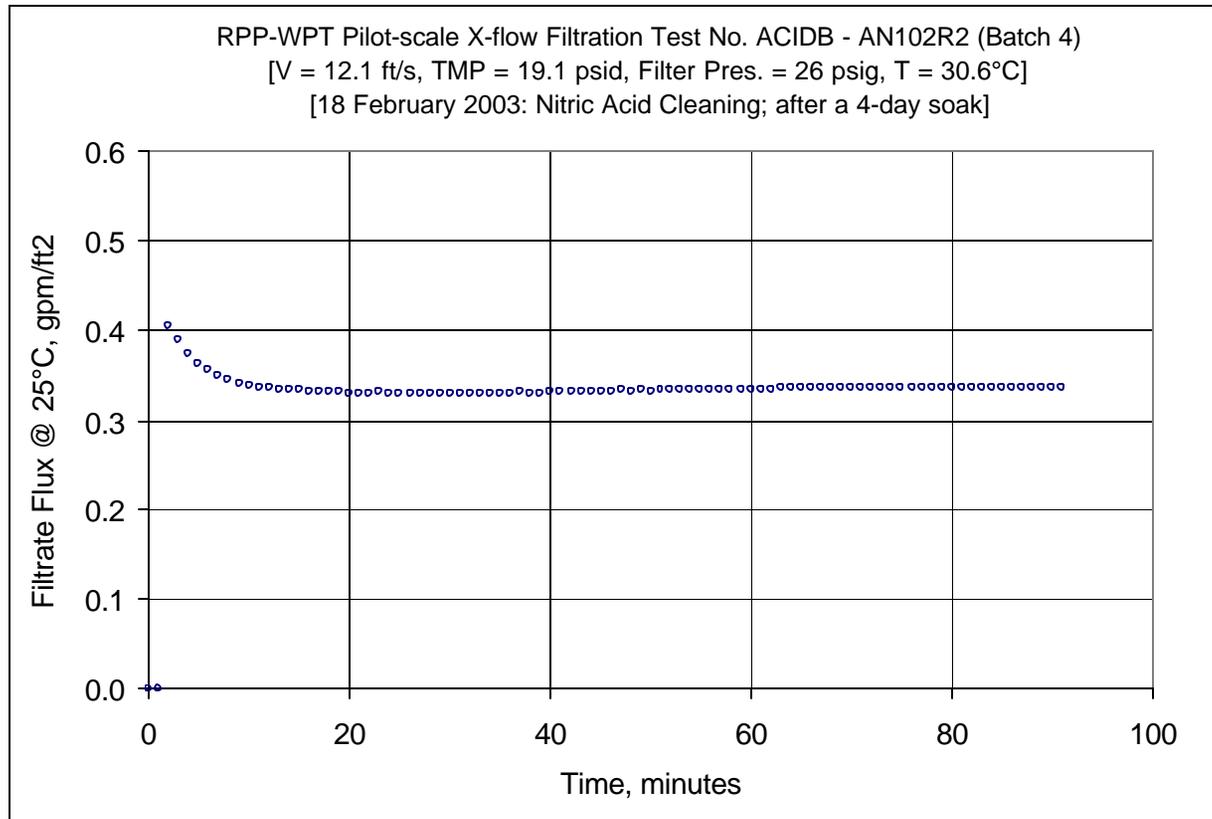


Figure C19: ACIDB: Before AN-102R2, Batch 4 – 2 M Nitric Acid Cleaning – Last 90 minutes of a 4-day soak



WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

2/18/2003	9:24:21 AM	31.034	18.266	30.72	20.886	18.95	21.167	27.354	4.669	17.466	0.472	0.849	49.226	0.001	2.616	0	46.00	0.76667	25.9	12.1	19.3	1.332	0.390	0.333	0.0172	17.240	14.67
2/18/2003	9:25:21 AM	31.011	18.288	30.673	20.924	18.962	21.01	27.207	4.637	17.186	0.412	0.852	49.263	0.001	2.616	0.001	47.00	0.78333	25.7	12.1	19.1	1.317	0.390	0.333	0.0175	17.460	14.86
2/18/2003	9:26:21 AM	30.969	18.305	30.65	20.916	18.974	21.111	27.286	4.669	17.29	0.426	0.849	49.398	0.001	2.612	0	48.00	0.8	25.8	12.1	19.2	1.324	0.390	0.333	0.0174	17.351	14.77
2/18/2003	9:27:21 AM	30.917	18.313	30.672	20.949	18.997	21.049	27.209	4.663	17.274	0.478	0.849	49.067	0.001	2.615	0.002	49.00	0.81667	25.7	12.0	19.2	1.321	0.390	0.333	0.0174	17.396	14.80
2/18/2003	9:28:21 AM	30.869	18.32	30.664	20.95	19.019	21.08	27.267	4.676	17.243	0.414	0.852	49.308	0.001	2.61	0	50.00	0.83333	25.8	12.1	19.2	1.321	0.389	0.333	0.0174	17.366	14.78
2/18/2003	9:29:21 AM	30.84	18.336	30.606	20.982	19.015	21.068	27.203	4.66	17.241	0.412	0.855	49.406	0.001	2.61	0.001	51.00	0.85	25.7	12.1	19.2	1.321	0.389	0.333	0.0174	17.400	14.81
2/18/2003	9:30:21 AM	30.817	18.338	30.533	20.949	19.027	21.093	27.275	4.612	17.317	0.412	0.852	49.404	0.001	2.612	0	52.00	0.86667	25.8	12.1	19.2	1.324	0.389	0.334	0.0174	17.402	14.81
2/18/2003	9:31:21 AM	30.805	18.345	30.506	20.956	19.04	21.105	27.185	4.604	17.4	0.409	0.852	49.406	0.001	2.611	0.001	53.00	0.88333	25.7	12.1	19.3	1.327	0.389	0.334	0.0174	17.365	14.78
2/18/2003	9:32:21 AM	30.791	18.352	30.502	20.937	19.041	21.136	27.327	4.582	17.36	0.409	0.852	49.262	0.001	2.613	0.001	54.00	0.9	25.9	12.1	19.2	1.327	0.390	0.335	0.0174	17.384	14.79
2/18/2003	9:33:21 AM	30.768	18.364	30.564	20.964	19.078	20.966	27.098	4.584	17.278	0.481	0.849	49.383	0.001	2.613	0.001	55.00	0.91667	25.6	12.1	19.1	1.318	0.390	0.334	0.0175	17.469	14.87
2/18/2003	9:34:21 AM	30.745	18.371	30.531	20.936	19.085	21.153	27.313	4.671	17.278	0.423	0.849	49.337	0.001	2.611	0.002	56.00	0.93333	25.8	12.1	19.2	1.325	0.389	0.334	0.0174	17.387	14.80
2/18/2003	9:35:21 AM	30.733	18.389	30.484	20.933	19.108	21.111	27.253	4.595	17.392	0.403	0.849	49.287	0.001	2.61	0.001	57.00	0.95	25.8	12.1	19.3	1.327	0.389	0.334	0.0174	17.370	14.78
2/18/2003	9:36:21 AM	30.714	18.38	30.416	20.884	19.094	21.215	27.402	4.677	17.39	0.469	0.849	49.377	0.001	2.612	0	58.00	0.96667	25.9	12.1	19.3	1.331	0.389	0.335	0.0174	17.369	14.78
2/18/2003	9:37:21 AM	30.726	18.396	30.417	20.835	19.091	21.155	27.346	4.704	17.319	0.458	0.849	49.312	0.001	2.61	0.001	59.00	0.98333	25.9	12.1	19.2	1.326	0.389	0.335	0.0174	17.414	14.82
2/18/2003	9:38:21 AM	30.701	18.386	30.467	20.755	19.07	21.01	27.135	4.646	17.192	0.409	0.849	49.327	0.001	2.612	0.001	60.00	1	25.7	12.1	19.1	1.317	0.389	0.335	0.0175	17.528	14.92
2/18/2003	9:39:21 AM	30.682	18.397	30.463	20.67	19.092	21.163	27.354	4.619	17.343	0.472	0.847	49.446	0.001	2.616	0	61.00	1.01667	25.9	12.1	19.3	1.327	0.390	0.335	0.0174	17.418	14.82
2/18/2003	9:40:21 AM	30.672	18.402	30.423	20.584	19.061	21.018	27.145	4.621	17.229	0.412	0.849	49.255	0.001	2.61	0	62.00	1.03333	25.7	12.1	19.1	1.318	0.389	0.335	0.0175	17.515	14.91
2/18/2003	9:41:21 AM	30.677	18.403	30.374	20.484	19.057	21.219	27.367	4.606	17.409	0.475	0.849	49.272	0.001	2.615	0.001	63.00	1.05	25.9	12.1	19.3	1.332	0.390	0.336	0.0174	17.399	14.81
2/18/2003	9:42:21 AM	30.677	18.402	30.358	20.408	19.051	21.047	27.158	4.615	17.317	0.409	0.852	49.371	0.001	2.615	0.001	64.00	1.06667	25.7	12.1	19.2	1.323	0.390	0.336	0.0175	17.526	14.91
2/18/2003	9:43:21 AM	30.657	18.408	30.423	20.337	19.016	21.101	27.28	4.641	17.327	0.412	0.849	49.456	0.001	2.615	0	65.00	1.08333	25.8	12.1	19.2	1.325	0.390	0.336	0.0175	17.466	14.86
2/18/2003	9:44:21 AM	30.647	18.413	30.433	20.276	18.996	21.093	27.28	4.625	17.341	0.481	0.849	49.438	0.001	2.615	0.002	66.00	1.1	25.8	12.1	19.2	1.325	0.390	0.335	0.0175	17.458	14.86
2/18/2003	9:45:21 AM	30.652	18.413	30.378	20.211	19.001	21.217	27.377	4.675	17.401	0.432	0.849	49.289	0.001	2.614	0	67.00	1.11667	25.9	12.1	19.3	1.331	0.390	0.336	0.0174	17.394	14.80
2/18/2003	9:46:21 AM	30.647	18.408	30.338	20.15	18.985	21.105	27.309	4.622	17.321	0.472	0.849	49.371	0.001	2.613	0.001	68.00	1.13333	25.8	12.1	19.2	1.325	0.390	0.336	0.0175	17.494	14.89
2/18/2003	9:47:21 AM	30.661	18.407	30.343	20.155	18.934	20.943	27.081	4.598	17.173	0.449	0.847	49.375	0.001	2.616	0	69.00	1.15	25.6	12.1	19.1	1.314	0.390	0.336	0.0177	17.654	15.02
2/18/2003	9:48:21 AM	30.647	18.428	30.453	20.221	18.945	21.074	27.276	4.66	17.306	0.519	0.849	49.291	0.001	2.618	0.003	70.00	1.16667	25.8	12.1	19.2	1.323	0.390	0.336	0.0175	17.493	14.89
2/18/2003	9:49:21 AM	30.619	18.414	30.409	20.243	18.931	21.188	27.302	4.649	17.401	0.446	0.847	49.358	0.001	2.62	0	71.00	1.18333	25.8	12.1	19.3	1.330	0.391	0.336	0.0174	17.433	14.84
2/18/2003	9:50:21 AM	30.619	18.414	30.36	20.278	18.942	21.179	27.385	4.643	17.315	0.412	0.847	49.429	0.001	2.611	0	72.00	1.2	25.9	12.1	19.2	1.327	0.389	0.336	0.0174	17.439	14.84
2/18/2003	9:51:21 AM	30.624	18.425	30.35	20.329	18.967	21.122	27.28	4.605	17.452	0.481	0.852	49.347	0.001	2.62	0.001	73.00	1.21667	25.8	12.1	19.3	1.330	0.391	0.337	0.0175	17.468	14.87
2/18/2003	9:52:21 AM	30.663	18.431	30.346	20.355	18.983	21.14	27.321	4.677	17.321	0.455	0.844	49.301	0.001	2.616	0	74.00	1.23333	25.9	12.1	19.2	1.326	0.390	0.336	0.0175	17.494	14.89
2/18/2003	9:53:21 AM	30.626	18.437	30.436	20.401	19.004	20.941	27.149	4.68	17.052	0.481	0.849	49.454	0.001	2.619	0.002	75.00	1.25	25.7	12.1	19.0	1.310	0.390	0.336	0.0177	17.687	15.05
2/18/2003	9:54:21 AM	30.617	18.442	30.407	20.427	19.01	21.138	27.35	4.68	17.292	0.412	0.847	49.433	0.001	2.618	0.001	76.00	1.26667	25.9	12.1	19.2	1.325	0.390	0.336	0.0175	17.493	14.89
2/18/2003	9:55:21 AM	30.612	18.438	30.353	20.428	19.011	20.977	27.112	4.754	17.01	0.475	0.847	49.361	0.001	2.617	0.002	77.00	1.28333	25.6	12.1	19.0	1.310	0.390	0.336	0.0177	17.716	15.08
2/18/2003	9:56:21 AM	30.623	18.438	30.334	20.443	19.001	20.989	27.182	4.65	17.151	0.432	0.847	49.429	0.001	2.618	0.001	78.00	1.3	25.7	12.1	19.1	1.315	0.390	0.337	0.0177	17.661	15.03
2/18/2003	9:57:21 AM	30.628	18.449	30.359	20.489	18.981	21.078	27.3	4.653	17.253	0.478	0.847	49.421	0.001	2.62	0.002	79.00	1.31667	25.8	12.1	19.2	1.321	0.391	0.337	0.0176	17.574	14.96
2/18/2003	9:58:21 AM	30.619	18.46	30.425	20.531	19.003	21.024	27.234	4.64	17.208	0.513	0.849	49.435	0.001	2.62	0.002	80.00	1.33333	25.8	12.1	19.1	1.318	0.391	0.336	0.0176	17.588	14.97
2/18/2003	9:59:21 AM	30.596	18.446	30.371	20.522	19.014	21.138	27.321	4.552	17.581	0.501	0.844	49.327	0.001	2.624	0	81.00	1.35	25.9	12.1	19.4	1.335	0.391	0.337	0.0174	17.419	14.82
2/18/2003	10:00:21 AM	30.606	18.457	30.352	20.553	19.004	21.093	27.327	4.665	17.206	0.478	0.847	49.436	0.001	2.616	0.001	82.00	1.36667	25.9	12.1	19.1	1.320	0.390	0.336	0.0176	17.565	14.95
2/18/2003	10:01:21 AM	30.617	18.473	30.333	20.604	19.005	21.153	27.36	4.618	17.448	0.478	0.847	49.389	0.001	2.615	0.002	83.00	1.38333	25.9	12.1	19.3	1.331	0.390	0.336	0.0174	17.430	14.83
2/18/2003	10:02:21 AM	30.618	18.469	30.369	20.61	19.037	21.188	27.46	4.685	17.306	0.478	0.849	49.456	0.001	2.622	0.002	84.00	1.4	26.0	12.1	19.2	1.327	0.391	0.337	0.0175	17.508	14.90
2/18/2003	10:03:21 AM	30.604	18.485	30.425	20.657	19.053	21.078	27.249	4.669	17.292	0.481	0.849	49.36	0.001	2.619	0.001	85.00	1.41667	25.8	12.1	19.2	1.323	0.390	0.336	0.0175	17.518	14.91
2/18/2003	10:04:21 AM	30.595	18.476	30.376	20.672	19.049	21.041	27.193	4.65	17.263	0.475	0.847	49.41	0.001	2.62	0.002	86.00	1.43333	25.7	12.1	19.2	1.320	0.390	0.337	0.0176	17.578	14.96
2/18/2003	10:05:21 AM	30.																									

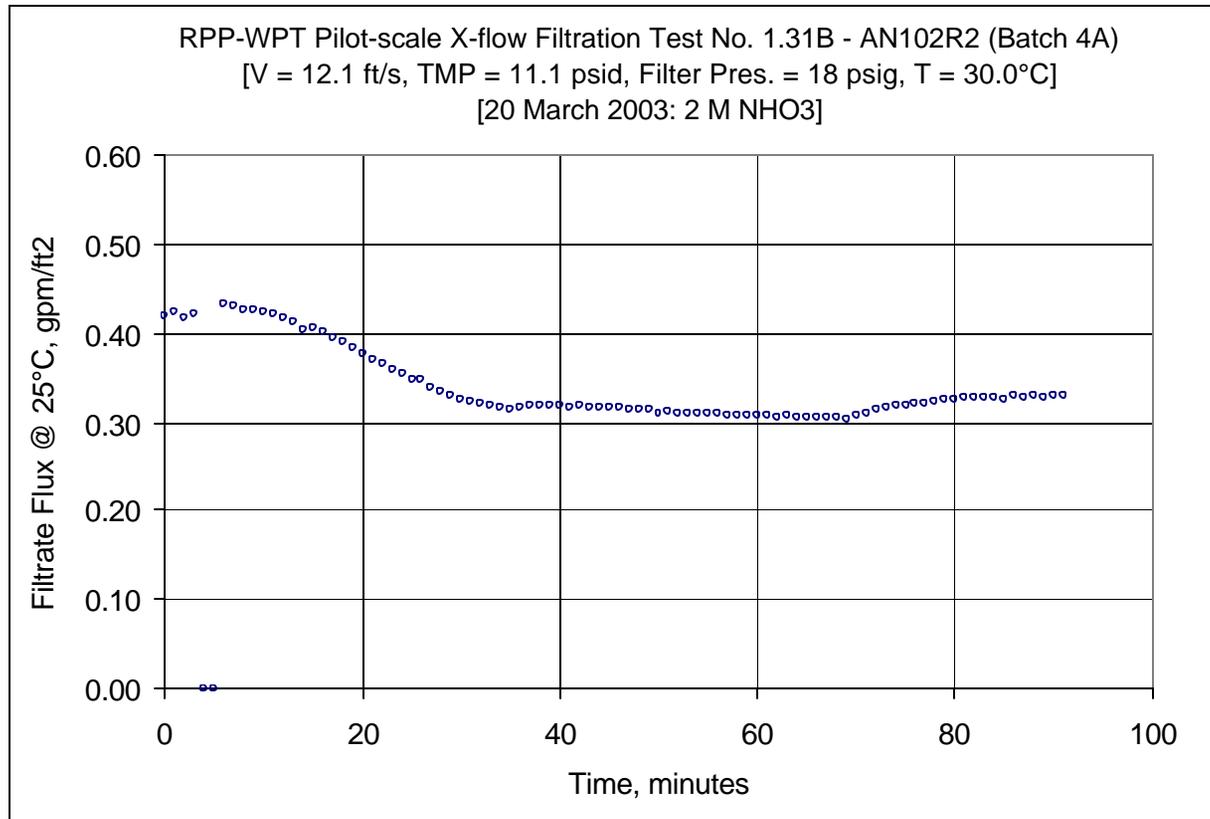


Figure C21: 1.31B: After AN-102R2, Batch 4A – 2 M Nitric Acid Cleaning – First Cleaning



WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

3/20/2003	3:15:50 PM	31.09	24.244	31.081	24.638	25.173	13.777	19.877	4.599	10.071	-0.052	0.547	48.917	0.002	2.51	0.001	46.00	0.76667	18.4	12.0	11.9	0.822	0.374	0.316	0.0265	26.536	22.58
3/20/2003	3:16:50 PM	31.269	24.255	31.26	24.679	25.178	13.886	19.933	4.577	10.204	-0.093	0.547	49.217	0.002	2.504	0	47.00	0.78333	18.5	12.1	12.0	0.830	0.373	0.314	0.0261	26.081	22.20
3/20/2003	3:17:50 PM	31.429	24.26	31.444	24.725	25.214	13.746	19.877	4.635	10.122	0.029	0.547	48.826	0.002	2.526	0.002	48.00	0.8	18.4	12.0	11.9	0.823	0.377	0.315	0.0264	26.423	22.49
3/20/2003	3:18:50 PM	31.598	24.261	31.599	24.691	25.245	13.746	19.904	4.677	9.987	0.063	0.55	48.977	0.002	2.536	0.001	49.00	0.81667	18.4	12.0	11.9	0.818	0.378	0.315	0.0266	26.567	22.61
3/20/2003	3:19:50 PM	31.782	24.287	31.788	24.732	25.256	13.511	19.459	4.733	9.721	-0.099	0.547	49.619	0.002	2.513	0	50.00	0.83333	18.0	12.2	11.6	0.801	0.375	0.311	0.0268	26.757	22.77
3/20/2003	3:20:50 PM	31.957	24.303	31.982	24.778	25.287	13.638	19.788	4.652	9.897	0.066	0.55	49.298	0.002	2.536	0	51.00	0.85	18.3	12.1	11.8	0.811	0.378	0.312	0.0265	26.516	22.57
3/20/2003	3:21:50 PM	32.131	24.314	32.152	24.819	25.303	13.634	19.788	4.698	9.809	0.052	0.55	49.689	0.002	2.536	0.001	52.00	0.86667	18.3	12.2	11.7	0.808	0.378	0.311	0.0265	26.499	22.55
3/20/2003	3:22:50 PM	32.291	24.316	32.312	24.83	25.324	13.584	19.757	4.684	9.989	0.069	0.547	49.506	0.002	2.544	0.002	53.00	0.88333	18.3	12.1	11.8	0.813	0.379	0.310	0.0263	26.323	22.40
3/20/2003	3:23:50 PM	32.476	24.352	32.511	24.872	25.361	13.364	19.65	4.616	9.704	0.127	0.547	49.456	0.002	2.55	0.001	54.00	0.9	18.2	12.1	11.5	0.795	0.380	0.309	0.0268	26.819	22.82
3/20/2003	3:24:50 PM	32.651	24.359	32.671	24.818	25.377	13.487	19.778	4.676	9.731	0.179	0.544	49.37	0.002	2.559	0.001	55.00	0.91667	18.3	12.1	11.6	0.800	0.382	0.309	0.0266	26.625	22.86
3/20/2003	3:25:50 PM	32.815	24.374	32.84	24.789	25.373	13.367	19.788	4.605	9.702	0.28	0.547	49.126	0.001	2.587	0	56.00	0.93333	18.3	12.0	11.5	0.795	0.386	0.311	0.0270	26.968	22.95
3/20/2003	3:26:50 PM	32.985	24.411	33.029	24.806	25.385	13.377	19.695	4.634	9.671	0.222	0.547	49.43	0.002	2.575	0.001	57.00	0.95	18.2	12.1	11.5	0.795	0.384	0.308	0.0267	26.732	22.75
3/20/2003	3:27:50 PM	33.143	24.396	33.163	24.74	25.365	13.298	19.687	4.581	9.708	0.208	0.547	49.466	0.002	2.587	0.001	58.00	0.96667	18.2	12.1	11.5	0.793	0.386	0.308	0.0268	26.810	22.82
3/20/2003	3:28:50 PM	33.311	24.411	33.326	24.73	25.385	13.159	19.558	4.743	9.317	0.283	0.547	49.374	0.002	2.597	0.001	59.00	0.98333	18.1	12.1	11.2	0.775	0.387	0.308	0.0274	27.429	23.34
3/20/2003	3:29:50 PM	33.469	24.415	33.479	24.725	25.379	13.367	19.823	4.606	9.716	0.289	0.544	49.676	0.001	2.601	0.001	60.00	1	18.4	12.2	11.5	0.796	0.388	0.307	0.0266	26.640	22.67
3/20/2003	3:30:50 PM	33.621	24.425	33.621	24.749	25.353	13.149	19.643	4.697	9.413	0.349	0.544	49.386	0.002	2.61	0	61.00	1.01667	18.2	12.1	11.3	0.778	0.389	0.307	0.0272	27.246	23.19
3/20/2003	3:31:50 PM	33.788	24.433	33.788	24.737	25.332	13.259	19.757	4.7	9.54	0.387	0.544	49.401	0.002	2.614	0	62.00	1.03333	18.3	12.1	11.4	0.786	0.390	0.306	0.0269	26.885	22.88
3/20/2003	3:32:50 PM	33.946	24.447	33.945	24.707	25.336	13.201	19.77	4.605	9.59	0.367	0.544	49.359	0.002	2.628	0.001	63.00	1.05	18.3	12.1	11.4	0.786	0.392	0.307	0.0269	26.926	22.91
3/20/2003	3:33:50 PM	34.092	24.451	34.097	24.58	25.314	13.05	19.573	4.813	9.199	0.315	0.544	49.839	0.002	2.621	0.001	64.00	1.06667	18.1	12.2	11.1	0.767	0.391	0.305	0.0274	27.398	23.32
3/20/2003	3:34:50 PM	34.255	24.465	34.264	24.524	25.319	13.083	19.736	4.581	9.53	0.526	0.547	49.464	0.002	2.645	0	65.00	1.08333	18.3	12.1	11.3	0.780	0.394	0.306	0.0271	27.083	23.05
3/20/2003	3:35:50 PM	34.402	24.475	34.406	24.513	25.338	13.093	19.736	4.636	9.416	0.526	0.544	49.462	0.002	2.644	0.002	66.00	1.1	18.3	12.1	11.3	0.776	0.394	0.305	0.0271	27.096	23.06
3/20/2003	3:36:50 PM	34.554	24.484	34.559	24.522	25.342	13.093	19.83	4.641	9.514	0.569	0.55	49.579	0.002	2.657	0.001	67.00	1.11667	18.4	12.2	11.3	0.779	0.396	0.305	0.0270	27.002	22.98
3/20/2003	3:37:50 PM	34.703	24.494	34.702	24.512	25.367	13.019	19.767	4.673	9.317	0.586	0.547	49.481	0.002	2.661	0.001	68.00	1.13333	18.3	12.1	11.2	0.770	0.397	0.305	0.0273	27.267	23.20
3/20/2003	3:38:50 PM	34.836	24.494	34.845	24.497	25.387	13.132	19.889	4.613	9.571	0.598	0.544	49.401	0.002	2.668	0.002	69.00	1.15	18.4	12.1	11.4	0.783	0.398	0.304	0.0268	26.796	22.80
3/20/2003	3:39:50 PM	34.841	24.504	34.401	24.573	25.372	13.103	19.817	4.71	9.475	0.586	0.544	49.508	0.002	2.66	0.001	70.00	1.16667	18.3	12.1	11.3	0.778	0.397	0.307	0.0272	27.180	23.13
3/20/2003	3:40:50 PM	34.461	24.504	33.862	24.838	25.422	13.062	19.801	4.666	9.344	0.543	0.541	49.516	0.002	2.656	0.002	71.00	1.18333	18.3	12.1	11.2	0.772	0.396	0.311	0.0277	27.741	23.61
3/20/2003	3:41:50 PM	34.012	24.53	33.364	25.094	25.428	12.946	19.53	4.624	9.381	0.523	0.547	48.745	0.002	2.645	0.002	72.00	1.2	18.1	11.9	11.2	0.770	0.394	0.314	0.0281	28.094	23.91
3/20/2003	3:42:50 PM	33.578	24.536	32.876	25.241	25.425	13.213	19.861	4.62	9.588	0.468	0.541	49.344	0.002	2.633	0.001	73.00	1.21667	18.4	12.1	11.4	0.786	0.393	0.316	0.0277	27.744	23.61
3/20/2003	3:43:50 PM	33.163	24.542	32.49	25.387	25.44	13.103	19.587	4.705	9.321	0.367	0.541	50.513	0.001	2.62	0.001	74.00	1.23333	18.1	12.4	11.2	0.773	0.391	0.318	0.0284	28.362	24.14
3/20/2003	3:44:50 PM	32.795	24.575	32.196	25.485	25.473	13.282	19.796	4.581	9.729	0.367	0.547	49.298	0.002	2.612	0	75.00	1.25	18.3	12.1	11.5	0.793	0.389	0.320	0.0278	27.772	23.63
3/20/2003	3:45:50 PM	32.451	24.572	31.906	25.527	25.506	13.284	19.846	4.659	9.594	0.375	0.541	49.227	0.001	2.608	0.001	76.00	1.26667	18.4	12.1	11.4	0.789	0.389	0.322	0.0281	28.109	23.92
3/20/2003	3:46:50 PM	32.176	24.605	31.681	25.6	25.538	13.418	19.838	4.647	9.778	0.289	0.544	49.223	0.002	2.598	0	77.00	1.28333	18.4	12.1	11.6	0.800	0.387	0.322	0.0278	27.785	23.65
3/20/2003	3:47:50 PM	31.922	24.608	31.451	25.678	25.557	13.191	19.621	4.659	9.508	0.289	0.541	49.252	0.002	2.589	0	78.00	1.3	18.2	12.1	11.3	0.783	0.386	0.323	0.0285	28.471	24.23
3/20/2003	3:48:50 PM	31.691	24.621	31.265	25.726	25.564	13.404	19.863	4.69	9.708	0.289	0.544	49.162	0.002	2.595	0	79.00	1.31667	18.4	12.0	11.6	0.797	0.387	0.326	0.0282	28.168	23.97
3/20/2003	3:49:50 PM	31.479	24.622	31.063	25.697	25.565	13.522	19.962	4.64	9.983	0.26	0.544	49.191	0.001	2.589	0	80.00	1.33333	18.5	12.1	11.8	0.810	0.386	0.327	0.0278	27.785	23.65
3/20/2003	3:50:50 PM	31.302	24.629	30.906	25.654	25.567	13.201	19.558	4.77	9.362	0.266	0.547	49.177	0.002	2.58	0	81.00	1.35	18.1	12.1	11.3	0.778	0.385	0.327	0.0290	28.967	24.65
3/20/2003	3:51:50 PM	31.149	24.639	30.758	25.599	25.543	13.445	19.815	4.67	9.717	0.208	0.547	49.099	0.002	2.572	0	82.00	1.36667	18.3	12.0	11.6	0.798	0.383	0.327	0.0282	28.243	24.04
3/20/2003	3:52:50 PM	31.02	24.65	30.624	25.545	25.548	13.362	19.664	4.615	9.653	0.231	0.547	49.179	0.002	2.566	0.001	83.00	1.38333	18.2	12.1	11.5	0.793	0.383	0.328	0.0285	28.460	24.22
3/20/2003	3:53:50 PM	30.896	24.66	30.505	25.495	25.533	13.383	19.759	4.819	9.506	0.231	0.547	49.193	0.002	2.564	0	84.00	1.4	18.3	12.1	11.4	0.789	0.382	0.328	0.0287	28.687	24.41
3/20/2003	3:54:50 PM	30.786	24.654	30.38	25.394	25.512	13.588	19.895	4.674	9.843	0.121	0.55	49.569	0.001	2.541	0.001	85.00	1.41667	18.4	12.1	11.7	0.808	0.379	0.326	0.0279	27.867	23.71
3/20/2003	3:55:50 PM	30.701	24.659	30.295	25.368	25.482	13.617	19.91	4.623	9.956	0.138	0.547	49.271	0.001	2.557	0.001	86.00	1.43333	18.4	12.1	11.8	0.813	0.381	0.329	0.0279	27.938	23.78
3/20/2003	3:56:50 PM	30.62	24.657	30.234	25.352	25.4																					

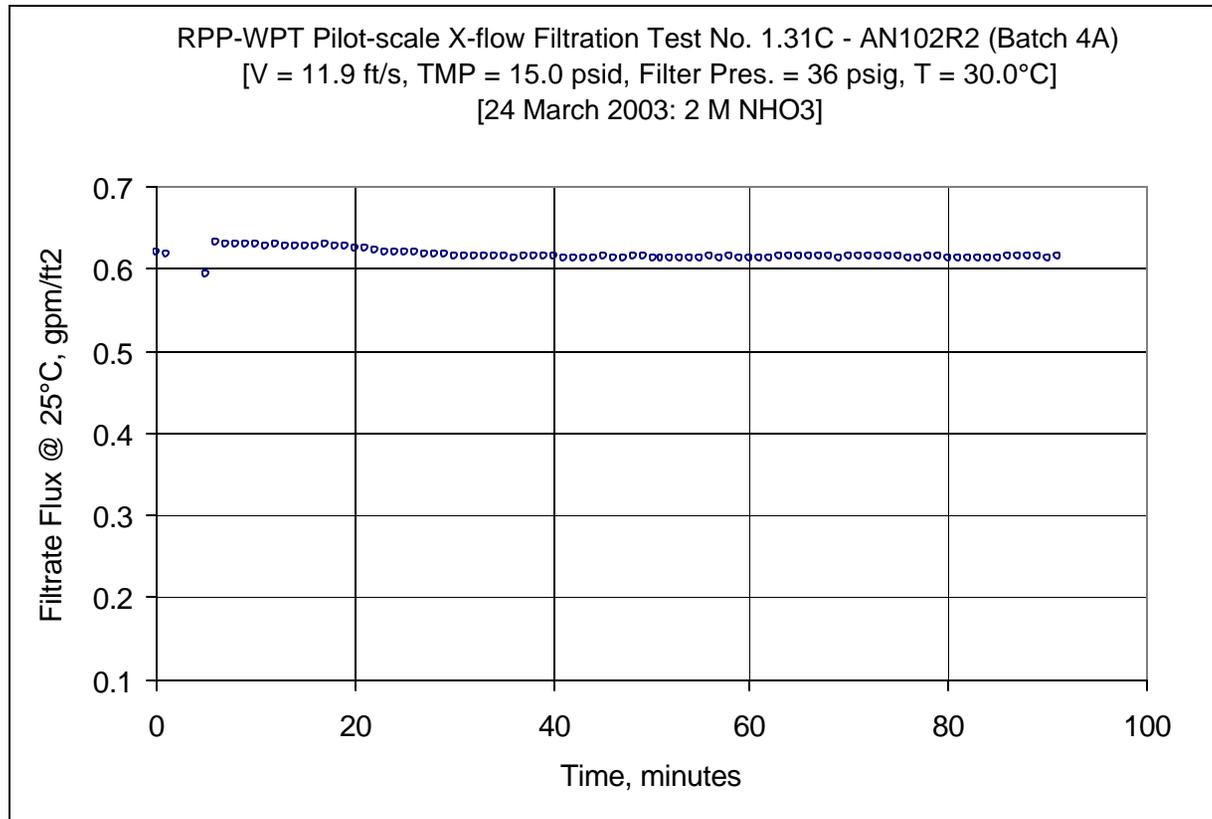


Figure C23: 1.31C: After AN-102R2, Batch 4A – 2 M Nitric Acid Cleaning – Second Cleaning



3/24/2003	10:15:37 AM	30.175	21.735	30.106	23.765	23.356	16.61	37.48	4.358	14.611	13.859	1.604	48.703	0.001	4.743	0.001	46.00	0.76667	36.0	11.9	15.6	1.076	0.707	0.614	0.0393	39.329	33.47
3/24/2003	10:16:37 AM	30.181	21.772	30.102	23.831	23.412	16.529	37.313	4.346	14.597	13.813	1.606	48.661	0.002	4.739	0.001	47.00	0.78333	35.8	11.9	15.6	1.073	0.707	0.613	0.0394	39.420	33.55
3/24/2003	10:17:37 AM	30.186	21.813	30.093	23.827	23.458	16.676	37.503	4.384	14.609	13.885	1.601	48.743	0.001	4.749	0	48.00	0.8	36.0	11.9	15.6	1.078	0.708	0.615	0.0393	39.312	33.46
3/24/2003	10:18:37 AM	30.17	21.817	30.067	23.8	23.503	16.595	37.449	4.35	14.679	13.934	1.598	48.642	0.001	4.744	0.001	49.00	0.81667	36.0	11.9	15.6	1.078	0.707	0.615	0.0393	39.312	33.46
3/24/2003	10:19:37 AM	30.181	21.868	30.112	23.816	23.554	16.508	37.323	4.361	14.527	13.903	1.604	48.644	0.001	4.742	0.001	50.00	0.83333	35.9	11.9	15.5	1.070	0.707	0.614	0.0395	39.550	33.66
3/24/2003	10:20:37 AM	30.186	21.892	30.107	23.836	23.583	16.492	37.236	4.351	14.609	13.946	1.598	48.701	0.001	4.744	0	51.00	0.85	35.8	11.9	15.6	1.072	0.707	0.614	0.0395	39.488	33.60
3/24/2003	10:21:37 AM	30.197	21.934	30.128	23.902	23.624	16.552	37.317	4.315	14.634	13.784	1.601	48.598	0.002	4.741	0.001	52.00	0.86667	35.8	11.9	15.6	1.075	0.707	0.613	0.0393	39.333	33.47
3/24/2003	10:22:37 AM	30.186	21.953	30.113	23.862	23.664	16.432	37.217	4.308	14.406	13.877	1.601	48.617	0.001	4.74	0.002	53.00	0.88333	35.7	11.9	15.4	1.063	0.707	0.613	0.0398	39.785	33.86
3/24/2003	10:23:37 AM	30.221	22.009	30.158	23.937	23.7	16.602	37.371	4.346	14.734	13.906	1.604	48.665	0.001	4.739	0.001	54.00	0.9	35.9	11.9	15.7	1.080	0.707	0.613	0.0391	39.096	33.27
3/24/2003	10:24:37 AM	30.205	22.028	30.132	23.991	23.734	16.498	37.327	4.406	14.492	13.871	1.604	48.627	0.001	4.741	0	55.00	0.91667	35.9	11.9	15.5	1.068	0.707	0.613	0.0396	39.577	33.68
3/24/2003	10:25:37 AM	30.215	22.058	30.116	24.036	23.784	16.627	37.437	4.323	14.752	13.819	1.604	48.525	0.001	4.751	0.001	56.00	0.93333	36.0	11.9	15.7	1.082	0.708	0.615	0.0392	39.186	33.35
3/24/2003	10:26:37 AM	30.22	22.093	30.126	24.116	23.833	16.571	37.31	4.31	14.707	13.868	1.606	48.422	0.001	4.745	0.002	57.00	0.95	35.8	11.9	15.6	1.078	0.707	0.614	0.0393	39.253	33.40
3/24/2003	10:27:37 AM	30.219	22.126	30.121	24.151	23.868	16.504	37.385	4.321	14.568	14.007	1.606	48.457	0.002	4.749	0	58.00	0.96667	35.9	11.9	15.5	1.071	0.708	0.614	0.0396	39.551	33.66
3/24/2003	10:28:37 AM	30.224	22.163	30.135	24.211	23.918	16.564	37.358	4.308	14.679	13.917	1.601	48.537	0.001	4.75	0.001	59.00	0.98333	35.9	11.9	15.6	1.077	0.708	0.614	0.0393	39.328	33.47
3/24/2003	10:29:37 AM	30.224	22.188	30.115	24.175	23.953	16.569	37.486	4.337	14.63	13.903	1.601	48.403	0.001	4.742	0	60.00	1	36.0	11.9	15.6	1.076	0.707	0.614	0.0393	39.339	33.48
3/24/2003	10:30:37 AM	30.238	22.223	30.13	24.18	23.993	16.405	37.315	4.3	14.447	13.949	1.604	48.583	0.001	4.749	0	61.00	1.01667	35.8	11.9	15.4	1.060	0.708	0.614	0.0400	39.953	34.00
3/24/2003	10:31:37 AM	30.252	22.257	30.124	24.249	24.037	16.446	37.277	4.318	14.311	13.903	1.604	48.575	0.001	4.746	0.002	62.00	1.03333	35.8	11.9	15.4	1.064	0.708	0.614	0.0398	39.799	33.87
3/24/2003	10:32:37 AM	30.256	22.295	30.137	24.273	24.065	16.577	37.451	4.36	14.581	13.88	1.606	48.485	0.001	4.751	0.001	63.00	1.05	36.0	11.9	15.6	1.074	0.708	0.614	0.0394	39.442	33.57
3/24/2003	10:33:37 AM	30.245	22.315	30.107	24.282	24.095	16.521	37.311	4.234	14.771	13.963	1.606	48.457	0.001	4.752	0	64.00	1.06667	35.8	11.9	15.6	1.079	0.708	0.615	0.0393	39.313	33.46
3/24/2003	10:34:37 AM	30.254	22.344	30.096	24.241	24.129	16.593	37.517	4.332	14.63	13.874	1.601	48.472	0.001	4.747	0	65.00	1.08333	36.0	11.9	15.6	1.076	0.708	0.615	0.0394	39.370	33.50
3/24/2003	10:35:37 AM	30.249	22.359	30.076	24.206	24.159	16.558	37.373	4.337	14.65	13.848	1.601	48.512	0.001	4.746	0	66.00	1.1	35.9	11.9	15.6	1.072	0.708	0.615	0.0395	39.529	33.64
3/24/2003	10:36:37 AM	30.263	22.413	30.095	24.28	24.208	16.529	37.339	4.313	14.701	13.877	1.606	48.512	0.001	4.747	0	67.00	1.11667	35.9	11.9	15.6	1.077	0.708	0.615	0.0394	39.363	33.50
3/24/2003	10:37:37 AM	30.251	22.436	30.078	24.308	24.231	16.457	37.217	4.358	14.505	13.937	1.601	48.554	0.001	4.748	0.001	68.00	1.13333	35.7	11.9	15.5	1.067	0.708	0.615	0.0397	39.730	33.81
3/24/2003	10:38:37 AM	30.27	22.475	30.082	24.362	24.265	16.506	37.296	4.276	14.685	13.851	1.604	48.504	0.001	4.741	0	69.00	1.15	35.8	11.9	15.6	1.075	0.707	0.614	0.0394	39.376	33.51
3/24/2003	10:39:37 AM	30.253	22.493	30.05	24.365	24.308	16.351	37.12	4.247	14.466	13.9	1.601	48.506	0.001	4.743	0	70.00	1.16667	35.6	11.9	15.4	1.062	0.707	0.615	0.0399	39.905	33.96
3/24/2003	10:40:37 AM	30.262	22.533	30.07	24.41	24.348	16.523	37.292	4.271	14.671	13.88	1.604	48.52	0.001	4.744	0	71.00	1.18333	35.8	11.9	15.6	1.075	0.707	0.615	0.0394	39.410	33.54
3/24/2003	10:41:37 AM	30.256	22.567	30.068	24.428	24.367	16.461	37.25	4.318	14.601	13.949	1.606	48.543	0.001	4.746	0	72.00	1.2	35.8	11.9	15.5	1.071	0.708	0.615	0.0396	39.596	33.70
3/24/2003	10:42:37 AM	30.27	22.607	30.062	24.493	24.426	16.678	37.534	4.331	14.769	13.81	1.609	48.504	0.002	4.747	0	73.00	1.21667	36.1	11.9	15.7	1.084	0.708	0.615	0.0391	39.126	33.30
3/24/2003	10:43:37 AM	30.259	22.63	30.051	24.541	24.459	16.498	37.294	4.294	14.675	13.822	1.604	48.527	0.001	4.743	0	74.00	1.23333	35.8	11.9	15.6	1.075	0.707	0.615	0.0394	39.449	33.57
3/24/2003	10:44:37 AM	30.267	22.664	30.059	24.57	24.488	16.417	37.257	4.268	14.513	13.978	1.604	48.493	0.001	4.753	0	75.00	1.25	35.8	11.9	15.5	1.066	0.709	0.616	0.0398	39.834	33.90
3/24/2003	10:45:37 AM	30.266	22.698	30.063	24.558	24.527	16.589	37.41	4.307	14.675	13.822	1.604	48.503	0.001	4.741	0.002	76.00	1.26667	35.9	11.9	15.6	1.078	0.707	0.614	0.0393	39.304	33.45
3/24/2003	10:46:37 AM	30.261	22.733	30.068	24.598	24.577	16.562	37.41	4.353	14.566	13.825	1.604	48.512	0.001	4.74	0.001	77.00	1.28333	35.9	11.9	15.6	1.073	0.707	0.614	0.0395	39.475	33.59
3/24/2003	10:47:37 AM	30.255	22.752	30.082	24.608	24.621	16.579	37.368	4.391	14.466	13.958	1.606	48.587	0.001	4.747	0.001	78.00	1.3	35.9	11.9	15.5	1.070	0.708	0.615	0.0396	39.611	33.71
3/24/2003	10:48:37 AM	30.255	22.787	30.102	24.693	24.646	16.569	37.389	4.262	14.8	13.868	1.606	48.575	0.002	4.748	0	79.00	1.31667	35.9	11.9	15.7	1.081	0.708	0.615	0.0392	39.189	33.35
3/24/2003	10:49:37 AM	30.258	22.816	30.105	24.732	24.65	16.595	37.461	4.332	14.638	13.793	1.606	48.438	0.001	4.744	0.001	80.00	1.33333	36.0	11.9	15.6	1.077	0.707	0.614	0.0393	39.323	33.46
3/24/2003	10:50:37 AM	30.248	22.836	30.125	24.752	24.675	16.627	37.447	4.371	14.564	13.804	1.606	48.39	0.001	4.745	0	81.00	1.35	36.0	11.9	15.6	1.075	0.707	0.614	0.0394	39.363	33.50
3/24/2003	10:51:37 AM	30.263	22.881	30.15	24.792	24.68	16.591	37.424	4.286	14.707	13.9	1.606	48.424	0.001	4.742	0.001	82.00	1.36667	36.0	11.9	15.6	1.079	0.707	0.613	0.0392	39.177	33.34
3/24/2003	10:52:37 AM	30.253	22.901	30.135	24.706	24.709	16.554	37.449	4.319	14.542	13.929	1.601	48.42	0.001	4.75	0	83.00	1.38333	36.0	11.9	15.5	1.072	0.708	0.614	0.0395	39.514	33.63
3/24/2003	10:53:37 AM	30.246	22.939	30.163	24.684	24.718	16.438	37.186	4.339	14.427	13.923	1.606	48.541	0.001	4.747	0	84.00	1.4	35.7	11.9	15.4	1.064	0.708	0.614	0.0398	39.755	33.83
3/24/2003	10:54:37 AM	30.254	22.957	30.141	24.657	24.701	16.72	37.613	4.382	14.929	13.88	1.606	48.548	0.001	4.749	0	85.00	1.41667	36.1	11.9	15.8	1.091	0.708	0.614	0.0388	38.809	33.03
3/24/2003	10:55:37 AM	30.24	22.978	30.112	24.673	24.671	16.897	37.563	4.312	14.83	13.865	1.606	48.392	0.001	4.751	0	86.00	1.43333	36.1	11.9	15.8	1.087	0.708	0.615	0.0390	39.007	33.20</

## Appendix D: Slurry Dewatering, Test Run 1.16 – AN-102R2

While this task filtered slurry under steady state conditions, i.e., both the flow parameters and slurry solids concentration were held constant, the most important test runs dealt with “dewatering” the slurry, which means allowing the solids concentration to increase with time. Initially there were to be just two dewatering tests for this organic based slurry: Batch 3 and Batch 4, which would differ only in mixing regimes while the slurry was prepared before filtration. However, problems with filtering Batch 3 led to reformulating the slurry; therefore it was followed with a Batch 3B and a Batch 3A. The first batch was named Batch 3C. Instead of having two batch it turned out to be four, for which the data are included herein.

The general test matrix was to first test the cross filter with water and then a standard slurry. The slurry dewatering test run, No. 1.16, began by preparing the test slurry and introducing into the test at a insoluble solids concentration near 1.0 wt %. During the dewatering test the slurry axial velocity,  $V$ , was maintained at approximately 12 ft/s and the Transmembrane Pressure, TMP, at approximately 40 psid. This process continued until the solids concentration reached the target of 20 wt. This Appendix includes the following dewatering test runs:

1.16, Batch 3C	This AN-102 simulant was precipitated under NOC, see below
1.16, Batch 3B	This AN-102 simulant was precipitated under BC, see below
1.16, Batch 3A	This AN-102 simulant was precipitated under BC at 25°C, see below
1.16, Batch 4A	This AN-102 simulant was precipitated using PJM, see below

NOC – Newly Optimized Conditions – Initially there was to be only a single Batch 3 simulant prepared under the newly optimized conditions, however poor filterability forced a formulation of the slurry simulant and two more Batch 3 test. The conditions that were being “optimized” are called Baseline Conditions, explained below, and basically means using less reagents during the precipitation phase of the slurry preparation, i.e., are 0.03 M SrCO<sub>3</sub>, 0.03 M NaMn<sub>4</sub>, bring the free hydroxide concentration to 0.3 M, and precipitate at 20°C. Unfortunately only the decontamination factors were optimized while the filterability of the slurry became worse. This slurry was made while being well mixed.

BC – Baseline Conditions – These were the precipitation conditions used to test another organic based slurry in the past, i.e., AN-107 slurry (Duignan, 2000), which were 0.075 M SrCO<sub>3</sub>, 0.05 M, bring the free hydroxide concentration to 1 M, and precipitate at 50°C. This slurry was made while being well mixed.

BC at 20°C – Baseline Conditions but at the lower temperature of 20°C. This slurry was made while being well mixed.

PJM – Pulse Jetpump Mixer – This AN-102 simulated slurry was precipitated at the baseline conditions, however, the mixing environment during precipitation was made to mock that which was planned for actual plant operation. A scaled version of the air driven jetpumps were used to determine its effect on the overall process.

Each dewatering test in this Appendix contains a graph of the filtrate flux with time and tables of the data taken and calculated. To better understand the presented information important aspects of the graphs and tables are explained below:

Graphs – Each graph contains time averages of some of the important parameters taken during the run at the top of the figures, i.e. Slurry velocity in the filter tube,  $V$ ; transmembrane pressure, TMP; slurry pressure at the entrance of the filter tube, Filter Pres; and the slurry temperature,  $T$ .

Tables – Each table is divided into raw data (the first 17 columns) and calculations (the last 10 columns) which are based on the raw data. The raw data section is divided into three parts:

Individual Entries – Raw Data

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used, except for tests Clean 1 & 2) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid with has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column and corrected for a 40.9-inch water column that exists from the transducer to the point where P1 is measured.)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.  
Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.87 ft<sup>2</sup>)  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T))-(1/298)]$  as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)  
Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing  
Permiability – Same as Permiability but in metric units, meter/day/bar

Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 x Std Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not included the points taken during the backpulse sequence of each test. This is explained below.

Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is were the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

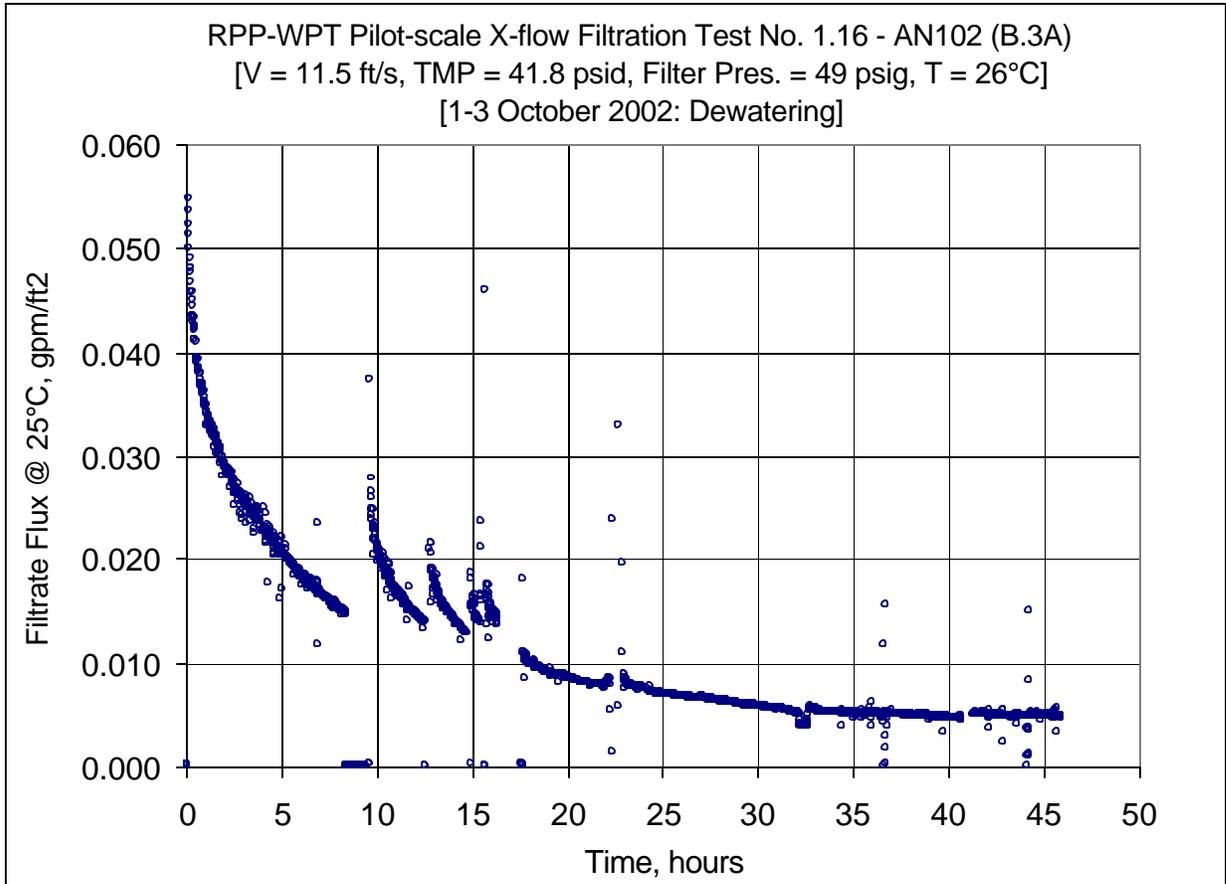


Figure D1: Dewatering of the AN-102R2, batch 3C, insoluble solids concentrations from 1 to 8.5 wt%

(Data from 26 Files)  
(1.16-rpp-pxu-100102-1710, -1910, -2110, -2310)  
(1.16-rpp-pxu-100202-0132, -0240, -0335, -0534, -0541, -0549, -0756, -0840, -1040)  
(1.16-rpp-pxu-100202-1251, -1501, -1524, -1600, -1800, -2000, -2359)  
(1.16-rpp-pxu-100302-0200, -0400, -0834, -1031, -1248)



131	10/1/2002	7:04.06 PM	26.256	26.279	24.933	27.266	26.695	46.71	48.695	7.751	39.94	-1.289	-5.473	45.75	0.198	0.001	113.83	1.89722	47.2	11.2	43.3	2.987	0.030	0.030	0.001	0.683	0.58
132	10/1/2002	7:05.06 PM	26.239	26.258	24.967	27.206	26.689	46.712	48.96	7.758	39.803	-1.289	-5.403	46.031	0.198	0.001	114.83	1.91389	47.5	11.3	43.3	2.982	0.030	0.030	0.001	0.683	0.58
133	10/1/2002	7:06.06 PM	26.253	26.257	24.972	27.205	26.649	46.658	48.724	7.77	39.944	-1.289	-5.608	46.186	0.197	0.001	116.83	1.93056	47.3	11.3	43.3	2.985	0.029	0.029	0.001	0.679	0.58
134	10/1/2002	7:07.06 PM	26.242	26.241	24.916	27.164	26.663	46.447	48.669	7.704	39.878	-1.289	-5.938	45.796	0.195	0.001	118.83	1.94722	47.0	11.2	43.0	2.986	0.029	0.029	0.001	0.681	0.58
135	10/1/2002	7:08.06 PM	26.263	26.257	25.022	27.25	26.659	46.654	48.761	7.842	39.732	-1.289	-5.608	45.907	0.197	0.002	117.83	1.96389	47.1	11.3	43.3	2.978	0.029	0.029	0.001	0.680	0.58
136	10/1/2002	7:09.06 PM	26.279	26.268	24.947	27.271	26.674	46.636	48.736	7.671	40.022	-1.281	-5.519	45.857	0.196	0.002	118.83	1.98056	47.3	11.2	43.3	2.987	0.029	0.029	0.001	0.675	0.57
137	10/1/2002	7:10.06 PM	26.273	26.257	25.022	27.195	26.669	46.648	48.685	7.759	39.957	-1.264	-5.54	46.177	0.197	0.001	119.83	1.99722	47.2	11.3	43.3	2.986	0.029	0.029	0.001	0.678	0.58
138	10/1/2002	7:11.03 PM	26.263	26.267	25.027	27.215	26.679	46.19	48.242	7.736	39.236	-1.286	-5.569	45.485	0.196	0.001	120.83	1.99917	46.8	11.1	42.7	2.945	0.029	0.029	0.001	0.684	0.58
139	10/1/2002	7:11.13 PM	26.242	26.247	24.992	27.175	26.665	46.253	48.693	7.783	39.705	-1.286	-5.666	45.592	0.195	0.001	123.83	1.91583	47.1	11.2	43.1	2.974	0.029	0.029	0.001	0.684	0.57
140	10/1/2002	7:12.13 PM	26.278	26.247	24.972	27.15	26.684	46.679	49.146	7.802	39.629	-1.282	-5.412	45.485	0.195	0.001	121.95	2.0325	47.7	11.1	43.1	2.972	0.029	0.029	0.001	0.668	0.57
141	10/1/2002	7:13.13 PM	26.288	26.252	25.032	27.185	26.669	46.161	48.418	7.738	39.31	-1.289	-5.686	46.135	0.19	0.001	122.95	2.04917	46.9	11.2	42.7	2.946	0.028	0.028	0.001	0.662	0.56
142	10/1/2002	7:14.13 PM	26.292	26.266	24.961	27.189	26.673	46.277	48.422	7.792	39.379	-1.289	-5.636	45.962	0.195	0.001	123.95	2.06583	46.9	11.2	42.6	2.953	0.029	0.029	0.001	0.680	0.58
143	10/1/2002	7:15.13 PM	26.302	26.261	25.04	27.189	26.673	46.632	49.016	7.937	39.673	-1.289	-5.647	45.962	0.194	0.001	124.95	2.0825	47.5	11.3	43.1	2.973	0.029	0.029	0.001	0.670	0.57
144	10/1/2002	7:16.13 PM	26.307	26.266	24.946	27.139	26.696	46.209	48.55	7.809	39.257	-1.292	-5.611	46.251	0.192	0.001	125.95	2.09917	47.1	11.3	43.2	2.946	0.028	0.028	0.001	0.671	0.57
145	10/1/2002	7:17.13 PM	26.307	26.261	25.025	27.149	26.697	46.806	48.898	7.803	39.904	-1.292	-5.661	46.138	0.192	0.001	126.95	2.11583	47.4	11.3	43.4	2.989	0.029	0.029	0.001	0.660	0.56
146	10/1/2002	7:18.13 PM	26.306	26.25	25.004	27.147	26.671	46.509	48.767	7.811	39.643	-1.289	-5.668	46.01	0.192	0.001	127.95	2.1325	47.3	11.3	43.0	2.966	0.029	0.029	0.001	0.665	0.57
147	10/1/2002	7:19.13 PM	26.317	26.261	25	27.113	26.682	46.085	48.254	7.712	39.295	-1.289	-5.632	46.026	0.192	0.001	128.95	2.14917	46.8	11.3	42.7	2.943	0.029	0.029	0.001	0.671	0.57
148	10/1/2002	7:20.13 PM	26.316	26.25	25.064	27.088	26.671	45.998	48.192	7.698	39.774	-1.289	-5.669	45.961	0.194	0.001	129.95	2.16583	46.7	11.2	43.1	2.979	0.029	0.029	0.001	0.662	0.56
149	10/1/2002	7:21.13 PM	26.321	26.245	24.979	27.063	26.651	46.18	48.529	7.81	39.126	-1.286	-5.628	46.261	0.188	0.001	130.95	2.1825	47.1	11.3	43.2	2.941	0.028	0.028	0.001	0.668	0.56
150	10/1/2002	7:22.13 PM	26.321	26.25	25.079	27.048	26.651	46.472	48.666	7.769	39.649	-1.289	-5.661	45.565	0.193	0.001	131.95	2.19917	47.2	11.2	43.0	2.965	0.029	0.029	0.001	0.668	0.57
151	10/1/2002	7:23.13 PM	26.325	26.239	24.978	27.052	26.646	46.335	48.507	7.764	39.496	-1.286	-5.748	45.898	0.194	0.001	132.95	2.21583	47.0	11.2	42.9	2.959	0.029	0.029	0.001	0.674	0.57
152	10/1/2002	7:24.13 PM	26.33	26.239	25.059	27.022	26.66	46.46	48.366	7.795	39.089	-1.292	-5.641	45.988	0.191	0.001	133.95	2.2325	46.9	11.2	42.6	2.936	0.028	0.028	0.001	0.686	0.57
153	10/1/2002	7:25.13 PM	26.329	26.238	25.048	27.091	26.655	45.909	48.062	7.781	38.892	-1.286	-5.748	45.81	0.19	0.001	134.95	2.24917	46.6	11.2	42.4	2.923	0.028	0.028	0.001	0.667	0.57
154	10/1/2002	7:26.13 PM	26.329	26.238	25.013	27.061	26.64	45.942	48.205	7.771	38.878	-1.289	-5.698	45.947	0.192	0.001	135.95	2.26583	46.7	11.2	42.4	2.924	0.029	0.029	0.001	0.675	0.57
155	10/1/2002	7:27.13 PM	26.334	26.238	25.093	26.986	26.626	46.269	48.569	7.87	39.197	-1.289	-5.656	46.169	0.192	0.001	136.95	2.2825	47.1	11.3	42.7	2.946	0.029	0.029	0.001	0.668	0.57
156	10/1/2002	7:28.13 PM	26.333	26.239	25.019	26.983	26.63	45.903	48.219	7.839	39.021	-1.289	-5.768	45.962	0.191	0.001	137.95	2.29917	46.7	11.2	42.9	2.928	0.028	0.028	0.001	0.662	0.56
157	10/1/2002	7:29.13 PM	26.324	26.213	25.089	27.031	26.6	46.18	48.6	7.836	39.042	-1.289	-5.71	46.996	0.191	0.001	138.95	2.31583	47.1	11.5	42.6	2.938	0.028	0.028	0.001	0.632	0.54
158	10/1/2002	7:30.13 PM	26.326	26.225	24.994	27.088	26.601	46.093	48.434	7.741	39.134	-1.289	-5.677	46.825	0.188	0.001	139.95	2.3325	47.0	11.2	42.6	2.938	0.028	0.028	0.001	0.668	0.56
159	10/1/2002	7:31.13 PM	26.331	26.215	25.064	27.058	26.586	46.222	48.449	7.699	39.455	-1.292	-5.686	46.798	0.191	0.001	140.95	2.34917	47.0	11.2	42.6	2.954	0.028	0.028	0.001	0.664	0.56
160	10/1/2002	7:32.13 PM	26.335	26.209	25.049	27.047	26.5	46.269	48.653	7.859	39.185	-1.292	-5.696	45.754	0.186	0.001	141.95	2.36583	47.2	11.2	42.7	2.946	0.028	0.028	0.001	0.648	0.55
161	10/1/2002	7:33.13 PM	26.33	26.219	25.045	26.965	26.605	46.864	48.908	7.84	39.688	-1.289	-5.78	45.794	0.187	0.001	142.95	2.3825	47.0	11.2	42.6	2.932	0.028	0.028	0.001	0.656	0.55
162	10/1/2002	7:34.13 PM	26.339	26.208	25.128	27.026	26.6	46.199	48.412	7.769	39.349	-1.284	-5.67	45.695	0.188	0.001	143.95	2.39917	46.9	11.2	42.4	2.949	0.028	0.028	0.001	0.653	0.56
163	10/1/2002	7:35.13 PM	26.339	26.208	24.993	27.026	26.6	46.248	48.567	7.857	39.148	-1.289	-5.676	45.725	0.186	0.001	144.95	2.41583	47.1	11.2	42.7	2.944	0.028	0.028	0.001	0.646	0.55
164	10/1/2002	7:36.13 PM	26.333	26.202	25.102	26.97	26.594	46.831	49.102	7.899	39.711	-1.289	-5.742	45.938	0.187	0.001	145.95	2.4325	47.6	11.2	43.3	2.983	0.028	0.028	0.001	0.642	0.55
165	10/1/2002	7:37.13 PM	26.338	26.202	25.017	27.026	26.6	46.38	48.616	7.837	39.186	-1.286	-5.636	45.962	0.186	0.001	146.95	2.44917	47.1	11.2	43.1	2.987	0.028	0.028	0.001	0.651	0.55
166	10/1/2002	7:38.13 PM	26.343	26.197	25.025	27.005	26.594	46.104	48.403	7.927	39.276	-1.286	-5.832	45.636	0.179	0.001	147.95	2.46583	46.9	11.2	42.4	2.924	0.027	0.027	0.001	0.629	0.54
167	10/1/2002	7:39.13 PM	26.339	26.198	24.977	27.001	26.6	46.002	48.209	7.81	39.244	-1.289	-5.803	45.544	0.186	0.001	148.95	2.4825	46.7	11.2	42.6	2.938	0.028	0.028	0.001	0.649	0.56
168	10/1/2002	7:40.13 PM	26.338	26.187	24.731	26.985	26.594	46.385	48.699	7.656	39.484	-1.286	-5.76	45.125	0.181	0.001	149.95	2.49917	47.2	11.1	42.9	2.960	0.027	0.027	0.001	0.633	0.54
169	10/1/2002	7:41.13 PM	26.288	26.187	24.716	26.95	26.594	46.497	48.676	7.602	39.742	-1.286	-5.667	45.364	0.184	0.001	150.95	2.51583	47.2	11.1	43.1	2.973	0.027	0.027	0.001	0.641	0.55
170	10/1/2002	7:42.13 PM	26.218	26.181	24.845	26.945	26.585	47.112	49.469	7.811	40.311	-1.289	-5.698	45.136	0.183	0.001	151.95	2.5325	47.0	11.1	43.1	2.974	0.026	0.026	0.001	0.612	0.52
171	10/1/2002	7:43.13 PM	26.183	26.187	24.756	26.91	26.574	46.478	48.589	7.572	39.803	-1.289	-5.777	45.146	0.176	0.001	152.95	2.54917	47.2	11.1	43.1	2.974	0.026	0.026	0.001	0.612	0.52
172	10/1/2002	7:44.13 PM	26.153	26.181	24.756	26.92	26.568	46.789	48.736	7.654	40.057	-1.286	-5.794	45.2	0												

261	10/1/2002	9:18:23 PM	26.304	26.168	25.176	26.806	26.634	47.462	49.21	7.523	40.008	-2.989	-8.029	44.426	0.154	0.001	248.12	4.13628	47.7	10.9	44.1	3.043	0.023	0.023	0.001	0.518	0.44
262	10/1/2002	9:19:23 PM	26.302	26.161	25.076	26.869	26.613	48.16	50.064	7.649	41.205	-1.292	-6.209	44.69	0.147	0.001	249.12	4.15194	48.6	11.0	44.7	3.081	0.022	0.022	0.000	0.489	0.42
263	10/1/2002	9:20:23 PM	26.312	26.176	25.196	26.834	26.613	47.586	49.148	7.438	41.023	-1.289	-6.214	44.699	0.155	0.001	250.12	4.16661	47.7	11.0	44.3	3.095	0.023	0.023	0.001	0.519	0.44
264	10/1/2002	9:21:23 PM	26.31	26.164	25.103	26.812	26.61	47.527	49.195	7.653	40.643	-1.286	-6.246	44.526	0.144	0.001	251.12	4.18528	47.7	10.9	44.1	3.043	0.023	0.023	0.001	0.519	0.44
265	10/1/2002	9:22:23 PM	26.313	26.162	25.157	26.777	26.613	47.377	49.044	7.526	40.329	-1.289	-6.214	44.317	0.151	0.001	252.12	4.20194	47.6	10.9	44.0	3.034	0.022	0.022	0.001	0.506	0.43
266	10/1/2002	9:23:23 PM	26.307	26.156	25.121	26.779	26.578	47.524	49.28	7.657	40.676	-1.289	-6.249	44.191	0.145	0.001	253.12	4.21861	47.8	10.8	44.0	3.037	0.022	0.022	0.000	0.488	0.42
267	10/1/2002	9:24:23 PM	26.311	26.155	25.126	26.754	26.567	47.589	49.03	7.651	40.753	-1.289	-6.249	44.667	0.157	0.001	254.12	4.23528	47.6	10.9	44.2	3.045	0.023	0.023	0.001	0.528	0.45
268	10/1/2002	9:25:23 PM	26.316	26.15	25.225	26.744	26.572	48.376	50.093	7.67	41.1	-1.286	-6.391	44.5	0.153	0.001	255.12	4.25194	48.6	10.9	45.0	3.098	0.023	0.023	0.001	0.504	0.43
269	10/1/2002	9:26:23 PM	26.32	26.146	25.116	26.794	26.606	47.929	49.667	7.804	40.684	-1.289	-6.206	44.21	0.119	0.001	256.12	4.26861	47.5	10.8	44.0	3.037	0.019	0.019	0.000	0.401	0.34
270	10/1/2002	9:27:23 PM	26.327	26.151	25.206	26.789	26.618	48.077	49.738	7.699	41.107	-1.289	-6.395	44.435	0.151	0.001	257.12	4.28528	48.3	10.9	44.6	3.074	0.023	0.023	0.001	0.502	0.43
271	10/1/2002	9:28:23 PM	26.333	26.142	25.177	26.856	26.624	47.939	49.382	7.646	41.079	-1.289	-6.258	44.525	0.155	0.001	258.12	4.30194	47.9	10.9	44.5	3.069	0.023	0.023	0.001	0.517	0.44
272	10/1/2002	9:29:23 PM	26.33	26.149	25.168	26.937	26.655	47.845	49.39	7.648	40.923	-1.289	-6.431	44.216	0.151	0.001	259.12	4.31861	47.9	10.8	44.4	3.060	0.023	0.023	0.001	0.505	0.43
273	10/1/2002	9:30:23 PM	26.336	26.157	25.255	26.976	26.687	47.444	49.618	7.556	40.916	-1.289	-6.44	44.299	0.151	0.001	260.12	4.33528	47.3	11.0	44.3	3.042	0.023	0.023	0.001	0.507	0.43
274	10/1/2002	9:31:23 PM	26.333	26.147	25.107	27.075	26.696	48.123	49.605	7.792	40.999	-1.292	-6.296	44.763	0.156	0.001	261.12	4.35194	48.1	11.0	44.6	3.072	0.023	0.023	0.001	0.520	0.44
275	10/1/2002	9:32:23 PM	26.35	26.164	25.238	27.116	26.72	47.932	49.456	7.646	41.166	-1.289	-6.408	44.609	0.153	0.001	262.12	4.36861	48.0	10.9	44.5	3.071	0.023	0.023	0.001	0.509	0.43
276	10/1/2002	9:33:23 PM	26.367	26.176	25.171	27.239	26.747	47.727	49.107	7.717	40.767	-1.289	-6.449	44.168	0.149	0.001	263.12	4.38528	47.6	10.8	44.2	3.051	0.022	0.022	0.000	0.500	0.43
277	10/1/2002	9:34:23 PM	26.359	26.163	25.213	27.275	26.769	47.794	49.298	7.716	40.819	-1.286	-6.491	44.701	0.159	0.001	264.12	4.40194	47.8	11.0	44.3	3.055	0.022	0.022	0.000	0.498	0.42
278	10/1/2002	9:35:23 PM	26.372	26.196	25.241	27.313	26.782	47.924	49.461	7.841	40.676	-1.292	-6.601	45.005	0.148	0.001	265.12	4.41861	47.5	11.0	44.3	3.052	0.022	0.022	0.000	0.492	0.42
279	10/1/2002	9:36:23 PM	26.38	26.214	25.169	27.352	26.821	47.885	49.351	7.745	40.936	-1.289	-6.481	44.571	0.146	0.001	266.12	4.43528	47.9	10.9	44.4	3.062	0.022	0.022	0.000	0.488	0.42
280	10/1/2002	9:37:23 PM	26.383	26.222	25.217	27.364	26.813	47.93	49.433	7.69	41.021	-1.289	-6.478	44.37	0.148	0.001	267.12	4.45194	48.0	10.9	44.5	3.066	0.022	0.022	0.000	0.493	0.42
281	10/1/2002	9:38:23 PM	26.374	26.218	24.903	27.326	26.795	47.82	49.187	7.592	41.111	-1.289	-6.4	44.363	0.149	0.001	268.12	4.46861	47.7	10.9	44.5	3.066	0.022	0.022	0.001	0.501	0.43
282	10/1/2002	9:39:23 PM	26.347	26.216	24.93	27.308	26.772	47.516	49.131	7.575	40.869	-1.289	-6.429	44.216	0.146	0.001	269.12	4.48528	47.7	10.8	44.1	3.040	0.022	0.022	0.000	0.496	0.42
283	10/1/2002	9:40:23 PM	26.292	26.211	24.7	27.298	26.762	47.359	49.447	7.462	40.553	-1.289	-6.51	44.351	0.144	0.001	270.12	4.50194	47.5	10.9	44.0	3.031	0.021	0.021	0.000	0.493	0.42
284	10/1/2002	9:41:23 PM	26.242	26.221	24.688	27.204	26.742	47.908	49.179	7.461	41.341	-1.289	-6.524	44.399	0.145	0.001	271.12	4.51861	47.7	10.9	44.6	3.077	0.022	0.022	0.000	0.489	0.42
285	10/1/2002	9:42:23 PM	26.193	26.227	24.791	27.115	26.778	47.698	49.198	7.537	41.064	-1.289	-6.342	44.768	0.136	0.001	272.12	4.53528	47.7	10.9	44.4	3.060	0.020	0.020	0.000	0.460	0.39
286	10/1/2002	9:43:23 PM	26.259	26.163	24.931	27.05	26.798	47.794	49.298	7.617	40.819	-1.286	-6.391	44.701	0.139	0.001	273.12	4.55194	47.9	10.9	44.4	3.062	0.021	0.021	0.000	0.491	0.43
287	10/1/2002	9:44:23 PM	26.134	26.228	24.637	27.05	26.804	48.065	49.605	7.509	41.47	-1.289	-6.431	44.519	0.144	0.001	274.12	4.56861	48.1	10.9	44.8	3.087	0.022	0.022	0.000	0.495	0.43
288	10/1/2002	9:45:23 PM	26.134	26.233	24.862	27.04	26.814	47.881	49.394	7.482	41.351	-1.289	-6.46	44.405	0.151	0.001	275.12	4.58528	47.9	10.9	44.6	3.078	0.023	0.023	0.001	0.497	0.43
289	10/1/2002	9:46:23 PM	26.109	26.218	24.627	26.976	26.804	47.63	49.235	7.569	40.763	-1.295	-6.399	44.546	0.141	0.001	276.12	4.60194	47.8	10.9	44.2	3.047	0.021	0.021	0.000	0.478	0.41
290	10/1/2002	9:47:23 PM	26.124	26.233	24.967	27.01	26.819	47.615	49.047	7.545	40.89	-1.286	-6.391	44.497	0.146	0.001	277.12	4.61861	47.6	10.9	44.3	3.051	0.022	0.022	0.000	0.492	0.42
291	10/1/2002	9:48:23 PM	26.129	26.228	24.802	26.976	26.804	48.141	49.715	7.575	40.969	-1.289	-6.429	44.526	0.145	0.001	278.12	4.63528	48.2	10.9	44.5	3.068	0.021	0.021	0.000	0.498	0.42
292	10/1/2002	9:49:23 PM	26.133	26.232	24.976	26.905	26.793	47.976	49.316	7.608	41.197	-1.286	-6.443	44.683	0.149	0.001	279.12	4.65194	47.8	10.9	44.6	3.074	0.022	0.022	0.000	0.499	0.42
293	10/1/2002	9:50:23 PM	26.147	26.236	25.001	26.894	26.822	47.995	49.644	7.607	41.072	-1.286	-6.327	44.321	0.144	0.001	280.12	4.66861	48.2	10.9	44.5	3.070	0.021	0.021	0.000	0.482	0.41
294	10/1/2002	9:51:23 PM	26.145	26.229	24.954	26.872	26.781	47.77	49.142	7.466	41.038	-1.289	-6.379	44.501	0.147	0.001	281.12	4.68528	47.7	10.9	44.4	3.069	0.022	0.022	0.000	0.495	0.42
295	10/1/2002	9:52:23 PM	26.154	26.233	24.967	26.856	26.769	47.943	49.436	7.564	41.031	-1.286	-6.379	44.403	0.145	0.001	282.12	4.70194	47.6	10.8	44.3	3.062	0.021	0.021	0.000	0.477	0.41
296	10/1/2002	9:53:23 PM	26.163	26.232	24.976	26.865	26.783	48.069	49.287	7.563	41.289	-1.286	-6.504	45.06	0.148	0.001	283.12	4.71861	47.8	11.0	44.7	3.080	0.022	0.022	0.000	0.494	0.42
297	10/1/2002	9:54:23 PM	26.162	26.231	25.056	26.849	26.762	48.141	49.512	7.625	41.195	-1.286	-6.397	44.8	0.144	0.001	284.12	4.73528	48.0	11.0	44.7	3.079	0.021	0.021	0.000	0.480	0.41
298	10/1/2002	9:55:23 PM	26.185	26.234	25.074	26.882	26.786	47.692	49.078	7.487	41.005	-1.286	-6.395	44.4													

391	10/1/2002	11:28:18 PM	26.169	24.967	25.222	26.351	24.738	47.104	49.673	7.609	40.237	-1.286	-6.753	44.567	0.119	0.001	378.03	6.30056	47.8	10.9	43.7	3.011	0.018	0.018	0.000	0.404	0.34
392	10/1/2002	11:29:18 PM	26.162	24.934	25.275	26.239	24.706	47.557	49.595	7.7	40.688	-1.286	-6.811	45.001	0.123	0.001	379.03	6.31722	48.1	11.0	44.1	3.042	0.018	0.018	0.000	0.412	0.35
393	10/1/2002	11:30:18 PM	26.177	24.939	25.3	26.294	24.706	47.823	50.137	7.756	40.767	-1.286	-6.814	44.672	0.121	0.001	380.03	6.33389	48.7	10.9	44.3	3.054	0.018	0.018	0.000	0.404	0.34
394	10/1/2002	11:31:18 PM	26.183	24.931	25.246	26.275	24.711	47.752	49.916	7.711	40.749	-1.286	-6.808	44.741	0.122	0.001	381.03	6.35056	48.4	11.0	44.3	3.051	0.018	0.018	0.000	0.406	0.35
395	10/1/2002	11:32:18 PM	26.191	24.934	25.339	26.253	24.73	47.692	49.855	7.736	40.564	-1.286	-6.812	44.359	0.117	0.001	382.03	6.36722	48.4	10.9	44.2	3.045	0.017	0.017	0.000	0.391	0.33
396	10/1/2002	11:33:18 PM	26.183	24.921	25.236	26.225	24.727	47.526	49.858	7.688	40.51	-1.286	-6.805	44.476	0.121	0.001	383.03	6.38389	48.4	10.9	44.0	3.038	0.018	0.018	0.000	0.407	0.36
397	10/1/2002	11:34:18 PM	26.181	24.889	25.289	26.173	24.67	47.566	49.692	7.642	40.716	-1.286	-6.814	44.594	0.121	0.001	384.03	6.40056	48.2	10.9	44.1	3.043	0.018	0.018	0.000	0.406	0.34
398	10/1/2002	11:35:18 PM	26.188	24.881	25.317	26.219	24.643	47.088	49.216	7.573	40.137	-1.281	-6.834	44.253	0.122	0.002	385.03	6.41722	47.7	10.9	43.6	3.007	0.018	0.018	0.000	0.402	0.35
399	10/1/2002	11:36:18 PM	26.191	24.879	25.249	26.193	24.615	47.655	49.275	7.665	40.659	-1.284	-6.763	44.326	0.122	0.001	386.03	6.43389	48.2	10.9	44.2	3.051	0.018	0.018	0.000	0.402	0.34
400	10/1/2002	11:37:18 PM	26.162	24.865	25.32	26.155	24.591	47.462	48.795	7.651	40.697	-1.289	-6.805	44.395	0.122	0.001	387.03	6.45056	48.3	10.9	44.0	3.038	0.018	0.018	0.000	0.409	0.35
401	10/1/2002	11:38:18 PM	26.169	24.836	25.237	26.156	24.562	47.419	48.709	7.711	40.354	-1.284	-6.819	44.411	0.118	0.001	388.03	6.46722	48.2	10.9	43.9	3.028	0.017	0.017	0.000	0.398	0.34
402	10/1/2002	11:39:18 PM	26.165	24.832	25.298	26.107	24.543	47.497	48.913	7.672	40.421	-1.289	-6.846	44.437	0.122	0.001	389.03	6.48389	48.4	10.9	44.0	3.031	0.018	0.018	0.000	0.410	0.35
403	10/1/2002	11:40:18 PM	26.157	24.819	25.295	26.139	24.525	47.481	48.937	7.719	40.469	-1.286	-6.819	44.399	0.12	0.001	390.03	6.50056	48.1	10.9	44.0	3.033	0.018	0.018	0.000	0.403	0.34
404	10/1/2002	11:41:18 PM	26.163	24.801	25.236	26.136	24.512	47.559	48.916	7.735	40.501	-1.292	-6.822	44.346	0.12	0.001	391.03	6.51722	48.3	10.9	44.0	3.036	0.018	0.018	0.000	0.404	0.34
405	10/1/2002	11:42:18 PM	26.165	24.787	25.343	26.077	24.488	46.911	48.16	7.581	40.153	-1.286	-6.837	44.391	0.121	0.001	392.03	6.53389	47.7	10.9	43.5	3.001	0.018	0.018	0.000	0.410	0.35
406	10/1/2002	11:43:18 PM	26.158	24.775	25.236	26.05	24.471	47.346	48.525	7.688	40.448	-1.292	-6.846	44.365	0.122	0.001	393.03	6.55056	48.1	10.9	43.9	3.027	0.018	0.018	0.000	0.412	0.35
407	10/1/2002	11:44:18 PM	26.17	24.767	25.323	26.037	24.446	47.514	48.958	7.676	40.681	-1.286	-6.843	44.356	0.121	0.001	394.03	6.56722	48.4	10.9	44.1	3.040	0.018	0.018	0.000	0.405	0.34
408	10/1/2002	11:45:18 PM	26.178	24.765	25.366	26.045	24.461	47.479	48.988	7.743	40.487	-1.286	-6.831	44.321	0.119	0.001	395.03	6.58389	48.1	10.9	44.0	3.032	0.018	0.018	0.000	0.399	0.34
409	10/1/2002	11:46:18 PM	26.181	24.764	25.289	26.089	24.47	47.384	48.946	7.695	40.374	-1.284	-6.877	44.325	0.117	0.001	396.03	6.60056	48.0	10.9	43.9	3.025	0.017	0.017	0.000	0.394	0.34
410	10/1/2002	11:47:18 PM	26.181	24.758	25.374	26.073	24.494	47.355	48.906	7.642	40.689	-1.289	-6.814	44.211	0.12	0.001	397.03	6.61722	48.0	10.9	44.0	3.032	0.018	0.018	0.000	0.403	0.34
411	10/1/2002	11:48:18 PM	26.18	24.763	25.308	26.132	24.524	47.34	48.967	7.757	40.217	-1.289	-6.825	44.223	0.117	0.001	398.03	6.63389	48.2	10.9	43.8	3.018	0.017	0.017	0.000	0.395	0.34
412	10/1/2002	11:49:18 PM	26.175	24.763	25.336	26.147	24.564	47.33	48.934	7.611	40.436	-1.289	-6.837	44.474	0.118	0.001	399.03	6.65056	48.2	10.9	43.9	3.026	0.018	0.018	0.000	0.397	0.34
413	10/1/2002	11:50:18 PM	26.186	24.779	25.399	26.229	24.62	47.431	49.537	7.646	40.618	-1.286	-6.86	44.497	0.117	0.001	400.03	6.66722	48.1	10.9	44.0	3.035	0.017	0.017	0.000	0.392	0.33
414	10/1/2002	11:51:18 PM	26.198	24.79	25.311	26.215	24.672	47.4	49.655	7.753	40.301	-1.286	-6.86	44.325	0.118	0.001	401.03	6.68389	48.2	10.9	43.9	3.023	0.018	0.018	0.000	0.398	0.34
415	10/1/2002	11:52:18 PM	26.199	24.812	25.407	26.337	24.723	47.448	49.664	7.712	40.53	-1.284	-6.951	44.284	0.118	0.001	402.03	6.70056	48.2	10.9	44.0	3.033	0.018	0.018	0.000	0.395	0.34
416	10/1/2002	11:53:18 PM	26.202	24.816	25.346	26.299	24.736	47.361	49.627	7.611	40.423	-1.286	-6.903	44.379	0.117	0.001	403.03	6.71722	48.1	10.9	44.1	3.037	0.018	0.018	0.000	0.392	0.33
417	10/1/2002	11:54:18 PM	26.213	24.861	25.381	26.201	24.862	47.259	49.525	7.646	40.403	-1.286	-6.863	44.344	0.117	0.001	404.03	6.73389	48.1	10.9	43.9	3.022	0.018	0.018	0.000	0.394	0.34
418	10/1/2002	11:55:18 PM	26.228	24.889	25.446	26.275	24.942	47.355	49.916	7.817	40.174	-1.289	-6.861	44.279	0.118	0.001	405.03	6.75056	48.4	10.9	43.8	3.017	0.018	0.018	0.000	0.397	0.34
419	10/1/2002	11:56:18 PM	26.225	24.893	25.323	26.238	24.99	47.454	49.897	7.834	40.17	-1.292	-6.868	44.554	0.115	0.001	406.03	6.76722	48.4	10.9	43.8	3.021	0.017	0.017	0.000	0.388	0.33
420	10/1/2002	11:57:18 PM	26.225	24.917	25.433	26.557	24.994	47.199	49.576	7.663	40.35	-1.286	-6.892	44.468	0.116	0.001	407.03	6.78389	48.1	10.9	43.8	3.018	0.017	0.017	0.000	0.390	0.33
421	10/1/2002	11:58:18 PM	26.225	24.899	25.414	26.153	24.925	47.508	49.576	7.713	40.612	-1.286	-6.903	44.015	0.115	0.001	408.03	6.80056	48.6	10.9	43.9	3.026	0.017	0.017	0.000	0.385	0.33
422	10/1/2002	11:59:18 PM	26.223	24.931	25.386	26.43	24.962	47.197	49.537	7.652	40.229	-1.281	-6.892	44.166	0.117	0.001	409.03	6.81722	48.1	10.9	43.7	3.014	0.017	0.017	0.000	0.395	0.34
423	10/2/2002	12:00:18 AM	26.231	24.934	25.439	26.373	24.97	47.191	49.615	7.687	40.262	-1.281	-6.513	44.363	0.081	0.001	410.03	6.83389	48.1	10.9	43.7	3.015	0.017	0.017	0.000	0.273	0.23
424	10/2/2002	12:01:18 AM	26.228	24.936	25.311	26.39	24.947	47.675	50.191	7.855	40.614	-1.286	-6.796	44.242	0.121	0.001	411.03	6.85056	48.7	10.8	44.1	3.040	0.018	0.018	0.000	0.406	0.35
425	10/2/2002	12:02:18 AM	26.23	24.936	25.336	26.335	24.927	47.348	49.677	7.611	40.348	-1.286	-6.796	44.379	0.121	0.001	412.03	6.86722	48.7	10.8	44.1	3.041	0.018	0.018	0.000	0.395	0.34
426	10/2/2002	12:03:18 AM	26.232	24.936	25.395	26.335	24.927	47.185	49.818	7.92	40.17	-1.286	-6.394	44.999	0.112	0.001	413.03	6.88389	48.3	11.0	43.7	3.011	0.017	0.017	0.000	0.379	0.32
427	10/2/2002	12:04:18 AM	26.224	24.921	25.362	26.246	24.883	47.528	50.178	7.777	40.378	-1.286	-6.232	44.426	0.159	0.002	414.03	6.90056	48.7	10.9	44.0	3.030	0.024	0.023	0.001	0.534	0.46
428	10/2/2002	12:05:18 AM	26.219	24.911	25.402	26.196	24.863	47.427	50.025	7.																	

521	10/2/2002	1:38:07 AM	26.146	24.493	25.374	25.598	24.199	46.377	49.735	7.805	39.334	-1.286	-7.155	0.099	0.001	0	507.85	6.46417	48.3	0	42.9	2.955	0.000	0.000	0.003	0.00
522	10/2/2002	1:39:07 AM	26.139	24.466	25.453	25.511	24.197	45.778	49.158	7.719	38.724	-1.289	-7.138	0.099	0.001	0	508.85	6.46083	47.7	0.0	42.3	2.913	0.000	0.000	0.003	0.00
523	10/2/2002	1:40:07 AM	26.153	24.47	25.451	25.535	24.211	46.176	49.603	7.793	39.081	-1.292	-7.123	0.099	0.001	0	509.85	6.4975	48.1	0.0	42.6	2.939	0.000	0.000	0.003	0.00
524	10/2/2002	1:41:07 AM	26.157	24.474	25.453	25.604	24.23	45.735	49.3	7.838	39.597	-1.286	-7.15	0.1	0.1	0.1	510.85	6.51417	48.5	0.0	42.7	2.946	0.000	0.000	0.003	0.00
525	10/2/2002	1:42:07 AM	26.167	24.473	25.415	25.609	24.264	45.362	49.895	7.807	39.269	-1.293	-7.109	0.101	0.001	0	511.85	6.53083	48.4	0.0	42.6	2.952	0.000	0.000	0.003	0.00
526	10/2/2002	1:43:07 AM	26.172	24.499	25.03	25.729	24.31	45.043	49.634	7.589	39.196	-1.292	-7.092	0.099	0.001	0	512.85	6.5475	48.2	0.0	42.6	2.938	0.000	0.000	0.003	0.00
527	10/2/2002	1:44:07 AM	26.116	24.483	24.843	25.763	24.339	46.532	50.311	7.559	39.691	-1.286	-7.119	0.098	0.001	0	513.85	6.56417	48.6	0.0	43.1	2.972	0.000	0.000	0.003	0.00
528	10/2/2002	1:45:07 AM	26.072	24.513	24.964	25.624	24.405	46.132	49.522	7.572	39.393	-1.286	-7.141	0.097	0.001	0	514.85	6.58083	48.0	0.0	42.7	2.945	0.000	0.000	0.004	0.00
529	10/2/2002	1:46:07 AM	26.087	24.536	24.945	25.909	24.455	45.031	49.565	7.508	39.154	-1.286	-7.144	0.097	0.001	0	515.85	6.5975	48.1	0.0	42.6	2.937	0.000	0.000	0.004	0.00
530	10/2/2002	1:47:07 AM	26.062	24.564	24.98	25.935	24.511	45.814	49.231	7.438	39.169	-1.286	-7.129	0.095	0.001	0	516.85	6.61417	47.8	0.0	42.5	2.930	0.000	0.000	0.004	0.00
531	10/2/2002	1:48:07 AM	26.028	24.575	24.951	25.975	24.577	46.083	49.624	7.608	39.259	-1.292	-7.147	0.097	0.001	0	517.85	6.63083	48.2	0.0	42.7	2.942	0.000	0.000	0.003	0.00
532	10/2/2002	1:49:07 AM	26.019	24.611	25.021	26.056	24.637	46.128	49.689	7.645	39.076	-1.286	-7.158	0.098	0.001	0	518.85	6.6475	48.2	0.0	42.6	2.937	0.000	0.000	0.003	0.00
533	10/2/2002	1:50:07 AM	26.035	24.637	25.093	26.087	24.644	45.245	49.87	7.659	39.352	-1.286	-7.133	0.096	0.001	0	519.85	6.66417	48.4	0.0	42.6	2.952	0.000	0.000	0.003	0.00
534	10/2/2002	1:51:07 AM	26.001	24.649	25.029	26.129	24.726	46.211	49.551	7.591	39.293	-1.286	-7.106	0.099	0.001	0	520.85	6.68083	48.1	0.0	42.6	2.948	0.000	0.000	0.003	0.00
535	10/2/2002	1:52:07 AM	26.003	24.67	25.116	26.115	24.747	45.967	49.647	7.623	39.015	-1.284	-7.132	0.097	0.001	0	521.85	6.6975	48.2	0.0	42.5	2.930	0.000	0.000	0.003	0.00
536	10/2/2002	1:53:07 AM	26.006	24.682	25.143	26.082	24.734	46.209	50.019	7.693	39.113	-1.289	-7.126	0.094	0.001	0	522.85	6.71417	48.5	0.0	42.7	2.942	0.000	0.000	0.003	0.00
537	10/2/2002	1:54:07 AM	26.007	24.684	25.094	26.019	24.705	46.253	49.812	7.65	39.302	-1.284	-7.15	0.098	0.001	0	523.85	6.73083	48.3	0.0	42.6	2.952	0.000	0.000	0.003	0.00
538	10/2/2002	1:55:07 AM	26.012	24.684	25.195	26.07	24.691	45.923	49.598	7.632	39.968	-1.286	-7.096	0.099	0.001	0	524.85	6.7475	48.1	0.0	42.6	2.937	0.000	0.000	0.003	0.00
539	10/2/2002	1:56:07 AM	26.013	24.685	25.146	25.94	24.657	46.087	49.816	7.644	39.034	-1.286	-7.121	0.096	0.001	0	525.85	6.76417	48.3	0.0	42.6	2.934	0.000	0.000	0.003	0.00
540	10/2/2002	1:57:07 AM	26.007	24.684	25.155	25.865	24.621	45.894	49.502	7.611	39.817	-1.292	-7.132	0.096	0.001	0	526.85	6.78083	48.0	0.0	42.4	2.924	0.000	0.000	0.004	0.00
541	10/2/2002	1:58:07 AM	26.008	24.649	25.224	25.809	24.58	46.087	49.725	7.597	39.336	-1.286	-7.118	0.095	0.001	0	527.85	6.7975	48.3	0.0	42.7	2.945	0.000	0.000	0.003	0.00
542	10/2/2002	1:59:07 AM	26.029	24.636	25.142	25.777	24.536	45.889	49.529	7.632	39.962	-1.286	-7.109	0.098	0.001	0	528.85	6.81417	48.1	0.0	42.4	2.926	0.000	0.000	0.003	0.00
543	10/2/2002	2:00:07 AM	26.044	24.636	25.237	25.671	24.512	45.352	50.342	7.804	39.866	-1.286	-7.106	0.095	0.001	0	529.85	6.83083	48.9	0.0	42.7	2.941	0.000	0.000	0.003	0.00
544	10/2/2002	2:01:07 AM	26.058	24.635	25.236	25.666	24.491	46.093	49.713	7.656	39.156	-1.284	-7.095	0.097	0.001	0	530.85	6.8475	48.2	0.0	42.6	2.939	0.000	0.000	0.003	0.00
545	10/2/2002	2:02:07 AM	26.066	24.603	25.204	25.638	24.439	46.267	49.971	7.767	39.126	-1.289	-7.096	0.095	0.001	0	531.85	6.86417	48.5	0.0	42.7	2.944	0.000	0.000	0.003	0.00
546	10/2/2002	2:03:07 AM	26.065	24.598	25.263	25.57	24.408	45.25	49.986	7.691	39.391	-1.286	-7.103	0.095	0.001	0	532.85	6.88083	48.5	0.0	42.7	2.945	0.000	0.000	0.003	0.00
547	10/2/2002	2:04:07 AM	26.068	24.58	25.211	25.622	24.376	46.162	49.725	7.642	39.197	-1.289	-7.144	0.095	0.001	0	533.85	6.8975	48.3	0.0	42.7	2.943	0.000	0.000	0.003	0.00
548	10/2/2002	2:05:07 AM	26.072	24.569	25.285	25.574	24.35	46.139	49.661	7.691	39.14	-1.286	-7.152	0.096	0.001	0	534.85	6.91417	48.2	0.0	42.6	2.940	0.000	0.000	0.003	0.00
549	10/2/2002	2:06:07 AM	26.082	24.568	25.31	25.679	24.33	46.07	49.615	7.679	39.142	-1.286	-7.152	0.097	0.001	0	535.85	6.93083	48.1	0.0	42.6	2.938	0.000	0.000	0.003	0.00
550	10/2/2002	2:07:07 AM	26.087	24.538	25.245	25.654	24.305	45.751	49.545	7.689	39.796	-1.284	-7.121	0.094	0.001	0	536.85	6.9475	48.1	0.0	42.3	2.915	0.000	0.000	0.004	0.00
551	10/2/2002	2:08:07 AM	26.091	24.518	25.329	25.662	24.281	45.807	49.4	7.611	39.222	-1.284	-7.173	0.095	0.001	0	537.85	6.96417	47.9	0.0	42.4	2.921	0.000	0.000	0.003	0.00
552	10/2/2002	2:09:07 AM	26.09	24.512	25.288	25.532	24.243	46.143	49.973	7.72	39.034	-1.286	-7.147	0.094	0.001	0	538.85	6.98083	48.5	0.0	42.6	2.936	0.000	0.000	0.003	0.00
553	10/2/2002	2:10:07 AM	26.088	24.49	25.291	25.475	24.211	46.033	49.694	7.696	39.023	-1.289	-7.167	0.096	0.001	0	539.85	6.9975	48.2	0.0	42.5	2.932	0.000	0.000	0.003	0.00
554	10/2/2002	2:11:07 AM	26.072	24.464	25.34	25.404	24.17	46.28	50.095	7.784	39.111	-1.289	-7.129	0.093	0.001	0	540.85	6.91417	48.6	0.0	42.7	2.944	0.000	0.000	0.003	0.00
555	10/2/2002	2:12:07 AM	26.068	24.44	25.153	25.428	24.153	45.361	49.894	7.708	39.167	-1.286	-7.181	0.095	0.001	0	541.85	6.93083	48.5	0.0	42.6	2.937	0.000	0.000	0.003	0.00
556	10/2/2002	2:13:07 AM	26.071	24.453	25.384	25.463	24.136	46.323	49.332	7.711	38.665	-1.289	-7.129	0.095	0.001	0	542.85	6.9475	47.9	0.0	42.7	2.907	0.000	0.000	0.004	0.00
557	10/2/2002	2:14:07 AM	26.099	24.42	25.352	25.446	24.151	46.294	49.88	7.679	39.353	-1.284	-7.156	0.096	0.001	0	543.85	6.96417	48.4	0.0	42.8	2.953	0.000	0.000	0.003	0.00
558	10/2/2002	2:15:07 AM	26.002	24.413	25.305	25.514	24.164	46.099	49.8	7.666	39.305	-1.286	-7.123	0.094	0.001	0	544.85	6.98083	48.3	0.0	42.7	2.943	0.000	0.000	0.003	0.00
559	10/2/2002	2:16:07 AM	26.015	24.427	25.396	25.537	24.198	45.961	49.661	7.703	39.745	-1.286	-7.152	0.095	0.001	0	545.85	6.9975	48.2	0.0	42.3	2.917	0.000	0.000	0.003	0.00
560	10/2/2002	2:17:07 AM	26.024	24.418	25.322	25.662	24.242	45.342	50.35	7.711	39.222	-1.284	-7.138	0.095	0.001											

651	10/2/2002	3:59.04 AM	26.079	24.506	25.507	26.016	24.557	48.419	49.971	7.776	41.629	-1.286	-6.625	43.929	0.12	0.001	0	648.80	10.8133	48.5	10.8	45.0	3.104	0.018	0.018	0.000	0.392	0.33
652	10/2/2002	4:00.04 AM	26.081	24.518	25.609	26.038	24.58	48.231	49.978	7.785	41.617	-1.281	-6.625	43.95	0.117	0.001	0	649.90	10.83	48.5	10.8	44.8	3.088	0.017	0.017	0.000	0.383	0.33
653	10/2/2002	4:01.04 AM	26.089	24.526	25.503	26.087	24.608	48.291	49.939	7.773	41.617	-1.286	-6.724	43.986	0.119	0.001	0	650.80	10.8467	48.4	10.8	45.0	3.099	0.018	0.017	0.000	0.389	0.33
654	10/2/2002	4:03.04 AM	26.101	24.538	25.595	25.973	24.611	48.259	49.786	7.775	41.549	-1.286	-6.889	43.954	0.119	0.001	0	651.90	10.8623	48.3	10.8	44.9	3.097	0.018	0.017	0.000	0.385	0.33
655	10/2/2002	4:03.04 AM	26.082	24.518	25.54	26.884	24.596	47.997	49.595	7.771	41.177	-1.289	-6.724	43.908	0.118	0.001	0	652.80	10.88	48.1	10.8	44.6	3.074	0.018	0.017	0.000	0.389	0.33
656	10/2/2002	4:04.04 AM	26.09	24.517	25.523	26.844	24.564	48.077	49.783	7.741	41.363	-1.289	-6.721	43.946	0.119	0.001	0	653.80	10.8967	48.3	10.8	44.7	3.083	0.018	0.017	0.000	0.391	0.33
657	10/2/2002	4:05.04 AM	26.099	24.521	25.598	26.712	24.538	48.332	50.027	7.782	41.457	-1.286	-6.854	44.063	0.118	0.001	0	654.80	10.9133	48.6	10.8	44.9	3.095	0.018	0.017	0.000	0.386	0.33
658	10/2/2002	4:06.04 AM	26.093	24.489	25.465	26.51	24.511	48.046	49.534	7.684	41.462	-1.289	-6.735	43.984	0.118	0.001	0	655.80	10.919	48.2	10.8	44.8	3.086	0.018	0.017	0.000	0.388	0.33
659	10/2/2002	4:07.04 AM	26.107	24.503	25.585	26.579	24.485	48.413	50.046	7.787	41.514	-1.286	-6.889	43.954	0.118	0.001	0	656.80	10.9467	48.6	10.8	45.0	3.103	0.018	0.017	0.000	0.384	0.33
660	10/2/2002	4:08.04 AM	26.105	24.502	25.518	26.677	24.474	48.16	49.951	7.701	41.517	-1.289	-6.896	44.101	0.114	0.001	0	657.80	10.9633	48.4	10.8	44.8	3.091	0.017	0.017	0.000	0.374	0.32
661	10/2/2002	4:09.04 AM	26.104	24.491	25.542	26.696	24.452	47.947	49.76	7.785	41.001	-1.289	-6.738	43.862	0.117	0.001	0	658.80	10.98	48.3	10.7	44.5	3.066	0.017	0.017	0.000	0.386	0.33
662	10/2/2002	4:10.04 AM	26.102	24.483	25.605	26.629	24.425	48.168	49.901	7.796	41.337	-1.286	-6.932	43.964	0.116	0.001	0	659.80	10.9967	48.4	10.7	44.6	3.088	0.017	0.017	0.000	0.380	0.32
663	10/2/2002	4:11.04 AM	26.104	24.471	25.597	26.593	24.392	47.613	49.56	7.932	40.739	-1.284	-6.744	43.797	0.115	0.001	0	660.80	11.0133	48.1	10.7	44.2	3.046	0.017	0.017	0.000	0.379	0.32
664	10/2/2002	4:12.04 AM	26.112	24.473	25.611	26.514	24.37	48.245	49.963	7.753	41.496	-1.286	-6.898	43.917	0.116	0.001	0	661.80	11.03	48.5	10.8	44.9	3.094	0.017	0.017	0.000	0.379	0.32
665	10/2/2002	4:13.04 AM	26.115	24.461	25.528	26.537	24.338	48.429	50.482	7.8	41.543	-1.289	-6.707	43.896	0.112	0.001	0	662.80	11.0467	49.0	10.8	45.0	3.102	0.017	0.016	0.000	0.366	0.31
666	10/2/2002	4:14.04 AM	26.113	24.449	25.571	26.55	24.311	48.365	50.447	7.894	41.382	-1.286	-6.899	43.812	0.117	0.001	0	663.80	11.0633	49.0	10.7	44.9	3.094	0.017	0.017	0.000	0.383	0.33
667	10/2/2002	4:15.04 AM	26.128	24.464	25.636	26.455	24.301	48.03	49.989	7.799	41.242	-1.286	-6.721	43.945	0.117	0.001	0	664.80	11.08	48.5	10.7	44.6	3.077	0.017	0.017	0.000	0.384	0.33
668	10/2/2002	4:16.04 AM	26.115	24.437	25.544	26.462	24.368	48.16	49.884	7.799	41.15	-1.286	-6.733	44.002	0.116	0.001	0	665.80	11.0967	48.6	10.8	44.5	3.075	0.017	0.017	0.000	0.383	0.33
669	10/2/2002	4:17.04 AM	26.12	24.437	25.639	26.407	24.253	47.808	49.783	7.748	41.023	-1.286	-6.733	43.753	0.116	0.001	0	666.80	11.1133	48.3	10.7	44.4	3.062	0.017	0.017	0.000	0.382	0.33
670	10/2/2002	4:18.04 AM	26.12	24.427	25.599	26.498	24.248	48.206	49.93	7.882	41.234	-1.284	-6.895	43.81	0.113	0.001	0	667.80	11.13	48.5	10.7	44.7	3.083	0.017	0.017	0.000	0.371	0.32
671	10/2/2002	4:19.04 AM	26.126	24.427	25.624	26.553	24.248	47.928	49.978	7.822	41.034	-1.284	-6.701	43.931	0.112	0.001	0	668.80	11.1467	48.5	10.8	44.5	3.067	0.017	0.016	0.000	0.369	0.31
672	10/2/2002	4:20.04 AM	26.125	24.422	25.549	26.563	24.251	47.984	50.131	7.923	40.947	-1.289	-6.704	44.122	0.113	0.001	0	669.80	11.1633	48.7	10.8	44.4	3.062	0.017	0.017	0.000	0.372	0.32
673	10/2/2002	4:21.04 AM	26.136	24.433	25.574	26.668	24.289	47.999	49.613	7.705	41.45	-1.289	-6.738	43.977	0.115	0.001	0	670.80	11.18	48.1	10.8	44.7	3.084	0.017	0.017	0.000	0.377	0.32
674	10/2/2002	4:22.04 AM	26.143	24.429	25.681	26.655	24.311	47.812	49.742	7.811	40.892	-1.286	-6.709	43.145	0.115	0.001	0	671.80	11.1967	48.3	10.6	44.4	3.068	0.017	0.017	0.000	0.379	0.32
675	10/2/2002	4:23.04 AM	26.138	24.43	25.566	26.731	24.311	47.845	49.786	7.847	40.946	-1.292	-6.878	43.87	0.114	0.001	0	672.80	11.2133	48.3	10.6	44.4	3.061	0.017	0.017	0.000	0.377	0.32
676	10/2/2002	4:24.04 AM	26.139	24.428	25.595	26.709	24.365	48.153	50.123	7.823	41.023	-1.286	-6.833	43.954	0.115	0.001	0	673.80	11.229	48.5	10.7	44.6	3.077	0.017	0.017	0.000	0.372	0.32
677	10/2/2002	4:25.04 AM	26.157	24.464	25.681	26.785	24.406	48.164	50.067	7.826	41.455	-1.286	-6.727	43.807	0.111	0.001	0	674.80	11.2467	48.6	10.7	44.8	3.089	0.017	0.016	0.000	0.362	0.31
678	10/2/2002	4:26.04 AM	26.16	24.456	25.618	26.887	24.443	48.156	50.232	7.904	41.04	-1.289	-6.704	43.923	0.113	0.001	0	675.80	11.2633	48.8	10.6	44.6	3.075	0.017	0.017	0.000	0.371	0.32
679	10/2/2002	4:27.04 AM	26.177	24.484	25.731	26.895	24.486	48.137	50.404	7.819	41.377	-1.286	-6.868	43.789	0.112	0.001	0	676.80	11.28	48.6	10.7	44.8	3.086	0.017	0.016	0.000	0.366	0.31
680	10/2/2002	4:28.04 AM	26.169	24.486	25.612	26.021	24.537	47.773	49.939	7.805	40.804	-1.289	-6.707	43.747	0.114	0.001	0	677.80	11.2967	48.4	10.7	44.3	3.054	0.017	0.017	0.000	0.377	0.32
681	10/2/2002	4:29.04 AM	26.186	24.518	25.695	26.913	24.575	48.296	50.18	7.923	41.162	-1.286	-6.888	43.849	0.113	0.001	0	678.80	11.3133	48.7	10.7	44.7	3.101	0.017	0.016	0.000	0.368	0.31
682	10/2/2002	4:30.04 AM	26.195	24.512	25.683	26.088	24.614	48.092	50.033	7.859	41.226	-1.289	-6.735	43.796	0.113	0.001	0	679.80	11.33	48.6	10.7	44.7	3.079	0.017	0.017	0.000	0.370	0.31
683	10/2/2002	4:31.04 AM	26.193	24.53	25.661	26.135	24.647	47.642	49.632	7.821	40.7	-1.286	-6.689	43.778	0.113	0.001	0	680.80	11.3467	48.2	10.7	44.2	3.045	0.017	0.017	0.000	0.374	0.32
684	10/2/2002	4:32.04 AM	26.202	24.543	25.75	26.049	24.666	47.81	49.908	7.843	41.017	-1.289	-6.704	43.895	0.107	0.001	0	681.80	11.3633	48.3	10.7	44.4	3.062	0.016	0.016	0.000	0.352	0.30
685	10/2/2002	4:33.04 AM	26.229	24.468	25.626	26.077	24.668	47.901	49.744	7.823	41.156	-1.286	-6.833	44.099	0.111	0.001	0	682.80	11.38	48.5	10.8	44.6	3.076	0.016	0.016	0.000	0.363	0.31
686	10/2/2002	4:34.04 AM	26.217	24.548	25.74	26.964	24.655	48.16	50.176	7.934	41.038	-1.289	-6.695	44.036	0.108	0.001	0	683.80	11.3967	48.7	10.8	44.6	3.075	0.016	0.016	0.000	0.354	0.30
687	10/2/2002	4:35.04 AM	26.207	24.533	25.67	26.934	24.625	48.119	49.991	7.831	41.256	-1.286	-6.764	43.736	0.111	0.001	0	684.80	11.4133	48.4	11.1	44.7	3.087	0.017	0.016	0.000	0.363	0.31
688	10/2/2002	4:36.04 AM	26.207	24.539	25.185	26.89	24.606	47.763	49.847	7.843	40.849	-1.289	-6.773	43.518	0.109	0.001	0	685.80	11.43	48.4	10.7	44.3	3.056	0.016	0.016	0.000	0.365	0.31
689	10/2/2002	4:37.04 AM	26.167	24.534	24.91	26.785	24.571	47.823	50.099	7.8	41.017	-1.286	-6.741	43.063	0.106	0.001	0	686.80	11.4467	48.6	10.6	44.4	3.063	0.016	0.016	0.000	0.357	0.30
690	10/2/2002	4:38.04 AM	26.186	24.518	25.695	26.913	24.575	47.804	49.663	7.823	41.162	-1.286	-6.803	43.803	0.103	0.001	0	687.80	11.4633	48.7	10.7	44.7	3.101	0.016	0.016	0.000	0.368	0.31
691	10/2/2002	4:39.04 AM	26.195	24.512	25.683	26.088	24.614	48.092	50.033	7.859	41.226	-1.289	-6.735	43.796	0.113	0.001	0	688.80	11.48	48								

761	10/2/2002	6:22.40 AM	26.805	24.392	25.048	25.382	24.253	48.181	49.818	7.65	41.547	-1.284	-6.712	43.964	0.113	0.001	0	792.40	13.2067	48.3	10.8	44.9	3.093	0.017	0.017	0.000	0.375	0.32
762	10/2/2002	6:23.40 AM	26.779	24.38	24.961	25.461	24.262	48.21	49.922	7.746	41.263	-1.286	-6.704	43.726	0.111	0.001	0	793.40	13.2233	48.4	10.7	44.7	3.084	0.016	0.016	0.000	0.367	0.31
763	10/2/2002	6:24.40 AM	26.754	24.365	24.881	25.516	24.262	47.934	49.464	7.621	41.382	-1.284	-6.751	42.494	0.111	0.001	0	794.40	13.24	48.0	10.4	44.7	3.079	0.017	0.017	0.000	0.372	0.32
764	10/2/2002	6:25.40 AM	26.719	24.366	24.927	25.516	24.297	48.241	50.009	7.751	41.4	-1.286	-6.744	43.901	0.111	0.001	0	796.40	13.2667	48.5	10.7	44.8	3.080	0.016	0.016	0.000	0.367	0.31
765	10/2/2002	6:26.40 AM	26.7	24.402	24.823	25.612	24.333	48.452	50.773	7.655	41.382	-1.286	-6.741	43.943	0.111	0.001	0	796.40	13.2733	48.7	10.7	45.2	3.116	0.016	0.016	0.000	0.365	0.31
766	10/2/2002	6:27.40 AM	26.68	24.407	24.813	25.582	24.353	48.106	50.079	7.758	41.122	-1.286	-6.756	43.476	0.108	0.001	0	797.40	13.29	48.6	10.7	44.6	3.076	0.016	0.016	0.000	0.363	0.31
767	10/2/2002	6:28.40 AM	26.651	24.418	24.859	25.604	24.366	48.483	50.28	7.749	41.699	-1.286	-6.753	43.896	0.107	0.001	0	798.40	13.3067	48.8	10.8	45.1	3.109	0.016	0.016	0.000	0.365	0.30
768	10/2/2002	6:29.40 AM	26.638	24.43	24.736	25.756	24.432	48.398	50.283	7.776	41.468	-1.289	-6.798	43.936	0.106	0.001	0	799.40	13.3233	48.7	10.8	44.8	3.088	0.016	0.016	0.000	0.354	0.30
769	10/2/2002	6:30.40 AM	26.611	24.452	24.778	25.767	24.454	48.287	50.143	7.777	41.468	-1.286	-6.811	43.979	0.105	0.001	0	800.40	13.34	48.7	10.8	44.5	3.084	0.016	0.016	0.000	0.347	0.29
770	10/2/2002	6:31.40 AM	26.592	24.444	24.795	25.77	24.451	48.218	50.566	7.711	41.423	-1.289	-6.793	43.975	0.107	0.001	0	801.40	13.3567	48.6	10.8	44.9	3.090	0.016	0.016	0.000	0.358	0.30
771	10/2/2002	6:32.40 AM	26.569	24.451	24.667	25.827	24.543	48.092	49.783	7.749	41.248	-1.289	-6.753	43.938	0.104	0.001	0	802.40	13.3733	48.3	10.8	44.7	3.080	0.016	0.016	0.000	0.350	0.30
772	10/2/2002	6:33.40 AM	26.552	24.474	24.745	25.845	24.581	48.113	50.073	7.791	41.161	-1.284	-6.811	44.024	0.107	0.001	0	803.40	13.39	48.6	10.8	44.6	3.078	0.016	0.016	0.000	0.360	0.31
773	10/2/2002	6:34.40 AM	26.535	24.472	24.728	25.903	24.674	47.793	49.444	7.632	41.219	-1.289	-6.744	44.005	0.106	0.001	0	804.40	13.4067	48.0	10.8	44.5	3.068	0.016	0.016	0.000	0.359	0.30
774	10/2/2002	6:35.40 AM	26.497	24.479	24.711	25.695	24.601	47.974	49.787	7.707	41.334	-1.289	-6.814	43.841	0.106	0.001	0	806.40	13.44	48.3	10.7	44.7	3.079	0.016	0.016	0.000	0.357	0.30
775	10/2/2002	6:36.40 AM	26.483	24.49	24.665	25.41	24.587	47.953	49.915	7.76	41.136	-1.286	-6.792	43.826	0.102	0.001	0	807.40	13.4567	48.4	10.7	44.5	3.071	0.015	0.015	0.000	0.345	0.29
776	10/2/2002	6:37.40 AM	26.463	24.485	24.625	24.989	24.547	48.453	50.114	7.729	41.675	-1.281	-6.793	43.747	0.102	0.001	0	808.40	13.4733	48.6	10.7	45.2	3.115	0.015	0.015	0.000	0.340	0.29
777	10/2/2002	6:38.40 AM	26.431	24.468	24.824	24.768	24.485	48.102	50.666	7.698	41.006	-1.289	-6.811	43.96	0.103	0.001	0	809.40	13.49	48.6	10.7	44.7	3.079	0.016	0.016	0.000	0.347	0.29
778	10/2/2002	6:40.40 AM	26.415	24.458	24.623	24.662	24.439	48.026	49.988	7.644	41.248	-1.286	-6.822	43.667	0.103	0.001	0	810.40	13.5067	48.5	10.7	44.6	3.078	0.015	0.015	0.000	0.348	0.30
779	10/2/2002	6:41.40 AM	26.384	24.441	24.597	24.535	24.388	48.313	50.246	7.799	41.429	-1.289	-6.854	43.096	0.104	0.001	0	811.40	13.5233	48.8	10.6	44.9	3.084	0.016	0.016	0.000	0.350	0.30
780	10/2/2002	6:42.40 AM	26.357	24.424	24.675	24.467	24.33	48.141	50.038	7.77	41.396	-1.286	-6.819	44.007	0.101	0.001	0	812.40	13.54	48.6	10.8	44.8	3.087	0.015	0.015	0.000	0.339	0.29
781	10/2/2002	6:43.40 AM	26.344	24.396	24.572	24.414	24.277	48.208	50.307	7.887	41.154	-1.286	-6.834	43.797	0.101	0.001	0	813.40	13.5567	48.9	10.7	44.7	3.081	0.015	0.015	0.000	0.341	0.29
782	10/2/2002	6:44.40 AM	26.332	24.394	24.615	24.333	24.216	47.763	49.758	7.802	40.792	-1.281	-6.834	43.942	0.102	0.001	0	814.40	13.5733	48.3	10.8	44.3	3.053	0.015	0.015	0.000	0.347	0.30
783	10/2/2002	6:45.40 AM	26.321	24.378	24.679	24.316	24.174	48.376	50.364	7.761	41.541	-1.281	-6.872	43.822	0.103	0.002	0	816.40	13.59	48.9	10.7	45.0	3.100	0.015	0.015	0.000	0.345	0.29
784	10/2/2002	6:46.40 AM	26.31	24.361	24.562	24.29	24.133	48.41	50.234	7.741	41.669	-1.286	-6.912	43.996	0.101	0.001	0	816.40	13.6067	48.9	10.8	45.1	3.106	0.015	0.015	0.000	0.338	0.29
785	10/2/2002	6:47.40 AM	26.298	24.347	24.623	24.243	24.064	47.987	49.833	7.761	41.414	-1.286	-6.869	43.907	0.102	0.001	0	818.40	13.6233	48.4	10.8	44.5	3.071	0.015	0.015	0.000	0.340	0.29
786	10/2/2002	6:48.40 AM	26.283	24.322	24.641	24.128	24.011	48.011	50.328	7.87	40.966	-1.289	-6.857	43.747	0.1	0.001	0	818.40	13.64	48.8	10.7	44.5	3.069	0.015	0.015	0.000	0.338	0.29
787	10/2/2002	6:49.40 AM	26.24	24.287	24.538	24.1	23.968	47.76	49.504	7.768	40.986	-1.286	-6.924	43.762	0.11	0.001	0	819.40	13.6567	48.0	10.5	44.4	3.059	0.015	0.015	0.000	0.340	0.29
788	10/2/2002	6:50.40 AM	26.246	24.283	24.619	24.091	23.923	48.137	50.186	7.782	41.306	-1.286	-6.954	43.891	0.099	0.001	0	820.40	13.6733	48.7	10.8	44.7	3.083	0.015	0.015	0.000	0.334	0.28
789	10/2/2002	6:51.40 AM	26.222	24.254	24.611	24.077	23.895	47.968	49.913	7.764	41.205	-1.292	-6.892	43.627	0.099	0.001	0	821.40	13.69	48.7	10.7	44.6	3.075	0.015	0.015	0.000	0.335	0.29
790	10/2/2002	6:52.40 AM	26.205	24.232	24.593	24.021	23.863	47.907	49.707	7.891	41.384	-1.289	-6.915	43.931	0.099	0.001	0	822.40	13.7067	48.9	10.8	44.6	3.078	0.015	0.015	0.000	0.332	0.28
791	10/2/2002	6:53.40 AM	26.194	24.211	24.597	23.929	23.847	47.81	50.038	7.806	40.962	-1.282	-6.927	43.91	0.1	0.001	0	823.40	13.7233	48.6	10.8	44.4	3.060	0.015	0.015	0.000	0.340	0.29
792	10/2/2002	6:54.40 AM	26.189	24.19	24.667	23.998	23.831	47.752	49.944	7.761	41.031	-1.284	-6.898	43.914	0.1	0.001	0	824.40	13.74	48.5	10.8	44.4	3.061	0.015	0.015	0.000	0.339	0.29
793	10/2/2002	6:55.40 AM	26.196	24.192	24.678	24.025	23.842	48.249	50.344	7.776	41.433	-1.286	-6.927	43.996	0.099	0.001	0	826.40	13.7567	48.9	10.8	44.8	3.082	0.015	0.015	0.000	0.332	0.28
794	10/2/2002	6:56.40 AM	26.205	24.187	24.623	24.023	23.837	48.463	50.648	7.766	41.468	-1.286	-6.913	43.971	0.099	0.001	0	826.40	13.7733	48.9	10.8	44.7	3.073	0.015	0.015	0.000	0.331	0.28
795	10/2/2002	6:57.40 AM	26.201	24.178	24.795	24.106	23.849	48.038	50.197	7.778	41.122	-1.286	-6.921	43.577	0.099	0.001	0	827.40	13.79	48.7	10.7	44.6	3.073	0.015	0.015	0.000	0.333	0.28
796	10/2/2002	6:58.40 AM	26.212	24.163	24.825	24.106	23.854	48.527	50.95	7.933	41.574	-1.286	-6.912	44.193	0.099	0.001	0	828.40	13.8067	49.5	10.8	45.1	3.106	0.015	0.015	0.000	0.329	0.28
797	10/2/2002	6:59.40 AM	26.241	24.157	24.939	24.171	23.858	47.613	49.628	7.715	40.999	-1.284	-6.929	43.801	0.098	0.001	0	829.40	13.8233	48.2	10.7	44.3	3.055	0.015	0.015	0.000	0.330	0.28
798	10/2/2002	7:00.40 AM	26.256	24.152	24.948	24.155	23.876	47.984	50.054	7.815	41.146	-1.286	-6.947	43.556	0.097	0.001	0	830.40	13.84	48.6	10.7	44.6	3.073	0.014	0.014	0.000	0.326	0.28
799	10/2/2002	7:01.40 AM	26.263	24.142	24.928	24.121	23.863	47.893	49.988	7.801	41.384	-1.289	-6.932	43.91	0.099	0.001	0	832.40	13.8567	48.9	10.7	44.5	3.068	0.015	0.015	0.000	0.332	0.28
800	10/2/2002	7:02.40 AM	26.236	24.147	24.994	24.211	23.918	47.729	50.054	7.862	40.847	-1.286	-6.915	43.806	0.097	0.001	0	832.40	13.8733	48.6	10.7	44.3	3.054	0.014	0.014	0.000	0.327	0.28
801	10/2/2002	7:03.40 AM	26.222	24.153	24.93	24.161	23.949	47.68	49.94	7.836	40.766	-1.286	-6.933	43.646	0.097	0.001	0	833.40	13.89	48.5								

911	10/2/2002	8:52:18 AM	26.863	24.485	26.612	25.906	24.753	54.921	57.497	9.272	46.469	-1.289	-5.878	49.443	0.116	0.001	0	942.03	15.7006	56.0	12.1	80.7	3.495	0.017	0.000	0.326	0.28
912	10/2/2002	8:53:18 AM	26.843	24.465	26.637	25.676	24.743	55.401	57.769	9.267	46.966	-1.289	-6.246	49.527	0.12	0.001	0	943.03	15.7172	56.0	12.1	81.2	3.529	0.018	0.001	0.334	0.28
913	10/2/2002	8:54:18 AM	26.868	24.49	26.716	25.536	24.716	55.857	58.039	9.149	47.713	-1.286	-5.988	49.902	0.113	0.001	0	944.03	15.7339	56.6	12.2	81.6	3.570	0.017	0.001	0.310	0.26
914	10/2/2002	8:55:18 AM	26.838	24.477	26.549	25.443	24.655	55.478	57.495	9.13	47.372	-1.286	-6.188	50.541	0.114	0.001	0	945.03	15.7506	56.0	12.4	81.4	3.546	0.017	0.001	0.316	0.27
915	10/2/2002	8:56:18 AM	26.862	24.464	26.736	25.34	24.602	55.554	57.544	9.092	47.349	-1.286	-5.998	49.357	0.097	0.001	0	946.03	15.7672	56.2	12.1	81.5	3.547	0.014	0.001	0.304	0.28
916	10/2/2002	8:57:18 AM	26.888	24.44	26.646	25.225	24.537	55.165	57.158	9.028	47.109	-1.286	-6.041	49.129	0.124	0.001	0	947.03	15.7839	56.7	12.0	81.1	3.526	0.018	0.001	0.345	0.29
917	10/2/2002	8:58:18 AM	26.899	24.435	26.742	25.135	24.452	54.819	56.678	8.986	46.938	-1.286	-6.191	49.6	0.116	0.001	0	948.03	15.8006	55.2	12.2	80.9	3.508	0.017	0.001	0.324	0.28
918	10/2/2002	8:59:18 AM	26.935	24.437	26.728	25.122	24.424	55.094	57.934	9.167	47.633	-1.284	-5.804	49.846	0.089	0.001	0	949.03	15.8172	56.5	12.0	81.6	3.569	0.013	0.001	0.341	0.27
919	10/2/2002	9:00:18 AM	26.930	24.392	26.716	24.946	24.373	55.639	57.206	9.053	47.746	-1.286	-5.793	48.639	0.11	0.001	0	950.03	15.8339	56.2	12.0	81.5	3.570	0.016	0.001	0.302	0.26
920	10/2/2002	9:01:18 AM	26.94	24.362	26.778	24.871	24.328	56.207	58.143	9.086	48.0	-1.284	-6.278	49.373	0.103	0.001	0	951.03	15.8506	56.7	11.9	82.2	3.596	0.015	0.001	0.320	0.24
921	10/2/2002	9:02:18 AM	26.925	24.362	26.724	24.782	24.229	56.225	58.275	9.130	48.098	-1.286	-6.336	48.717	0.118	0.001	0	952.03	15.8672	56.8	11.9	82.2	3.596	0.018	0.001	0.321	0.27
922	10/2/2002	9:03:18 AM	26.962	24.354	26.825	24.863	24.19	56.77	57.584	9.116	47.588	-1.286	-6.078	48.376	0.108	0.001	0	953.03	15.8839	56.1	11.9	81.7	3.563	0.016	0.001	0.296	0.25
923	10/2/2002	9:04:18 AM	26.955	24.347	26.744	24.893	24.175	56.845	57.7	9.109	47.691	-1.286	-6.376	48.977	0.111	0.001	0	954.03	15.9006	56.2	12.0	81.8	3.569	0.017	0.001	0.304	0.26
924	10/2/2002	9:05:18 AM	26.982	24.334	26.841	24.889	24.136	55.627	57.534	9.114	47.382	-1.284	-6.466	49.019	0.111	0.001	0	955.03	15.9172	56.2	12.0	81.5	3.561	0.016	0.001	0.302	0.26
925	10/2/2002	9:06:18 AM	26.944	24.316	26.772	24.941	24.112	56.824	57.628	9.12	47.588	-1.286	-6.42	49.074	0.103	0.001	0	956.03	15.9339	56.2	12.0	81.7	3.565	0.015	0.001	0.305	0.24
926	10/2/2002	9:07:18 AM	27.007	24.308	26.825	24.863	24.111	56.101	57.906	9.089	47.939	-1.286	-6.423	48.964	0.112	0.001	0	957.03	15.9506	56.6	12.0	82.0	3.587	0.017	0.001	0.306	0.26
927	10/2/2002	9:08:18 AM	27.02	24.3	26.865	24.878	24.085	55.647	57.322	9.103	47.492	-1.281	-6.345	48.376	0.101	0.001	0	958.03	15.9672	55.9	11.9	81.6	3.567	0.015	0.001	0.277	0.24
928	10/2/2002	9:09:18 AM	27.027	24.278	26.81	24.793	23.989	56.381	57.88	9.104	48.258	-1.286	-6.431	48.791	0.109	0.001	0	959.03	15.9839	56.1	12.0	81.5	3.604	0.016	0.001	0.292	0.29
929	10/2/2002	9:10:18 AM	27.023	24.26	26.901	24.734	23.961	55.902	57.675	9.101	47.736	-1.289	-6.51	49.533	0.107	0.001	0	960.03	16.0006	56.2	12.1	81.8	3.574	0.016	0.001	0.292	0.26
930	10/2/2002	9:11:18 AM	27.022	24.249	26.801	24.794	23.945	55.991	57.831	9.042	47.982	-1.286	-6.492	49.051	0.099	0.001	0	961.03	16.0172	56.4	12.0	82.0	3.584	0.015	0.001	0.304	0.27
931	10/2/2002	9:12:18 AM	27.017	24.218	26.905	24.818	23.925	56.389	58.152	9.129	48.315	-1.286	-6.662	49.07	0.108	0.001	0	962.03	16.0339	56.7	12.0	82.4	3.609	0.016	0.001	0.292	0.25
932	10/2/2002	9:13:18 AM	27.015	24.206	26.913	24.851	23.912	55.594	57.543	9.097	47.525	-1.286	-6.894	48.973	0.105	0.001	0	963.03	16.0506	56.1	12.0	81.6	3.565	0.016	0.001	0.291	0.26
933	10/2/2002	9:14:18 AM	27.012	24.194	26.9	24.834	23.895	56.033	57.779	9.132	48.667	-1.286	-6.662	49.311	0.106	0.001	0	964.03	16.0672	56.3	12.0	82.0	3.582	0.016	0.001	0.288	0.25
934	10/2/2002	9:15:18 AM	27.01	24.162	26.883	24.772	23.817	55.917	57.75	9.141	47.628	-1.286	-6.666	48.989	0.103	0.001	0	965.03	16.0839	56.3	12.0	81.8	3.569	0.015	0.001	0.281	0.24
935	10/2/2002	9:16:18 AM	27.019	24.155	26.897	24.735	23.816	55.935	57.706	9.072	47.869	-1.284	-6.672	49.022	0.104	0.001	0	966.03	16.1006	56.2	12.0	81.9	3.578	0.015	0.001	0.283	0.24
936	10/2/2002	9:17:18 AM	27.02	24.148	26.913	24.633	23.775	55.603	57.473	9.063	47.628	-1.286	-6.773	49.016	0.107	0.001	0	967.03	16.1172	56.0	12.0	82.1	3.571	0.015	0.001	0.287	0.24
937	10/2/2002	9:18:18 AM	27.004	24.105	26.812	24.629	23.748	56.932	58.882	9.070	49.191	-1.292	-7.004	47.329	0.105	0.001	0	968.03	16.1339	57.4	11.6	82.1	3.669	0.016	0.001	0.280	0.24
938	10/2/2002	9:19:18 AM	27.013	24.109	26.821	24.699	23.73	56.874	58.959	9.117	49.136	-1.286	-6.657	47.341	0.103	0.001	0	969.03	16.1506	57.2	11.6	82.0	3.655	0.015	0.001	0.275	0.23
939	10/2/2002	9:20:18 AM	27.01	24.081	26.729	24.682	23.712	56.675	58.515	9.072	49.101	-1.286	-6.689	47.207	0.105	0.001	0	970.03	16.1672	57.0	11.6	82.0	3.645	0.016	0.001	0.282	0.24
940	10/2/2002	9:21:18 AM	27.012	24.078	26.625	24.688	23.653	56.794	58.706	9.113	49.22	-1.286	-6.701	46.612	0.103	0.001	0	971.03	16.1839	57.2	11.6	82.0	3.654	0.015	0.001	0.277	0.24
941	10/2/2002	9:22:18 AM	27.02	24.06	26.612	24.723	23.626	57.72	59.682	9.093	49.303	-1.286	-6.883	45.866	0.109	0.001	0	972.03	16.2006	56.1	12.0	81.6	3.622	0.016	0.001	0.282	0.24
942	10/2/2002	9:23:18 AM	26.981	24.041	26.524	24.672	23.612	56.685	58.726	9.051	49.013	-1.289	-6.73	46.943	0.103	0.001	0	973.03	16.2172	57.3	11.5	82.0	3.644	0.015	0.001	0.278	0.24
943	10/2/2002	9:24:18 AM	26.959	24.019	26.542	24.77	23.6	56.459	58.333	8.92	48.518	-1.284	-6.762	47.778	0.101	0.001	0	974.03	16.2339	56.9	11.7	82.5	3.619	0.015	0.001	0.275	0.23
944	10/2/2002	9:25:18 AM	26.935	23.996	26.468	24.721	23.571	56.001	57.968	8.952	48.029	-1.289	-6.715	48.069	0.102	0.001	0	975.03	16.2506	56.4	11.8	82.0	3.588	0.015	0.001	0.280	0.24
945	10/2/2002	9:26:18 AM	26.933	23.982	26.481	24.734	23.564	55.803	57.653	8.936	47.709	-1.289	-6.768	47.658	0.109	0.001	0	976.03	16.2672	56.1	11.9	82.7	3.631	0.014	0.001	0.287	0.24
946	10/2/2002	9:27:18 AM	26.883	23.974	26.506	24.889	23.544	56.001	58.542	8.993	48.521	-1.286	-6.666	48.068	0.107	0.001	0	977.03	16.2839	55.1	12.4	80.1	3.455	0.014	0.001	0.277	0.24
947	10/2/2002	9:28:18 AM	26.85	23.961	26.448	24.802	23.531	55.393	57.272	8.948	46.659	-1.286	-6.825	51.003	0.096	0.001	0	978.03	16.3006	55.8	12.5	81.0	3.518	0.014	0.001	0.269	0.23
948	10/2/2002	9:29:18 AM	26.725	23.223	26.298	25.047	22.973	50.463	58.111	9.202	42.202	-1.644	-8.893	48.898	0.002	0.001	0	1052.93	17.5489	56.6	12.0	83.3	3.194	0.000	0.000	0.006	0.01

1041	10/2/2002	12:16:12 PM	25.49	22.7	25.252	25.562	22.521	44.529	47.749	10.172	35.201	-1.284	-0.704	51.838	0.061	0.001	0.001	1145.93	19.0889	46.3	12.7	39.9	2.749	0.009	0.009	0.000	0.227	0.18
1042	10/2/2002	12:17:12 PM	25.499	22.699	25.176	25.627	22.505	44.275	47.458	10.141	34.989	-1.284	-0.708	52.6	0.061	0.001	0.001	1146.93	19.1156	46.0	12.9	39.6	2.733	0.009	0.009	0.000	0.228	0.19
1043	10/2/2002	12:18:12 PM	25.493	22.688	25.226	25.606	22.499	44.125	47.214	10.054	35.089	-1.289	-0.701	51.972	0.061	0.001	0.001	1147.93	19.1322	45.7	12.7	39.6	2.731	0.009	0.009	0.000	0.228	0.19
1044	10/2/2002	12:19:13 PM	25.503	22.703	25.261	25.586	22.495	44.308	47.406	10.055	35.114	-1.281	-0.701	51.874	0.061	0.001	0.001	1148.93	19.1489	45.9	12.7	39.9	2.741	0.009	0.009	0.000	0.227	0.18
1045	10/2/2002	12:20:12 PM	25.518	22.703	25.195	25.425	22.493	44.716	47.874	10.032	35.594	-1.289	-0.701	51.977	0.061	0.001	0.001	1149.93	19.1656	45.4	12.7	40.2	2.769	0.009	0.009	0.000	0.225	0.19
1046	10/2/2002	12:21:12 PM	25.513	22.693	25.236	25.326	22.519	44.834	48.116	9.958	35.748	-1.286	-0.706	50.704	0.062	0.001	0.001	1150.93	19.1822	45.6	12.4	40.3	2.778	0.009	0.009	0.000	0.228	0.19
1047	10/2/2002	12:22:12 PM	25.498	22.693	25.236	25.105	22.524	44.658	47.735	9.939	35.736	-1.286	-0.703	50.731	0.061	0.001	0.001	1151.93	19.1989	46.3	12.4	40.2	2.771	0.009	0.009	0.000	0.225	0.19
1048	10/2/2002	12:23:12 PM	25.503	22.688	25.16	25.155	22.519	44.902	48.043	9.929	36.123	-1.286	-0.703	50.889	0.061	0.001	0.001	1152.93	19.2156	46.6	12.5	40.5	2.793	0.009	0.009	0.000	0.223	0.19
1049	10/2/2002	12:24:13 PM	25.492	22.677	25.225	25.079	22.506	44.44	47.619	9.919	35.626	-1.286	-0.701	50.218	0.061	0.001	0.001	1153.93	19.2322	46.1	12.4	40.2	2.780	0.009	0.009	0.000	0.222	0.18
1050	10/2/2002	12:25:12 PM	25.503	22.698	25.23	25.085	22.524	44.583	47.907	9.732	35.689	-1.286	-0.706	50.67	0.061	0.001	0.001	1154.93	19.2489	46.4	12.4	40.1	2.767	0.009	0.009	0.000	0.225	0.19
1051	10/2/2002	12:26:12 PM	25.493	22.698	25.155	25.05	22.524	44.824	47.965	9.725	36.086	-1.284	-0.707	51.01	0.061	0.001	0.001	1155.93	19.2656	46.5	12.5	40.5	2.789	0.009	0.009	0.000	0.224	0.19
1052	10/2/2002	12:27:12 PM	25.498	22.703	25.24	25.08	22.529	45.111	48.374	9.884	36.037	-1.286	-0.707	51.136	0.061	0.001	0.001	1156.93	19.2822	46.9	12.5	40.6	2.797	0.009	0.009	0.000	0.223	0.19
1053	10/2/2002	12:28:12 PM	25.503	22.703	25.216	25.115	22.545	44.674	47.783	9.754	35.919	-1.286	-0.707	50.026	0.061	0.001	0.001	1157.93	19.2989	46.3	12.3	40.3	2.793	0.009	0.009	0.000	0.224	0.19
1054	10/2/2002	12:29:12 PM	25.503	22.703	25.161	25.28	22.554	45.103	48.426	9.823	36.229	-1.284	-0.707	50.234	0.061	0.001	0.001	1158.93	19.3156	47.0	12.3	40.7	2.804	0.009	0.009	0.000	0.223	0.19
1055	10/2/2002	12:30:12 PM	25.503	22.708	25.246	25.326	22.57	44.695	47.956	9.752	35.881	-1.284	-0.707	50.15	0.061	0.001	0.001	1159.93	19.3322	46.5	12.3	40.3	2.778	0.009	0.009	0.000	0.224	0.19
1056	10/2/2002	12:31:12 PM	25.513	22.708	25.201	25.366	22.569	44.921	48.052	9.791	36.073	-1.281	-0.707	50.133	0.061	0.001	0.001	1160.93	19.3489	46.6	12.3	40.5	2.792	0.009	0.009	0.000	0.223	0.19
1057	10/2/2002	12:32:12 PM	25.514	22.72	25.166	25.476	22.56	44.21	47.559	10.029	35.066	-1.284	-0.706	51.436	0.061	0.001	0.001	1161.93	19.3656	46.1	12.6	39.5	2.733	0.009	0.009	0.000	0.228	0.19
1058	10/2/2002	12:33:12 PM	25.497	22.709	25.257	25.361	22.575	44.594	47.97	10.077	35.416	-1.284	-0.701	51.162	0.061	0.001	0.001	1162.93	19.3822	46.1	12.4	40.0	2.763	0.009	0.009	0.000	0.222	0.18
1059	10/2/2002	12:34:12 PM	25.508	22.713	25.211	25.175	22.6	44.324	47.52	9.822	35.386	-1.286	-0.708	50.397	0.06	0.001	0.001	1163.93	19.3989	46.0	12.4	39.9	2.748	0.009	0.009	0.000	0.223	0.19
1060	10/2/2002	12:35:12 PM	25.504	22.719	25.186	25.371	22.62	44.61	47.764	9.862	35.688	-1.286	-0.708	51.046	0.06	0.001	0.001	1164.93	19.4156	46.3	12.5	40.1	2.767	0.009	0.009	0.000	0.222	0.19
1061	10/2/2002	12:36:12 PM	25.51	22.72	25.267	25.452	22.631	44.802	47.758	9.904	35.688	-1.286	-0.704	50.32	0.056	0.001	0.001	1165.93	19.4322	46.3	12.3	40.1	2.764	0.008	0.008	0.000	0.207	0.18
1062	10/2/2002	12:37:12 PM	25.515	22.71	25.198	25.473	22.652	44.832	48.008	9.79	35.903	-1.284	-0.704	50.414	0.06	0.001	0.001	1166.93	19.4489	46.5	12.4	40.4	2.789	0.009	0.009	0.000	0.220	0.19
1063	10/2/2002	12:38:12 PM	25.536	22.741	25.218	25.593	22.617	44.88	48.205	9.805	36.065	-1.284	-0.704	51.062	0.06	0.001	0.001	1167.93	19.4656	46.7	12.5	40.5	2.791	0.009	0.009	0.000	0.220	0.19
1064	10/2/2002	12:39:12 PM	25.528	22.723	25.215	25.69	22.629	44.6	47.809	9.672	35.86	-1.286	-0.704	50.115	0.06	0.001	0.001	1168.93	19.4822	46.3	12.4	40.2	2.773	0.009	0.009	0.000	0.221	0.19
1065	10/2/2002	12:40:12 PM	25.531	22.731	25.108	25.693	22.647	44.654	47.959	9.719	35.617	-1.286	-0.702	51.15	0.06	0.001	0.001	1169.93	19.4989	46.5	12.5	40.2	2.774	0.009	0.009	0.000	0.222	0.19
1066	10/2/2002	12:41:12 PM	25.527	22.723	25.165	25.736	22.653	44.47	47.721	9.719	35.617	-1.286	-0.707	50.716	0.056	0.001	0.001	1170.93	19.5156	46.7	12.4	40.1	2.763	0.009	0.009	0.000	0.221	0.19
1067	10/2/2002	12:42:12 PM	25.505	22.722	25.172	25.617	22.601	44.815	48.065	9.679	35.698	-1.284	-0.707	50.112	0.06	0.001	0.001	1171.93	19.5322	46.7	12.3	40.5	2.789	0.009	0.009	0.000	0.220	0.19
1068	10/2/2002	12:43:12 PM	25.502	22.717	25.089	25.914	22.598	44.538	47.896	9.718	35.701	-1.284	-0.702	50.502	0.06	0.001	0.001	1172.93	19.5489	46.4	12.4	40.1	2.766	0.009	0.009	0.000	0.222	0.19
1069	10/2/2002	12:44:12 PM	25.498	22.726	25.12	25.941	22.609	45.515	48.714	9.618	37.05	-1.284	-0.704	50.207	0.06	0.001	0.001	1173.93	19.5656	47.2	12.3	41.1	2.846	0.009	0.009	0.000	0.216	0.19
1070	10/2/2002	12:45:12 PM	25.508	22.729	25.181	25.976	22.625	45.128	48.5	9.578	36.544	-1.284	-0.704	50.769	0.06	0.001	0.001	1174.93	19.5822	47.0	12.4	40.8	2.815	0.009	0.009	0.000	0.218	0.19
1071	10/2/2002	12:46:12 PM	25.498	22.724	25.076	25.689	22.625	45.318	48.456	9.519	36.778	-1.284	-0.703	50.479	0.06	0.001	0.001	1175.93	19.5989	47.0	12.3	41.0	2.830	0.009	0.009	0.000	0.217	0.19
1072	10/2/2002	12:47:12 PM	25.498	22.719	25.112	25.937	22.671	45.02	48.366	9.551	36.427	-1.284	-0.704	49.904	0.06	0.001	0.001	1176.93	19.6156	45.9	12.2	40.7	2.808	0.009	0.009	0.000	0.219	0.19
1073	10/2/2002	12:48:12 PM	25.498	22.715	25.132	26.012	22.671	44.966	48.352	9.54	36.313	-1.284	-0.704	49.978	0.06	0.001	0.001	1177.93	19.6322	45.9	12.2	40.6	2.802	0.009	0.009	0.000	0.219	0.19
1074	10/2/2002	12:49:12 PM	25.498	22.736	25.073	26.029	22.643	45.07	48.143	9.477	36.577	-1.284	-0.704	50.207	0.06	0.001	0.001	1178.93	19.6489	46.7	12.3	40.6	2.815	0.009	0.009	0.000	0.219	0.19
1075	10/2/2002	12:50:12 PM	25.498	22.732	25.125	26.029	22.643	45.248	48.137	9.477	36.577	-1.284	-0.704	50.207	0.06	0.001	0.001	1179.93	19.6656	46.7	12.3	41.0	2.825	0.009	0.009	0.000	0.219	0.19
1076	10/2/2002	12:51:12 PM	25.472	22.712	25.119	25.904	22.633	44.944	48.476	9.538	36.184	-1.284	-0.703	50.049	0.06	0.001	0.001	1180.93	19.6822	47.0	12.3	40.6	2.797	0.009	0.009	0.000	0.220	0.19
1077	10/2/2002	12:52:12 PM	25.482	22.722	25.055	25.96	22.659	45.395	48.664	9.484	36.945	-1.284	-0.704	49.949	0.06	0.001	0.001	1181.93	19.6989	47.2	12.2	41.1	2.839	0.009	0.009	0.000	0.217	0.19
1078	10/2/2002	12:53:12 PM	25.482	22.727	25.125	25.985	22.659	45.031	48.5	9.576	36.384	-1.286	-0.701	49.974	0.06	0.001	0.001	1182.93	19.7156	47.0	12.2	40.7	2.807	0.009	0.009	0.000	0.219	0.19
1079	10/2/2002	12:54:12 PM	25.483	22.733	25.125	25.775	22.675	45.231	48.616	9.503	36.663	-1.284	-0.701	49.796	0.06	0.001	0.001	1183.93	19.7322	47.1	12.2	40.9	2.823	0.009	0.009	0.000	0.218	0.19
1080	10/2/2002	12:55:12 PM	25.482	22.724	25.065	25.689	22.665	45.078	48.655	9.519	36.778	-1.284	-0.703	50.257	0.06	0.001	0.001	1184.93	19.7489	47.1	12.3	41.						



1301	10/2/2002	5:10:52 PM	26.634	23.673	24.932	27.066	23.434	45.511	47.129	9.489	36.886	1.286	-6.947	49.529	0.051	0.001	0	1440.60	24.01	45.7	12.1	41.2	2.840	0.008	0.008	0.000	0.185	0.16
1302	10/2/2002	5:11:52 PM	26.628	23.667	24.875	27.015	23.423	45.093	46.566	9.417	36.816	-1.286	-9.951	49.152	0.051	0.001	0	1441.60	24.0267	45.1	12.0	40.9	2.817	0.008	0.008	0.000	0.187	0.16
1303	10/2/2002	5:12:52 PM	26.617	23.656	24.859	27.044	23.417	45.108	46.407	9.365	36.719	-1.284	-9.947	48.745	0.051	0.001	0	1442.60	24.0433	44.9	11.9	40.9	2.823	0.008	0.008	0.000	0.186	0.16
1304	10/2/2002	5:13:52 PM	26.611	23.651	24.934	27.063	23.401	45.095	46.49	9.361	36.787	-1.284	-9.953	49.137	0.051	0.001	0	1443.60	24.06	45.0	12.0	40.9	2.822	0.008	0.008	0.000	0.186	0.16
1305	10/2/2002	5:14:52 PM	26.616	23.65	24.858	27.028	23.391	45.263	46.837	9.461	36.784	-1.284	-9.947	49.579	0.051	0.001	0	1444.60	24.0767	45.4	12.2	41.0	2.828	0.008	0.008	0.000	0.186	0.16
1306	10/2/2002	5:15:52 PM	26.61	23.649	24.882	26.957	23.39	44.975	46.409	9.402	36.489	-1.286	-9.956	48.281	0.051	0.001	0	1445.60	24.0933	44.9	11.8	40.7	2.808	0.008	0.008	0.000	0.187	0.16
1307	10/2/2002	5:16:52 PM	26.599	23.634	24.922	27.017	23.374	44.823	46.185	9.384	36.505	-1.286	-9.961	48.805	0.051	0.001	0	1446.60	24.11	44.7	12.0	40.7	2.804	0.008	0.008	0.000	0.187	0.16
1308	10/2/2002	5:17:52 PM	26.615	23.644	24.862	27.057	23.37	45.337	46.681	9.441	36.962	-1.286	-9.944	49.537	0.05	0.001	0	1447.60	24.1267	45.2	11.9	41.1	2.838	0.007	0.007	0.000	0.182	0.15
1309	10/2/2002	5:18:52 PM	26.609	23.639	24.896	27.076	23.365	45.134	46.561	9.421	36.737	-1.286	-9.944	49.137	0.051	0.001	0	1448.60	24.1533	45.2	12.1	40.9	2.827	0.007	0.007	0.000	0.183	0.15
1310	10/2/2002	5:19:52 PM	26.608	23.632	24.941	27.08	23.363	44.859	46.252	9.386	36.423	-1.286	-9.947	50.335	0.05	0.001	0	1449.60	24.16	44.8	12.3	40.6	2.802	0.007	0.007	0.000	0.184	0.16
1311	10/2/2002	5:20:52 PM	26.597	23.616	24.844	27.124	23.352	45.194	46.707	9.451	36.737	-1.284	-9.944	49.827	0.05	0.001	0	1450.60	24.1767	45.5	12.2	41.0	2.824	0.007	0.007	0.000	0.183	0.16
1312	10/2/2002	5:21:52 PM	26.597	23.621	24.924	27.034	23.352	45.391	46.97	9.406	36.96	-1.284	-9.947	49.143	0.05	0.001	0	1451.60	24.1933	45.5	12.2	41.1	2.839	0.007	0.007	0.000	0.181	0.15
1313	10/2/2002	5:22:52 PM	26.596	23.62	24.918	27.038	23.365	45.534	46.861	9.405	37.209	-1.284	-9.947	51.331	0.05	0.001	0	1452.60	24.21	45.5	12.6	41.4	2.852	0.007	0.007	0.000	0.181	0.15
1314	10/2/2002	5:23:52 PM	26.595	23.609	24.843	27.037	23.36	45.221	46.852	9.474	36.765	-1.286	-9.927	49.393	0.05	0.001	0	1453.60	24.2267	45.4	12.1	41.0	2.836	0.007	0.007	0.000	0.183	0.16
1315	10/2/2002	5:24:52 PM	26.595	23.604	24.922	27.037	23.345	45.014	46.543	9.368	36.558	-1.286	-9.927	48.51	0.052	0.001	0	1454.60	24.2433	45.1	11.9	40.8	2.812	0.008	0.008	0.000	0.191	0.16
1316	10/2/2002	5:25:52 PM	26.588	23.607	24.911	26.986	23.348	44.287	46.905	9.976	35.326	-1.286	-9.956	51.043	0.049	0.001	0	1455.60	24.26	44.3	12.5	39.8	2.745	0.007	0.007	0.000	0.184	0.16
1317	10/2/2002	5:26:52 PM	26.577	23.596	24.917	27.024	23.357	44.602	46.016	9.97	35.533	-1.284	-9.956	51.578	0.049	0.001	0	1456.60	24.2767	44.5	12.6	40.1	2.768	0.007	0.007	0.000	0.183	0.16
1318	10/2/2002	5:27:52 PM	26.572	23.591	24.934	26.934	23.342	44.291	46.867	9.897	35.404	-1.286	-9.956	51.243	0.049	0.001	0	1457.60	24.2933	44.4	12.5	39.8	2.747	0.007	0.007	0.000	0.181	0.15
1319	10/2/2002	5:28:52 PM	26.586	23.59	24.919	26.819	23.356	44.333	46.018	9.901	35.437	-1.286	-9.956	51.073	0.049	0.002	0	1458.60	24.31	44.5	12.5	39.9	2.750	0.007	0.007	0.000	0.184	0.16
1320	10/2/2002	5:29:52 PM	26.591	23.595	24.914	26.839	23.346	44.606	46.165	9.789	35.801	-1.286	-9.956	50.748	0.049	0.002	0	1459.60	24.3267	44.7	12.4	40.2	2.772	0.007	0.007	0.000	0.182	0.16
1321	10/2/2002	5:30:52 PM	26.58	23.579	24.978	26.852	23.345	44.312	45.749	9.852	35.342	-1.286	-9.956	50.788	0.049	0.001	0	1460.60	24.3433	44.3	12.4	39.8	2.746	0.007	0.007	0.000	0.184	0.16
1322	10/2/2002	5:31:52 PM	26.595	23.609	24.927	26.877	23.345	44.598	46.007	9.803	35.709	-1.289	-9.956	50.658	0.049	0.001	0	1461.60	24.36	44.6	12.4	40.2	2.768	0.007	0.007	0.000	0.182	0.16
1323	10/2/2002	5:32:52 PM	26.574	23.598	24.912	26.827	23.345	44.411	46.03	9.903	35.386	-1.289	-9.961	50.792	0.049	0.001	0	1462.60	24.3767	44.6	12.4	39.9	2.751	0.007	0.007	0.000	0.184	0.16
1324	10/2/2002	5:33:52 PM	26.584	23.578	25.001	26.836	23.344	44.246	46.541	9.816	35.67	-1.286	-9.956	50.618	0.049	0.001	0	1463.60	24.3933	44.5	12.4	40.0	2.761	0.007	0.007	0.000	0.182	0.16
1325	10/2/2002	5:34:52 PM	26.597	23.617	24.915	26.73	23.317	44.315	46.945	9.78	35.455	-1.289	-9.956	49.888	0.049	0.001	0	1464.60	24.41	44.5	12.2	39.9	2.749	0.007	0.007	0.000	0.184	0.16
1326	10/2/2002	5:35:52 PM	26.591	23.613	24.917	26.773	23.316	44.24	46.577	9.821	35.431	-1.286	-9.956	50.136	0.049	0.001	0	1465.60	24.4267	44.8	12.3	39.9	2.747	0.007	0.007	0.000	0.182	0.16
1327	10/2/2002	5:36:52 PM	26.595	23.599	24.997	26.822	23.325	44.836	46.531	9.875	36.22	-1.286	-9.961	50.804	0.049	0.001	0	1466.60	24.4433	45.1	12.5	40.3	2.782	0.007	0.007	0.000	0.181	0.15
1328	10/2/2002	5:37:52 PM	26.593	23.597	24.916	26.666	23.308	44.132	45.681	9.786	35.628	-1.286	-9.961	50.649	0.049	0.001	0	1467.60	24.46	44.2	12.4	39.7	2.739	0.007	0.007	0.000	0.184	0.16
1329	10/2/2002	5:38:52 PM	26.578	23.547	24.966	26.661	23.298	43.941	45.486	9.733	35.211	-1.286	-9.979	50.198	0.049	0.001	0	1468.60	24.4767	44.0	12.3	39.6	2.729	0.007	0.007	0.000	0.185	0.16
1330	10/2/2002	5:39:52 PM	26.585	23.545	25.004	26.654	23.281	44.952	46.274	9.779	35.799	-1.286	-9.979	50.526	0.049	0.001	0	1469.60	24.4933	44.8	12.4	40.2	2.770	0.007	0.007	0.000	0.182	0.15
1331	10/2/2002	5:40:52 PM	26.5	23.55	24.983	26.617	23.265	44.45	46.466	9.773	35.628	-1.286	-9.979	50.19	0.049	0.001	0	1470.60	24.51	44.9	12.3	40.1	2.767	0.007	0.007	0.000	0.182	0.15
1332	10/2/2002	5:41:52 PM	26.596	23.565	25.023	26.708	23.265	44.695	46.359	9.711	35.903	-1.281	-9.973	50.171	0.049	0.001	0	1471.60	24.5267	44.9	12.3	40.3	2.778	0.007	0.007	0.000	0.181	0.15
1333	10/2/2002	5:42:52 PM	26.5	23.564	25.023	26.578	23.27	44.654	46.177	9.64	35.985	-1.281	-9.973	50.408	0.049	0.001	0	1472.60	24.5433	44.7	12.4	40.3	2.780	0.007	0.007	0.000	0.181	0.15
1334	10/2/2002	5:43:52 PM	26.59	23.544	24.922	26.558	23.25	44.656	46.56	9.795	35.617	-1.292	-9.987	50.402	0.048	0.001	0	1473.60	24.56	44.5	12.4	40.2	2.774	0.007	0.007	0.000	0.178	0.15
1335	10/2/2002	5:44:52 PM	26.593	23.55	24.98	26.623	23.25	44.591	46.31	9.78	35.801	-1.286	-9.986	50.136	0.048	0.001	0	1474.60	24.5767	44.8	12.3	40.1	2.757	0.007	0.007	0.000	0.178	0.15
1336	10/2/2002	5:45:52 PM	26.601	23.55	24.983	26.678	23.265	44.221	45.817	9.716	35.545	-1.292	-9.987	50.184	0.048	0.001	0	1475.60	24.5933	44.3	12.3	39.9	2.750	0.007	0.007	0.000	0.180	0.15
1337	10/2/2002	5:46:52 PM	26.601	23.56	24.974	26.774	23.256	44.378	45.987	9.716	35.666	-1.286	-9.987	51.122	0.048	0.001												

1431	10/2/2002	7:20:22 PM	26.506	23.067	25.112	26.157	22.269	44.117	46.45	9.721	35.988	-1.284	-6.967	49.992	0.046	0.001	0	1570.10	26.1683	45.0	12.2	39.8	2.741	0.007	0.007	0.000	0.172	0.15
1432	10/2/2002	7:21:22 PM	26.51	23.061	25.027	26.011	22.264	43.693	45.892	9.653	35.009	-1.281	-6.97	50.249	0.046	0.001	0	1571.10	26.1685	44.4	12.3	39.4	2.713	0.007	0.007	0.000	0.174	0.15
1433	10/2/2002	7:22:22 PM	26.496	23.026	25.052	26.026	22.229	44.074	46.55	9.718	35.211	-1.284	-6.976	49.926	0.046	0.001	0	1572.10	26.2017	45.1	12.0	39.6	2.733	0.007	0.007	0.000	0.173	0.15
1434	10/2/2002	7:23:22 PM	26.501	23.038	25.125	24.987	22.245	44.056	46.33	9.651	35.476	-1.284	-6.976	49.615	0.046	0.001	0	1573.10	26.2193	44.9	12.3	39.2	2.743	0.007	0.007	0.000	0.172	0.15
1435	10/2/2002	7:24:22 PM	26.476	23.012	25.003	24.817	22.23	44.036	46.289	9.724	35.218	-1.286	-6.982	49.621	0.046	0.001	0	1574.10	26.2326	44.8	12.2	39.6	2.732	0.007	0.007	0.000	0.173	0.15
1436	10/2/2002	7:25:22 PM	26.486	23.013	25.094	24.888	22.201	44.575	46.819	9.779	35.768	-1.284	-6.979	49.886	0.046	0.001	0	1575.10	26.2517	45.3	12.2	40.2	2.770	0.007	0.007	0.000	0.170	0.14
1437	10/2/2002	7:26:22 PM	26.492	23.009	25.099	24.818	22.216	44.507	46.595	9.749	35.842	-1.286	-6.995	49.535	0.046	0.001	0	1576.10	26.2683	45.1	12.1	40.2	2.770	0.007	0.007	0.000	0.170	0.14
1438	10/2/2002	7:27:22 PM	26.498	23.009	25.035	24.889	22.187	44.186	46.525	9.765	35.416	-1.284	-6.976	49.462	0.046	0.001	0	1577.10	26.2895	45.1	12.1	39.8	2.744	0.007	0.007	0.000	0.172	0.15
1439	10/2/2002	7:28:22 PM	26.48	23.021	25.122	24.888	22.174	44.287	46.568	9.74	35.476	-1.284	-6.976	49.403	0.046	0.002	0	1578.10	26.3017	45.1	12.1	39.9	2.763	0.007	0.007	0.000	0.171	0.15
1440	10/2/2002	7:29:22 PM	26.48	23.022	25.103	24.802	22.154	44.316	46.727	9.722	35.682	-1.284	-6.995	49.783	0.046	0.001	0	1579.10	26.3183	45.3	12.2	40.0	2.758	0.007	0.007	0.000	0.167	0.14
1441	10/2/2002	7:30:22 PM	26.472	23.069	25.055	24.784	22.146	44.268	46.754	9.746	35.476	-1.284	-6.979	49.571	0.046	0.001	0	1580.10	26.3335	45.3	12.1	39.9	2.749	0.007	0.007	0.000	0.172	0.15
1442	10/2/2002	7:31:22 PM	26.468	23.064	25.14	24.789	22.122	44.215	46.75	9.734	35.472	-1.284	-6.979	50.022	0.046	0.001	0	1581.10	26.3517	45.3	12.3	39.8	2.747	0.007	0.007	0.000	0.171	0.15
1443	10/2/2002	7:32:22 PM	26.469	23.065	25.101	24.815	22.123	44.44	46.789	9.715	35.76	-1.281	-6.985	49.737	0.046	0.001	0	1582.10	26.3693	45.3	12.2	40.1	2.765	0.007	0.007	0.000	0.167	0.14
1444	10/2/2002	7:33:22 PM	26.461	23.038	25.088	24.652	22.115	44.082	46.463	9.753	35.271	-1.281	-6.985	49.796	0.046	0.001	0	1583.10	26.386	45.0	12.2	39.7	2.738	0.007	0.007	0.000	0.169	0.14
1445	10/2/2002	7:34:22 PM	26.448	23.019	25.136	24.634	22.097	44.045	46.521	9.725	35.238	-1.289	-6.987	49.649	0.046	0.001	0	1584.10	26.4017	45.0	12.2	39.6	2.733	0.007	0.007	0.000	0.169	0.14
1446	10/2/2002	7:35:22 PM	26.46	23.021	25.077	24.585	22.103	44.219	46.717	9.758	35.408	-1.286	-6.99	49.51	0.046	0.001	0	1585.10	26.4183	45.2	12.1	39.8	2.745	0.007	0.007	0.000	0.168	0.14
1447	10/2/2002	7:36:22 PM	26.446	23.023	25.109	24.632	22.108	44.586	46.659	9.755	35.605	-1.284	-6.985	49.559	0.046	0.001	0	1586.10	26.435	45.5	12.1	40.2	2.772	0.007	0.007	0.000	0.170	0.14
1448	10/2/2002	7:37:22 PM	26.438	23.088	25.16	24.689	22.111	44.204	46.689	9.724	35.466	-1.284	-6.987	49.677	0.046	0.001	0	1587.10	26.4517	45.2	12.2	39.9	2.740	0.007	0.007	0.000	0.169	0.14
1449	10/2/2002	7:38:22 PM	26.445	23.092	25.078	24.566	22.079	44.212	46.55	9.732	35.371	-1.284	-6.99	49.122	0.046	0.001	0	1588.10	26.4683	45.1	12.0	39.8	2.743	0.007	0.007	0.000	0.168	0.14
1450	10/2/2002	7:39:22 PM	26.437	23.084	25.13	24.593	22.061	44.552	47.019	9.748	35.736	-1.284	-6.987	49.548	0.046	0.001	0	1589.10	26.4845	45.5	12.1	40.1	2.768	0.007	0.007	0.000	0.167	0.14
1451	10/2/2002	7:40:22 PM	26.429	23.07	25.162	24.505	22.037	44.198	46.685	9.811	35.281	-1.286	-6.993	49.357	0.046	0.001	0	1590.10	26.5017	45.2	12.1	39.7	2.740	0.007	0.007	0.000	0.168	0.14
1452	10/2/2002	7:41:22 PM	26.431	23.052	25.084	24.467	22.054	44.463	46.897	9.816	35.592	-1.284	-6.987	49.517	0.046	0.001	0	1591.10	26.5163	45.2	12.1	40.0	2.761	0.007	0.007	0.000	0.167	0.14
1453	10/2/2002	7:42:22 PM	26.434	23.085	25.151	24.505	22.012	44.558	47.087	9.856	35.723	-1.286	-6.99	49.626	0.046	0.001	0	1592.10	26.535	45.6	12.2	40.1	2.768	0.007	0.007	0.000	0.166	0.14
1454	10/2/2002	7:43:22 PM	26.427	23.032	25.141	24.377	22.021	44.329	46.897	9.831	35.441	-1.286	-6.941	49.621	0.046	0.001	0	1593.10	26.5517	45.4	12.2	39.9	2.757	0.007	0.007	0.000	0.168	0.14
1455	10/2/2002	7:44:22 PM	26.424	23.025	25.081	24.39	21.997	44.465	46.634	9.743	35.318	-1.284	-6.953	49.038	0.046	0.001	0	1594.10	26.5683	45.2	12.0	39.7	2.737	0.007	0.007	0.000	0.169	0.14
1456	10/2/2002	7:45:22 PM	26.393	23.023	25.109	24.311	21.986	44.28	46.573	9.781	35.654	-1.284	-6.953	49.542	0.046	0.002	0	1595.10	26.585	45.2	12.3	40.0	2.765	0.007	0.007	0.000	0.167	0.14
1457	10/2/2002	7:46:22 PM	26.407	23.028	25.119	24.207	21.97	44.494	46.894	9.837	35.605	-1.284	-6.961	49.973	0.046	0.001	0	1596.10	26.6017	45.5	12.2	40.0	2.761	0.007	0.007	0.000	0.167	0.14
1458	10/2/2002	7:47:22 PM	26.404	23.028	25.076	24.234	21.962	43.778	46.047	9.63	35.181	-1.286	-6.961	49.359	0.046	0.001	0	1597.10	26.6183	44.6	12.1	39.5	2.722	0.007	0.007	0.000	0.170	0.14
1459	10/2/2002	7:48:22 PM	26.401	23.027	25.188	24.2	21.938	44.217	46.508	9.73	35.469	-1.278	-6.998	49.688	0.046	0.001	0	1598.10	26.635	45.0	12.2	39.8	2.747	0.007	0.007	0.000	0.168	0.14
1460	10/2/2002	7:49:22 PM	26.398	23.023	25.105	24.112	21.92	43.724	46.191	9.728	34.915	-1.284	-6.967	49.493	0.046	0.001	0	1599.10	26.6517	44.7	12.1	39.3	2.711	0.007	0.007	0.000	0.170	0.14
1461	10/2/2002	7:50:22 PM	26.392	23.042	25.169	24.091	21.902	44.246	46.663	9.639	35.424	-1.281	-6.97	49.545	0.046	0.001	0	1600.10	26.6683	45.2	12.3	39.7	2.741	0.007	0.007	0.000	0.168	0.14
1462	10/2/2002	7:51:22 PM	26.384	23.025	25.191	24.074	21.896	44.084	46.639	9.752	35.349	-1.284	-6.967	49.363	0.046	0.001	0	1601.10	26.6865	45.2	12.1	39.7	2.738	0.007	0.007	0.000	0.168	0.14
1463	10/2/2002	7:52:22 PM	26.409	23.027	25.156	24.119	21.888	44.072	46.529	9.744	35.453	-1.281	-6.961	49.319	0.046	0.001	0	1602.10	26.7017	45.1	12.1	39.8	2.741	0.007	0.007	0.000	0.168	0.14
1464	10/2/2002	7:53:22 PM	26.384	23.025	25.171	24.089	21.866	44.108	46.713	9.742	35.361	-1.284	-6.964	49.527	0.046	0.001	0	1603.10	26.7183	45.2	12.1	39.7	2.739	0.007	0.007	0.000	0.168	0.14
1465	10/2/2002	7:54:22 PM	26.393	23.023	25.166	24.069	21.84	44.242	46.583	9.781	35.681	-1.284	-6.965	49.545	0.046	0.001	0	1604.10	26.735	45.2	12.1	39.5	2.735	0.007	0.007	0.000	0.167	0.14
1466	10/2/2002	7:55:22 PM	26.367	23.02	25.089	24.021	21.823	44.165	46.473	9.74	35.306	-1.286	-6.967	49.141	0.046	0.001	0	1605.10	26.7517	45.3	12.0	39.7	2.740	0.007	0.007	0.000	0.168	0.14
1467	10/2/2002	7:56:22 PM	26.359	23.029	25.161	24.003	21.805	43.904	46.477	9.639	35.109	-1.284	-6.97	49.363	0.046	0.001	0	1606.10	26.7683	45.1	12.1	39.5	2.724	0.007	0.007	0.000	0.169	0.14
1468	10/2/2002	7:57:22 PM	26.357	23.027	25.194	23.966	21.809	43.999	46.665	9.733	35.091	-1.284	-6.967	49.365	0.046	0.001	0	1607.10	26.785	45.2	12.1	39.5	2.726	0.007	0.007	0.000	0.169	0.14
1469	10/2/2002	7:58:22 PM	26.35	23.025	25.117	23.969	21.776	44.146	46.497	9.665	35.74	-1.281	-6.967	49.602	0.046	0.001	0	1608.10	26.8017	45.0	12.2	39.9	2.754	0.007	0.007	0.000	0.167	0.14
1470	10/2/2002	7:59:22 PM	26.352	23.042	25.169	23.917	21.738	44.058	46.687	9.816	35.424	-1.281	-6.97	49.154	0.046	0.001	0	1609.10	26.8183	45.2	12.3	39.7	2.741	0.007	0.007	0.000	0.168	0.14
1471	10/2/2002	8:00:22 PM	26.351	23.036	25.128	23.869	21.732	43.438	46.591	9.8																		

1561	10/2/2002	9:20:25 PM	24.968	21.716	25	23.069	21.01	44.894	47.696	9.751	36.129	-1.284	-6.967	50.265	0.043	0.001	0	1699.15	26.3192	46.2	12.3	40.5	2.793	0.006	0.006	0.000	0.158	0.13
1562	10/2/2002	9:30:25 PM	24.957	21.702	25	23.048	20.968	44.714	47.576	9.753	35.965	-1.281	-6.967	48.883	0.043	0.001	0	1700.15	26.3368	46.1	12.0	40.3	2.791	0.006	0.006	0.000	0.158	0.13
1563	10/2/2002	9:31:25 PM	24.961	21.695	25.043	22.996	20.951	44.79	47.716	9.762	35.944	-1.284	-6.967	49.669	0.043	0.001	0	1701.15	26.3525	46.2	12.1	40.4	2.793	0.006	0.006	0.000	0.159	0.13
1564	10/2/2002	9:32:25 PM	24.965	21.686	25.117	22.992	20.931	44.589	47.811	9.741	35.979	-1.284	-6.967	50.562	0.043	0.001	0	1702.15	26.3693	46.3	12.3	40.3	2.792	0.006	0.006	0.000	0.159	0.13
1565	10/2/2002	9:33:25 PM	24.964	21.674	25.091	22.986	20.925	44.699	47.59	9.727	35.954	-1.284	-6.967	50.175	0.043	0.001	0	1703.15	26.3868	46.1	12.3	40.3	2.797	0.006	0.006	0.000	0.159	0.14
1566	10/2/2002	9:34:25 PM	24.942	21.657	25.019	23.049	20.908	45.045	47.987	9.832	36.219	-1.284	-6.967	50.326	0.042	0.001	0	1704.15	26.4025	46.5	12.3	40.6	2.801	0.006	0.006	0.000	0.154	0.13
1567	10/2/2002	9:35:25 PM	24.951	21.656	25.138	22.997	20.912	44.805	47.69	9.748	36.03	-1.281	-6.964	49.467	0.043	0.001	0	1705.15	26.4192	46.2	12.1	40.4	2.787	0.006	0.006	0.000	0.158	0.13
1568	10/2/2002	9:36:25 PM	24.964	21.65	25.063	23.002	20.911	44.925	47.874	9.752	36.155	-1.284	-6.967	50.042	0.042	0.001	0	1706.15	26.4358	46.4	12.1	40.5	2.795	0.006	0.006	0.000	0.154	0.13
1569	10/2/2002	9:37:25 PM	24.963	21.639	25.136	22.99	20.914	44.836	47.626	9.696	36.151	-1.284	-6.964	49.634	0.042	0.001	0	1707.15	26.4525	46.3	12.2	40.5	2.793	0.006	0.006	0.000	0.154	0.13
1570	10/2/2002	9:38:25 PM	24.963	21.628	25.105	22.994	20.904	44.924	47.803	9.704	36.002	-1.284	-6.964	49.621	0.042	0.001	0	1708.15	26.4692	46.3	12.2	40.4	2.786	0.006	0.006	0.000	0.154	0.13
1571	10/2/2002	9:39:25 PM	24.962	21.622	25.049	23.038	20.862	44.736	47.841	9.788	35.734	-1.281	-6.964	50.097	0.042	0.001	0	1709.15	26.4858	46.4	12.3	40.2	2.774	0.006	0.006	0.000	0.155	0.13
1572	10/2/2002	9:40:25 PM	24.947	21.611	25.144	22.962	20.867	44.705	47.7	9.801	35.783	-1.281	-6.964	49.36	0.042	0.001	0	1710.15	26.5025	46.2	12.1	40.2	2.775	0.006	0.006	0.000	0.155	0.13
1573	10/2/2002	9:41:25 PM	24.941	21.605	25.027	22.977	20.861	44.611	47.629	9.719	35.891	-1.289	-6.967	49.645	0.042	0.001	0	1711.15	26.5192	46.2	12.2	40.3	2.775	0.006	0.006	0.000	0.155	0.13
1574	10/2/2002	9:42:25 PM	24.946	21.605	25.153	22.971	20.861	44.662	47.681	9.845	35.709	-1.281	-6.953	50.033	0.043	0.001	0	1712.15	26.5358	46.2	12.3	40.2	2.771	0.006	0.006	0.000	0.159	0.14
1575	10/2/2002	9:43:25 PM	24.95	21.599	25.117	22.995	20.865	45.101	48.016	9.782	36.245	-1.278	-6.961	50.309	0.042	0.001	0	1713.15	26.5525	46.5	12.3	40.7	2.804	0.006	0.006	0.000	0.153	0.13
1576	10/2/2002	9:44:25 PM	24.944	21.578	25.066	22.964	20.854	44.621	47.642	9.716	35.903	-1.284	-6.97	49.917	0.042	0.001	0	1714.15	26.5692	46.2	12.2	40.3	2.776	0.006	0.006	0.000	0.155	0.13
1577	10/2/2002	9:45:25 PM	24.937	21.566	25.139	22.992	20.837	44.735	47.687	9.753	35.94	-1.284	-6.97	50.568	0.042	0.001	0	1715.15	26.5858	46.2	12.3	40.3	2.781	0.006	0.006	0.000	0.155	0.13
1578	10/2/2002	9:46:25 PM	24.952	21.56	25.048	22.947	20.847	44.554	47.626	9.696	36.162	-1.281	-6.967	49.708	0.042	0.001	0	1716.15	26.6025	46.2	12.2	40.2	2.769	0.006	0.006	0.000	0.154	0.13
1579	10/2/2002	9:47:25 PM	24.935	21.549	25.158	22.881	20.861	44.884	48.049	9.77	36.043	-1.281	-6.973	49.965	0.042	0.001	0	1717.15	26.6192	46.6	12.2	40.5	2.790	0.006	0.006	0.000	0.154	0.13
1580	10/2/2002	9:48:25 PM	24.939	21.538	25.091	22.905	20.849	44.881	47.89	9.815	35.993	-1.284	-6.97	49.573	0.042	0.001	0	1718.15	26.6358	46.4	12.1	40.4	2.788	0.006	0.006	0.000	0.154	0.13
1581	10/2/2002	9:49:25 PM	24.953	21.547	25.105	22.903	20.843	44.896	47.942	9.828	36.03	-1.278	-6.97	49.292	0.042	0.001	0	1719.15	26.6525	46.5	12.1	40.5	2.790	0.006	0.006	0.000	0.154	0.13
1582	10/2/2002	9:50:25 PM	24.943	21.547	25.165	22.908	20.843	44.817	47.872	9.779	36.051	-1.278	-6.967	50.184	0.042	0.001	0	1720.15	26.6692	46.4	12.3	40.4	2.788	0.006	0.006	0.000	0.154	0.13
1583	10/2/2002	9:51:25 PM	24.947	21.541	25.074	22.902	20.852	44.904	48.051	9.812	36.03	-1.278	-6.967	50.144	0.042	0.001	0	1721.15	26.6858	46.6	12.3	40.5	2.790	0.006	0.006	0.000	0.154	0.13
1584	10/2/2002	9:52:25 PM	24.946	21.52	25.183	22.877	20.856	45.95	47.857	9.787	36.11	-1.281	-6.97	49.942	0.042	0.001	0	1722.15	26.7025	46.4	12.2	40.5	2.794	0.006	0.006	0.000	0.154	0.13
1585	10/2/2002	9:53:25 PM	24.94	21.514	25.107	22.886	20.836	44.356	47.894	9.625	35.490	-1.281	-6.97	49.041	0.042	0.001	0	1723.15	26.7192	46.2	12.3	39.9	2.753	0.006	0.006	0.000	0.156	0.13
1586	10/2/2002	9:54:25 PM	24.937	21.505	25.194	22.872	20.815	44.865	47.829	9.635	35.94	-1.284	-6.97	49.523	0.042	0.001	0	1724.15	26.7358	46.3	12.2	40.4	2.784	0.006	0.006	0.000	0.154	0.13
1587	10/2/2002	9:55:25 PM	24.939	21.492	25.151	22.834	20.786	44.674	47.646	9.630	36.169	-1.284	-6.97	49.523	0.042	0.001	0	1725.15	26.7525	46.2	12.2	40.2	2.776	0.006	0.006	0.000	0.155	0.13
1588	10/2/2002	9:56:25 PM	24.948	21.491	25.07	22.888	20.797	44.78	47.843	9.658	35.84	-1.281	-6.97	49.963	0.042	0.001	0	1726.15	26.7692	46.4	12.2	40.3	2.779	0.006	0.006	0.000	0.155	0.13
1589	10/2/2002	9:57:25 PM	24.942	21.486	25.189	22.842	20.807	44.879	47.934	9.652	36.006	-1.281	-6.967	50.026	0.042	0.001	0	1727.15	26.7858	46.5	12.3	40.4	2.788	0.006	0.006	0.000	0.154	0.13
1590	10/2/2002	9:58:25 PM	24.947	21.47	25.109	22.852	20.796	44.474	47.536	9.632	35.592	-1.284	-6.967	50.429	0.042	0.001	0	1728.15	26.8025	46.1	12.4	40.0	2.780	0.006	0.006	0.000	0.156	0.13
1591	10/2/2002	9:59:25 PM	24.932	21.465	25.194	22.807	20.786	44.756	47.629	9.625	35.975	-1.281	-6.97	49.477	0.042	0.001	0	1729.15	26.8192	46.3	12.1	40.4	2.784	0.006	0.006	0.000	0.151	0.13
1592	10/2/2002	9:59:31 PM	24.946	21.469	25.198	22.786	20.781	44.813	47.901	9.603	35.932	-1.281	-6.964	49.743	0.041	0.001	0	1729.25	26.8208	46.4	12.2	40.4	2.784	0.006	0.006	0.000	0.151	0.13
1593	10/2/2002	10:00:31 PM	24.946	21.454	25.143	22.785	20.755	44.813	47.816	9.786	36.045	-1.284	-6.97	50.146	0.041	0.001	0	1730.25	26.8375	46.3	12.3	40.4	2.787	0.006	0.006	0.000	0.151	0.13
1594	10/2/2002	10:01:31 PM	24.96	21.458	25.122	22.82	20.729	44.482	47.619	9.672	35.672	-1.281	-6.97	50.035	0.041	0.001	0	1731.25	26.8542	46.1	12.3	40.0	2.780	0.006	0.006	0.000	0.152	0.13
1595	10/2/2002	10:02:31 PM	24.945	21.45	25.107	22.82	20.711	44.651	47.629	9.625	36.043	-1.284	-6.964	50.003	0.042	0.001	0	1732.25	26.8708	46.4	12.3	40.3	2.783	0.006	0.006	0.000	0.151	0.13
1596	10/2/2002	10:03:31 PM	24.945	21.418	25.092	22.8	20.659	44.703	47.783	9.609	35.842	-1.286	-6.976	49.739	0.041	0.001	0	1733.25	26.8875	46.2	12.3	40.3	2.777	0.006	0.006	0.000	0.151	0.13
1597	10/2/2002	10:04:31 PM	24.935	21.408	25.212	22.725	20.659	44.517	47.576	9.796	35.639	-1.284	-6.967	49.953														

1691	10/2/2002	11:38:31 PM	26.125	20.642	25.657	22.02	20.053	45.161	48.67	9.799	36.365	-1.281	-6.973	49.519	0.039	0.001	1628.25	30.4708	47.2	12.1	40.8	2.811	0.006	0.006	0.000	0.140	0.12
1692	10/2/2002	11:39:31 PM	26.149	20.646	25.711	21.959	20.052	45.364	48.962	9.886	36.503	-1.281	-6.973	49.414	0.039	0.001	1629.25	30.4875	47.5	12.1	40.9	2.822	0.006	0.006	0.000	0.139	0.12
1693	10/2/2002	11:40:31 PM	26.144	20.635	25.711	21.963	19.996	45.516	49.272	9.951	36.489	-1.281	-6.973	49.005	0.039	0.001	1630.25	30.5042	47.9	12.0	41.0	2.827	0.006	0.006	0.000	0.139	0.12
1694	10/2/2002	11:41:31 PM	26.139	20.624	25.744	21.997	19.996	45.401	49.171	9.929	36.331	-1.272	-6.967	49.144	0.039	0.001	1631.25	30.5208	47.7	12.1	40.9	2.818	0.006	0.006	0.000	0.139	0.13
1695	10/2/2002	11:42:31 PM	26.147	20.608	25.728	21.986	20.004	44.915	48.627	9.809	36.036	-1.281	-6.973	49.163	0.039	0.001	1632.25	30.5375	47.2	12.1	40.5	2.791	0.006	0.006	0.000	0.141	0.12
1696	10/2/2002	11:43:31 PM	26.162	20.608	25.693	22.007	20.069	45.149	48.862	9.839	36.211	-1.281	-6.973	49.233	0.039	0.001	1633.25	30.5542	47.4	12.1	40.7	2.805	0.006	0.006	0.000	0.140	0.12
1697	10/2/2002	11:44:31 PM	26.162	20.623	25.789	22.032	20.141	44.888	48.767	9.842	36.501	-1.284	-6.964	49.08	0.039	0.001	1634.25	30.5708	47.3	12.0	40.4	2.786	0.006	0.006	0.000	0.141	0.12
1698	10/2/2002	11:45:31 PM	26.184	20.625	25.7	22.124	20.236	45.184	48.946	9.821	36.288	-1.284	-6.964	49.236	0.039	0.001	1635.25	30.5875	47.4	12.1	40.7	2.809	0.006	0.006	0.000	0.140	0.12
1699	10/2/2002	11:46:31 PM	26.18	20.636	25.943	22.067	20.335	45.277	49.033	9.824	36.471	-1.284	-6.964	49.296	0.039	0.001	1636.25	30.6042	47.6	12.1	40.8	2.814	0.006	0.006	0.000	0.143	0.12
1700	10/2/2002	11:47:31 PM	26.203	20.644	25.739	22.455	20.418	45.271	48.918	9.833	36.272	-1.281	-6.964	49.898	0.039	0.001	1637.25	30.6208	47.4	12.0	40.8	2.814	0.006	0.006	0.000	0.140	0.12
1701	10/2/2002	11:48:31 PM	26.226	20.667	25.882	22.569	20.497	45.113	48.91	9.801	36.227	-1.281	-6.963	48.831	0.04	0.001	1638.25	30.6375	47.4	12.0	40.7	2.804	0.006	0.006	0.000	0.143	0.12
1702	10/2/2002	11:49:31 PM	26.23	20.676	25.796	22.708	20.582	45.265	49.274	9.865	36.448	-1.281	-6.963	48.719	0.039	0.001	1639.25	30.6542	47.8	11.9	40.9	2.822	0.006	0.006	0.000	0.139	0.12
1703	10/2/2002	11:50:31 PM	26.259	20.696	25.921	22.869	20.667	45.329	49.045	9.804	36.522	-1.281	-6.963	48.805	0.039	0.001	1640.25	30.6708	47.6	12.0	40.9	2.822	0.006	0.006	0.000	0.139	0.12
1704	10/2/2002	11:51:31 PM	26.279	20.731	25.871	23.07	20.748	45.242	48.982	9.826	36.372	-1.278	-6.944	49.936	0.039	0.001	1641.25	30.6875	47.5	12.0	40.8	2.813	0.006	0.006	0.000	0.139	0.12
1705	10/2/2002	11:52:31 PM	26.279	20.746	25.751	23.115	20.884	45.076	48.682	9.757	36.372	-1.284	-6.947	47.36	0.039	0.001	1642.25	30.7042	47.2	11.6	40.7	2.808	0.006	0.006	0.000	0.140	0.12
1706	10/2/2002	11:53:31 PM	26.29	20.767	25.886	23.166	20.975	45.039	48.962	9.696	36.303	-1.284	-6.939	48.95	0.039	0.001	1643.25	30.7208	47.4	12.0	40.7	2.804	0.006	0.006	0.000	0.139	0.12
1707	10/2/2002	11:54:31 PM	26.311	20.789	25.807	23.222	21.082	44.94	48.716	9.74	36.028	-1.284	-6.934	49.087	0.039	0.001	1644.25	30.7375	47.2	12.0	40.4	2.786	0.006	0.006	0.000	0.141	0.12
1708	10/2/2002	11:55:31 PM	26.332	20.845	25.943	23.419	21.204	45.006	48.831	9.829	36.028	-1.281	-6.939	49.668	0.039	0.001	1645.25	30.7542	47.4	12.0	40.5	2.794	0.006	0.006	0.000	0.140	0.12
1709	10/2/2002	11:56:31 PM	26.338	20.866	25.86	23.486	21.306	45.066	48.852	9.789	36.215	-1.284	-6.932	49.829	0.039	0.001	1646.25	30.7708	47.4	12.0	40.6	2.802	0.006	0.006	0.000	0.140	0.12
1710	10/2/2002	11:57:31 PM	26.346	20.914	25.787	23.593	21.429	45.277	49.15	9.783	36.372	-1.281	-6.928	48.668	0.039	0.001	1647.25	30.7875	47.7	11.9	40.8	2.815	0.006	0.006	0.000	0.139	0.12
1711	10/2/2002	11:58:31 PM	26.35	20.933	25.907	23.648	21.494	45.097	48.963	9.82	36.2	-1.284	-6.941	49.141	0.039	0.001	1648.25	30.7981	47.5	12.0	40.6	2.803	0.006	0.006	0.000	0.139	0.12
1712	10/2/2002	11:59:31 PM	26.357	20.966	25.954	23.786	21.592	44.948	48.821	9.693	36.178	-1.281	-6.913	48.375	0.04	0.001	1649.25	30.8147	47.3	11.9	40.6	2.797	0.006	0.006	0.000	0.144	0.12
1713	10/2/2002	12:00:09 AM	26.395	21.009	25.787	23.909	21.71	45.174	48.995	9.754	36.407	-1.284	-6.944	48.648	0.039	0.001	1649.88	30.8313	47.5	11.9	40.3	2.812	0.006	0.006	0.000	0.139	0.12
1714	10/2/2002	12:01:09 AM	26.383	21.042	25.909	23.932	21.784	45.327	49.16	9.826	36.246	-1.284	-6.938	47.753	0.039	0.001	1650.88	30.848	47.7	11.9	40.3	2.819	0.006	0.006	0.000	0.139	0.12
1715	10/2/2002	12:02:09 AM	26.401	21.081	25.818	24.045	21.893	45.037	48.979	9.723	36.308	-1.286	-6.941	48.344	0.039	0.001	1651.88	30.8647	47.7	11.8	40.6	2.801	0.006	0.006	0.000	0.140	0.12
1716	10/2/2002	12:03:09 AM	26.418	21.125	25.868	24.212	21.986	44.743	48.643	9.621	36.331	-1.284	-6.933	48.226	0.039	0.001	1652.88	30.8813	47.2	11.8	40.4	2.788	0.006	0.006	0.000	0.141	0.12
1717	10/2/2002	12:04:09 AM	26.432	21.168	25.879	24.112	22.09	45.219	49.14	9.748	36.434	-1.284	-6.935	48.058	0.039	0.001	1653.88	30.898	47.7	11.9	40.5	2.815	0.006	0.006	0.000	0.139	0.12
1718	10/2/2002	12:05:09 AM	26.44	21.211	25.792	24.306	22.184	44.997	48.817	9.677	36.339	-1.284	-6.928	48.961	0.039	0.001	1654.88	30.9147	47.3	12.0	40.7	2.804	0.006	0.006	0.000	0.140	0.12
1719	10/2/2002	12:06:09 AM	26.453	21.249	25.92	24.288	22.267	45.004	48.997	9.759	36.12	-1.284	-6.927	47.748	0.039	0.001	1655.88	30.9313	47.5	11.7	40.6	2.797	0.006	0.006	0.000	0.140	0.12
1720	10/2/2002	12:07:09 AM	26.461	21.287	25.843	24.426	22.35	44.911	48.734	9.631	36.307	-1.284	-7.037	48.147	0.039	0.001	1656.88	30.948	47.3	11.8	40.6	2.800	0.006	0.006	0.000	0.136	0.12
1721	10/2/2002	12:08:09 AM	26.484	21.346	25.961	24.614	22.454	44.954	48.763	9.703	36.229	-1.281	-6.987	48.202	0.039	0.001	1657.88	30.9647	47.3	11.8	40.6	2.799	0.006	0.006	0.000	0.139	0.12
1722	10/2/2002	12:09:09 AM	26.491	21.373	25.898	24.482	22.532	44.979	48.813	9.626	36.38	-1.281	-6.982	48.491	0.039	0.001	1658.88	30.9813	47.3	11.9	40.7	2.805	0.006	0.006	0.000	0.139	0.12
1723	10/2/2002	12:10:09 AM	26.515	21.427	25.817	24.581	22.638	45.089	49.148	9.714	36.278	-1.281	-6.982	48.201	0.039	0.001	1659.88	30.998	47.7	11.8	40.7	2.805	0.006	0.006	0.000	0.140	0.12
1724	10/2/2002	12:11:09 AM	26.538	21.476	25.93	24.609	22.74	44.774	48.726	9.715	35.963	-1.286	-6.982	48.002	0.039	0.001	1660.88	31.0147	47.3	11.8	40.4	2.783	0.006	0.006	0.000	0.140	0.12
1725	10/2/2002	12:12:09 AM	26.557	21.524	25.884	24.683	22.824	45.017	48.913	9.623	36.103	-1.284	-6.976	48.202	0.039	0.001	1661.88	31.0313	47.3	11.8	40.3	2.783	0.006	0.006	0.000	0.140	0.12
1726	10/2/2002	12:13:09 AM	26.555	21.563	25.802	24.741	22.912	44.704	48.763	9.601	36.382	-1.284	-6.976	48.082	0.039	0.001	1662.88	31.048	47.5	11.8	40.7	2.808	0.006	0.006	0.000	0.140	0.12
1727	10/2/2002	12:14:09 AM	26.573	21.607	25.96	24.769	23.001	44.712	48.629	9.56	36.281	-1.281	-6.964	48.61	0.039	0.001	1663.88	31.0647	47.2	11.9	40.5	2.790	0.006	0.006	0.000	0.140	0.12
1728	10/2/2002	12:15:09 AM	26.597	21.67</																							

1821	10/9/2002	1:48:09 AM	26.892	24.869	25.376	26.679	26.627	39.323	44.419	10.982	29.664	-1.165	-6.744	50.15	0.031	0.001	0	1957.88	32.6313	42.9	12.3	34.5	2.378	0.005	0.005	0.000	0.133	0.11
1822	10/9/2002	1:49:09 AM	26.886	24.884	25.375	26.683	26.636	45.451	50.757	11.206	34.972	-1.162	-6.724	52.486	0.036	0.001	0	1958.88	32.6448	49.3	12.9	40.2	2.772	0.005	0.005	0.000	0.128	0.11
1823	10/9/2002	1:50:09 AM	26.929	24.907	25.593	26.681	26.66	45.961	51.268	11.098	35.736	-1.106	-6.724	53.298	0.04	0.001	0	1959.88	32.6647	49.8	13.1	40.9	2.817	0.005	0.005	0.000	0.144	0.12
1824	10/9/2002	1:51:09 AM	26.973	24.946	25.793	26.685	26.665	45.998	51.924	9.975	36.1	-1.006	-6.741	50.402	0.039	0.001	0	1960.88	32.6913	49.8	12.4	41.4	2.958	0.005	0.005	0.000	0.137	0.13
1825	10/9/2002	1:52:09 AM	26.95	24.947	25.784	26.712	26.66	45.971	51.908	9.975	36.05	-1.012	-6.744	49.948	0.038	0.001	0	1961.88	32.6986	49.5	12.0	41.4	2.952	0.005	0.005	0.000	0.134	0.11
1826	10/9/2002	1:53:09 AM	26.033	24.971	25.922	26.725	26.703	45.646	50.988	9.525	36.978	-1.003	-6.733	49.931	0.039	0.001	0	1962.88	32.7147	49.5	12.0	41.3	2.848	0.005	0.005	0.000	0.137	0.12
1827	10/9/2002	1:54:09 AM	26.08	24.983	25.954	26.708	26.701	45.043	50.404	9.933	36.243	-1.009	-6.739	49.405	0.038	0.001	0	1963.88	32.7313	49.1	12.1	40.6	2.802	0.005	0.005	0.000	0.136	0.12
1828	10/9/2002	1:55:09 AM	26.133	25.063	26.007	26.795	26.696	45.472	50.675	9.441	36.874	-0.997	-6.733	49.16	0.038	0.001	0	1964.88	32.7449	49.2	12.0	41.1	2.842	0.005	0.005	0.000	0.134	0.11
1829	10/9/2002	1:56:09 AM	26.18	25.049	26.005	26.863	26.725	45.142	50.435	9.442	36.628	-0.954	-6.743	49.143	0.039	0.001	0	1965.88	32.7547	49.0	12.0	40.9	2.819	0.005	0.005	0.000	0.135	0.11
1830	10/9/2002	1:57:09 AM	26.23	25.046	25.958	26.851	26.729	45.161	50.379	9.901	36.679	-0.954	-6.733	49.952	0.038	0.001	0	1966.88	32.7813	48.9	12.0	40.9	2.821	0.005	0.005	0.000	0.135	0.11
1831	10/9/2002	1:57:35 AM	26.235	25.088	25.974	26.887	26.74	45.41	50.776	9.523	36.761	-0.954	-6.733	49.296	0.038	0.001	0	1967.31	32.7886	49.3	12.1	41.1	2.833	0.005	0.005	0.000	0.134	0.11
1832	10/9/2002	1:58:35 AM	26.263	25.09	26.142	26.835	26.758	45.722	51.06	9.611	37.042	-0.917	-6.718	49.558	0.039	0.001	0	1968.31	32.8052	49.6	12.1	41.4	2.853	0.005	0.005	0.000	0.136	0.12
1833	10/9/2002	1:59:35 AM	26.302	25.105	26.171	26.869	26.771	45.056	51.33	9.751	37.51	-0.898	-6.713	49.2	0.039	0.001	0	1969.31	32.8219	49.8	12.1	41.8	2.881	0.005	0.005	0.000	0.135	0.11
1834	10/9/2002	2:00:35 AM	26.34	25.143	26.169	26.907	26.79	45.816	51.192	9.533	37.248	-0.888	-6.715	49.376	0.039	0.001	0	1970.31	32.8386	49.7	12.1	41.5	2.863	0.005	0.005	0.000	0.135	0.12
1835	10/9/2002	2:01:35 AM	26.372	25.155	26.146	26.924	26.796	45.985	51.242	9.507	37.383	-0.888	-6.712	49.409	0.039	0.001	0	1971.31	32.8552	49.8	12.1	41.7	2.874	0.005	0.005	0.000	0.135	0.12
1836	10/9/2002	2:02:35 AM	26.406	25.169	26.09	26.963	26.801	45.869	51.202	9.497	37.265	-0.893	-6.715	49.08	0.039	0.001	0	1972.31	32.8719	49.7	12.0	41.6	2.866	0.005	0.005	0.000	0.136	0.12
1837	10/9/2002	2:03:35 AM	26.438	25.186	26.072	27.04	26.828	45.913	51.395	9.403	37.255	-0.899	-6.717	49.466	0.039	0.001	0	1973.31	32.8886	49.9	12.1	41.6	2.867	0.005	0.005	0.000	0.136	0.12
1838	10/9/2002	2:04:35 AM	26.46	25.14	26.04	27.062	26.846	45.933	51.194	9.933	37.969	-0.859	-6.703	49.179	0.039	0.001	0	1974.31	32.9052	49.7	12.1	41.6	2.868	0.005	0.005	0.000	0.135	0.12
1839	10/9/2002	2:05:35 AM	26.469	25.237	26.013	27.086	26.859	45.816	51.27	9.561	37.186	-0.86	-6.704	49.947	0.039	0.001	0	1975.31	32.9219	49.8	12.2	41.5	2.861	0.005	0.005	0.000	0.136	0.12
1840	10/9/2002	2:06:35 AM	26.477	25.26	25.986	27.104	26.882	46.108	51.608	9.479	37.508	-0.838	-6.709	48.634	0.039	0.001	0	1976.31	32.9386	50.1	11.9	41.8	2.883	0.005	0.005	0.000	0.135	0.12
1841	10/9/2002	2:07:35 AM	26.485	25.278	25.949	27.087	26.886	46.097	51.58	9.539	37.349	-0.841	-6.709	48.47	0.039	0.001	0	1977.31	32.9552	50.2	11.9	41.7	2.877	0.005	0.005	0.000	0.136	0.12
1842	10/9/2002	2:08:35 AM	26.487	25.3	25.916	27.084	26.897	45.027	51.488	9.937	37.408	-0.841	-6.711	48.96	0.039	0.001	0	1978.31	32.9719	50.0	12.0	41.7	2.876	0.005	0.005	0.000	0.132	0.11
1843	10/9/2002	2:09:35 AM	26.484	25.323	25.904	27.151	26.91	45.847	51.403	9.508	37.171	-0.798	-6.675	48.457	0.039	0.001	0	1979.31	32.9886	49.9	11.9	41.5	2.862	0.005	0.005	0.000	0.137	0.12
1844	10/9/2002	2:10:35 AM	26.477	25.33	25.861	27.134	26.937	46.041	51.597	9.482	37.49	-0.778	-6.678	49.015	0.038	0.001	0	1980.31	33.0052	50.1	12.0	41.8	2.880	0.005	0.005	0.000	0.132	0.11
1845	10/9/2002	2:11:35 AM	26.484	25.363	25.854	27.166	26.94	45.934	51.341	9.406	37.519	-0.772	-6.675	49.077	0.038	0.001	0	1981.31	33.0219	49.9	12.0	41.7	2.877	0.005	0.005	0.000	0.133	0.11
1846	10/9/2002	2:12:35 AM	26.487	25.378	25.865	27.189	26.957	45.92	51.303	9.425	37.505	-0.768	-6.678	49.075	0.038	0.001	0	1982.31	33.0386	49.9	12.0	41.6	2.886	0.005	0.005	0.000	0.132	0.11
1847	10/9/2002	2:13:35 AM	26.469	25.403	26.014	27.096	26.964	45.721	51.282	9.387	37.216	-0.772	-6.666	49.248	0.038	0.001	0	1983.31	33.0552	49.8	12.1	41.5	2.885	0.005	0.005	0.000	0.133	0.11
1848	10/9/2002	2:14:35 AM	26.467	25.415	26.061	27.079	26.982	45.602	51.148	9.609	36.927	-0.772	-6.657	49.867	0.039	0.001	0	1984.31	33.0719	49.7	12.2	41.4	2.845	0.005	0.005	0.000	0.137	0.12
1849	10/9/2002	2:15:35 AM	26.489	25.443	26.104	27.076	26.999	44.836	50.937	9.006	36.000	-0.72	-6.666	50.163	0.038	0.001	0	1985.31	33.0886	49.8	12.3	40.4	2.787	0.005	0.005	0.000	0.136	0.12
1850	10/9/2002	2:16:35 AM	26.493	25.454	26.12	27.123	27.011	44.907	50.013	9.733	35.733	-0.772	-6.669	50.345	0.037	0.001	0	1986.31	33.1052	48.5	12.3	40.1	2.786	0.005	0.005	0.000	0.133	0.11
1851	10/9/2002	2:17:35 AM	26.518	25.428	26.113	27.15	27.025	44.952	50.288	9.784	36.055	-0.747	-6.671	50.142	0.037	0.001	0	1987.31	33.1219	49.1	12.2	40.6	2.798	0.005	0.005	0.000	0.132	0.11
1852	10/9/2002	2:18:35 AM	26.521	25.484	26.085	27.148	27.036	44.649	50.311	9.972	36.6	-0.711	-6.669	50.355	0.037	0.001	0	1988.31	33.1386	48.8	12.3	40.1	2.766	0.005	0.005	0.000	0.133	0.11
1853	10/9/2002	2:19:35 AM	26.548	25.512	26.093	27.2	27.059	44.432	49.978	9.682	35.727	-0.717	-6.663	50.211	0.037	0.001	0	1989.31	33.1552	48.5	12.3	40.1	2.763	0.005	0.005	0.000	0.133	0.11
1854	10/9/2002	2:20:35 AM	26.57	25.539	26.084	27.257	27.075	45.225	50.908	9.711	36.489	-0.688	-6.657	49.805	0.037	0.001	0	1990.31	33.1719	49.4	12.0	40.9	2.818	0.005	0.005	0.000	0.131	0.11
1855	10/9/2002	2:21:35 AM	26.57	25.543	26.083	27.284	27.086	45.14	50.83	9.425	36.369	-0.687	-6.653	49.756	0.037	0.001	0	1991.31	33.1904	49.1	12.0	40.6	2.886	0.005	0.005	0.000	0.131	0.11
1856	10/9/2002	2:22:35 AM	26.575	25.564	26.229	27.217	27.105	45.456	50.733	9.842	36.45	-0.619	-6.652	49.94	0.037	0.001	-0.001	1992.31	33.2052	49.3	12.2	40.8	2.813	0.005	0.005	0.000	0.131	0.11
1857	10/9/2002	2:23:35 AM	26.583	25.586	26.272	27.194	27.108	45.37	51.033	9.735	36.509	-0.61	-6.649	49.881	0.038	0.001	0	1993.31	33.2219	49.6	12.2	40.9	2.823	0.005	0.005	0.000	0.134	0.11
1858	10/9/2002	2:24:35 AM	26.605	25.609	26.299	27.247	27.12	45.103	50.716	9.61	36.428	-0.607	-6.646	49.332	0.038	0.001	0	1994.31	33.2386	49.2	12.1	40.8	2.811	0.005	0.005	0.000	0.134	0.11
1859	10/9/2002	2:25:35 AM	26.612	25.606	26.246	27.254	27.127	45.068	50.619	9.651	36.305	-0.578	-6.649	49.328	0.037	0.001	0	1995.31	33.2552	49.3	12.1	40.7	2.805	0.005	0.005	0.000	0.131	0.11
1860	10/9/2002	2:26:35 AM	26.644	25.628	26.268	27.265	27.164	44.952	50.984	9.604	36.263	-0.587	-6.646	49.779	0.037	0.001	0	1996.31	33.2719	49.1	12.1	40.6	2.804	0.005	0.005	0.000	0.131	0.11
1861	10/9/2002	2:27:35 AM	26.651	25.635	26.21	27.263	27.166	45.296	51.026	9.641																		



2081	10/9/2002	6:07:03 AM	26.845	26.189	26.289	26.052	24.864	45.969	53.252	10.311	36.466	9.93	-4.673	51.012	0.039	0.001	0.001	2216.78	36.9463	51.8	12.5	41.2	2.842	0.006	0.006	0.000	0.136	0.12	
2082	10/9/2002	6:08:03 AM	26.634	26.153	26.243	26.046	24.773	46.122	53.306	10.283	36.73	9.936	-4.678	51.645	0.036	0.001	0.001	0.001	2217.78	36.963	51.8	12.7	41.4	2.856	0.005	0.005	0.000	0.125	0.11
2083	10/9/2002	6:09:03 AM	26.823	26.103	26.187	26.001	24.676	46.973	53.217	10.272	36.469	9.962	-4.681	50.913	0.036	0.001	0.001	0.001	2218.78	36.9797	51.7	12.5	41.2	2.842	0.005	0.005	0.000	0.126	0.11
2084	10/9/2002	6:10:03 AM	26.721	26.161	26.221	26.069	24.631	45.778	52.962	10.153	36.903	9.977	-4.57	51.679	0.036	0.001	0.001	0.001	2219.78	36.9963	51.5	12.5	41.1	2.837	0.005	0.005	0.000	0.126	0.11
2085	10/9/2002	6:11:03 AM	26.802	26.037	26.371	26.855	24.562	46.076	53.281	10.227	36.649	9.96	-4.57	51.155	0.036	0.001	0.001	0.001	2220.78	37.013	51.8	12.5	41.3	2.850	0.005	0.005	0.000	0.125	0.11
2086	10/9/2002	6:12:03 AM	26.777	26.262	26.306	26.765	24.496	45.606	52.758	10.05	36.36	9.98	-4.581	51.245	0.036	0.001	0.001	0.001	2221.78	37.0297	51.3	12.6	41.0	2.826	0.005	0.005	0.000	0.126	0.11
2087	10/9/2002	6:13:03 AM	26.772	26.242	26.251	26.775	24.436	45.956	53.43	10.316	36.303	9.98	-4.584	49.992	0.036	0.001	0.001	0.001	2222.78	37.0463	52.0	12.0	41.1	2.836	0.005	0.005	0.000	0.126	0.11
2088	10/9/2002	6:14:03 AM	26.769	26.208	26.213	26.752	24.346	45.669	52.959	10.169	36.299	1.026	-4.575	50.555	0.036	0.001	0.001	0.001	2223.78	37.063	51.5	12.4	41.0	2.828	0.005	0.005	0.000	0.126	0.11
2089	10/9/2002	6:15:03 AM	26.749	26.263	26.363	26.52	24.263	46.054	53.443	10.267	36.644	1.037	-4.576	51.27	0.036	0.001	0.001	0.001	2224.78	37.0797	51.7	12.6	41.3	2.861	0.005	0.005	0.000	0.125	0.11
2090	10/9/2002	6:16:03 AM	26.734	26.214	26.353	26.507	24.183	45.043	53.387	10.222	36.690	1.043	-4.673	50.524	0.036	0.001	0.001	0.001	2225.78	37.0963	51.9	12.5	41.4	2.845	0.005	0.005	0.000	0.125	0.11
2091	10/9/2002	6:17:03 AM	26.761	26.295	26.349	26.543	24.143	45.961	53.374	10.239	36.679	1.075	-4.57	51.584	0.036	0.001	0.001	0.001	2226.78	37.113	51.9	12.6	41.3	2.845	0.005	0.005	0.000	0.125	0.11
2092	10/9/2002	6:18:03 AM	26.736	26.273	26.259	26.523	24.074	46.898	53.298	10.139	36.667	1.075	-4.673	50.963	0.036	0.001	0.001	0.001	2227.78	37.1297	51.9	12.5	41.2	2.843	0.005	0.005	0.000	0.126	0.11
2093	10/9/2002	6:19:03 AM	26.721	26.095	26.32	26.388	23.995	45.971	53.155	10.194	36.497	1.059	-4.57	51.164	0.036	0.001	0.001	0.001	2228.78	37.1463	51.7	12.6	41.2	2.839	0.005	0.005	0.000	0.126	0.11
2094	10/9/2002	6:20:03 AM	26.713	26.647	26.402	26.405	23.915	45.806	53.066	10.156	36.229	1.101	-4.564	51.903	0.036	0.001	0.001	0.001	2229.78	37.163	51.6	12.7	40.9	2.821	0.005	0.005	0.000	0.126	0.11
2095	10/9/2002	6:21:03 AM	26.716	26.6	26.374	26.353	23.853	45.64	53.027	10.077	36.374	1.086	-4.57	51.568	0.036	0.001	0.001	0.001	2230.78	37.1797	51.6	12.6	41.0	2.827	0.005	0.005	0.000	0.126	0.11
2096	10/9/2002	6:22:03 AM	26.707	26.596	26.321	26.314	23.804	45.94	53.41	10.229	36.489	1.07	-4.541	51.186	0.036	0.001	0.001	0.001	2231.78	37.1963	51.9	12.5	41.2	2.842	0.005	0.005	0.000	0.125	0.11
2097	10/9/2002	6:23:03 AM	26.772	26.519	26.283	26.29	23.731	45.987	53.548	10.267	36.416	1.173	-4.541	51.014	0.036	0.001	0.001	0.001	2232.78	37.213	52.1	12.5	41.2	2.841	0.005	0.005	0.000	0.126	0.11
2098	10/9/2002	6:24:03 AM	26.688	26.467	26.42	26.165	23.674	45.826	53.319	10.093	36.981	1.047	-4.967	51.364	0.036	0.001	0.001	0.001	2233.78	37.2297	51.7	12.6	41.3	2.850	0.005	0.005	0.000	0.125	0.11
2099	10/9/2002	6:25:03 AM	26.669	26.407	26.387	26.136	23.63	46.124	53.614	10.254	36.961	1.188	-4.675	51.42	0.036	0.001	0.001	0.001	2234.78	37.2463	52.1	12.6	41.3	2.850	0.005	0.005	0.000	0.125	0.11
2100	10/9/2002	6:26:03 AM	26.676	26.385	26.389	26.133	23.562	46.027	53.439	10.182	36.775	1.191	-4.57	51.018	0.036	0.001	0.001	0.001	2235.78	37.263	52.0	12.5	41.4	2.854	0.005	0.005	0.000	0.125	0.11
2101	10/9/2002	6:27:03 AM	26.659	26.328	26.303	26.146	23.5	45.956	53.482	10.073	36.677	1.188	-4.673	50.773	0.036	0.001	0.001	0.001	2236.78	37.2797	52.0	12.4	41.3	2.849	0.005	0.005	0.000	0.125	0.11
2102	10/9/2002	6:28:03 AM	26.642	26.276	26.425	26.059	23.426	45.526	52.944	10.039	36.247	1.208	-4.57	50.626	0.036	0.001	0.001	0.001	2237.78	37.2963	51.5	12.4	40.9	2.819	0.005	0.005	0.000	0.126	0.11
2103	10/9/2002	6:29:03 AM	26.624	26.227	26.432	26.049	23.374	45.917	53.339	10.197	36.631	1.211	-4.667	50.609	0.036	0.001	0.001	0.001	2238.78	37.313	51.9	12.4	41.2	2.843	0.005	0.005	0.000	0.125	0.11
2104	10/9/2002	6:30:03 AM	26.616	26.18	26.379	24.927	23.326	46.381	53.976	10.319	36.79	1.208	-4.675	51.247	0.036	0.001	0.001	0.001	2239.78	37.3297	52.5	12.6	41.6	2.867	0.005	0.005	0.000	0.124	0.11
2105	10/9/2002	6:31:03 AM	26.608	26.131	26.311	24.929	23.277	46.096	53.561	10.169	36.794	1.272	-4.667	50.981	0.036	0.001	0.001	0.001	2240.78	37.3463	52.1	12.5	41.4	2.867	0.005	0.005	0.000	0.125	0.11
2106	10/9/2002	6:32:03 AM	26.598	26.103	26.247	24.929	23.222	45.95	53.525	10.127	36.797	1.396	-4.564	51.04	0.036	0.001	0.001	0.001	2241.78	37.363	51.9	12.5	41.2	2.844	0.005	0.005	0.000	0.125	0.11
2107	10/9/2002	6:33:03 AM	26.6	26.074	26.463	24.842	23.122	45.702	53.581	10.193	36.342	1.272	-4.658	50.393	0.036	0.001	0.001	0.001	2242.78	37.3797	51.8	12.4	41.0	2.829	0.005	0.005	0.000	0.126	0.11
2108	10/9/2002	6:34:03 AM	26.59	26.023	26.418	24.801	23.149	45.71	53.219	10.169	36.348	1.315	-4.658	50.473	0.036	0.001	0.001	0.001	2243.78	37.3963	51.7	12.4	41.0	2.829	0.005	0.005	0.000	0.126	0.11
2109	10/9/2002	6:35:03 AM	26.59	24.983	26.348	24.801	23.079	45.938	53.503	10.136	36.689	1.324	-4.57	50.744	0.036	0.001	0.001	0.001	2244.78	37.413	52.0	12.4	41.3	2.845	0.005	0.005	0.000	0.125	0.11
2110	10/9/2002	6:36:03 AM	26.586	24.944	26.499	24.707	23.045	45.903	53.511	10.193	36.462	1.329	-4.654	51.339	0.036	0.001	0.001	0.001	2245.78	37.4297	52.0	12.6	41.2	2.839	0.005	0.005	0.000	0.125	0.11
2111	10/9/2002	6:37:03 AM	26.587	24.9	26.495	24.689	23.0	45.821	53.536	10.261	36.497	1.324	-4.664	51.625	0.036	0.001	0.001	0.001	2246.78	37.4463	52.2	12.6	41.1	2.831	0.005	0.005	0.000	0.126	0.11
2112	10/9/2002	6:38:03 AM	26.568	24.851	26.446	24.649	22.916	45.64	53.106	10.164	36.417	1.326	-4.564	50.114	0.036	0.001	0.001	0.001	2247.78	37.463	51.6	12.3	41.0	2.829	0.005	0.005	0.000	0.126	0.11
2113	10/9/2002	6:39:03 AM	26.563	24.811	26.386	24.654	22.876	45.84	53.546	10.212	36.327	1.341	-4.561	51.169	0.036	0.001	0.001	0.001	2248.78	37.4797	52.1	12.5	41.1	2.833	0.005	0.005	0.000	0.126	0.11
2114	10/9/2002	6:40:03 AM	26.546	24.773	26.518	24.581	22.843	45.468	53.105	10.125	36.302	1.393	-4.664	50.597	0.036	0.001	0.001	0.001	2249.78	37.4963	51.6	12.4	40.7	2.809	0.005	0.005	0.000	0.126	0.11
2115	10/9/2002	6:41:03 AM	26.527	24.736	26.509	24.577	22.795	45.542	53.36	10.127	36.297	1.396	-4.564	51.025	0.036	0.001	0.001	0.001	2250.78	37.513	51.8	12.4	41.0	2.825	0.005	0.005	0.000	0.126	0.11
2116	10/9/2002	6:42:03 AM	26.517	24.669	26.44	24.492	22.719	45.546	53.209	10.151	36.094	1.393	-4.561	50.89	0.036	0.001	0.001	0.001	2251.78	37.5297	51.7	12.5	40.9	2.814	0.005	0.005	0.000	0.126	0.11
2117	10/9/2002	6:43:03 AM	26.51	24.617	26.357	24.45	22.676	45.594	53.101	10.153	36.368	1.407	-4.655	50.24	0.036	0.001	0.001	0.001	2252.78	37.5463	51.6	12.3	41.0	2.825	0.005	0.005	0.000	0.126	0.11
2118	10/9/2002	6:44:03 AM	26.497	24.574	26.43	24.372	22.649	45.985	53.648	10.19	36.693	1.396	-4.661	51.662	0.036	0.001	0.001	0.001	2253.78	37.563	52.2	12.7	41.3	2.847	0.005	0.005	0.000	0.125	0.11
2119	10/9/2002	6:45:03 AM	26.486	24.533	26.314	24.291	22.613	45.582	53.31	10.212	36.692	1.399	-4.661	51.206	0.036	0.001	0.0												

2211	10/9/2002	8:17:03 AM	26.905	22.454	26.217	23.572	21.746	45.497	53.887	10.362	36.049	3.327	-1.453	51.637	0.034	0.001	0.2346	78	39.113	52.4	12.7	40.8	2.811	0.005	0.005	0.000	0.120	0.10
2212	10/9/2002	8:18:03 AM	26.893	22.431	26.136	23.57	21.688	45.321	53.712	10.294	35.922	3.238	-1.453	51.794	0.034	0.001	0.2347	78	39.1297	52.2	12.7	40.6	2.801	0.005	0.005	0.000	0.121	0.10
2213	10/9/2002	8:19:03 AM	26.907	22.425	26.178	23.519	21.692	45.167	53.579	10.297	35.686	3.241	-1.444	51.496	0.034	0.001	0.2348	78	39.1463	52.1	12.6	40.4	2.787	0.005	0.005	0.000	0.121	0.10
2214	10/9/2002	8:20:03 AM	25.9	22.424	26.227	23.512	21.7	45.151	53.561	10.273	35.703	3.238	-1.411	51.981	0.034	0.001	0.2349	78	39.163	52.1	12.5	40.4	2.788	0.005	0.005	0.000	0.121	0.10
2215	10/9/2002	8:21:03 AM	26.915	22.418	26.216	23.492	21.655	45.36	53.656	10.334	35.779	3.241	-1.444	50.688	0.034	0.001	0.2350	78	39.1797	52.4	12.6	40.6	2.797	0.005	0.005	0.000	0.121	0.10
2216	10/9/2002	8:22:03 AM	26.919	22.417	26.156	23.511	21.624	45.116	53.542	10.289	35.627	3.241	-1.438	49.795	0.034	0.001	0.2351	78	39.1963	52.1	12.2	40.4	2.785	0.005	0.005	0.000	0.121	0.10
2217	10/9/2002	8:23:03 AM	26.924	22.397	26.281	23.421	21.589	45.447	53.749	10.372	35.967	3.241	-1.438	50.804	0.034	0.001	0.2352	78	39.213	52.3	12.5	40.7	2.806	0.005	0.005	0.000	0.120	0.10
2218	10/9/2002	8:24:03 AM	26.914	22.372	26.246	23.365	21.563	45.461	53.865	10.372	35.832	3.238	-1.427	51.253	0.034	0.001	0.2353	78	39.2297	52.4	12.6	40.6	2.802	0.005	0.005	0.000	0.120	0.10
2219	10/9/2002	8:25:03 AM	26.924	22.372	26.226	23.381	21.546	45.553	53.927	10.367	35.789	3.247	-1.411	51.468	0.034	0.001	0.2354	78	39.2465	51.8	12.6	40.6	2.802	0.005	0.005	0.000	0.120	0.10
2220	10/9/2002	8:26:03 AM	26.946	22.374	26.203	23.343	21.541	45.449	53.904	10.407	35.819	3.238	-1.411	51.595	0.034	0.001	0.2355	78	39.2622	52.4	12.6	40.6	2.802	0.005	0.005	0.000	0.121	0.10
2221	10/9/2002	8:27:03 AM	26.94	22.383	26.357	23.341	21.529	45.045	53.521	10.263	35.512	3.284	-1.406	51.618	0.034	0.001	0.2356	78	39.2788	52.0	12.6	40.3	2.777	0.005	0.005	0.000	0.125	0.11
2222	10/9/2002	8:28:03 AM	26.933	22.381	26.32	23.364	21.527	45.403	53.956	10.427	35.689	3.236	-1.412	50.971	0.034	0.001	0.2357	78	39.2955	52.5	12.6	40.6	2.796	0.005	0.005	0.000	0.120	0.10
2223	10/9/2002	8:29:03 AM	26.934	22.389	26.261	23.391	21.513	45.265	53.732	10.339	35.762	3.244	-1.413	51.798	0.034	0.001	0.2358	78	39.3122	52.3	12.7	40.5	2.793	0.005	0.005	0.000	0.121	0.10
2224	10/9/2002	8:30:03 AM	26.936	22.316	26.322	23.361	21.519	44.931	53.461	10.279	35.406	3.284	-1.401	51.587	0.034	0.001	0.2359	78	39.3288	52.0	12.6	40.4	2.789	0.005	0.005	0.000	0.122	0.10
2225	10/9/2002	8:31:03 AM	26.94	22.303	26.337	23.437	21.538	45.422	53.902	10.317	35.673	3.247	-1.401	51.736	0.034	0.002	0.2360	78	39.3456	52.4	12.7	40.6	2.803	0.005	0.005	0.000	0.120	0.10
2226	10/9/2002	8:32:03 AM	26.949	22.292	26.286	23.521	21.548	45.099	53.501	10.307	35.682	3.299	-1.408	51.314	0.034	0.001	0.2361	78	39.3622	52.1	12.6	40.3	2.781	0.005	0.005	0.000	0.121	0.10
2227	10/9/2002	8:33:03 AM	26.959	22.281	26.21	23.506	21.552	45.422	54.028	10.31	35.995	3.236	-1.401	51.595	0.035	0.001	0.2362	78	39.3789	52.6	12.6	40.7	2.803	0.005	0.005	0.000	0.124	0.11
2228	10/9/2002	8:34:03 AM	26.943	22.265	26.316	23.495	21.552	44.824	53.264	10.273	35.381	3.459	-1.401	51.654	0.033	0.001	0.2363	78	39.3955	51.8	12.6	40.6	2.785	0.005	0.005	0.000	0.119	0.10
2229	10/9/2002	8:35:03 AM	26.942	22.265	26.329	23.565	21.622	44.942	53.681	10.396	35.226	3.535	-1.362	51.526	0.033	0.001	0.2364	78	39.4122	52.2	12.6	40.1	2.764	0.005	0.005	0.000	0.118	0.10
2230	10/9/2002	8:36:03 AM	26.962	22.29	26.289	23.695	21.642	45.101	53.772	10.306	35.584	3.564	-1.399	51.168	0.034	0.001	0.2365	78	39.4288	52.3	12.5	40.3	2.781	0.005	0.005	0.000	0.121	0.10
2231	10/9/2002	8:37:03 AM	26.957	22.274	26.203	23.785	21.652	45.174	53.982	10.337	35.686	3.564	-1.397	51.798	0.035	0.001	0.2366	78	39.4455	52.4	12.7	40.4	2.788	0.005	0.005	0.000	0.125	0.11
2232	10/9/2002	8:38:03 AM	26.952	22.29	26.304	23.815	21.726	45.35	53.966	10.402	35.801	3.569	-1.397	51.653	0.035	0.001	0.2367	78	39.4622	52.5	12.7	40.5	2.798	0.005	0.005	0.000	0.124	0.11
2233	10/9/2002	8:39:03 AM	26.953	22.295	26.195	23.826	21.743	45.314	53.939	10.417	35.74	3.564	-1.397	51.991	0.035	0.001	0.2368	78	39.4788	52.5	12.7	40.5	2.794	0.005	0.005	0.000	0.125	0.11
2234	10/9/2002	8:40:03 AM	26.954	22.312	26.166	23.872	21.768	45.345	54.008	10.519	35.651	3.569	-1.392	51.863	0.034	0.001	0.2369	78	39.4955	52.6	12.7	40.4	2.789	0.005	0.005	0.000	0.121	0.10
2235	10/9/2002	8:41:03 AM	26.979	22.302	26.061	23.938	21.8	45.65	54.407	10.557	35.979	3.564	-1.394	52.52	0.034	0.001	0.2370	78	39.5122	52.9	12.9	40.8	2.814	0.005	0.005	0.000	0.121	0.10
2236	10/9/2002	8:42:03 AM	26.979	22.302	26.061	23.938	21.8	45.65	54.407	10.557	35.979	3.564	-1.394	52.52	0.034	0.001	0.2371	78	39.5289	52.9	12.9	40.8	2.814	0.005	0.005	0.000	0.121	0.10
2237	10/9/2002	8:43:03 AM	26.965	22.318	26.177	23.949	21.861	45.04	53.672	10.431	35.412	3.564	-1.392	51.83	0.034	0.001	0.2372	78	39.5455	52.2	12.7	40.1	2.786	0.005	0.005	0.000	0.122	0.10
2238	10/9/2002	8:44:03 AM	26.966	22.318	26.137	23.999	21.902	45.215	53.948	10.479	35.494	3.566	-1.395	51.994	0.034	0.001	0.2373	78	39.5622	52.5	12.7	40.4	2.782	0.005	0.005	0.000	0.122	0.10
2239	10/9/2002	8:45:03 AM	26.961	22.324	26.073	24.06	21.933	45.352	54.022	10.506	35.633	3.566	-1.395	51.538	0.034	0.001	0.2374	78	39.5788	52.5	12.6	40.5	2.792	0.005	0.005	0.000	0.121	0.10
2240	10/9/2002	8:46:03 AM	26.978	22.351	26.1	24.067	21.97	45.144	53.984	10.525	35.31	3.566	-1.392	51.759	0.034	0.001	0.2375	78	39.5955	52.4	12.7	40.2	2.774	0.005	0.005	0.000	0.122	0.10
2241	10/9/2002	8:47:03 AM	26.942	22.342	26.154	24.013	21.92	45.242	53.94	10.514	35.748	3.566	-1.391	51.616	0.034	0.001	0.2376	78	39.6122	52.4	12.7	40.5	2.785	0.005	0.005	0.000	0.121	0.10
2242	10/9/2002	8:48:03 AM	26.94	22.342	26.151	24.074	21.937	45.383	53.972	10.499	35.622	3.483	-1.391	52.338	0.035	0.001	0.2377	78	39.6288	52.5	12.8	40.5	2.794	0.005	0.005	0.000	0.125	0.11
2243	10/9/2002	8:49:03 AM	26.961	22.374	26.117	24.14	22.053	45.091	54.003	10.462	35.433	3.568	-1.345	51.326	0.034	0.001	0.2378	78	39.6455	52.5	12.6	40.3	2.778	0.004	0.003	0.000	0.126	0.11
2244	10/9/2002	8:50:03 AM	26.942	22.365	26.034	24.161	22.074	44.496	53.699	10.38	34.666	3.302	-1.312	51.614	0.033	0.001	0.2379	78	39.6622	52.2	12.6	39.7	2.736	0.005	0.005	0.000	0.120	0.10
2245	10/9/2002	8:51:03 AM	26.944	22.365	26.034	24.161	22.074	44.496	53.699	10.38	34.666	3.302	-1.312	51.614	0.033	0.001	0.2380	78	39.6788	52.2	12.6	39.7	2.736	0.005	0.005	0.000	0.120	0.10
2246	10/9/2002	8:52:03 AM	26.942	22.365	26.034	24.161	22.074	44.496	53.699	10.38	34.666	3.302	-1.312	51.614	0.033	0.001	0.2381	78	39.6955	52.2	12.7	39.8	2.746	0.005	0.005	0.000	0.123	0.10
2247	10/9/2002	8:53:03 AM	26.941	22.394	26.108	24.141	22.084	44.631	53.937	10.387	3																	

2341	10/9/2002	11:02.42 AM	26.57	22.654	26.781	24.455	22.123	47.972	54.421	10.495	38.198	1.13	-6.345	51.427	0.036	0.001	0	2512.43	41.8738	52.9	12.6	43.1	2.971	0.005	0.005	0.000	0.119	0.10
2342	10/9/2002	11:03.42 AM	26.567	22.541	26.699	24.437	22.13	47.949	54.349	10.495	38.198	1.13	-6.342	51.729	0.036	0.001	0	2513.43	41.8905	52.9	12.7	43.1	2.970	0.005	0.005	0.000	0.119	0.10
2343	10/9/2002	11:04.42 AM	26.575	22.544	26.837	24.43	22.154	47.806	54.08	10.452	38.296	1.13	-6.345	51.131	0.037	0.001	0	2514.43	41.9072	52.6	12.5	43.0	2.967	0.005	0.005	0.000	0.122	0.10
2344	10/9/2002	11:05.42 AM	26.573	22.542	26.949	24.438	22.165	47.868	54.25	10.479	38.217	1.13	-6.338	50.995	0.037	0.001	0	2515.43	41.9238	52.8	12.5	43.0	2.968	0.005	0.005	0.000	0.122	0.10
2345	10/9/2002	11:06.42 AM	26.591	22.55	26.823	24.497	22.19	47.763	53.991	10.423	38.204	1.136	-6.342	51.161	0.036	0.001	0	2516.43	41.9405	52.5	12.5	43.0	2.964	0.005	0.005	0.000	0.119	0.10
2346	10/9/2002	11:07.42 AM	26.599	22.553	26.745	24.494	22.193	47.916	54.283	10.435	38.299	1.13	-6.345	50.097	0.036	0.001	0	2517.43	41.9572	52.8	12.3	43.1	2.972	0.005	0.005	0.000	0.119	0.10
2347	10/9/2002	11:08.42 AM	26.602	22.561	26.804	24.498	22.201	47.936	54.347	10.449	38.362	1.133	-6.345	52.058	0.036	0.001	0	2518.43	41.9738	52.9	12.8	43.1	2.975	0.005	0.005	0.000	0.118	0.10
2348	10/9/2002	11:09.42 AM	26.615	22.554	26.881	24.455	22.215	47.719	53.979	10.428	38.165	1.133	-6.345	51.236	0.036	0.001	0	2519.43	41.9805	52.5	12.5	43.0	2.961	0.005	0.005	0.000	0.119	0.10
2349	10/9/2002	11:10.42 AM	26.603	22.557	26.865	24.609	22.197	47.837	54.419	10.443	38.405	1.132	-6.313	51.24	0.037	0.001	0	2520.43	41.9972	52.7	12.6	43.2	2.976	0.005	0.005	0.000	0.121	0.10
2350	10/9/2002	11:11.42 AM	26.622	22.561	26.798	24.602	22.195	47.734	54.049	10.397	38.172	1.133	-6.339	51.415	0.036	0.001	0	2521.43	42.0238	52.6	12.6	43.0	2.961	0.005	0.005	0.000	0.119	0.10
2351	10/9/2002	11:12.42 AM	26.61	22.549	26.806	24.535	22.203	47.802	54.196	10.477	38.1	1.13	-6.33	51.291	0.037	0.001	0	2522.43	42.0405	52.7	12.6	43.0	2.961	0.005	0.005	0.000	0.122	0.10
2352	10/9/2002	11:13.42 AM	26.644	22.573	26.94	24.559	22.192	47.881	54.059	10.396	38.43	1.112	-6.292	51.568	0.039	0.001	0	2523.43	42.0572	52.6	12.6	43.2	2.975	0.005	0.005	0.000	0.128	0.11
2353	10/9/2002	11:14.42 AM	26.639	22.562	26.899	24.548	22.2	47.763	54.183	10.423	38.268	1.295	-6.116	51.333	0.037	0.001	0	2524.43	42.0738	52.7	12.6	43.0	2.966	0.004	0.004	0.000	0.089	0.08
2354	10/9/2002	11:15.42 AM	26.646	22.561	26.843	24.522	22.175	47.303	53.968	10.391	37.73	1.026	-6.748	50.873	0.034	0.001	0	2525.43	42.0905	52.5	12.5	42.5	2.931	0.005	0.005	0.000	0.113	0.10
2355	10/9/2002	11:16.42 AM	26.649	22.563	26.766	24.63	22.268	47.628	54.276	10.263	38.153	1.056	-6.719	50.884	0.036	0.001	0	2526.43	42.1072	52.8	12.5	42.9	2.957	0.005	0.005	0.000	0.119	0.10
2356	10/9/2002	11:17.42 AM	26.659	22.569	26.915	24.619	22.268	47.412	54.098	10.456	37.815	1.092	-6.673	51.117	0.036	0.001	0	2527.43	42.1238	52.6	12.5	42.6	2.938	0.005	0.005	0.000	0.116	0.10
2357	10/9/2002	11:18.42 AM	26.640	22.557	26.919	24.648	22.276	47.855	54.066	10.453	37.867	1.092	-6.673	51.186	0.037	0.001	0	2528.43	42.1405	53.0	12.5	42.6	2.948	0.005	0.005	0.000	0.122	0.10
2358	10/9/2002	11:19.42 AM	26.672	22.581	26.883	24.718	22.361	47.638	54.089	10.447	38.088	1.092	-6.708	51.215	0.036	0.001	0	2529.43	42.1572	52.9	12.5	42.6	2.936	0.005	0.005	0.000	0.119	0.10
2359	10/9/2002	11:20.42 AM	26.676	22.581	26.848	24.853	22.376	47.7	54.581	10.542	37.887	1.092	-6.708	51.083	0.036	0.001	0	2530.43	42.1738	53.1	12.5	42.8	2.950	0.005	0.005	0.000	0.119	0.10
2360	10/9/2002	11:21.42 AM	26.686	22.58	26.777	24.832	22.38	47.566	54.38	10.458	37.967	1.018	-6.71	51.09	0.036	0.001	0	2531.43	42.1905	52.9	12.5	42.8	2.948	0.005	0.005	0.000	0.119	0.10
2361	10/9/2002	11:22.42 AM	26.696	22.586	26.868	24.812	22.386	47.377	54.19	10.466	37.703	1.015	-6.702	51.033	0.036	0.001	0	2532.43	42.2072	52.7	12.5	42.5	2.933	0.005	0.005	0.000	0.120	0.10
2362	10/9/2002	11:23.42 AM	26.686	22.6	26.932	24.732	22.37	47.763	54.746	10.580	38.035	1.055	-6.684	50.958	0.036	0.001	0	2533.43	42.2238	53.3	12.4	42.9	2.958	0.005	0.005	0.000	0.119	0.10
2363	10/9/2002	11:24.42 AM	26.691	22.61	26.907	24.762	22.411	47.731	54.593	10.472	38.106	1.015	-6.702	51.165	0.036	0.001	0	2534.43	42.2405	53.1	12.5	42.9	2.959	0.005	0.005	0.000	0.119	0.10
2364	10/9/2002	11:25.42 AM	26.69	22.605	26.841	24.806	22.415	47.126	53.948	10.341	37.75	1.088	-6.687	50.806	0.036	0.001	0	2535.43	42.2572	52.5	12.5	42.5	2.929	0.005	0.005	0.000	0.120	0.10
2365	10/9/2002	11:26.42 AM	26.706	22.625	26.807	24.817	22.421	47.56	54.419	10.449	37.883	1.047	-6.679	50.783	0.036	0.001	0	2536.43	42.2738	52.9	12.4	42.7	2.945	0.005	0.005	0.000	0.116	0.10
2366	10/9/2002	11:27.42 AM	26.7	22.619	26.819	24.815	22.425	47.56	54.419	10.449	37.883	1.047	-6.679	50.783	0.036	0.001	0	2537.43	42.2905	52.7	12.4	42.7	2.944	0.005	0.005	0.000	0.116	0.10
2367	10/9/2002	11:28.42 AM	26.7	22.619	26.819	24.815	22.425	47.56	54.419	10.449	37.883	1.047	-6.679	50.783	0.036	0.001	0	2538.43	42.3072	52.8	12.5	42.4	2.926	0.005	0.005	0.000	0.120	0.10
2368	10/9/2002	11:29.42 AM	26.705	22.634	26.906	24.766	22.43	47.417	54.171	10.446	37.984	1.019	-6.698	50.97	0.036	0.001	0	2539.43	42.3238	52.7	12.5	42.7	2.941	0.005	0.005	0.000	0.119	0.10
2369	10/9/2002	11:30.42 AM	26.715	22.639	26.841	24.811	22.443	47.297	54.252	10.465	37.819	1.019	-6.684	50.9	0.036	0.001	0	2540.43	42.3405	52.8	12.4	42.5	2.927	0.005	0.005	0.000	0.120	0.10
2370	10/9/2002	11:31.42 AM	26.722	22.639	26.766	24.786	22.44	47.303	54.065	10.419	37.785	1.022	-6.661	50.871	0.036	0.001	0	2541.43	42.3572	52.6	12.5	42.5	2.933	0.005	0.005	0.000	0.120	0.10
2371	10/9/2002	11:32.42 AM	26.722	22.639	26.766	24.786	22.44	47.106	54.062	10.419	37.431	1.048	-6.661	51.344	0.036	0.001	0	2542.43	42.3738	52.8	12.4	42.4	2.914	0.005	0.005	0.000	0.121	0.10
2372	10/9/2002	11:33.42 AM	26.691	22.645	26.512	24.777	22.461	47.41	54.336	10.442	37.746	1.015	-6.67	51.413	0.036	0.001	0	2543.43	42.3905	52.9	12.6	42.6	2.936	0.005	0.005	0.000	0.117	0.10
2373	10/9/2002	11:34.42 AM	26.682	22.657	26.354	24.808	22.452	47.176	54.041	10.348	37.58	1.075	-6.667	51.079	0.035	0.001	0	2544.43	42.4072	52.6	12.5	42.4	2.922	0.005	0.005	0.000	0.119	0.10
2374	10/9/2002	11:35.42 AM	26.648	22.658	26.29	24.899	22.443	47.413	54.392	10.599	37.57	1.028	-6.67	51.21	0.035	0.001	0	2545.43	42.4238	52.9	12.8	42.5	2.930	0.005	0.005	0.000	0.118	0.10
2375	10/9/2002	11:36.42 AM	26.599	22.671	26.41	24.915	22.426	47.176	54.062	10.599	37.604	1.075	-6.664	51.242	0.035	0.001	0	2546.43	42.4405	52.7	12.8	42.7	2.942	0.005	0.005	0.000	0.118	0.10
2376	10/9/2002	11:37.42 AM	26.58	22.675	26.442	24.942	22.425	47.653	54.554	10.596	37.989	1.012	-6.658	52.103	0.035	0.001	0	2547.43	42.4572	53.1	12.8	42.8	2.952	0.005	0.005	0.000	0.117	0.10
2377	10/9/2002	11:38.42 AM	26.561	22.666	26.483	24.927	22.411	47.522	54.438	10.575	37.795	1.012	-6.655	52.216	0.035	0.001	0	2548.43	42.4738	53.0	12.8	42.7	2.941	0.005	0.005	0.000	0.117	0.10
2378	10/9/2002	11:39.42 AM	26.532	22.671	26.543	24.913	22.431	47.288	54.13	10.539	37.619	1.012	-6.655	52.126	0.035	0.001	0	2549.43	42.4905	52.7	12.8	42.5	2.927	0.005	0.005	0.000	0.118	0.10
2379	10/9/2002	11:40.42 AM	26.517	22.667	26.599	24.923	22.502	47.811	54.57	10.635	37.758	1.012	-6.653	52.291	0.035	0.001	0	2550.43	42.5072	53.1	12.8	42.7	2.943	0.005	0.005	0.000	0.120	0.10
2380	10/9/2002	11:41.42 AM	26.512	22.672	26.844	24.938	22.452	47.328	54.287	10.639	37.625	1.015	-6.653	51.545	0.036	0.001	0	2551.43	42.5238	52.8	12.8	42.4	2.914	0.005	0.005	0.000	0.121	0.10
2381	10/9/2002	11:42.42 AM	26.517	22.68																								

2471	10/3/2002	1:12:10 PM	27.714	23.343	27.954	26.058	23.279	46.634	54.833	10.662	36.751	2.11	-4.399	52.491	0.036	0.001	0	2641.90	44.0316	53.4	12.9	41.7	2.875	0.005	0.005	0.000	0.119	0.10
2472	10/3/2002	1:13:10 PM	27.735	23.359	27.97	26.099	23.306	46.567	54.885	10.622	36.681	2.075	-4.378	52.413	0.036	0.001	0	2642.90	44.0483	53.4	12.8	41.6	2.870	0.005	0.005	0.000	0.119	0.10
2473	10/3/2002	1:14:10 PM	27.736	23.354	27.965	26.234	23.311	49.438	55.013	10.714	39.562	-0.607	-4.105	51.966	0.028	0.001	0	2643.90	44.0649	53.5	12.7	44.5	3.069	0.004	0.004	0.000	0.086	0.07
2474	10/3/2002	1:15:10 PM	27.737	23.354	27.965	26.234	23.311	47.707	54.911	10.738	37.666	1.046	-3.168	52.107	0.028	0.001	0	2644.90	44.0815	53.4	12.7	41.8	2.864	0.001	0.001	0.000	0.029	0.03
2475	10/3/2002	1:16:10 PM	27.755	23.375	27.986	26.409	23.316	46.772	54.965	10.692	36.97	2.11	-4.104	51.943	0.028	0.001	0	2645.90	44.0983	53.5	12.7	41.9	2.887	0.000	0.000	0.000	0.007	0.01
2476	10/3/2002	1:17:10 PM	27.756	23.381	27.991	26.47	23.302	46.035	54.933	10.769	39.691	2.931	-5.312	52.707	0.028	0.001	0	2646.90	44.1149	53.7	12.9	41.0	2.827	0.001	0.001	0.000	0.027	0.02
2477	10/3/2002	1:18:10 PM	27.756	23.381	27.992	26.466	23.302	47.675	54.940	10.686	37.811	1.098	-3.258	52.363	0.031	0.001	0	2647.90	44.1316	53.5	12.9	42.7	2.947	0.001	0.001	0.000	0.032	0.03
2478	10/3/2002	1:19:10 PM	27.757	23.387	27.998	26.486	23.328	46.744	54.891	10.723	36.796	2.061	-3.386	52.107	0.028	0.001	0	2648.90	44.1483	53.4	12.7	41.8	2.860	0.004	0.004	0.000	0.089	0.08
2479	10/3/2002	1:20:10 PM	27.757	23.387	27.998	26.486	23.328	47.798	54.744	10.737	37.169	0.965	-3.844	52.226	0.111	0.001	0	2649.90	44.1649	53.3	12.9	42.9	2.966	0.016	0.016	0.000	0.352	0.30
2480	10/3/2002	1:21:10 PM	27.783	23.423	28.034	26.562	23.354	48.877	54.998	10.728	39.072	0.663	-5.851	52.071	0.026	0.001	0	2650.90	44.1816	53.5	12.8	44.0	3.032	0.004	0.004	0.000	0.081	0.07
2481	10/3/2002	1:22:10 PM	27.778	23.408	28.009	26.407	23.354	48.268	54.899	10.712	38.35	0.523	-4.717	51.949	0.028	0.001	0	2651.90	44.1983	53.4	12.7	43.3	2.986	0.004	0.004	0.000	0.089	0.08
2482	10/3/2002	1:23:10 PM	27.774	23.419	28.034	26.353	23.35	46.26	54.911	10.713	38.419	0.996	-4.796	52.055	0.061	0.001	0	2652.90	44.2149	53.4	13.0	43.3	2.989	0.009	0.009	0.000	0.193	0.16
2483	10/3/2002	1:24:10 PM	27.784	23.419	28.02	26.279	23.376	49.024	54.969	10.702	39.165	0.179	-6.676	52.346	0.039	0.001	0	2653.90	44.2316	53.5	12.8	44.1	3.040	0.006	0.006	0.000	0.119	0.10
2484	10/3/2002	1:25:10 PM	27.806	23.441	28.037	26.305	23.387	48.926	54.964	10.731	39.04	0.153	-6.524	52.444	0.036	0.001	0	2654.90	44.2483	53.5	12.9	44.0	3.032	0.005	0.005	0.000	0.112	0.10
2485	10/3/2002	1:26:10 PM	27.802	23.447	28.047	26.301	23.378	49.018	55.061	10.728	39.224	-0.096	-6.408	52.008	0.037	0.001	0	2655.90	44.2649	53.6	12.7	44.1	3.042	0.006	0.006	0.000	0.115	0.10
2486	10/3/2002	1:27:10 PM	27.812	23.453	28.053	26.367	23.399	48.844	55.089	10.7	39.841	-0.064	-6.411	52.984	0.038	0.001	0	2656.90	44.2816	53.6	13.0	43.9	3.026	0.006	0.006	0.000	0.119	0.10
2487	10/3/2002	1:28:10 PM	27.820	23.456	28.060	26.472	23.389	48.904	54.87	10.702	38.931	-0.078	-6.405	52.107	0.038	0.001	0	2657.90	44.2983	53.4	12.8	43.9	3.025	0.006	0.006	0.000	0.119	0.10
2488	10/3/2002	1:29:10 PM	27.818	23.454	28.039	26.433	23.415	49.042	55.226	10.672	39.212	-0.049	-6.405	52.283	0.037	0.001	0	2658.90	44.3149	53.8	12.8	44.1	3.042	0.006	0.006	0.000	0.115	0.10
2489	10/3/2002	1:30:10 PM	27.839	23.474	28.09	26.493	23.421	49.063	55.207	10.789	39.1	0.41	-6.417	52.503	0.038	0.001	0	2659.90	44.3316	53.7	12.9	44.1	3.040	0.006	0.006	0.000	0.118	0.10
2490	10/3/2002	1:31:10 PM	27.845	23.491	28.076	26.49	23.432	48.655	54.907	10.717	38.728	-0.029	-6.414	52.021	0.038	0.001	0	2660.90	44.3483	53.4	12.7	43.7	3.012	0.006	0.006	0.000	0.119	0.10
2491	10/3/2002	1:32:10 PM	27.851	23.497	28.092	26.471	23.433	48.916	55.137	10.724	38.929	0.02	-6.414	52.138	0.038	0.001	0	2661.90	44.3649	53.3	12.8	43.9	3.028	0.006	0.006	0.000	0.118	0.10
2492	10/3/2002	1:33:10 PM	27.857	23.503	28.093	26.406	23.439	48.779	55.013	10.718	38.905	0.037	-6.42	52.398	0.038	0.001	0	2662.90	44.3816	53.5	12.8	43.8	3.023	0.006	0.006	0.000	0.119	0.10
2493	10/3/2002	1:34:10 PM	27.863	23.513	28.108	26.317	23.464	49.204	55.425	10.8	39.255	0.022	-6.423	52.132	0.038	0.001	0	2663.90	44.3983	54.0	12.8	44.2	3.049	0.006	0.006	0.000	0.117	0.10
2494	10/3/2002	1:35:10 PM	27.863	23.513	28.109	26.303	23.46	48.624	54.723	10.674	38.86	0.043	-6.414	51.97	0.038	0.001	0	2664.90	44.4149	53.3	12.7	43.7	3.016	0.006	0.006	0.000	0.119	0.10
2495	10/3/2002	1:36:10 PM	27.884	23.53	28.109	26.283	23.436	48.738	55.009	10.686	38.847	0.066	-6.42	52.793	0.038	0.001	0	2665.90	44.4316	53.5	12.9	43.8	3.019	0.006	0.006	0.000	0.119	0.10
2496	10/3/2002	1:37:10 PM	27.933	23.581	28.154	26.333	23.551	49.057	55.348	10.672	39.159	0.066	-6.414	51.969	0.038	0.001	0	2666.90	44.4483	53.8	12.8	44.1	3.076	0.006	0.006	0.000	0.118	0.10
2497	10/3/2002	1:38:10 PM	27.925	23.561	28.146	26.305	23.498	48.419	54.69	10.641	38.548	0.066	-6.408	52.025	0.038	0.001	0	2667.90	44.4649	53.2	12.7	43.5	2.998	0.006	0.006	0.000	0.119	0.10
2498	10/3/2002	1:39:10 PM	27.926	23.562	28.137	26.268	23.543	48.955	55.332	10.7	39.046	0.089	-6.431	51.675	0.037	0.001	0	2668.90	44.4816	53.9	12.7	44.0	3.034	0.006	0.006	0.000	0.115	0.10
2499	10/3/2002	1:40:10 PM	27.932	23.573	28.143	26.327	23.565	48.96	55.369	10.796	39.943	0.066	-6.379	51.626	0.037	0.001	0	2669.90	44.4983	53.9	12.7	44.0	3.030	0.006	0.006	0.000	0.115	0.10
2500	10/3/2002	1:41:10 PM	27.933	23.59	28.154	26.333	23.551	49.057	55.348	10.672	39.159	0.066	-6.414	51.969	0.038	0.001	0	2670.90	44.5149	54.3	12.8	44.3	3.051	0.006	0.006	0.000	0.118	0.10
2501	10/3/2002	1:42:10 PM	27.935	23.596	28.165	26.419	23.562	48.643	55.042	10.679	38.651	0.066	-6.414	52.168	0.038	0.001	0	2671.90	44.5316	53.6	12.8	43.6	3.009	0.006	0.006	0.000	0.119	0.10
2502	10/3/2002	1:43:10 PM	27.936	23.597	28.161	26.43	23.573	48.891	55.203	10.743	39.97	0.069	-6.408	52.428	0.038	0.001	0	2672.90	44.5483	53.7	12.8	43.9	3.029	0.006	0.006	0.000	0.118	0.10
2503	10/3/2002	1:44:10 PM	27.947	23.613	28.198	26.487	23.565	48.871	55.207	10.813	38.896	0.072	-6.411	52.333	0.038	0.001	0	2673.90	44.5649	53.7	12.8	43.9	3.026	0.006	0.006	0.000	0.118	0.10
2504	10/3/2002	1:45:10 PM	27.923	23.594	28.153	26.487	23.565	49.239	55.557	10.887	39.226	0.063	-6.414	52.002	0.038	0.001	0	2674.90	44.5816	54.1	12.7	44.2	3.050	0.006	0.006	0.000	0.117	0.10
2505	10/3/2002	1:46:10 PM	27.949	23.621	28.19	26.534	23.607	49.075	55.364	10.807	39.087	0.066	-6.408	51.754	0.038	0.001	0	2675.90	44.5983	53.8	12.8	44.1	3.056	0.006	0.006	0.000	0.118	0.10
2506	10/3/2002	1:47:10 PM	27.95	23.621	28.198	26.52	23.593	48.871	55.181	10.867	39.005	0.093	-6.411	52.017	0.038	0.001	0	2676.90	44.6149	53.7	12.7	43.9	3.029	0.006	0.006	0.000	0.118	0.10
2507	10/3/2002	1:48:10 PM	27.96	23.626	28.201	26.555	23.593	48.724	54.976	10.893	39.841	0.118	-6.398	52.006	0.038	0.001	0	2677.90	44.6316	53.5	12.7	43.8	3.022	0.006	0.006	0.000	0.121	0.10
2508	10/3/2002	1:49:10 PM	27.971	23.638	28.207	26.501	23.599	49.123	55.425	10.751	39.226	0.066	-6.384	52.002	0.038	0.001	0	2678.90	44.6483	54.0	12.7	44.2	3.046	0.006	0.006	0.000	0.117	0.10
2509	10/3/2002	1:50:10 PM	27.977	23.643	28.207	26.533	23.613	48.719	55.024	10.715	38.929	0.075	-6.387	52.079	0.038	0.001	0	2679.90	44.6649	53.6	12.7	44.1	3.048	0.006	0.006	0.000	0.118	0.10
2510	10/3/2002	1:51:10 PM	27.967	23.654	28.213	26.662	23.62	49.082	55.356	10.743	39.226	0.092	-6.388	52.266	0.038	0.001	0	2680.90	44.6816	53.9	12.8	44.2	3.044	0.006	0.006	0.000	0.117	0.10
2511	10/3/2002																											

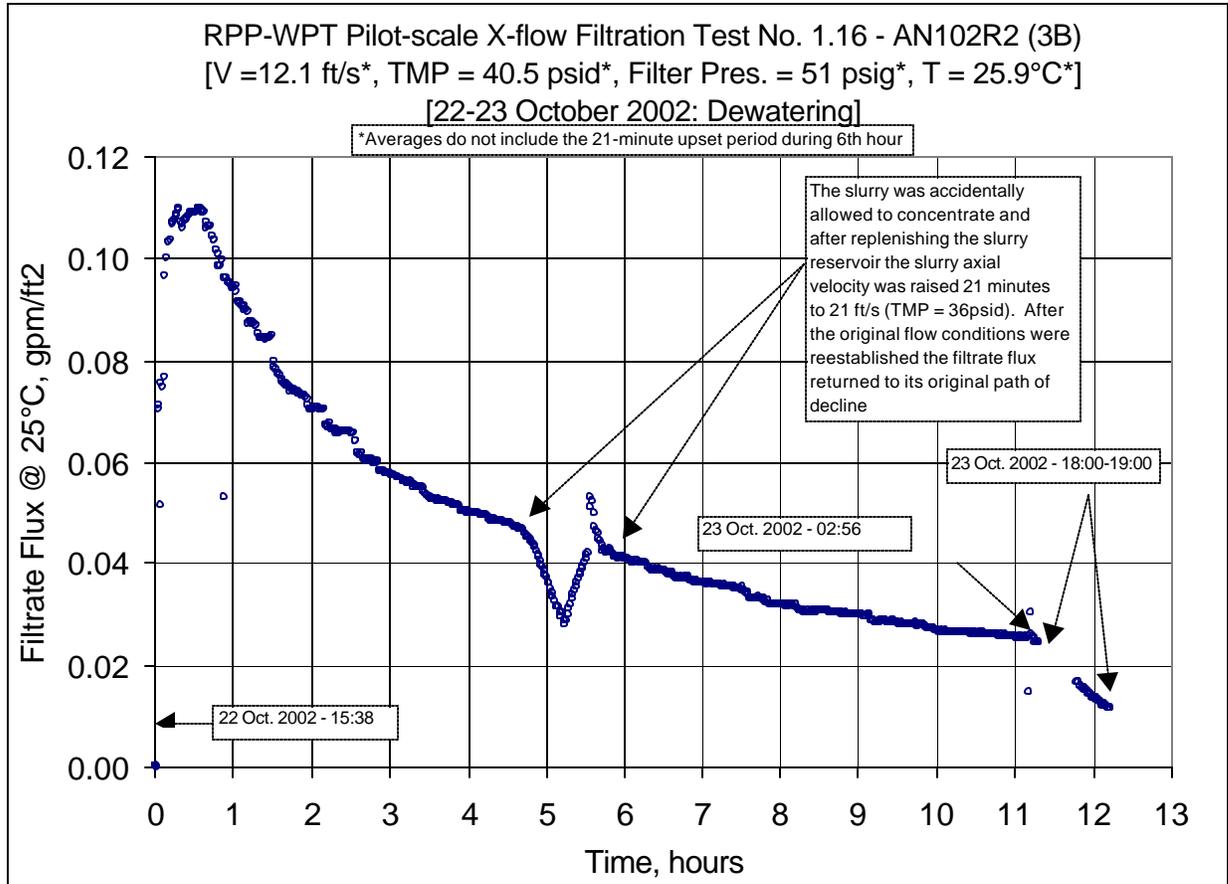


Figure D3: Dewatering of the AN-102R2, batch 3B, insoluble solids concentrations from 1 to 22 wt%

(Data from 6 Files)  
(1.163b-rpp-pxu-102202-1539, -1739, -1939, -2139)  
(1.163b-rpp-pxu-102302-0139, -1835)





261	10/22/2002	7:39:05 PM	26.334	24.41	25.612	25.501	25.369	44.826	49.913	9.884	35.91	-1.012	-2.407	49.502	0.342	0.001	0	240.27	4.00444	48.4	12.1	40.4	2.783	0.051	0.050	0.001	1.242	1.06
262	10/22/2002	7:40:05 PM	26.282	24.423	25.611	25.479	25.292	44.875	49.946	9.868	36	-1.07	-2.401	48.961	0.34	0.001	0	241.27	4.02111	48.5	12.0	40.4	2.788	0.051	0.050	0.001	1.232	1.06
263	10/22/2002	7:41:05 PM	26.239	24.446	25.468	25.546	25.309	44.807	49.901	9.862	35.772	-1.093	-2.433	49.173	0.34	0.001	0	242.27	4.03778	48.4	12.3	40.3	2.778	0.051	0.050	0.001	1.242	1.06
264	10/22/2002	7:42:05 PM	26.181	24.453	25.42	25.534	25.307	44.759	49.769	9.819	35.869	-1.102	-2.447	49.179	0.339	0.001	0	243.27	4.05444	48.3	12.1	40.4	2.786	0.051	0.050	0.001	1.236	1.05
265	10/22/2002	7:43:05 PM	26.14	24.453	25.468	25.546	25.307	44.759	49.769	9.819	35.869	-1.102	-2.447	49.179	0.339	0.001	0	244.27	4.07111	48.3	12.1	40.4	2.786	0.051	0.050	0.001	1.236	1.05
266	10/22/2002	7:44:05 PM	26.092	24.474	25.256	25.564	25.307	44.908	49.886	9.713	36.215	-1.165	-2.47	48.612	0.338	0.001	0	245.27	4.08778	48.4	11.9	40.6	2.797	0.050	0.050	0.001	1.233	1.05
267	10/22/2002	7:45:05 PM	26.044	24.491	25.278	25.582	25.345	44.948	50.12	9.778	36.084	-1.162	-2.479	48.787	0.338	0.001	0	246.27	4.10444	48.6	12.0	40.5	2.793	0.050	0.050	0.001	1.234	1.05
268	10/22/2002	7:46:05 PM	26.007	24.513	25.245	25.639	25.342	45.289	50.619	9.909	36.082	-1.223	-2.517	49.007	0.336	0.001	0	247.27	4.12111	49.1	12.0	40.7	2.805	0.050	0.050	0.001	1.223	1.04
269	10/22/2002	7:47:05 PM	25.97	24.516	25.245	25.639	25.342	45.167	50.619	9.909	36.082	-1.223	-2.517	49.007	0.336	0.001	0	248.27	4.13778	49.6	12.0	40.6	2.801	0.050	0.050	0.001	1.229	1.04
270	10/22/2002	7:48:05 PM	25.939	24.522	25.499	25.639	25.342	44.884	49.619	9.862	36.131	-1.12	-2.491	48.604	0.337	0.001	0	249.27	4.15444	49.5	11.9	40.5	2.793	0.050	0.050	0.001	1.223	1.04
271	10/22/2002	7:49:05 PM	25.912	24.533	25.36	25.614	25.372	45.06	50.172	9.75	36.108	-1.206	-2.505	48.395	0.336	0.001	0	250.27	4.17111	48.7	11.9	40.6	2.798	0.050	0.050	0.001	1.222	1.04
272	10/22/2002	7:50:05 PM	25.923	24.56	25.322	25.605	25.394	45.167	50.441	9.784	36.174	-1.223	-2.505	48.233	0.336	0.001	0	251.27	4.18778	49.0	11.8	40.7	2.804	0.050	0.050	0.001	1.221	1.04
273	10/22/2002	7:51:05 PM	25.895	24.562	25.319	25.577	25.41	45.414	50.424	9.844	36.456	-1.22	-2.523	47.706	0.334	0.001	0	252.27	4.20444	49.0	11.7	40.9	2.822	0.050	0.049	0.001	1.206	1.03
274	10/22/2002	7:52:05 PM	25.753	24.61	25.106	25.555	25.408	45.171	49.835	10.17	36.954	-1.289	-2.718	47.071	0.326	0.001	0	253.27	4.22111	48.7	11.9	40.8	2.828	0.050	0.049	0.001	1.207	1.03
275	10/22/2002	7:53:05 PM	25.895	24.581	25.193	25.572	25.408	45.24	50.118	9.771	36.407	-1.275	-2.554	48.899	0.334	0.001	0	254.27	4.23778	48.6	12.0	40.8	2.815	0.050	0.049	0.001	1.206	1.03
276	10/22/2002	7:54:05 PM	25.826	24.598	25.16	25.638	25.402	45.383	50.271	9.862	36.284	-1.289	-2.578	48.267	0.332	0.001	0	255.27	4.25444	48.1	12.0	40.8	2.815	0.049	0.049	0.001	1.207	1.03
277	10/22/2002	7:55:05 PM	25.782	24.599	25.041	25.599	25.392	44.866	49.553	10.222	36.65	-1.289	-2.578	48.267	0.332	0.001	0	256.27	4.27111	48.1	12.3	40.3	2.776	0.049	0.049	0.001	1.210	1.03
278	10/22/2002	7:56:05 PM	25.753	24.61	25.106	25.555	25.408	45.171	49.835	10.17	36.954	-1.289	-2.718	47.071	0.326	0.001	0	257.27	4.28778	48.5	12.1	40.7	2.803	0.049	0.049	0.001	1.197	1.03
279	10/22/2002	7:57:05 PM	25.728	24.616	25.037	25.633	25.429	45.171	49.715	10.117	36.077	-1.289	-2.718	47.071	0.326	0.001	0	258.27	4.30444	48.2	12.2	40.6	2.801	0.048	0.048	0.001	1.188	1.01
280	10/22/2002	7:58:05 PM	25.699	24.621	25.003	25.622	25.405	45.356	49.977	10.089	36.258	-1.289	-2.705	49.498	0.324	0.001	0	259.27	4.32111	48.5	12.1	40.8	2.813	0.049	0.049	0.001	1.191	1.01
281	10/22/2002	7:59:05 PM	25.668	24.642	25.069	25.625	25.376	45.254	49.944	10.089	36.088	-1.286	-2.698	49.147	0.326	0.001	0	260.27	4.33778	48.5	12.0	40.7	2.804	0.049	0.049	0.001	1.193	1.02
282	10/22/2002	8:00:05 PM	25.641	24.633	25.034	25.653	25.306	45.314	49.899	10.011	36.299	-1.292	-2.708	48.952	0.325	0.001	0	261.27	4.35444	48.4	12.0	40.8	2.813	0.048	0.048	0.001	1.190	1.01
283	10/22/2002	8:01:05 PM	25.581	24.648	24.979	25.573	25.403	45.255	49.918	10.008	36.213	-1.289	-2.708	48.942	0.325	0.001	0	262.27	4.37111	48.4	12.0	40.7	2.807	0.048	0.048	0.001	1.191	1.01
284	10/22/2002	8:02:05 PM	25.502	24.658	24.969	25.598	25.401	45.292	50.000	10.15	36.063	-1.266	-2.734	49.116	0.324	0.001	0	263.27	4.38778	48.5	12.0	40.7	2.804	0.048	0.048	0.001	1.188	1.01
285	10/22/2002	8:03:05 PM	25.466	24.674	24.905	25.624	25.407	45.36	50.172	10.003	36.296	-1.289	-2.717	47.755	0.324	0.001	0	264.27	4.40444	48.7	11.7	40.8	2.815	0.048	0.048	0.001	1.186	1.01
286	10/22/2002	8:04:05 PM	25.577	24.68	24.917	25.56	25.423	45.362	50.116	10.005	36.178	-1.289	-2.737	49.063	0.323	0.001	0	265.27	4.42111	48.6	12.0	40.8	2.811	0.048	0.048	0.001	1.182	1.01
287	10/22/2002	8:05:05 PM	25.547	24.717	24.976	25.59	25.418	45.582	49.933	10.037	36.741	-1.289	-2.738	48.617	0.321	0.001	0	266.27	4.43778	48.6	12.2	40.7	2.804	0.047	0.047	0.001	1.187	1.01
288	10/22/2002	8:06:05 PM	25.490	24.696	24.898	25.571	25.43	45.182	49.988	10.042	36.022	-1.289	-2.751	48.999	0.323	0.001	0	267.27	4.45444	48.4	12.0	40.6	2.799	0.048	0.048	0.001	1.189	1.01
289	10/22/2002	8:07:05 PM	25.461	24.713	24.989	25.568	25.426	45.466	50.344	10.175	36.034	-1.289	-2.763	49.116	0.322	0.001	0	268.27	4.47111	48.9	12.0	40.8	2.810	0.048	0.048	0.001	1.178	1.00
290	10/22/2002	8:08:05 PM	25.536	24.724	24.915	25.604	25.447	45.513	50.208	10.109	36.219	-1.284	-2.763	48.881	0.321	0.001	0	269.27	4.48778	48.8	12.0	40.9	2.818	0.048	0.048	0.001	1.174	1.00
291	10/22/2002	8:09:05 PM	25.537	24.73	24.961	25.555	25.448	45.54	50.211	10.057	36.469	-1.286	-2.768	48.921	0.321	0.001	0	270.27	4.50444	48.7	12.0	41.0	2.827	0.048	0.048	0.001	1.169	0.99
292	10/22/2002	8:10:05 PM	25.584	24.741	25.003	25.581	25.444	45.582	49.975	10.046	36.388	-1.286	-2.768	48.617	0.321	0.001	0	271.27	4.52111	48.9	11.9	41.1	2.834	0.048	0.048	0.001	1.167	0.99
293	10/22/2002	8:11:05 PM	25.535	24.747	24.903	25.562	25.445	45.592	50.205	10.131	36.469	-1.286	-2.768	48.673	0.321	0.001	0	272.27	4.53778	48.7	12.0	41.0	2.830	0.048	0.048	0.001	1.166	0.99
294	10/22/2002	8:12:05 PM	25.52	24.753	24.994	25.568	25.451	45.731	50.354	10.173	36.446	-1.289	-2.768	48.571	0.321	0.001	0	273.27	4.55444	48.9	11.9	41.1	2.833	0.048	0.048	0.001	1.165	0.99
295	10/22/2002	8:13:05 PM	25.541	24.764	24.99	25.634	25.427	45.892	50.528	10.244	36.516	-1.289	-2.801	48.948	0.321	0.001	0	274.27	4.57111	49.1	12.0	41.2	2.841	0.048	0.048	0.001	1.158	0.99
296	10/22/2002	8:14:05 PM	25.547	24.77	24.976	25.59	25.403	45.882	49.933	10.037	36.741	-1.289	-2.808	48.617	0.321	0.001	0	275.27	4.58778	48.6	12.2	40.7	2.804	0.047	0.047	0.001	1.159	0.99
297	10/22/2002	8:15:05 PM	25.534	24.771	25.068	25.576	25.49	45.721	49.893	10.344	36.83	-1.289	-2.808	48.475	0.316													

391	10/22/2002	9:49:03 PM	25.708	25.186	24.606	25.815	25.699	45.913	49.543	10.98	35.721	-1.292	-3.71	46.93	0.269	0.001	0	370.23	6.17056	48.1	11.5	40.8	2.814	0.040	0.041	0.001	0.994	0.86
392	10/22/2002	9:50:03 PM	25.672	25.205	24.695	25.774	25.723	46.248	49.957	11.056	35.991	-1.286	-3.74	49.172	0.268	0.001	0	371.23	6.18722	48.5	12.1	41.1	2.835	0.040	0.040	0.001	0.980	0.83
393	10/22/2002	9:51:03 PM	25.63	25.208	24.698	25.828	25.761	46.106	49.489	10.972	36.137	-1.286	-3.73	49.816	0.266	0.001	0	372.23	6.20389	49.0	12.2	41.1	2.835	0.040	0.040	0.001	0.973	0.83
394	10/22/2002	9:52:03 PM	25.598	25.203	24.602	25.802	25.725	45.814	49.237	10.623	35.971	-1.292	-3.74	49.042	0.266	0.001	0	373.23	6.22056	47.8	12.0	40.9	2.819	0.040	0.040	0.001	0.981	0.89
395	10/22/2002	9:53:03 PM	25.568	25.208	24.618	25.761	25.719	45.725	49.237	10.623	35.971	-1.286	-3.73	48.409	0.267	0.001	0	374.23	6.23722	48.3	11.9	41.2	2.843	0.039	0.039	0.001	0.989	0.82
396	10/22/2002	9:54:03 PM	25.538	25.227	24.642	25.816	25.739	46.41	49.771	10.981	36.434	-1.284	-3.72	48.245	0.267	0.001	0	375.23	6.25389	48.3	11.8	41.4	2.856	0.040	0.040	0.001	0.971	0.83
397	10/22/2002	9:55:03 PM	25.513	25.227	24.657	25.781	25.719	46.377	49.616	10.912	36.448	-1.289	-3.73	48.487	0.266	0.001	0	376.23	6.27056	48.1	11.9	41.4	2.855	0.040	0.040	0.001	0.967	0.82
398	10/22/2002	9:56:03 PM	25.493	25.227	24.722	25.786	25.739	45.843	49.245	11.136	35.623	-1.289	-3.814	48.324	0.262	0.001	0	377.23	6.28722	47.8	12.1	40.7	2.808	0.039	0.039	0.001	0.967	0.82
399	10/22/2002	9:57:03 PM	25.468	25.238	24.618	25.761	25.719	45.618	49.237	10.623	35.971	-1.286	-3.74	47.528	0.266	0.001	0	378.23	6.30389	47.7	12.4	40.8	2.798	0.039	0.039	0.001	0.966	0.83
400	10/22/2002	9:58:03 PM	25.438	25.237	24.583	25.681	25.739	45.936	49.239	11.067	35.86	-1.284	-3.769	48.475	0.263	0.001	0	379.23	6.32056	47.8	12.1	40.9	2.819	0.039	0.039	0.001	0.949	0.81
401	10/22/2002	9:59:03 PM	25.413	25.243	24.579	25.647	25.735	45.629	48.852	10.898	35.664	-1.289	-3.738	48.615	0.265	0.001	0	380.23	6.33722	47.4	12.2	40.6	2.802	0.040	0.039	0.001	0.956	0.81
402	10/22/2002	10:00:03 PM	25.723	25.231	25.677	25.65	25.729	45.693	49.073	10.837	35.687	-1.289	-3.724	49.611	0.265	0.001	0	381.23	6.35389	47.6	12.2	40.8	2.812	0.040	0.039	0.001	0.950	0.81
403	10/22/2002	10:01:03 PM	25.649	25.247	25.733	25.681	25.729	45.913	49.295	10.878	35.988	-1.286	-3.718	50.182	0.265	0.001	0	382.23	6.37056	47.8	12.3	41.0	2.824	0.040	0.039	0.001	0.945	0.80
404	10/22/2002	10:02:03 PM	25.528	25.246	25.492	25.712	25.744	45.603	49.03	11.08	35.697	-1.289	-3.176	48.623	0.264	0.001	0	383.23	6.38722	47.6	12.2	40.6	2.794	0.039	0.039	0.001	0.958	0.82
405	10/22/2002	10:03:03 PM	25.968	25.241	25.417	25.615	25.689	45.689	49.002	10.874	35.664	-1.289	-3.768	50.381	0.263	0.001	0	384.23	6.40389	47.6	12.3	40.7	2.805	0.039	0.039	0.001	0.953	0.81
406	10/22/2002	10:04:03 PM	25.953	25.241	25.297	25.725	25.664	45.726	49.028	10.754	36.034	-1.289	-3.737	49.051	0.261	0.001	0	385.23	6.42056	47.6	12.0	40.9	2.819	0.039	0.039	0.001	0.944	0.80
407	10/22/2002	10:05:03 PM	25.903	25.241	25.162	25.715	25.664	45.977	49.036	10.927	35.965	-1.289	-3.802	49.712	0.262	0.001	0	386.23	6.43722	47.9	12.2	41.0	2.825	0.039	0.039	0.001	0.949	0.81
408	10/22/2002	10:06:03 PM	25.873	25.246	25.147	25.665	25.654	45.867	48.877	10.779	35.871	-1.289	-3.825	49.112	0.261	0.001	0	387.23	6.45389	47.6	12.2	40.8	2.797	0.039	0.039	0.001	0.946	0.81
409	10/22/2002	10:07:03 PM	25.853	25.251	25.001	25.745	25.614	45.983	49.251	10.885	35.94	-1.289	-3.849	49.156	0.259	0.001	0	388.23	6.47056	47.8	12.0	41.0	2.834	0.039	0.039	0.001	0.943	0.80
410	10/22/2002	10:08:03 PM	25.818	25.246	24.971	25.705	25.609	46.039	49.392	10.861	36.063	-1.289	-3.852	49.495	0.259	0.001	0	389.23	6.48722	47.9	12.1	41.0	2.830	0.039	0.039	0.001	0.942	0.80
411	10/22/2002	10:09:03 PM	25.787	25.24	24.931	25.729	25.688	46.05	49.282	10.818	36.149	-1.286	-3.868	50.001	0.258	0.001	0	390.23	6.50389	47.8	12.3	41.1	2.834	0.038	0.038	0.001	0.938	0.80
412	10/22/2002	10:10:03 PM	25.738	25.236	24.801	25.695	25.653	45.996	49.230	10.884	36.125	-1.289	-3.869	49.326	0.258	0.001	0	391.23	6.52056	47.7	12.1	41.1	2.831	0.038	0.038	0.001	0.942	0.80
413	10/22/2002	10:11:03 PM	25.738	25.241	24.843	25.62	25.653	46.137	49.415	10.806	36.254	-1.289	-3.868	49.273	0.259	0.001	0	392.23	6.53722	47.9	12.1	41.2	2.840	0.038	0.038	0.001	0.938	0.80
414	10/22/2002	10:12:03 PM	25.708	25.241	24.741	25.71	25.643	45.724	48.891	11.154	36.461	-1.292	-3.965	49.531	0.254	0.001	0	393.23	6.55389	47.4	12.1	40.6	2.799	0.038	0.038	0.001	0.943	0.80
415	10/22/2002	10:13:03 PM	25.673	25.241	24.731	25.665	25.623	46.211	49.229	11.083	36.127	-1.289	-3.986	49.972	0.254	0.001	0	394.23	6.57056	47.8	12.2	41.2	2.838	0.038	0.038	0.001	0.927	0.79
416	10/22/2002	10:14:03 PM	25.632	25.24	24.755	25.644	25.498	46.93	48.995	11.19	36.633	-1.289	-3.989	49.898	0.253	0.001	0	395.23	6.58722	47.5	12.2	40.8	2.812	0.038	0.038	0.001	0.931	0.79
417	10/22/2002	10:15:03 PM	25.598	25.245	24.64	25.649	25.498	45.819	48.663	11.187	35.811	-1.289	-3.825	49.211	0.253	0.001	0	396.23	6.60389	47.6	12.0	40.8	2.797	0.038	0.038	0.001	0.932	0.79
418	10/22/2002	10:16:03 PM	25.567	25.245	24.7	25.579	25.498	45.938	49.013	11.114	36.738	-1.289	-3.979	49.303	0.253	0.001	0	397.23	6.62056	47.5	12.1	40.8	2.816	0.038	0.038	0.001	0.931	0.79
419	10/22/2002	10:17:03 PM	25.532	25.245	24.675	25.629	25.608	46.029	49.119	11.161	36.67	-1.289	-3.962	49.441	0.252	0.001	0	398.23	6.63722	47.6	12.1	40.8	2.816	0.038	0.038	0.001	0.928	0.79
420	10/22/2002	10:18:03 PM	25.491	25.234	24.614	25.633	25.482	45.793	48.819	11.528	35.269	-1.289	-4.006	50.141	0.248	0.001	0	399.23	6.65389	47.3	12.3	40.5	2.794	0.037	0.037	0.001	0.922	0.78
421	10/22/2002	10:19:03 PM	25.481	25.249	24.719	25.578	25.462	45.927	48.984	11.466	35.369	-1.289	-4.077	50.636	0.247	0.001	0	400.23	6.67056	47.5	12.4	40.6	2.803	0.037	0.037	0.001	0.913	0.78
422	10/22/2002	10:20:03 PM	25.468	25.243	24.639	25.533	25.456	45.64	48.608	11.403	35.483	-1.286	-4.17	50.823	0.247	0.001	0	401.23	6.68722	47.9	12.1	40.9	2.780	0.037	0.037	0.001	0.923	0.78
423	10/22/2002	10:21:03 PM	25.451	25.239	24.643	25.533	25.436	45.925	49.003	11.47	35.363	-1.289	-4.075	50.607	0.247	0.001	0	402.23	6.70389	47.5	12.4	40.6	2.802	0.037	0.037	0.001	0.915	0.78
424	10/22/2002	10:22:03 PM	25.399	25.238	24.703	25.522	25.43	45.847	48.743	11.503	35.269	-1.289	-4.06	50.37	0.247	0.001	0	403.23	6.72056	47.3	12.3	40.6	2.796	0.037	0.037	0.001	0.916	0.78
425	10/22/2002	10:23:03 PM	25.384	25.243	24.613	25.557	25.43	45.952	49.013	11.487	35.388	-1.286	-4.063	50.192	0.247	0.001	0	404.23	6.73722	47.6	12.3	40.7	2.804	0.037	0.037	0.001	0.915	0.78
426	10/22/2002	10:24:03 PM	25.368	25.245	24.64	25.533	25.436	45.873	48.663	11.403	35.449	-1.289	-4.068	49.667	0.247	0.001	0	405.23	6.75389	47.4	12.3	40.8	2.810	0.037	0.037	0.001	0.912	0.78
427	10/22/2002	10:25:03 PM	25.363	25.237	24.672	25.546	25.414	45.712	48.689	11.459	35.099	-1.289	-4.06	50.188	0.246	0.001	0	406.23	6.77056	47.2	12.3	40.4	2.786	0.037	0.037	0.001	0.916	0.78
428	10/22/2002	10:26:03 PM	25.347	25.23	24.625	25.554	25.398	46.054	49.189	11.295	35.652	-1.289	-4.04	50.082	0.246	0.001	0	407.23	6.78722	47.7	12.3	40.9	2.817	0.037	0.037	0.001	0.915	0.78
429	10/22/2002	10:27:03 PM	25.34	25.239	24.729	25.573	25.417	46.168	49.142	11.255	35.688	-1.286	-4.04	50.026	0.246	0.001	0	408.23	6.80389	47.7	12.3	41.0	2.828	0.037	0.037	0.001	0.908	0.77
430	10/22/2002	10:28:03 PM	25.33	25.229	24.638	25.583	25.411	46.267	49.301	11.314	35.817	-1.289	-4.051	49.714	0.247	0.001	0	409.23	6.82056	47.8	12.2	41.0	2.830	0.037	0.037	0.001	0.906	0.77
431	10/22/2002	10:29:03 PM	25.322	25.245	24.64	25.533	25.4																					

521	10/22/2002	11:58:32 PM	25.406	23.824	25.506	22.878	23.614	44.975	47.067	11.338	34.444	-1.284	-4.684	50.169	2.208	0.001	0	499.72	8.32661	45.6	12.3	39.8	2.745	0.031	0.031	0.001	0.768	0.66
522	10/22/2002	11:59:32 PM	25.446	23.805	25.347	22.849	23.695	44.811	46.994	11.505	34.196	-1.284	-4.684	50.169	2.208	0.001	0	500.72	8.34528	45.5	12.3	39.5	2.724	0.031	0.031	0.001	0.777	0.66
523	10/22/2002	12:00:32 AM	25.443	23.793	25.355	22.842	23.649	44.836	47.044	11.347	34.466	-1.284	-4.703	50.416	2.207	0.001	0	501.72	8.362	45.6	12.4	39.6	2.733	0.031	0.031	0.001	0.773	0.66
524	10/22/2002	12:01:32 AM	25.425	23.775	25.197	22.834	23.551	44.971	47.116	11.33	34.667	-1.286	-4.713	50.083	2.206	0.001	0	502.72	8.37667	45.6	12.3	39.8	2.745	0.031	0.031	0.001	0.767	0.65
525	10/22/2002	12:02:32 AM	25.487	23.851	25.261	22.891	23.681	44.869	47.162	11.694	34.273	-1.284	-4.724	50.231	2.205	0.001	0	503.72	8.39533	45.7	12.3	39.6	2.730	0.031	0.031	0.001	0.762	0.65
526	10/22/2002	12:03:32 AM	25.365	23.755	25.057	22.844	23.5	45.231	47.306	11.43	34.761	-1.281	-4.729	50.475	2.205	0.001	0	504.72	8.412	45.9	12.4	40.0	2.758	0.031	0.031	0.001	0.763	0.66
527	10/22/2002	12:04:32 AM	25.301	23.732	24.949	22.781	23.437	44.84	47.007	11.384	34.522	-1.286	-4.744	50.746	2.205	0.001	0	505.72	8.42867	45.5	12.4	39.6	2.730	0.031	0.031	0.001	0.773	0.66
528	10/22/2002	12:05:32 AM	25.28	23.73	24.872	22.759	23.446	45.207	47.185	11.272	34.995	-1.284	-4.738	50.162	2.204	0.001	0	506.72	8.44533	45.7	12.3	40.1	2.765	0.031	0.031	0.001	0.761	0.65
529	10/22/2002	12:06:32 AM	25.25	23.718	24.81	22.771	23.453	45.207	47.185	11.272	34.995	-1.284	-4.738	50.162	2.204	0.001	0	507.72	8.462	45.7	12.3	39.7	2.750	0.031	0.031	0.001	0.762	0.65
530	10/22/2002	12:07:32 AM	25.205	23.695	24.802	22.759	23.436	45.207	47.185	11.272	34.995	-1.284	-4.738	50.162	2.204	0.001	0	508.72	8.47867	45.9	12.2	40.0	2.759	0.031	0.031	0.001	0.764	0.65
531	10/22/2002	12:08:32 AM	25.152	23.667	24.749	22.701	23.413	45.207	47.185	11.272	34.995	-1.284	-4.738	50.162	2.204	0.001	0	509.72	8.49533	45.8	12.3	39.8	2.745	0.031	0.031	0.001	0.769	0.66
532	10/22/2002	12:09:32 AM	25.126	23.666	24.763	22.705	23.411	45.416	47.538	11.351	35.04	-1.286	-4.743	50.032	2.204	0.001	0	510.72	8.512	46.1	12.3	40.2	2.774	0.031	0.031	0.001	0.761	0.65
533	10/22/2002	12:10:32 AM	25.095	23.645	24.657	22.719	23.365	45.236	47.365	11.236	35.025	-1.284	-4.744	50.42	2.204	0.001	0	511.72	8.52867	45.9	12.4	40.2	2.769	0.031	0.031	0.001	0.765	0.65
534	10/22/2002	12:11:32 AM	25.063	23.633	24.617	22.697	23.368	45.302	47.598	11.259	34.607	-1.286	-4.748	50.759	2.204	0.001	0	512.72	8.54533	46.1	12.2	40.1	2.762	0.031	0.031	0.001	0.766	0.65
535	10/22/2002	12:12:32 AM	25.039	23.619	24.676	22.683	23.339	45.476	47.373	11.192	35.206	-1.284	-4.726	49.95	2.204	0.001	0	513.72	8.562	46.2	12.1	40.4	2.786	0.031	0.031	0.001	0.760	0.65
536	10/22/2002	12:13:32 AM	25.01	23.61	24.582	22.691	23.371	45.356	47.459	11.152	35.212	-1.284	-4.726	49.397	2.204	0.001	0	514.72	8.57867	46.0	12.1	40.3	2.777	0.031	0.031	0.001	0.764	0.65
537	10/22/2002	12:14:32 AM	24.971	23.581	24.623	22.607	23.361	45.598	47.953	11.209	35.33	-1.284	-4.74	49.271	2.204	0.001	0	515.72	8.59533	46.4	12.1	40.5	2.790	0.031	0.031	0.001	0.760	0.65
538	10/22/2002	12:15:32 AM	24.941	23.566	24.568	22.607	23.376	45.307	47.621	11.249	35.125	-1.289	-4.758	49.638	2.204	0.001	0	516.72	8.612	46.3	12.1	40.3	2.776	0.031	0.031	0.001	0.746	0.64
539	10/22/2002	12:16:32 AM	24.914	23.554	24.531	23.196	23.415	45.501	47.663	11.274	35.097	-1.286	-4.758	49.254	2.202	0.001	0	517.72	8.62867	46.2	12.1	40.3	2.779	0.031	0.031	0.001	0.757	0.64
540	10/22/2002	12:17:32 AM	24.893	23.553	24.586	23.24	23.429	45.751	47.781	11.283	35.433	-1.289	-4.761	49.141	2.202	0.001	0	518.72	8.64533	46.3	12.0	40.6	2.799	0.031	0.031	0.001	0.751	0.64
541	10/22/2002	12:18:32 AM	24.899	23.569	24.536	23.367	23.45	45.331	47.35	11.263	35.06	-1.284	-4.74	49.193	2.202	0.001	0	519.72	8.662	45.9	12.1	40.2	2.771	0.031	0.031	0.001	0.759	0.65
542	10/22/2002	12:19:32 AM	24.88	23.555	24.573	23.437	23.446	45.372	47.512	11.339	34.943	-1.284	-4.758	49.555	2.202	0.001	0	520.72	8.67867	46.0	12.1	40.2	2.769	0.031	0.031	0.001	0.759	0.65
543	10/22/2002	12:20:32 AM	24.866	23.551	24.594	23.489	23.452	45.605	47.7	11.221	35.394	-1.286	-4.754	49.673	2.202	0.001	0	521.72	8.69533	46.2	12.0	40.5	2.792	0.031	0.031	0.001	0.752	0.64
544	10/22/2002	12:21:32 AM	24.847	23.547	24.515	23.606	23.489	45.652	47.81	11.207	35.461	-1.284	-4.758	49.378	2.202	0.001	0	522.72	8.712	46.3	12.1	40.6	2.796	0.031	0.031	0.001	0.753	0.64
545	10/22/2002	12:22:32 AM	24.838	23.549	24.588	23.602	23.475	45.662	47.792	11.349	35.242	-1.286	-4.767	49.347	2.202	0.001	0	523.72	8.72867	46.3	12.1	40.5	2.789	0.031	0.031	0.001	0.753	0.64
546	10/22/2002	12:23:32 AM	24.83	23.545	24.548	23.729	23.476	45.577	47.594	11.306	35.216	-1.286	-4.778	49.28	2.201	0.001	0	524.72	8.74533	46.1	12.1	40.4	2.785	0.031	0.031	0.001	0.751	0.64
547	10/22/2002	12:24:32 AM	24.822	23.547	24.529	23.776	23.413	45.602	47.612	11.349	35.216	-1.286	-4.778	49.28	2.201	0.001	0	525.72	8.762	46.1	12.1	40.7	2.805	0.031	0.031	0.001	0.742	0.64
548	10/22/2002	12:25:32 AM	24.813	23.538	24.596	23.735	23.536	45.443	47.605	11.404	34.984	-1.284	-4.779	49.38	2.201	0.001	0	526.72	8.77867	46.1	12.1	40.2	2.773	0.031	0.031	0.001	0.750	0.64
549	10/22/2002	12:26:32 AM	24.82	23.55	24.627	23.839	23.577	45.493	47.313	11.449	35.05	-1.286	-4.774	49.531	2.2	0.001	0	527.72	8.79533	45.8	12.1	40.3	2.777	0.031	0.031	0.001	0.750	0.64
550	10/22/2002	12:27:32 AM	24.822	23.552	24.559	23.816	23.699	45.645	47.708	11.317	35.56	-1.286	-4.778	48.738	2.2	0.001	0	528.72	8.812	46.2	11.9	40.7	2.806	0.031	0.031	0.001	0.742	0.63
551	10/22/2002	12:28:32 AM	24.818	23.548	24.611	23.827	23.695	45.638	47.953	11.404	35.492	-1.284	-4.775	49.624	2.2	0.001	0	529.72	8.82867	46.5	12.2	40.7	2.804	0.031	0.031	0.001	0.741	0.63
552	10/22/2002	12:29:32 AM	24.833	23.558	24.646	23.909	23.675	45.55	47.79	11.406	35.451	-1.286	-4.778	49.107	2.2	0.001	0	530.72	8.84533	46.7	12.1	40.5	2.790	0.031	0.031	0.001	0.745	0.64
553	10/22/2002	12:30:32 AM	24.836	23.566	24.624	23.906	23.673	45.7	47.663	11.314	35.24	-1.281	-4.801	49.502	2.2	0.001	0	531.72	8.862	46.2	12.1	40.5	2.790	0.031	0.031	0.001	0.745	0.63
554	10/22/2002	12:31:32 AM	24.827	23.557	24.595	23.937	23.604	45.577	47.611	11.611	34.872	-1.284	-4.822	49.682	2.199	0.001	0	532.72	8.87867	46.1	12.2	40.2	2.773	0.031	0.031	0.001	0.746	0.63
555	10/22/2002	12:32:32 AM	24.828	23.558	24.55	23.897	23.674	45.536	47.629	11.378	35.111	-1.286	-4.822	49.493	2.199	0.001	0	533.72	8.89533	46.2	12.1	40.3	2.780	0.031	0.031	0.001	0.745	0.63
556	10/22/2002	12:33:32 AM	24.832	23.567	24.59	23.911	23.692	45.55	47.79	11.406	35.451	-1.286	-4.778	49.107	2.199	0.001	0	534.72	8.912	46.0	12.1	40.3	2.775	0.031	0.031	0.001	0.745	0.63
557	10/22/2002	12:34:32 AM	24.843	23.563	24.596	23.983	23.58	45.911	47.915	11.435	35.48	-1.286	-4.816	49.128	2.199	0.001	0	535.72	8.92867	46.4	12.0	40.7	2.806	0.031	0.031	0.001	0.738	0.63
558	10/22/2002	12:35:32 AM	24.833	23.563	24.601	23.953	23.58	45.259	48.329	11.41	35.844	-1.286	-4.796	49.937	2.2	0.001	0	536.72	8.94533	46.9	12.2	41.1	2.830	0.031	0.031	0.001	0.735	0.63
559	10/22/2002	12:36:32 AM	24.833	23.563	24.671	23.993	23.695	45.909	47.907	11.436	35.314	-1.286	-4.796	50.915	2.2	0.001	0	537.72	8.962	46.5	12.5	40.8	2.800	0.031	0.031	0.001	0.741	0.63
560	10/22/2002	12:37:32 AM	24.868	23.558	24.581	24.013	23.665	46.103	48.265	11.402	35.572	-1.289	-4.793	49.258	2.199	0.001	0	538.72	8.97867	46.8	12.0	40.6	2.816	0.031	0.031	0.001	0.735	0.63
561	10/22/2002	12:38:32 AM	24.846	23.558	24.646	23.98	23.675	45.946	48.265	11.3																		

651	10/23/2002	2:08:24 AM	25.096	23.862	24.705	24.332	24.055	45.323	47.282	11.662	34.606	-1.286	-4.966	49.527	0.175	0.001	0	629.59	10.4931	45.8	12.1	40.0	2.755	0.026	0.026	0.001	0.658	0.56
652	10/23/2002	2:09:24 AM	25.092	23.868	24.72	24.318	24.045	45.441	47.487	11.769	34.583	-1.286	-4.949	50.079	0.175	0.001	0	630.59	10.5098	46.0	12.3	40.0	2.759	0.026	0.026	0.001	0.657	0.56
653	10/23/2002	2:10:24 AM	25.093	23.868	24.765	24.318	24.04	45.397	47.391	11.744	34.636	-1.286	-4.949	49.705	0.175	0.001	0	631.59	10.5264	45.9	12.2	40.0	2.759	0.026	0.026	0.001	0.656	0.56
654	10/23/2002	2:11:24 AM	25.088	23.863	24.686	24.353	24.051	45.374	47.435	11.699	34.556	-1.289	-4.988	50.119	0.175	0.001	0	632.59	10.5431	46.0	12.3	40.0	2.755	0.026	0.026	0.001	0.659	0.56
655	10/23/2002	2:12:24 AM	25.093	23.863	24.736	24.348	24.051	45.345	47.199	11.798	34.436	-1.289	-5.001	49.653	0.177	0.001	0	633.59	10.5598	45.7	12.2	39.9	2.760	0.026	0.026	0.001	0.656	0.57
656	10/23/2002	2:13:24 AM	25.103	23.853	24.721	24.233	24.046	45.432	47.065	11.741	34.679	-1.289	-5.079	49.37	0.175	0.001	0	634.59	10.5764	45.6	12.1	40.0	2.762	0.026	0.026	0.001	0.657	0.56
657	10/23/2002	2:14:24 AM	25.098	23.879	24.706	24.303	24.011	45.556	47.581	11.777	34.695	-1.286	-5.091	49.332	0.175	0.001	0	635.59	10.5931	46.1	12.1	40.0	2.766	0.026	0.026	0.001	0.656	0.56
658	10/23/2002	2:15:24 AM	25.098	23.868	24.776	24.253	24.011	45.464	47.162	11.707	34.737	-1.284	-5.094	50.19	0.175	0.001	0	636.59	10.6098	45.7	12.3	40.0	2.765	0.026	0.026	0.001	0.655	0.56
659	10/23/2002	2:16:24 AM	25.088	23.863	24.711	24.288	24.011	45.521	47.454	11.821	34.732	-1.288	-5.088	49.544	0.174	0.001	0	637.59	10.6264	46.0	12.1	40.2	2.770	0.026	0.026	0.001	0.651	0.56
660	10/23/2002	2:17:24 AM	25.093	23.873	24.741	24.288	24.036	45.71	47.601	11.798	34.888	-1.289	-5.091	49.544	0.175	0.001	0	638.59	10.6431	46.1	12.1	40.3	2.778	0.026	0.026	0.001	0.652	0.56
661	10/23/2002	2:18:24 AM	25.093	23.873	24.801	24.268	24.016	45.526	47.379	11.819	34.599	-1.286	-5.091	49.227	0.174	0.001	0	639.59	10.6598	45.9	12.1	40.1	2.762	0.026	0.026	0.001	0.651	0.56
662	10/23/2002	2:19:24 AM	25.098	23.863	24.716	24.273	23.996	45.592	47.476	11.839	34.579	-1.286	-5.095	49.607	0.174	0.001	0	640.59	10.6764	46.0	12.2	40.1	2.764	0.026	0.026	0.001	0.652	0.56
663	10/23/2002	2:20:24 AM	25.096	23.868	24.791	24.200	23.976	45.722	47.532	11.749	35.005	-1.284	-5.078	49.069	0.174	0.001	0	641.59	10.6931	46.1	12.0	40.4	2.763	0.026	0.026	0.001	0.647	0.56
664	10/23/2002	2:21:24 AM	25.113	23.883	24.806	24.210	23.986	45.476	47.309	11.669	34.566	-1.286	-5.076	50.232	0.174	0.001	0	642.59	10.7098	45.8	12.3	40.2	2.773	0.026	0.026	0.001	0.649	0.55
665	10/23/2002	2:22:24 AM	25.113	23.883	24.751	24.253	23.976	45.832	47.566	11.766	35.097	-1.286	-5.076	49.294	0.174	0.001	0	643.59	10.7264	46.1	12.1	40.5	2.790	0.026	0.026	0.001	0.646	0.55
666	10/23/2002	2:23:24 AM	25.113	23.879	24.831	24.230	23.986	45.457	47.319	11.631	34.533	-1.286	-5.073	49.768	0.174	0.001	0	644.59	10.7431	45.8	12.2	40.0	2.757	0.026	0.026	0.001	0.652	0.56
667	10/23/2002	2:24:24 AM	25.118	23.873	24.776	24.268	23.996	45.662	47.493	11.962	34.739	-1.289	-5.073	49.288	0.174	0.001	0	645.59	10.7598	46.0	12.1	40.2	2.772	0.026	0.026	0.001	0.649	0.55
668	10/23/2002	2:25:24 AM	25.128	23.879	24.948	24.26	23.982	45.836	47.641	11.902	34.861	-1.289	-5.088	49.233	0.174	0.001	0	646.59	10.7764	46.2	12.0	40.3	2.782	0.026	0.026	0.001	0.640	0.54
669	10/23/2002	2:26:24 AM	25.138	23.879	24.872	24.279	23.971	45.509	47.296	11.815	34.634	-1.286	-5.071	48.55	0.173	0.001	0	647.59	10.7931	45.8	11.9	40.1	2.763	0.026	0.026	0.001	0.646	0.55
670	10/23/2002	2:27:24 AM	25.143	23.879	24.782	24.314	23.961	45.774	47.441	11.815	34.96	-1.286	-5.065	49.25	0.173	0.001	0	648.59	10.8098	46.1	12.1	40.4	2.783	0.026	0.026	0.001	0.643	0.55
671	10/23/2002	2:28:24 AM	25.149	23.89	24.873	24.295	23.967	45.82	47.805	11.879	34.89	-1.284	-5.069	49.696	0.174	0.001	0	649.59	10.8264	46.3	12.2	40.4	2.782	0.026	0.026	0.001	0.645	0.55
672	10/23/2002	2:29:24 AM	25.159	23.88	24.876	24.315	23.987	45.851	47.596	11.895	35.037	-1.289	-5.088	49.718	0.173	0.001	0	650.59	10.8431	46.1	12.2	40.4	2.788	0.026	0.026	0.001	0.640	0.54
673	10/23/2002	2:30:24 AM	25.164	23.888	24.823	24.3	23.987	45.695	47.368	11.796	34.666	-1.289	-5.082	49.238	0.173	0.001	0	651.59	10.8598	46.1	12.1	40.3	2.777	0.026	0.026	0.001	0.644	0.55
674	10/23/2002	2:31:24 AM	25.159	23.87	24.908	24.204	23.982	45.909	47.783	11.874	34.943	-1.289	-5.062	49.519	0.173	0.001	0	652.59	10.8764	46.3	12.1	40.4	2.787	0.026	0.026	0.001	0.640	0.54
675	10/23/2002	2:32:24 AM	25.169	23.87	24.853	24.29	23.992	45.782	47.735	11.92	34.778	-1.289	-5.062	49.473	0.173	0.001	0	653.59	10.8931	46.3	12.1	40.3	2.787	0.026	0.026	0.001	0.643	0.56
676	10/23/2002	2:33:24 AM	25.168	23.869	24.862	24.234	23.976	45.793	47.716	11.837	34.951	-1.292	-5.059	49.827	0.173	0.001	0	654.59	10.9098	46.2	12.0	40.4	2.784	0.026	0.026	0.001	0.641	0.55
677	10/23/2002	2:34:24 AM	25.184	23.879	24.948	24.26	23.982	45.836	47.641	11.902	34.861	-1.289	-5.088	49.149	0.173	0.001	0	655.59	10.9264	46.2	12.0	40.3	2.782	0.026	0.026	0.001	0.640	0.54
678	10/23/2002	2:35:24 AM	25.199	23.88	24.873	24.27	24.007	45.849	47.738	11.877	35.009	-1.286	-5.089	49.074	0.173	0.001	0	656.59	10.9431	46.2	12.0	40.4	2.787	0.026	0.026	0.001	0.640	0.54
679	10/23/2002	2:36:24 AM	25.183	23.868	25.036	24.223	23.991	45.714	47.658	11.815	34.861	-1.286	-5.059	50.066	0.173	0.001	0	657.59	10.9598	46.2	12.3	40.3	2.778	0.026	0.026	0.001	0.640	0.54
680	10/23/2002	2:37:24 AM	25.213	23.873	25.172	24.278	23.996	45.586	47.52	11.802	34.734	-1.289	-5.046	49.739	0.174	0.001	0	658.59	10.9764	46.0	12.2	40.2	2.769	0.026	0.026	0.001	0.643	0.55
681	10/23/2002	2:38:24 AM	25.204	23.869	25.122	24.274	24.017	45.395	47.156	11.696	34.726	-1.289	-5.15	49.562	0.172	0.001	0	659.59	10.9931	45.7	11.9	40.1	2.762	0.026	0.026	0.001	0.638	0.54
682	10/23/2002	2:39:24 AM	25.204	23.869	25.167	24.249	23.997	45.426	47.346	11.729	34.702	-1.289	-5.059	49.447	0.171	0.001	0	660.59	11.0098	45.9	12.1	40.1	2.762	0.025	0.025	0.001	0.633	0.54
683	10/23/2002	2:40:24 AM	25.214	23.879	25.057	24.259	23.992	45.687	47.58	11.663	34.99	-1.289	-5.066	49.777	0.171	0.001	0	661.59	11.0264	46.1	12.2	40.3	2.781	0.025	0.025	0.001	0.631	0.54
684	10/23/2002	2:41:24 AM	25.239	23.879	25.067	24.244	23.961	45.59	47.321	11.616	35.021	-1.284	-5.042	49.799	0.173	0.001	0	662.59	11.0431	45.8	12.0	40.3	2.779	0.026	0.026	0.001	0.639	0.54
685	10/23/2002	2:42:24 AM	25.219	23.87	25.073	24.25	23.962	45.681	47.468	11.642	34.97	-1.289	-5.048	49.568	0.172	0.001	0	663.59	11.0598	46.0	11.9	40.3	2.780	0.026	0.026	0.001	0.635	0.54
686	10/23/2002	2:43:24 AM	25.236	23.886	24.974	24.25	23.968	45.944	47.911	11.749	35.177	-1.286	-5.046	47.681	0.171	0.001	0	664.59	11.0764	46.5	11.7	40.6	2.788	0.026	0.026	0.001	0.629	0.53
687	10/23/2002	2:44:24 AM	25.219	23.895	25.028	24.214	23.967	45.685	47.493	11.691	35.019	-1.289	-5.042	48.923	0.171	0.001	0	665.59	11.0931	46.0	12.0	40.4	2.782	0.025	0.025	0.001	0.631	0.54
688	10/23/2002	2:45:24 AM	25.219	23.88	25.008	24.234	23.967	45.799	47.822	11.721	34.929	-1.289	-5.046	49.017	0.171	0.001	0	666.59	11.1098	46.3	12.0	40.4	2.783	0.025	0.025	0.001	0.631	0.54
689	10/23/2002	2:46:24 AM	25.214	23.884	24.947	24.204	23.941	45.724	47.574	11.661	35.027	-1.289	-5.047	48.757	0.171	0.001	0	667.59	11.1264	46.1	11.9	40.4	2.784	0.025	0.025	0.001	0.632	0.54
690	10/23/2002	2:47:24 AM	25.204	23.879	25.027	24.209	23.941	45.956	47.909	11.684	35.295	-1.286	-5.042	49.393	0.171	0.001	0	668.59	11.1431	46.3	12.0	40.6	2.801	0.025	0.025	0.001	0.627	0.53
691	10/23/2002	2:48:24 AM	25.213	23.878</																								

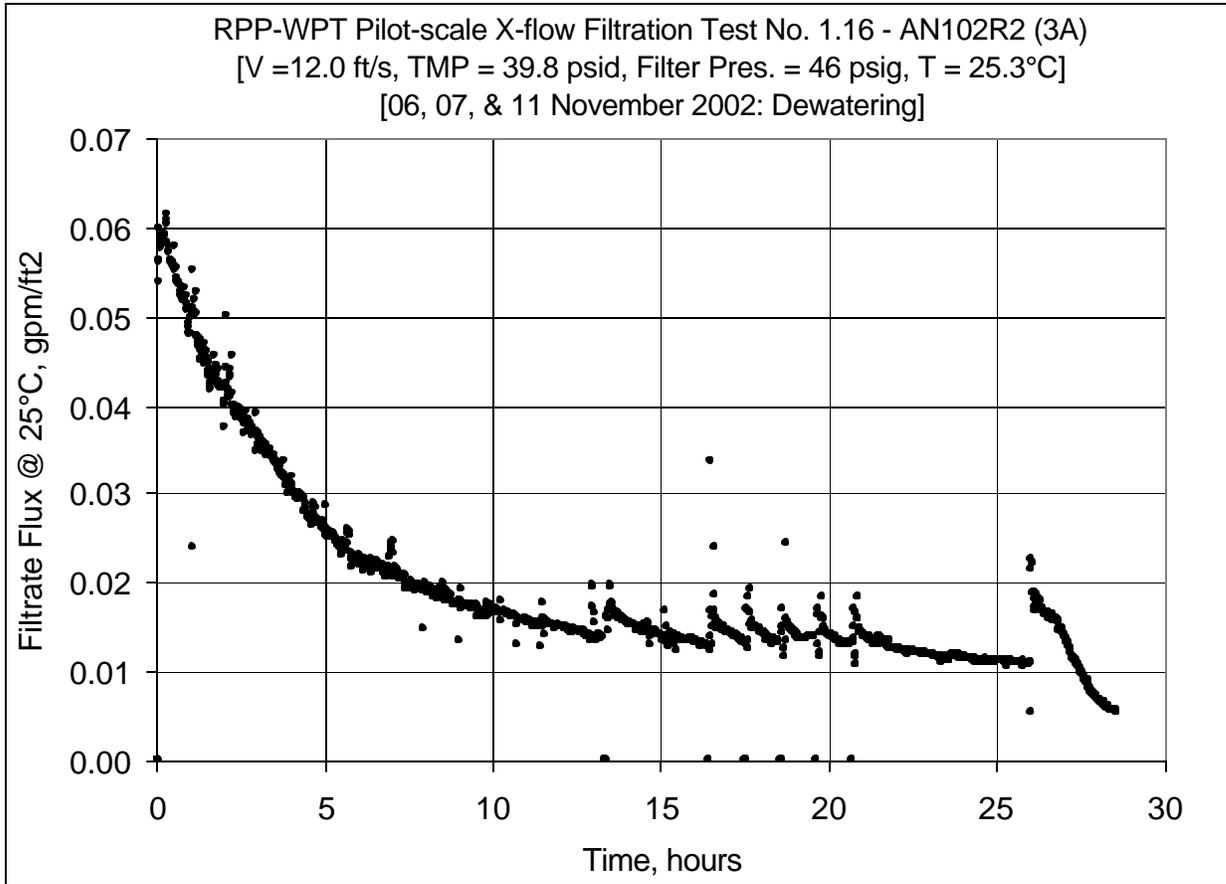


Figure D5: Dewatering of the AN-102R2, batch 3A, insoluble solids concentrations from 1.6 to 25 wt%

(Data from 18 Files)  
(1.16-3a-rpp-pxu-110602-1515, -1715, -1915, -2015, -2115, -2305)  
(1.16-3a-rpp-pxu-110702-0101, -0301, -0432, -0712, -0740, -0843, -947, -1050, -1400, -1600)  
(1.16-3a-rpp-pxu-111102-0855, -1055)



131	11/6/2002	4:56:08 PM	25.296	23.181	24.845	24.5	24.247	44.778	47.686	9.137	36.381	-1.288	-4.064	49.941	0.293	0.001	0	100.40	1.67333	46.2	12.2	40.6	2.798	0.044	0.044	0.001	1.081	0.91
132	11/6/2002	4:57:08 PM	25.266	23.171	24.95	24.6	24.247	44.54	47.374	9.381	35.945	-1.291	-4.125	50.767	0.294	0.001	0	101.40	1.689	45.9	12.4	40.2	2.775	0.044	0.044	0.001	1.091	0.93
133	11/6/2002	4:57:08 PM	25.311	23.177	24.991	24.441	24.238	44.903	47.125	9.056	36.275	-1.291	-4.177	49.989	0.289	0.001	0	102.40	1.70667	45.7	12.3	40.4	2.795	0.043	0.043	0.001	1.063	0.90
134	11/6/2002	4:57:08 PM	25.351	23.187	24.961	24.446	24.202	44.48	47.243	9.207	35.913	-1.288	-4.093	49.761	0.291	0.001	0	103.40	1.72333	45.8	12.2	40.2	2.771	0.043	0.043	0.001	1.081	0.92
135	11/6/2002	4:59:08 PM	25.902	23.02	25.016	24.401	24.191	45.781	50.026	7.475	44.683	-1.291	-3.788	44.846	0.336	0.001	0	104.40	1.74	48.6	11.0	40.5	2.987	0.044	0.044	0.001	1.054	0.86
136	11/6/2002	5:00:08 PM	25.427	23.213	24.952	24.462	24.208	44.917	47.806	8.797	36.916	-1.288	-3.899	48.811	0.299	0.001	0	105.40	1.76667	46.3	12.0	40.9	2.821	0.045	0.045	0.001	1.091	0.93
137	11/6/2002	5:01:08 PM	25.397	23.213	25.012	24.447	24.218	44.653	47.33	9.075	36.402	-1.288	-4.066	48.345	0.292	0.001	0	106.40	1.77333	45.9	11.8	40.5	2.795	0.044	0.044	0.001	1.074	0.91
138	11/6/2002	5:02:08 PM	25.419	23.234	25.069	24.519	24.245	44.984	47.746	8.936	36.883	-1.288	-4.056	48.915	0.292	0.001	0	107.40	1.79	46.9	12.0	40.9	2.823	0.044	0.044	0.001	1.061	0.90
139	11/6/2002	5:03:08 PM	25.434	23.219	25.003	24.496	24.245	45.719	49.842	8.603	37.989	-1.291	-3.928	48.140	0.296	0.001	0	108.40	1.80667	47.4	11.7	41.9	2.866	0.044	0.044	0.001	1.054	0.86
140	11/6/2002	5:04:08 PM	25.449	23.24	25.104	24.479	24.245	43.655	46.726	9.574	34.934	-1.288	-3.934	51.072	0.297	0.001	0	109.40	1.82333	45.5	12.5	39.4	2.716	0.044	0.044	0.001	1.121	0.96
141	11/6/2002	5:05:08 PM	25.449	23.24	25.064	24.544	24.271	44.265	47.103	9.455	36.491	-1.291	-4.18	50.344	0.287	0.001	0	110.40	1.84	45.3	12.3	39.9	2.750	0.043	0.043	0.001	1.071	0.91
142	11/6/2002	5:06:08 PM	25.457	23.252	25.116	24.481	24.273	44.689	47.322	9.187	36.294	-1.291	-4.154	49.796	0.295	0.001	0	111.40	1.86667	45.8	12.2	40.5	2.792	0.042	0.042	0.001	1.046	0.89
143	11/6/2002	5:07:08 PM	25.462	23.252	25.152	24.557	24.299	44.795	47.576	9.191	36.359	-1.288	-4.231	49.695	0.295	0.001	0	112.40	1.88333	46.3	12.2	40.6	2.796	0.042	0.042	0.001	1.042	0.89
144	11/6/2002	5:08:08 PM	25.484	23.284	25.124	24.523	24.3	44.686	47.252	9.272	36.167	-1.291	-4.273	50.038	0.283	0.001	0	113.40	1.89	45.8	12.3	40.4	2.788	0.042	0.042	0.001	1.040	0.88
145	11/6/2002	5:09:08 PM	25.456	23.296	25.23	24.55	24.322	45.097	47.986	9.206	36.723	-1.288	-4.197	50.232	0.285	0.001	0	114.40	1.90667	46.3	12.3	40.9	2.821	0.042	0.042	0.001	1.032	0.88
146	11/6/2002	5:10:08 PM	25.536	23.301	25.18	24.626	24.322	44.934	47.653	9.158	36.386	-1.288	-4.2	49.694	0.286	0.001	0	115.40	1.92333	46.2	12.2	40.7	2.803	0.043	0.043	0.001	1.043	0.89
147	11/6/2002	5:11:08 PM	25.542	23.302	25.207	24.627	24.318	44.561	47.603	9.079	36.167	-1.288	-4.208	48.081	0.286	0.001	0	116.40	1.94	45.6	11.8	40.4	2.783	0.042	0.042	0.001	1.047	0.89
148	11/6/2002	5:12:08 PM	25.553	23.319	25.268	24.643	24.384	44.582	47.181	9.083	36.181	-1.284	-4.232	49.213	0.285	0.001	0	117.40	1.96667	45.7	12.1	40.4	2.786	0.042	0.042	0.001	1.044	0.89
149	11/6/2002	5:13:08 PM	25.575	23.33	25.19	24.604	24.316	44.894	47.545	8.673	36.94	-1.288	-4.203	48.267	0.284	0.001	0	118.40	1.97333	46.1	11.8	40.9	2.821	0.042	0.042	0.001	1.029	0.88
150	11/6/2002	5:14:08 PM	25.58	23.33	25.275	24.509	24.331	43.596	46.087	9.821	34.568	-1.291	-4.401	46.275	0.273	0.001	0	119.40	1.99	44.6	12.9	39.1	2.695	0.041	0.041	0.001	1.033	0.88
151	11/6/2002	5:15:08 PM	25.6	23.34	25.245	24.579	24.301	44.428	47.026	9.476	35.557	-1.291	-4.504	49.977	0.271	0.001	0	120.40	2.00667	45.6	12.2	40.0	2.757	0.040	0.040	0.001	1.003	0.85
152	11/6/2002	5:15:11 PM	25.606	23.366	25.27	24.605	24.312	44.199	46.734	9.36	35.456	-1.291	-4.51	51.032	0.274	0.001	0	120.45	2.005	45.7	12.4	38.8	2.677	0.038	0.038	0.001	0.971	0.83
153	11/6/2002	5:16:08 PM	25.615	23.366	25.285	24.529	24.311	43.231	46.37	9.486	34.437	-1.285	-4.250	50.799	0.255	0.001	0	121.45	2.02417	45.2	12.4	38.8	2.677	0.038	0.038	0.001	1.003	0.85
154	11/6/2002	5:17:11 PM	25.606	23.361	25.341	24.56	24.312	39.279	47.063	9.303	34.014	1.944	-4.041	50.279	0.34	0.001	0	122.45	2.04083	45.6	12.3	38.4	2.603	0.051	0.051	0.001	1.441	1.23
155	11/6/2002	5:18:11 PM	25.606	23.362	25.246	24.531	24.307	42.749	46.132	9.649	33.53	-1.291	-3.63	52.69	0.3	0.001	0	123.45	2.0575	44.8	12.9	38.1	2.630	0.055	0.055	0.001	1.165	0.99
156	11/6/2002	5:19:11 PM	25.601	23.372	25.321	24.516	24.327	44.917	47.519	8.995	36.392	-1.288	-4.234	48.276	0.288	0.001	0	124.45	2.07417	45.4	12.9	39.1	2.817	0.043	0.043	0.001	0.941	0.89
157	11/6/2002	5:20:11 PM	25.624	23.381	25.29	24.519	24.296	44.685	47.303	8.888	36.656	-1.291	-4.388	48.253	0.285	0.001	0	125.45	2.09083	45.8	11.8	40.7	2.804	0.042	0.042	0.001	1.036	0.88
158	11/6/2002	5:21:11 PM	25.621	23.381	25.275	24.53	24.322	45.368	46.333	8.692	37.299	-1.288	-4.371	47.954	0.284	0.001	0	126.45	2.1075	46.9	11.7	41.3	2.849	0.042	0.042	0.001	1.017	0.87
159	11/6/2002	5:22:11 PM	25.611	23.376	25.32	24.509	24.316	44.134	46.881	9.444	35	-1.291	-4.444	48.443	0.282	0.001	0	127.45	2.12417	45.4	11.9	39.6	2.728	0.042	0.042	0.001	1.053	0.90
160	11/6/2002	5:23:11 PM	25.623	23.39	25.239	24.539	24.305	44.708	47.353	8.939	36.437	-1.291	-4.451	48.905	0.277	0.001	0	128.45	2.14083	45.9	12.0	40.6	2.797	0.041	0.041	0.001	1.011	0.86
161	11/6/2002	5:24:11 PM	25.625	23.411	25.326	24.514	24.316	44.388	47.173	9.233	35.741	-1.288	-4.478	48.389	0.277	0.001	0	129.45	2.1575	46.1	12.3	40.1	2.762	0.041	0.041	0.001	1.022	0.87
162	11/6/2002	5:25:11 PM	25.665	23.416	25.24	24.529	24.356	46.477	49.314	7.639	39.626	-1.288	-4.103	44.995	0.292	0.001	0	130.45	2.17417	47.0	11.0	43.1	2.968	0.044	0.044	0.001	1.004	0.86
163	11/6/2002	5:26:11 PM	25.676	23.422	25.185	24.505	24.342	46.527	49.651	7.813	39.315	-1.288	-4.128	44.366	0.293	0.001	0	131.45	2.19083	48.2	10.9	42.9	2.959	0.044	0.044	0.001	1.012	0.86
164	11/6/2002	5:27:11 PM	25.671	23.422	25.225	24.485	24.352	47.388	50.746	7.142	40.91	-1.288	-4.019	42.426	0.298	0.001	0	132.45	2.2075	49.3	10.4	44.2	3.044	0.044	0.044	0.001	1.000	0.85
165	11/6/2002	5:28:11 PM	25.671	23.422	25.266	24.485	24.351	47.031	51.265	6.606	42.602	-1.291	-4.512	39.975	0.297	0.001	0	133.45	2.22417	49.7	9.8	45.9	3.102	0.039	0.039	0.001	0.942	0.80
166	11/6/2002	5:29:11 PM	25.698	23.409	25.168	24.362	24.364	48.772	47.707	8.116	38.484	-1.291	-4.319	48.079	0.279	0.001	0	134.45	2.24083	48.2	11.8	40.7	2.805	0.042	0.042	0.001	1.018	0.97
167	11/6/2002	5:30:11 PM	25.604	23.435	25.194	24.433	24.31	45.081	47.651	8.829	36.967	-1.288	-4.635	48.14	0.27	0.001	0	135.45	2.2575	46.2	12.0	41.0	2.828	0.040				

261	11/6/2002	7:04:11 PM	26.663	23.293	25.477	23.629	23.732	45.303	47.22	9.415	36.359	-1.282	-5.445	49.398	0.211	0.001	0	229.45	3.82417	45.7	12.1	40.8	2.815	0.031	0.001	0.001	0.760	0.65
262	11/6/2002	7:05:11 PM	26.668	23.283	25.352	23.689	23.732	45.704	47.66	9.161	37.106	-1.291	-5.445	49.398	0.215	0.001	0	230.45	3.84083	46.1	11.9	41.4	2.855	0.032	0.002	0.001	0.767	0.65
263	11/6/2002	7:06:11 PM	26.643	23.273	25.367	23.619	23.691	44.896	46.958	9.207	36.076	-1.291	-5.437	50.695	0.216	0.001	0	231.45	3.8575	45.5	12.4	40.5	2.791	0.032	0.002	0.001	0.767	0.67
264	11/6/2002	7:07:11 PM	26.623	23.274	25.283	23.633	23.737	44.027	46.214	9.239	34.613	-1.288	-5.437	51.636	0.203	0.001	0	232.45	3.87417	44.5	12.7	39.3	2.711	0.030	0.001	0.001	0.764	0.65
265	11/6/2002	7:08:11 PM	26.603	23.283	25.232	23.614	23.732	44.478	46.233	9.232	35.661	-1.291	-5.437	49.398	0.215	0.001	0	233.45	3.89083	44.9	12.2	40.1	2.763	0.032	0.001	0.001	0.767	0.65
266	11/6/2002	7:09:11 PM	26.577	23.263	25.232	23.614	23.722	44.776	46.589	9.06	36.261	-1.291	-5.535	45.991	0.21	0.001	0	234.45	3.9075	45.1	11.2	40.5	2.794	0.031	0.001	0.001	0.768	0.66
267	11/6/2002	7:10:11 PM	26.538	23.264	25.097	23.645	23.692	44.261	45.992	9.043	35.798	-1.288	-5.5	48.876	0.209	0.001	0	235.45	3.92417	44.5	12.0	40.5	2.760	0.031	0.001	0.001	0.776	0.66
268	11/6/2002	7:11:11 PM	26.512	23.268	25.142	23.609	23.701	44.913	46.858	9.044	36.402	-1.288	-5.5	47.609	0.204	0.001	0	236.45	3.94083	45.4	11.7	40.7	2.803	0.030	0.001	0.001	0.745	0.63
269	11/6/2002	7:12:11 PM	26.472	23.258	25.042	23.634	23.732	44.834	46.594	9.017	36.322	-1.291	-5.437	49.398	0.215	0.001	0	237.45	3.9575	45.1	11.9	40.6	2.786	0.031	0.001	0.001	0.767	0.65
270	11/6/2002	7:13:11 PM	26.458	23.259	25.032	23.601	23.717	44.356	46.412	9.014	35.958	-1.288	-5.049	48.731	0.211	0.001	0	238.45	3.97417	44.5	11.9	40.2	2.769	0.031	0.001	0.001	0.763	0.57
271	11/6/2002	7:14:11 PM	26.427	23.258	25.042	23.639	23.701	44.453	46.3	9.086	36.982	-1.288	-5.266	48.204	0.216	0.001	0	239.45	3.99083	44.8	11.8	40.2	2.773	0.032	0.002	0.001	0.800	0.68
272	11/6/2002	7:15:11 PM	26.392	23.248	24.932	23.614	23.691	44.575	46.441	9.299	35.796	-1.288	-5.515	48.246	0.205	0.001	0	240.45	4.0075	45.0	11.8	40.2	2.771	0.031	0.001	0.001	0.762	0.65
273	11/6/2002	7:15:14 PM	26.392	23.248	24.932	23.614	23.691	44.575	46.441	9.299	35.796	-1.288	-5.515	48.246	0.205	0.001	0	240.50	4.0075	45.0	11.8	40.2	2.771	0.031	0.001	0.001	0.762	0.65
274	11/6/2002	7:16:14 PM	26.362	23.247	24.976	23.663	23.681	44.779	46.565	9.007	36.298	-1.288	-5.623	47.944	0.207	0.001	0	241.50	4.025	45.1	11.7	40.5	2.795	0.031	0.001	0.001	0.762	0.65
275	11/6/2002	7:17:14 PM	26.336	23.236	24.889	23.667	23.674	45.176	47.118	8.929	36.796	-1.288	-5.638	47.756	0.208	0.001	0	242.50	4.04167	45.5	11.7	40.1	2.824	0.031	0.001	0.001	0.759	0.66
276	11/6/2002	7:18:14 PM	26.319	23.235	24.894	23.396	23.699	44.209	45.990	9.41	35.342	-1.288	-5.628	48.731	0.202	0.001	0	243.50	4.05833	44.5	11.9	39.8	2.744	0.030	0.001	0.001	0.759	0.65
277	11/6/2002	7:19:14 PM	26.288	23.229	24.927	23.389	23.712	44.526	46.453	9.484	35.425	-1.288	-5.729	49.297	0.202	0.001	0	244.50	4.075	45.0	11.2	40.0	2.756	0.030	0.001	0.001	0.755	0.64
278	11/6/2002	7:20:14 PM	26.257	23.233	24.927	23.416	23.707	44.871	46.333	9.391	36.814	-1.288	-5.688	48.647	0.203	0.001	0	245.50	4.09167	44.9	11.9	40.2	2.786	0.030	0.001	0.001	0.758	0.64
279	11/6/2002	7:21:14 PM	26.241	23.216	24.88	23.337	23.71	44.315	46.091	9.56	35.208	-1.288	-5.698	50.939	0.199	0.001	0	246.50	4.10833	44.6	12.5	39.4	2.741	0.030	0.001	0.001	0.745	0.63
280	11/6/2002	7:22:14 PM	26.236	23.226	24.836	23.421	23.695	44.381	46.052	9.562	35.401	-1.288	-5.738	49.188	0.199	0.001	0	247.50	4.125	44.6	12.1	39.9	2.760	0.030	0.001	0.001	0.747	0.64
281	11/6/2002	7:23:14 PM	26.209	23.214	24.818	23.339	23.673	44.443	46.589	9.242	35.729	-1.288	-5.706	48.441	0.201	0.001	0	248.50	4.14167	44.6	11.9	40.1	2.764	0.030	0.001	0.001	0.751	0.64
282	11/6/2002	7:24:14 PM	26.186	23.209	24.862	23.374	23.632	44.343	45.905	9.263	35.693	-1.291	-5.703	49.106	0.198	0.001	0	249.50	4.15833	44.4	12.0	40.0	2.766	0.030	0.001	0.001	0.742	0.63
283	11/6/2002	7:25:14 PM	26.167	23.202	24.746	23.438	23.636	44.996	46.587	9.112	36.388	-1.288	-5.706	48.307	0.2	0.001	0	250.50	4.175	45.1	11.8	40.7	2.806	0.030	0.001	0.001	0.738	0.63
284	11/6/2002	7:26:14 PM	26.156	23.202	24.83	23.427	23.615	44.859	46.633	9.16	36.097	-1.285	-5.729	49.451	0.197	0.001	0	251.50	4.19167	45.2	12.1	40.5	2.791	0.029	0.001	0.001	0.729	0.62
285	11/6/2002	7:27:14 PM	26.15	23.2	24.774	23.426	23.699	44.696	46.308	9.389	35.774	-1.285	-5.744	47.56	0.199	0.001	0	252.50	4.20833	44.8	11.7	40.2	2.774	0.030	0.001	0.001	0.742	0.63
286	11/6/2002	7:28:14 PM	26.117	23.178	24.729	23.389	23.448	44.819	46.72	9.226	36.007	-1.288	-5.51	48.773	0.201	0.001	0	253.50	4.225	45.4	12.0	40.7	2.804	0.030	0.001	0.001	0.742	0.64
287	11/6/2002	7:29:14 PM	26.115	23.176	24.8	23.346	23.564	44.882	46.461	9.169	36.232	-1.291	-5.741	48.176	0.2	0.001	0	254.50	4.24167	45.0	11.8	40.6	2.796	0.030	0.001	0.001	0.739	0.63
288	11/6/2002	7:30:14 PM	26.103	23.174	24.693	23.364	23.497	44.983	46.313	9.223	36.179	-1.288	-5.706	48.716	0.198	0.001	0	255.50	4.25833	45.2	11.9	40.6	2.798	0.030	0.001	0.001	0.734	0.62
289	11/6/2002	7:31:14 PM	26.123	23.193	24.807	23.339	23.622	45.058	46.633	9.935	36.627	-1.285	-5.729	48.108	0.199	0.001	0	256.50	4.275	45.2	11.8	40.8	2.816	0.030	0.001	0.001	0.730	0.62
290	11/6/2002	7:32:14 PM	26.123	23.172	24.731	23.392	23.54	45.046	46.221	9.592	36.629	-1.288	-5.729	47.833	0.199	0.001	0	257.50	4.29167	45.1	11.7	40.8	2.816	0.030	0.001	0.001	0.732	0.62
291	11/6/2002	7:33:14 PM	26.101	23.187	24.761	23.377	23.55	45.031	46.669	9.898	36.641	-1.285	-5.732	47.993	0.199	0.001	0	258.50	4.30833	44.9	11.8	40.8	2.815	0.030	0.001	0.001	0.732	0.62
292	11/6/2002	7:34:14 PM	26.08	23.166	24.789	23.316	23.509	45.402	47.08	9.966	36.973	-1.288	-5.738	47.12	0.199	0.001	0	259.50	4.325	45.6	11.5	41.2	2.840	0.030	0.001	0.001	0.725	0.62
293	11/6/2002	7:35:14 PM	26.095	23.181	24.714	23.386	23.479	44.93	46.637	9.135	36.203	-1.285	-5.738	47.395	0.196	0.001	0	260.50	4.34167	45.2	11.6	40.6	2.797	0.029	0.001	0.001	0.726	0.62
294	11/6/2002	7:36:14 PM	26.063	23.138	24.742	23.269	23.431	45.257	46.867	9.196	36.621	-1.291	-5.729	50.742	0.197	0.001	0	261.50	4.35833	45.4	12.4	40.9	2.823	0.029	0.001	0.001	0.723	0.62
295	11/6/2002	7:37:14 PM	26.05	23.137	24.761	23.297	23.425	44.971	46.511	9.293	36.13	-1.288	-5.688	48.188	0.197	0.001	0	262.50	4.375	45.1	11.7	40.7	2.803	0.029	0.001	0.001	0.730	0.62
296	11/6/2002	7:38:14 PM	26.047	23.143	24.722	23.263	23.436	44.203	45.422	9.836	34.808	-1.288	-5.706	48.507	0.197	0.001	0	263.50	4.39167	44.3	12.5	39.5	2.728	0.028	0.002	0.001	0.711	0.51
297	11/6/2002	7:39:14 PM	26.026	23.122	24.776	23.197	23.44	44.42	46.408	9.63	35.421	-1.291	-5.822	50.189	0.19	0.001	0	264.50	4.40833	44.6	12.3	40.0	2.758	0.028	0.002	0.001	0.713	0.61
298	11/6/2002	7:40:14 PM	26.047	23.143	24.722	23.228	23.431	44.439	46.103	9.603	35.268	-1.282	-5.822	50.719	0.193	0.001	0	265.50	4.425	44.6	12.4	39.9	2.748	0.029	0.002	0.001	0.728	0.62
299	11/6/2002	7:41:14 PM	26.047	23.143	24.722	23.228	23.431	44.439	46.103	9.603	35.268	-1.282	-5.822	50.719	0.193	0.001	0	265.50	4.425	44.6	12.4	39.9	2.748	0.029	0.002	0.001	0.728	0.62
300	11/6/2002	7:42:14 PM	26.04	23.116	24.76	23.115	23.389	44.192	45.771	9.775	34.846	-1.291	-5.906	50.249	0.187	0.001	0	266.50	4.44167	44.2	12.3	39.5	2.725	0.028	0.002	0.001	0.710	0.60
301	11/6/2002	7:43:14 PM	26.014	23.099	24.743	23.043	23.377	43.476	45.088	10.126	33.757																	

391	11/6/2002	9 12 17 PM	24.98	22.467	24.844	22.572	22.635	44.72	46.215	9.639	35.475	-1.286	-6.291	49.559	0.152	0.001	0	367.55	5.95917	44.7	12.1	40.1	2.765	0.023	0.001	0.568	0.48
392	11/6/2002	9 13 17 PM	24.98	22.466	24.843	22.591	22.603	44.607	46.078	9.588	35.461	-1.286	-6.363	49.645	0.152	0.001	0	368.55	5.97583	44.6	12.2	40.0	2.760	0.022	0.001	0.561	0.48
393	11/6/2002	9 14 17 PM	24.943	22.45	24.762	22.623	22.623	44.779	46.24	9.507	35.579	-1.286	-6.326	48.678	0.153	0.001	0	369.55	5.9925	44.8	11.9	40.2	2.770	0.023	0.001	0.572	0.49
394	11/6/2002	9 15 17 PM	24.852	22.444	24.842	22.504	22.623	44.867	46.259	9.644	35.673	-1.286	-6.326	50.037	0.148	0.001	0	360.55	5.90917	44.8	12.6	40.3	2.776	0.022	0.001	0.550	0.47
395	11/6/2002	9 16 17 PM	24.947	22.444	24.773	22.609	22.637	44.644	46.244	9.733	35.389	-1.286	-6.363	49.489	0.153	0.001	0	361.55	5.92683	44.6	12.0	40.0	2.768	0.023	0.001	0.564	0.48
396	11/6/2002	9 17 17 PM	24.915	22.427	24.784	22.426	22.595	44.673	46.141	9.8	35.321	-1.286	-6.3	50.65	0.154	0.001	0	362.55	6.0425	44.7	12.4	40.0	2.758	0.023	0.001	0.578	0.49
397	11/6/2002	9 18 17 PM	24.905	22.432	24.819	22.467	22.579	44.696	45.954	9.469	35.737	-1.286	-6.346	49.622	0.15	0.001	0	363.55	6.06917	44.5	12.2	40.2	2.773	0.022	0.001	0.569	0.48
398	11/6/2002	9 19 17 PM	24.893	22.41	24.733	22.455	22.598	44.969	46.136	9.665	35.682	-1.286	-6.336	50.394	0.152	0.001	0	364.55	6.07983	44.7	12.3	40.4	2.787	0.023	0.001	0.565	0.48
399	11/6/2002	9 20 17 PM	24.892	22.409	24.807	22.454	22.587	45.021	46.463	9.698	35.597	-1.286	-6.336	49.853	0.15	0.001	0	365.55	6.0905	44.5	12.2	40.5	2.793	0.022	0.001	0.564	0.48
400	11/6/2002	9 21 17 PM	24.902	22.414	24.751	22.459	22.597	45.031	46.358	9.642	35.937	-1.291	-6.337	49.664	0.152	0.001	0	366.55	6.10917	44.9	12.2	40.5	2.791	0.023	0.001	0.564	0.48
401	11/6/2002	9 22 17 PM	24.886	22.408	24.77	22.518	22.586	44.959	46.209	9.588	35.819	-1.286	-6.349	49.322	0.151	0.001	0	367.55	6.12583	44.9	12.1	40.4	2.785	0.023	0.001	0.561	0.48
402	11/6/2002	9 23 17 PM	24.895	22.392	24.815	22.512	22.58	44.963	46.321	9.587	35.964	-1.286	-6.438	49.457	0.152	0.001	0	368.55	6.1425	44.8	12.1	40.4	2.787	0.023	0.001	0.564	0.48
403	11/6/2002	9 24 17 PM	24.899	22.376	24.699	22.521	22.589	44.694	45.96	9.458	35.731	-1.291	-6.378	51.339	0.147	0.001	0	369.55	6.15917	44.4	12.5	40.2	2.773	0.021	0.001	0.561	0.48
404	11/6/2002	9 25 17 PM	24.873	22.38	24.783	22.395	22.518	45.021	46.331	9.498	35.976	-1.288	-6.328	49.213	0.148	0.001	0	370.55	6.17583	44.9	12.1	40.5	2.792	0.022	0.001	0.568	0.47
405	11/6/2002	9 26 17 PM	24.863	22.369	24.747	22.419	22.542	44.853	46.215	9.583	35.647	-1.286	-6.308	49.899	0.15	0.001	0	371.55	6.1925	44.7	12.2	40.3	2.775	0.022	0.001	0.560	0.48
406	11/6/2002	9 27 17 PM	24.846	22.368	24.736	22.398	22.496	44.816	45.942	9.54	35.739	-1.291	-6.308	49.391	0.152	0.001	0	372.55	6.20917	44.5	12.1	40.3	2.777	0.023	0.001	0.567	0.48
407	11/6/2002	9 28 17 PM	24.841	22.362	24.81	22.357	22.52	44.971	46.333	9.588	35.798	-1.288	-6.441	51.179	0.148	0.001	0	373.55	6.22583	44.9	12.5	40.4	2.784	0.022	0.001	0.569	0.47
408	11/6/2002	9 29 17 PM	24.834	22.351	24.724	22.32	22.438	44.883	46.256	9.695	35.653	-1.286	-6.338	50.736	0.15	0.001	0	374.55	6.2425	44.5	11.7	40.2	2.788	0.022	0.001	0.560	0.47
409	11/6/2002	9 30 17 PM	24.813	22.33	24.767	22.279	22.437	44.582	45.94	9.814	35.295	-1.291	-6.396	50.033	0.148	0.001	0	375.55	6.25917	44.5	12.3	39.9	2.752	0.022	0.001	0.549	0.47
410	11/6/2002	9 31 17 PM	24.826	22.323	24.761	22.368	22.42	44.652	46.016	9.919	35.174	-1.288	-6.378	49.91	0.148	0.001	0	376.55	6.27583	44.5	12.2	39.9	2.752	0.022	0.001	0.557	0.47
411	11/6/2002	9 32 17 PM	24.819	22.316	24.734	22.431	22.443	44.729	46.112	9.842	35.321	-1.288	-6.467	50.193	0.147	0.001	0	377.55	6.2925	44.6	12.3	40.0	2.780	0.022	0.001	0.552	0.47
412	11/6/2002	9 33 17 PM	24.834	22.31	24.818	22.327	22.453	44.851	45.965	9.877	35.46	-1.288	-6.43	50.05	0.146	0.001	0	378.55	6.30917	44.5	12.3	40.2	2.783	0.022	0.001	0.546	0.46
413	11/6/2002	9 34 17 PM	24.864	22.32	24.778	22.451	22.478	44.769	46.035	9.872	35.372	-1.295	-6.43	50.893	0.145	0.001	0	379.55	6.32583	44.6	12.5	40.1	2.763	0.022	0.001	0.547	0.47
414	11/6/2002	9 35 17 PM	24.869	22.33	24.833	22.445	22.468	44.107	45.937	10.184	34.283	-1.285	-6.469	52.347	0.144	0.001	0	380.55	6.3425	44.1	12.8	39.2	2.702	0.021	0.001	0.550	0.47
415	11/6/2002	9 36 17 PM	24.869	22.31	24.848	22.466	22.468	44.733	45.959	9.803	35.518	-1.286	-6.382	49.796	0.142	0.001	0	381.55	6.35917	44.5	12.0	40.1	2.787	0.021	0.001	0.530	0.45
416	11/6/2002	9 37 17 PM	24.859	22.299	24.767	22.45	22.452	45.338	46.66	9.458	35.173	-1.285	-6.367	49.056	0.151	0.001	0	382.55	6.37583	45.2	12.6	40.8	2.816	0.023	0.001	0.557	0.47
417	11/6/2002	9 38 17 PM	24.867	22.289	24.837	22.359	22.487	45.108	45.72	9.774	35.688	-1.291	-6.352	49.891	0.15	0.001	0	383.55	6.3925	45.2	12.2	40.4	2.788	0.022	0.001	0.556	0.47
418	11/6/2002	9 39 17 PM	24.872	22.288	24.771	22.464	22.476	44.708	45.971	9.657	35.561	-1.286	-6.423	49.993	0.147	0.001	0	384.55	6.40917	44.5	12.0	40.1	2.787	0.022	0.001	0.550	0.47
419	11/6/2002	9 40 17 PM	24.876	22.282	24.79	22.413	22.49	45.321	46.714	9.518	35.23	-1.288	-6.438	49.423	0.15	0.001	0	385.55	6.42583	45.2	11.9	40.8	2.811	0.022	0.001	0.552	0.47
420	11/6/2002	9 41 17 PM	24.885	22.287	24.87	22.437	22.49	44.968	46.399	9.717	35.54	-1.285	-6.434	50.55	0.145	0.001	0	386.55	6.4425	44.9	12.4	40.3	2.779	0.022	0.001	0.538	0.46
421	11/6/2002	9 42 17 PM	24.874	22.286	24.733	22.421	22.484	44.824	46.681	9.733	35.19	-1.291	-6.388	49.755	0.149	0.001	0	387.55	6.45917	44.5	11.7	40.2	2.808	0.022	0.001	0.550	0.47
422	11/6/2002	9 43 17 PM	24.889	22.275	24.833	22.39	22.473	45.305	46.697	9.723	35.023	-1.288	-6.302	49.104	0.148	0.001	0	388.55	6.47583	45.2	12.0	40.7	2.804	0.022	0.001	0.545	0.46
423	11/6/2002	9 44 17 PM	24.894	22.28	24.793	22.435	22.473	44.981	46.35	9.678	35.698	-1.288	-6.32	49.077	0.146	0.001	0	389.55	6.4925	44.9	12.0	40.3	2.781	0.022	0.001	0.543	0.46
424	11/6/2002	9 45 17 PM	24.883	22.279	24.787	22.349	22.427	44.882	46.244	9.671	35.627	-1.288	-6.443	49.876	0.149	0.001	0	390.55	6.50917	44.8	12.2	40.4	2.783	0.022	0.001	0.554	0.47
425	11/6/2002	9 46 17 PM	24.871	22.269	24.804	22.32	22.366	44.971	46.289	9.674	35.371	-1.288	-6.438	49.129	0.148	0.001	0	391.55	6.52583	44.9	11.8	40.3	2.789	0.022	0.001	0.547	0.46
426	11/6/2002	9 47 17 PM	24.874	22.262	24.75	22.321	22.344	45.345	46.259	9.653	35.077	-1.288	-6.366	49.08	0.148	0.001	0	392.55	6.5425	45.1	11.3	40.7	2.805	0.022	0.001	0.546	0.46
427	11/6/2002	9 48 17 PM	24.849	22.25	24.819	22.265	22.353	45.628	46.904	9.455	35.517	-1.286	-6.401	50.935	0.15	0.001	0	393.55	6.55917	45.4	12.5	41.0	2.828	0.022	0.001	0.548	0.47
428	11/6/2002	9 49 17 PM	24.853	22.25	24.803	22.245	22.307	45.216	46.647	9.516	35.054	-1.286	-6.415	49.311	0.144	0.001	0	394.55	6.57583	45.2	11.8	40.6	2.802	0.021	0.001	0.531	0.45
429	11/6/2002	9 50 17 PM	24.853	22.253	24.762	22.278	22.321	44.938	46.585	9.499	35.38	-1.286	-6.441	49.056	0.151	0.001	0	395.55	6.5925	45.2	12.6	40.8	2.816	0.023	0.001	0.557	0.47
430	11/6/2002	9 51 17 PM	24.862	22.253	24.876	22.227	22.33	45.203	46.583	9.581	35.033	-1.288	-6.447	49.446	0.144	0.001	0	396.55	6.60917	45.1	12.1	40.6	2.800	0.021	0.001	0.530	0.45
431	11/6/2002	9 52 17 PM	24.871	22.247	24.786	22.267	22.365	45.234	46.496	9.624	35.034	-1.286	-6.398	49.548	0.147	0.001	0	397.55	6.62583	45.0	11.9	40.6	2.802	0.022	0.001	0.543	0.46
432	11/6/2002	9 53 17 PM	24.865	22.251	24.86	22.326	22.389	45.371	46.566	9.373	35.431	-1.286	-6.439	49.081	0.146	0.001	0	398.55	6.6425	45.2	11.8	40.9	2.820	0.022	0.001	0.534	0.45
433	11/6/2002	9 54 17 PM	24.8																								

521	11/6/2002	11:21:50 PM	24.809	21.692	24.999	21.52	21.734	44.996	46.062	10.109	35.288	-1.265	-6.601	48.278	0.128	0.001	0	487.10	8.11833	44.6	11.8	40.1	2.768	0.019	0.019	0.000	0.475	0.40
522	11/6/2002	11:22:50 PM	24.819	21.697	25.044	21.561	21.724	45.013	46.213	10.094	35.401	-1.268	-6.604	50.539	0.127	0.001	0	488.10	8.136	44.7	12.4	40.2	2.772	0.019	0.019	0.000	0.470	0.40
523	11/6/2002	11:23:50 PM	24.818	21.681	25.098	21.589	21.743	45.008	46.203	10.059	35.468	-1.268	-6.641	49.201	0.131	0.001	0	489.10	8.15167	44.7	12.1	40.2	2.774	0.019	0.019	0.000	0.480	0.41
524	11/6/2002	11:24:50 PM	24.814	21.676	25.013	21.685	21.783	45.122	46.219	10.201	35.247	-1.276	-6.593	49.693	0.133	0.001	0	490.10	8.16833	44.7	12.2	40.2	2.771	0.020	0.020	0.000	0.496	0.41
525	11/6/2002	11:25:50 PM	24.826	21.682	25.072	21.618	21.772	44.998	46.066	10.076	35.311	-1.268	-6.578	49.110	0.132	0.001	0	491.10	8.189	44.6	11.8	40.1	2.765	0.019	0.019	0.000	0.472	0.40
526	11/6/2002	11:26:50 PM	24.857	21.669	25.077	21.669	21.767	44.983	45.93	10.141	35.346	-1.265	-6.74	49.138	0.128	0.001	0	492.10	8.20167	44.5	12.0	40.2	2.769	0.019	0.019	0.000	0.474	0.40
527	11/6/2002	11:27:50 PM	24.856	21.649	25.046	21.704	21.807	45.18	46.428	10.21	35.37	-1.265	-6.536	49.811	0.125	0.001	0	493.10	8.21833	45.0	12.2	40.3	2.777	0.019	0.019	0.000	0.462	0.39
528	11/6/2002	11:28:50 PM	24.866	21.648	25.155	21.663	21.796	45.226	46.314	10.21	35.526	-1.265	-6.556	48.389	0.128	0.001	0	494.10	8.236	44.8	11.9	40.4	2.784	0.019	0.019	0.000	0.471	0.40
529	11/6/2002	11:29:50 PM	24.866	21.643	25.065	21.663	21.796	45.247	46.011	10.24	35.426	-1.265	-6.728	48.239	0.128	0.001	0	495.10	8.25167	45.0	12.3	40.3	2.781	0.019	0.019	0.000	0.472	0.40
530	11/6/2002	11:30:50 PM	24.871	21.633	25.1	21.638	21.791	45.135	46.314	10.21	35.382	-1.268	-6.595	48.368	0.128	0.001	0	496.10	8.26833	44.7	12.1	40.2	2.775	0.019	0.019	0.000	0.477	0.41
531	11/6/2002	11:31:50 PM	24.875	21.632	25.16	21.662	21.785	45.17	46.361	10.23	35.36	-1.265	-6.688	48.758	0.129	0.001	0	497.10	8.286	44.8	11.9	40.3	2.776	0.019	0.019	0.000	0.476	0.40
532	11/6/2002	11:32:50 PM	24.876	21.617	25.06	21.697	21.795	44.969	45.938	10.099	35.438	-1.265	-6.708	49.918	0.128	0.001	0	498.10	8.30167	44.5	12.2	40.2	2.772	0.019	0.019	0.000	0.474	0.40
533	11/6/2002	11:33:50 PM	24.885	21.62	25.17	21.622	21.84	45.174	46.244	10.242	35.468	-1.265	-6.702	49.102	0.123	0.001	0	499.10	8.31633	44.8	12.0	40.2	2.774	0.016	0.016	0.000	0.454	0.39
534	11/6/2002	11:34:50 PM	24.89	21.612	25.134	21.657	21.765	44.977	45.965	10.205	35.237	-1.265	-6.728	49.297	0.128	0.001	0	501.0	8.362	44.5	12.1	40.1	2.766	0.019	0.019	0.000	0.474	0.40
535	11/6/2002	11:35:50 PM	24.895	21.597	25.094	21.621	21.78	45.184	46.39	10.302	35.129	-1.291	-6.722	49.326	0.127	0.001	0	502.0	8.37867	44.9	12.1	40.2	2.769	0.019	0.019	0.000	0.470	0.40
536	11/6/2002	11:36:50 PM	24.919	21.601	25.234	21.676	21.784	45.118	46.023	10.195	35.489	-1.262	-6.609	50.9	0.131	0.001	0	503.0	8.39533	44.6	13.0	40.3	2.779	0.020	0.020	0.000	0.481	0.41
537	11/6/2002	11:37:50 PM	24.924	21.59	25.133	21.66	21.799	44.99	46.151	10.423	34.903	-1.265	-6.624	49.949	0.127	0.001	0	504.0	8.412	44.7	12.2	39.9	2.754	0.019	0.019	0.000	0.472	0.40
538	11/6/2002	11:38:50 PM	24.914	21.58	25.168	21.595	21.799	45.003	46.014	10.276	35.311	-1.268	-6.702	50.576	0.128	0.001	0	505.0	8.42867	44.5	11.9	40.1	2.765	0.019	0.019	0.000	0.459	0.39
539	11/6/2002	11:39:50 PM	24.924	21.595	25.248	21.62	21.799	44.989	46.074	10.395	35.008	-1.268	-6.74	50.006	0.128	0.001	0	506.0	8.44533	44.6	12.3	40.0	2.757	0.019	0.019	0.000	0.474	0.40
540	11/6/2002	11:40:50 PM	24.953	21.595	25.338	21.665	21.798	44.961	45.812	10.355	35.032	-1.262	-6.475	49.289	0.13	0.001	0	507.0	8.462	44.3	12.1	40.0	2.758	0.019	0.019	0.000	0.480	0.41
541	11/6/2002	11:41:50 PM	24.973	21.574	25.807	21.594	21.807	45.036	46.182	10.14	35.239	-1.265	-6.557	51.053	0.126	0.001	0	508.0	8.47867	44.7	12.5	40.1	2.767	0.019	0.019	0.000	0.458	0.39
542	11/6/2002	11:42:50 PM	25.042	21.583	26.002	21.588	21.837	45.708	46.848	9.243	35.826	-1.291	-6.598	48.134	0.129	0.001	0	509.0	8.49533	44.5	11.3	40.1	2.768	0.019	0.019	0.000	0.453	0.39
543	11/6/2002	11:43:50 PM	25.062	21.568	26.131	21.582	21.846	45.222	47.316	8.98	37.941	-1.295	-6.441	47.095	0.133	0.001	0	510.0	8.512	45.8	11.5	42.0	2.898	0.020	0.020	0.000	0.457	0.39
544	11/6/2002	11:44:50 PM	25.271	21.557	26.225	21.581	21.845	46.302	47.88	8.723	38.068	-1.285	-6.305	46.376	0.139	0.001	0	511.0	8.52867	46.2	11.4	42.2	2.911	0.021	0.021	0.000	0.474	0.40
545	11/6/2002	11:45:50 PM	25.371	21.552	26.97	21.627	21.86	46.493	47.824	8.735	38.171	-1.286	-6.401	44.775	0.134	0.001	0	512.0	8.54533	46.4	10.9	42.3	2.918	0.020	0.020	0.000	0.459	0.39
546	11/6/2002	11:46:50 PM	24.965	21.552	25.94	21.622	21.84	44.665	46.719	9.017	38.121	-1.285	-6.517	49.174	0.13	0.001	0	513.0	8.562	44.3	12.4	39.9	2.762	0.019	0.019	0.000	0.459	0.39
547	11/6/2002	11:47:50 PM	25.44	21.55	26.829	21.651	21.854	45.031	46.277	10.016	35.276	-1.279	-6.624	50.291	0.124	0.001	0	514.0	8.57867	44.8	12.3	40.2	2.768	0.016	0.016	0.000	0.450	0.38
548	11/6/2002	11:48:50 PM	25.418	21.538	26.697	21.603	21.832	44.888	46.035	9.888	35.483	-1.285	-6.722	49.889	0.127	0.001	0	515.0	8.59533	44.6	12.2	40.2	2.771	0.019	0.019	0.000	0.462	0.39
549	11/6/2002	11:49:50 PM	26.397	21.527	26.691	21.622	21.806	45.002	46.109	9.658	35.751	-1.295	-6.74	50.367	0.128	0.001	0	516.0	8.612	44.6	12.3	40.4	2.784	0.019	0.019	0.000	0.464	0.39
550	11/6/2002	11:50:50 PM	26.362	21.532	25.836	21.622	21.816	45.375	46.335	9.641	36.205	-1.295	-6.728	49.075	0.13	0.001	0	517.0	8.62867	44.9	12.0	40.8	2.812	0.019	0.019	0.000	0.468	0.40
551	11/6/2002	11:51:50 PM	25.388	21.627	25.633	21.612	21.83	45.402	46.16	9.624	36.208	-1.288	-6.588	51.812	0.125	0.001	0	518.0	8.64533	44.5	11.9	40.8	2.813	0.019	0.019	0.000	0.468	0.40
552	11/6/2002	11:52:50 PM	26.23	21.625	25.469	21.641	21.804	45.302	46.405	9.465	36.433	-1.288	-6.536	48.638	0.123	0.001	0	519.0	8.662	44.9	11.9	40.9	2.818	0.016	0.016	0.000	0.443	0.38
553	11/6/2002	11:53:50 PM	25.35	21.625	25.369	21.661	21.809	45.015	46.118	9.713	35.669	-1.285	-6.677	48.872	0.124	0.001	0	520.0	8.67867	44.6	11.9	40.3	2.781	0.018	0.018	0.000	0.454	0.39
554	11/6/2002	11:54:50 PM	25.276	21.52	25.399	21.626	21.794	45.189	46.368	9.688	35.561	-1.282	-6.621	49.4	0.126	0.001	0	521.0	8.69533	44.9	12.1	40.5	2.784	0.019	0.019	0.000	0.458	0.39
555	11/6/2002	11:55:50 PM	25.265	21.515	25.299	21.597	21.809	45.423	46.015	9.793	35.96	-1.291	-6.702	52.0	0.126	0.001	0	522.0	8.712	44.5	12.6	40.9	2.814	0.019	0.019	0.000	0.456	0.39
556	11/6/2002	11:56:50 PM	25.215	21.525	25.269	21.627	21.789	45.215	46.308	9.649	35.796	-1.282	-6.451	51.906	0.126	0.001	0	523.0	8.72867	44.5	12.5	40.5	2.789	0.019	0.019	0.000	0.461	0.39
557	11/6/2002	11:57:50 PM	25.175	21.51	25.324	21.565	21.764	44.907	46.925	10.072	35.229	-1.285	-6.471	50.287	0.122	0.001	0	524.0	8.74533	44.5	12.3	40.1	2.763	0.018	0.018	0.000	0.450	0.38
558	11/6/2002	11:58:50 PM	25.134	21.496	25.183	21.527	21.743	45.044	46.213	10.032	35.339	-1.288	-6.809	48.651	0.122	0.001	0	525.0	8.762	44.7	11.9	40.2	2.771	0.018	0.018	0.000	0.450	0.38
559	11/6/2002	11:59:50 PM	25.103	21.563	25.024	21.533	21.749	44.619	46.114	10.242	34.967	-1.285	-6.867	50.228	0.121	0.001	0	526.0	8.77867	44.3	12.3	39.9	2.738	0.016	0.016	0.000	0.445	0.38
560	11/6/2002	12:00:50 AM	25.059	21.474	25.193	21.534	21.753	44.789	46.006	10.26	34.975	-1.288	-6.841	51.1	0.12	0.001	0	527.0	8.79533	44.5	11.6	39.8	2.746	0.016	0.016	0.000	0.447	0.38
561	11/6/2002	12:01:50 AM	25.054	21.485	25.153	21.565	21.749	44.538	45.754	10.162	34.768	-1.286	-6.844	49.779	0.119	0.001	0	528.										

651	11/7/2002	1:30:35 AM	24.706	20.893	25.115	20.771	20.859	44.876	46.422	9.838	35.428	-1.286	-6.867	49.389	0.113	0.001	0	617.47	10.2912	44.9	12.1	40.2	2.768	0.017	0.017	0.000	0.418	0.36
652	11/7/2002	1:31:35 AM	24.675	20.871	24.994	20.771	20.828	44.853	46.652	9.839	35.481	-1.286	-6.873	51.747	0.113	0.001	0	618.47	10.3078	45.2	12.7	40.2	2.769	0.017	0.017	0.000	0.420	0.36
653	11/7/2002	1:32:35 AM	24.673	20.875	25.048	20.703	20.786	44.814	46.681	9.979	35.178	-1.282	-6.881	50.329	0.112	0.001	0	619.47	10.3245	45.2	12.3	40.0	2.768	0.017	0.017	0.000	0.417	0.36
654	11/7/2002	1:33:35 AM	24.663	20.87	25.062	20.763	20.801	44.988	46.292	9.912	35.098	-1.282	-6.982	50.356	0.112	0.001	0	620.47	10.3412	44.8	12.3	39.8	2.747	0.017	0.017	0.000	0.418	0.36
655	11/7/2002	1:34:35 AM	24.662	20.869	25.017	20.803	20.8	44.935	46.596	9.91	35.1	-1.282	-6.989	49.618	0.112	0.001	0	621.47	10.3579	45.1	12.2	40.0	2.767	0.017	0.017	0.000	0.417	0.36
656	11/7/2002	1:35:35 AM	24.661	20.863	25.076	20.696	20.754	44.737	46.523	9.909	35.147	-1.286	-6.87	49.293	0.112	0.001	0	622.47	10.3745	45.1	12.1	39.9	2.764	0.017	0.017	0.000	0.417	0.36
657	11/7/2002	1:36:35 AM	24.64	20.842	25.034	20.73	20.748	44.629	46.378	9.821	35.389	-1.285	-6.829	50.216	0.112	0.001	0	623.47	10.3912	44.9	12.3	40.0	2.758	0.017	0.017	0.000	0.417	0.36
658	11/7/2002	1:37:35 AM	24.634	20.831	25.009	20.705	20.757	44.805	46.589	9.928	35.278	-1.282	-6.876	49.492	0.111	0.001	0	624.47	10.4078	45.1	12.1	40.0	2.761	0.017	0.017	0.000	0.413	0.36
659	11/7/2002	1:38:35 AM	24.628	20.825	25.023	20.696	20.741	44.804	46.321	9.899	35.219	-1.282	-6.843	49.253	0.112	0.001	0	625.47	10.4245	44.8	12.1	39.9	2.752	0.017	0.017	0.000	0.417	0.36
660	11/7/2002	1:39:35 AM	24.618	20.819	25.022	20.688	20.715	44.53	46.182	9.978	35.147	-1.286	-6.87	49.876	0.112	0.001	0	626.47	10.4412	44.7	12.0	39.8	2.747	0.017	0.017	0.000	0.419	0.36
661	11/7/2002	1:40:35 AM	24.611	20.797	25.031	20.661	20.714	44.536	46.426	9.932	35.047	-1.286	-6.89	49.666	0.111	0.001	0	627.47	10.4578	45.0	12.2	39.8	2.743	0.017	0.017	0.000	0.416	0.36
662	11/7/2002	1:41:35 AM	24.61	20.797	25.09	20.636	20.718	44.339	46.244	9.893	34.993	-1.285	-6.955	48.364	0.111	0.001	0	628.47	10.4745	44.8	11.9	39.6	2.731	0.017	0.017	0.000	0.417	0.36
663	11/7/2002	1:42:35 AM	24.592	20.796	25.004	20.619	20.696	44.729	46.401	9.995	35.149	-1.282	-6.849	49.651	0.111	0.001	0	629.47	10.4912	44.9	12.1	40.0	2.755	0.017	0.017	0.000	0.414	0.36
664	11/7/2002	1:43:35 AM	24.604	20.795	25.063	20.643	20.661	44.638	46.532	9.952	35.118	-1.285	-6.882	48.76	0.111	0.001	0	630.47	10.5078	45.1	11.9	39.9	2.749	0.017	0.017	0.000	0.414	0.36
665	11/7/2002	1:44:35 AM	24.603	20.779	25.063	20.673	20.696	44.889	46.238	9.91	35.319	-1.286	-6.786	49.366	0.111	0.001	0	631.47	10.5245	44.8	12.1	40.0	2.758	0.016	0.016	0.000	0.409	0.36
666	11/7/2002	1:45:35 AM	24.578	20.764	24.982	20.622	20.65	44.762	46.447	9.989	35.178	-1.288	-6.774	50.102	0.111	0.001	0	632.47	10.5412	45.0	12.3	40.0	2.756	0.016	0.016	0.000	0.411	0.36
667	11/7/2002	1:46:35 AM	24.582	20.758	25.087	20.611	20.624	44.936	46.699	9.925	35.497	-1.285	-6.815	49.4	0.109	0.001	0	633.47	10.5578	45.2	12.1	40.2	2.773	0.016	0.016	0.000	0.393	0.34
668	11/7/2002	1:47:35 AM	24.581	20.757	25.025	20.641	20.603	44.876	46.604	9.997	35.438	-1.286	-6.847	49.269	0.111	0.001	0	634.47	10.5745	45.1	12.2	40.2	2.768	0.017	0.017	0.000	0.412	0.36
669	11/7/2002	1:48:35 AM	24.56	20.736	25.004	20.604	20.612	44.75	46.238	9.834	35.495	-1.286	-6.844	50.165	0.111	0.001	0	635.47	10.5912	44.8	12.3	40.1	2.766	0.017	0.017	0.000	0.412	0.36
670	11/7/2002	1:49:35 AM	24.564	20.74	25.089	20.594	20.601	44.795	46.686	9.999	35.17	-1.286	-6.873	47.401	0.111	0.001	0	636.47	10.6078	45.2	11.6	40.0	2.757	0.016	0.016	0.000	0.409	0.36
671	11/7/2002	1:50:35 AM	24.563	20.734	25.008	20.572	20.539	44.838	46.776	9.945	35.462	-1.286	-6.87	49.731	0.111	0.001	0	637.47	10.6245	45.3	12.2	40.2	2.768	0.016	0.016	0.000	0.408	0.36
672	11/7/2002	1:51:35 AM	24.552	20.718	25.037	20.511	20.553	44.889	46.35	9.999	35.135	-1.286	-6.888	47.395	0.111	0.001	0	638.47	10.6412	44.9	11.8	39.9	2.751	0.016	0.016	0.000	0.411	0.36
673	11/7/2002	1:52:35 AM	24.541	20.707	25.071	20.601	20.543	44.795	46.536	9.968	35.319	-1.285	-6.87	48.108	0.111	0.001	0	639.47	10.6578	45.1	11.8	40.1	2.761	0.016	0.016	0.000	0.409	0.36
674	11/7/2002	1:53:35 AM	24.565	20.701	24.99	20.564	20.562	44.779	46.604	10.058	35.42	-1.286	-6.436	49.463	0.088	0.001	0	640.47	10.6745	45.1	12.1	40.0	2.757	0.013	0.013	0.000	0.328	0.28
675	11/7/2002	1:54:35 AM	24.566	20.7	25.079	20.544	20.551	44.397	46.138	10.092	34.719	-1.286	-6.473	50.86	0.104	0.001	0	641.47	10.6912	44.7	12.5	39.6	2.727	0.016	0.016	0.000	0.391	0.33
676	11/7/2002	1:55:35 AM	24.564	20.69	25.054	20.563	20.54	44.712	46.457	10.086	35.149	-1.286	-6.58	49.825	0.109	0.001	0	642.47	10.7078	44.9	12.2	39.9	2.753	0.016	0.016	0.000	0.395	0.34
677	11/7/2002	1:56:35 AM	24.564	20.679	25.023	20.532	20.53	44.528	46.261	10.143	34.973	-1.285	-6.824	51.68	0.108	0.001	0	643.47	10.7245	44.8	12.7	39.7	2.737	0.016	0.016	0.000	0.405	0.34
678	11/7/2002	1:57:35 AM	24.552	20.688	25.102	20.471	20.468	44.501	46.409	10.18	34.797	-1.286	-6.867	50.822	0.108	0.001	0	644.47	10.7412	44.9	12.5	39.6	2.734	0.016	0.016	0.000	0.405	0.34
679	11/7/2002	1:58:35 AM	24.567	20.662	25.037	20.511	20.473	44.368	46.014	10.122	34.764	-1.286	-6.884	49.343	0.107	0.001	0	645.47	10.7578	44.5	12.1	39.6	2.728	0.016	0.016	0.000	0.403	0.34
680	11/7/2002	1:59:35 AM	24.566	20.652	25.066	20.52	20.482	44.48	46.246	10.205	34.689	-1.285	-6.929	50.179	0.108	0.001	0	646.47	10.7745	44.8	12.3	39.6	2.729	0.016	0.016	0.000	0.405	0.35
681	11/7/2002	1:59:35 AM	24.561	20.646	25.136	20.525	20.487	44.395	46.041	10.136	34.655	-1.286	-6.884	54.747	0.107	0.001	0	647.47	10.7912	44.6	12.2	39.7	2.734	0.016	0.016	0.000	0.402	0.34
682	11/7/2002	2:01:35 AM	24.55	20.64	25.044	20.529	20.48	44.41	46.229	10.204	34.793	-1.286	-6.996	49.071	0.107	0.001	0	648.47	10.8078	44.8	12.0	39.6	2.730	0.016	0.016	0.000	0.402	0.34
683	11/7/2002	2:03:35 AM	24.554	20.624	25.114	20.508	20.475	44.341	46.275	10.26	34.611	-1.286	-6.89	49.61	0.107	0.001	0	649.47	10.8245	44.8	12.2	39.5	2.722	0.016	0.016	0.000	0.403	0.34
684	11/7/2002	2:05:35 AM	24.554	20.609	25.113	20.452	20.489	44.431	46.256	10.265	34.537	-1.286	-6.905	49.236	0.107	0.001	0	650.47	10.8412	44.8	12.1	39.5	2.722	0.016	0.016	0.000	0.403	0.34
685	11/7/2002	2:07:35 AM	24.551	20.598	25.077	20.458	20.468	44.331	46.072	10.309	34.488	-1.286	-6.918	49.857	0.107	0.001	0	651.47	10.8578	44.5	12.3	39.4	2.717	0.016	0.016	0.000	0.403	0.34
686	11/7/2002	2:09:35 AM	24.551	20.596	25.156	20.424	20.467	44.598	46.374	10.259	34.797	-1.288	-6.905	50.237	0.107	0.001	0	652.47	10.8745	44.9	12.3	39.7	2.732	0.016	0.016	0.000	0.400	0.34
687	11/7/2002	2:09:35 AM	24.586	20.601	25.126	20.459	20.477	44.381	46.376	10.289	34.529	-1.286	-6.908	49.779	0.106	0.001	0	653.47	10.8912	44.9	12.2	39.5	2.720	0.016	0.016	0.000	0.399	0.34
688	11/7/2002	2:07:35 AM	24.596	20.691	25.121	20.464	20.471	44.354	46.161	10.238	34.736	-1.282	-6.908	50.977	0.109	0.001	0	654.47	10.9078	44.7	12.5	39.5	2.726	0.016	0.016	0.000	0.406	0.35
689	11/7/2002	2:08:35 AM	24.546	20.69	25.054	20.501	20.502	44.346	46.322	10.308	34.488	-1.286	-6.978	52.179	0.107	0.001	0	655.47	10.9245	44.8	12.8	39.4	2.715	0.016	0.016	0.000	0.411	0.36
690	11/7/2002	2:09:35 AM	24.61	20.675	25.14	20.549	20.471	44.348	46.285	10.134	34.783	-1.282	-6.876	50.386	0.106	0.001	0	656.47	10.9412	44.8	12.3	39.6	2.728	0.016	0.016	0.000	0.399	0.34
691	11/7/2002	2:10:35 AM	24.605	20.669	25.169	20.483	20.43	44.25	46.157	10.336	34.386	-1.286	-6.903	50.212	0.107	0.001												

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761	11/7/2002	3.39 36 AM	24.21	19.966	25.051	19.955	19.862	43.677	46.399	10.008	34.16	-1.286	-6.932	48.303	0.099	0.001	0	746.49	12.444	44.9	11.8	38.9	2.683	0.015	0.015	0.000	0.379	0.32
762	11/7/2002	3.40 36 AM	24.41	19.945	25.105	19.889	19.846	44.078	46.396	10.007	34.16	-1.286	-6.934	48.632	0.099	0.001	0	747.49	12.4581	45.5	11.9	39.2	2.706	0.015	0.015	0.000	0.375	0.32
763	11/7/2002	3.41 36 AM	24.42	19.949	25.111	19.849	19.845	43.813	46.821	10.007	34.24	-1.282	-6.91	50.566	0.099	0.001	0	748.49	12.4748	45.3	12.4	39.0	2.691	0.015	0.015	0.000	0.377	0.32
764	11/7/2002	3.42 36 AM	24.414	19.925	25.079	19.838	19.819	43.933	46.782	10.013	34.39	-1.282	-6.934	48.699	0.099	0.001	0	749.49	12.4894	45.3	11.9	39.2	2.700	0.015	0.015	0.000	0.376	0.32
765	11/7/2002	3.43 36 AM	24.419	19.933	25.109	19.912	19.873	44.149	46.732	10.004	34.283	-1.286	-6.937	48.749	0.099	0.001	0	750.49	12.5088	45.3	11.9	39.0	2.710	0.015	0.015	0.000	0.381	0.32
766	11/7/2002	3.44 36 AM	24.418	19.927	25.103	19.927	19.763	43.968	46.743	10.121	34.404	-1.282	-6.898	50.925	0.099	0.001	0	751.49	12.5248	45.3	12.5	39.2	2.701	0.015	0.015	0.000	0.376	0.32
767	11/7/2002	3.45 36 AM	24.422	19.921	25.112	19.901	19.777	44.002	47.036	10.059	34.369	-1.286	-6.931	48.695	0.099	0.001	0	752.49	12.5414	45.6	11.9	39.2	2.701	0.015	0.015	0.000	0.376	0.32
768	11/7/2002	3.46 36 AM	24.412	19.911	25.167	19.845	19.736	43.846	46.697	10.076	34.322	-1.286	-6.931	50.576	0.098	0.001	0	753.49	12.5581	45.2	12.4	39.1	2.695	0.015	0.015	0.000	0.372	0.32
769	11/7/2002	3.47 36 AM	24.401	19.924	25.108	19.824	19.744	44.149	47.189	10.115	34.476	-1.286	-6.937	48.749	0.098	0.001	0	754.49	12.5748	45.7	12.1	39.1	2.710	0.015	0.015	0.000	0.381	0.32
790	11/7/2002	3.48 36 AM	24.365	19.888	25.149	19.757	19.714	43.747	46.629	10.152	34.162	-1.282	-6.908	48.276	0.098	0.001	0	755.49	12.5914	45.6	11.8	39.0	2.686	0.015	0.015	0.000	0.374	0.32
791	11/7/2002	3.49 36 AM	24.389	19.888	25.204	19.721	19.713	44.012	47.063	10.194	34.22	-1.286	-6.928	48.687	0.098	0.001	0	756.49	12.6081	45.6	11.9	39.1	2.697	0.015	0.015	0.000	0.371	0.32
792	11/7/2002	3.50 36 AM	24.383	19.877	25.109	19.72	19.702	43.621	46.567	9.999	34.295	-1.286	-6.928	47.749	0.099	0.001	0	757.49	12.6248	45.1	11.7	39.0	2.686	0.015	0.015	0.000	0.378	0.32
793	11/7/2002	3.51 36 AM	24.387	19.875	25.105	19.686	19.681	43.952	46.597	10.020	34.312	-1.286	-6.948	48.017	0.098	0.001	0	758.49	12.6414	45.5	12.0	39.1	2.698	0.015	0.015	0.000	0.371	0.32
794	11/7/2002	3.52 36 AM	24.381	19.87	25.191	19.804	19.715	43.631	46.496	10.124	34.167	-1.286	-6.931	48.823	0.098	0.001	0	759.49	12.6581	45.0	12.0	39.0	2.682	0.015	0.015	0.000	0.374	0.32
795	11/7/2002	3.53 36 AM	24.39	19.849	25.125	19.798	19.684	44.149	47.022	10.086	34.594	-1.286	-6.939	48.301	0.099	0.001	0	760.49	12.6748	45.6	11.8	39.4	2.715	0.015	0.015	0.000	0.374	0.32
796	11/7/2002	3.54 36 AM	24.41	19.849	25.236	19.787	19.673	43.824	46.894	9.982	34.404	-1.286	-6.930	50.241	0.097	0.001	0	761.49	12.6914	45.4	12.3	39.1	2.697	0.014	0.014	0.000	0.367	0.31
797	11/7/2002	3.55 36 AM	24.425	19.853	25.205	19.823	19.678	43.710	46.771	10.301	33.943	-1.282	-6.937	48.899	0.097	0.001	0	762.49	12.7081	45.3	12.0	38.8	2.677	0.014	0.014	0.000	0.370	0.32
798	11/7/2002	3.56 36 AM	24.429	19.849	25.199	19.842	19.713	43.654	46.807	10.308	33.79	-1.286	-6.879	48.897	0.096	0.001	0	763.49	12.7248	45.0	12.1	38.9	2.670	0.014	0.014	0.000	0.369	0.32
799	11/7/2002	3.57 36 AM	24.444	19.848	25.294	19.802	19.733	43.681	46.836	10.213	34.074	-1.286	-6.939	49.991	0.096	0.001	0	764.49	12.7414	45.4	12.3	38.9	2.680	0.014	0.014	0.000	0.366	0.31
800	11/7/2002	3.58 36 AM	24.454	19.838	25.219	19.867	19.754	43.596	46.829	10.332	33.702	-1.282	-6.913	48.305	0.097	0.001	0	765.49	12.7581	45.4	11.8	38.6	2.665	0.014	0.014	0.000	0.372	0.32
801	11/7/2002	3.59 36 AM	24.448	19.822	25.249	19.776	19.748	43.621	46.637	10.282	33.896	-1.282	-6.922	49.303	0.095	0.001	0	766.49	12.7748	45.2	12.1	38.8	2.672	0.014	0.014	0.000	0.363	0.31
802	11/7/2002	4.00 36 AM	24.440	19.816	25.333	19.865	19.737	43.739	46.479	10.132	33.995	-1.286	-6.948	49.224	0.097	0.001	0	767.49	12.7914	45.3	12.1	38.9	2.680	0.014	0.014	0.000	0.369	0.31
803	11/7/2002	4.01 36 AM	24.448	19.801	25.363	19.818	19.737	43.167	46.298	10.033	33.695	-1.282	-6.912	49.756	0.095	0.001	0	768.49	12.8081	44.8	12.2	38.4	2.649	0.014	0.014	0.000	0.374	0.32
804	11/7/2002	4.02 36 AM	24.548	19.816	25.029	19.755	19.732	42.995	46.259	10.024	33.44	-1.286	-6.887	49.213	0.099	0.001	0	769.49	12.8248	44.8	12.1	38.2	2.635	0.014	0.014	0.000	0.370	0.32
805	11/7/2002	4.03 36 AM	24.577	19.81	26.447	19.774	19.706	43.401	46.42	9.636	34.07	-1.282	-6.91	49.872	0.098	0.001	0	770.49	12.8414	44.9	12.2	38.7	2.671	0.015	0.015	0.000	0.362	0.31
806	11/7/2002	4.04 36 AM	24.587	19.794	26.216	19.753	19.689	43.942	46.659	9.989	34.668	-1.286	-6.878	49.899	0.097	0.001	0	771.49	12.8581	45.1	12.1	38.7	2.688	0.015	0.015	0.000	0.369	0.32
807	11/7/2002	4.05 36 AM	24.686	19.798	25.16	19.757	19.709	43.44	46.637	9.774	34.097	-1.282	-6.844	48.406	0.097	0.001	0	772.49	12.8748	45.2	11.9	38.8	2.673	0.014	0.014	0.000	0.361	0.31
808	11/7/2002	4.06 36 AM	24.929	19.796	25.968	19.76	19.697	42.156	45.452	10.564	31.995	-1.279	-6.895	53.567	0.094	0.001	0	773.49	12.8914	44.0	13.1	37.1	2.556	0.014	0.014	0.000	0.368	0.31
809	11/7/2002	4.07 36 AM	24.968	19.795	25.787	19.744	19.691	49.448	45.97	5.77	44.191	-1.282	-6.666	34.624	0.119	0.001	0	774.49	12.9081	51.5	8.5	48.7	3.228	0.018	0.017	0.000	0.371	0.32
810	11/7/2002	4.08 36 AM	24.987	19.779	25.601	19.768	19.684	51.635	45.207	4.987	47.518	-1.286	-6.556	31.511	0.136	0.001	0	775.49	12.9248	52.7	7.7	49.7	3.425	0.020	0.020	0.000	0.368	0.34
811	11/7/2002	4.09 36 AM	24.947	19.793	25.205	19.782	19.679	51.684	45.436	5.271	47.416	-1.286	-6.907	29.927	0.133	0.001	0	776.49	12.9414	54.0	7.1	49.6	3.416	0.020	0.020	0.000	0.397	0.34
812	11/7/2002	4.10 36 AM	24.966	19.793	25.28	19.772	19.648	52.539	45.529	4.462	49.726	-1.282	-6.382	27.39	0.133	0.001	0	777.49	12.9581	53.8	6.7	50.6	3.491	0.020	0.020	0.000	0.389	0.33
813	11/7/2002	4.11 36 AM	24.91	19.761	25.144	19.731	19.642	43.791	46.283	9.934	34.476	-1.288	-6.184	50.547	0.112	0.001	0	778.49	12.9748	44.8	12.4	39.1	2.698	0.017	0.017	0.000	0.425	0.36
814	11/7/2002	4.12 36 AM	24.819	19.795	25.132	19.735	19.621	44.786	47.258	9.111	35.645	-1.286	-6.883	48.269	0.105	0.001	0	779.49	12.9914	45.6	11.8	40.2	2.722	0.016	0.016	0.000	0.398	0.33
815	11/7/2002	4.13 36 AM	24.804	19.715	25.172	19.749	19.615	44.299	47.475	9.062	35.179	-1.286	-6.907	46.036	0.094	0.001	0	780.49	13.0081	45.1	12.3	39.2	2.688	0.016	0.016	0.000	0.442	0.38
816	11/7/2002	4.14 36 AM	24.632	19.734	25.066	19.703	19.629	44.114	46.283	9.613	34.891	-1.282	-6.884	49.282	0.093	0.001	0	781.49	13.0248	44.8	12.1	39.5	2.724	0.014	0.014	0.000	0.350	0.30
817	11/7/2002	4.15 36 AM	24.591	19.738	25.1	19.626	19.542	44.867	47.063	9.502	35.88	-1.286	-6.925	48.464	0.093	0.001	0	782.49										

911	11/7/2002	5:53:46 AM	24.747	19.159	25.426	19.162	19.19	44.764	46.863	9.91	35.64	-1.282	-6.748	48.838	0.097	0.001	0	880.65	14.6776	45.4	12.0	40.2	2.772	0.014	0.000	0.355	0.30
912	11/7/2002	5:54:48 AM	24.707	19.158	25.366	19.167	19.2	45.013	47.227	9.878	35.86	-1.286	-6.835	48.267	0.098	0.001	0	881.65	14.6942	45.8	11.8	40.4	2.788	0.015	0.000	0.368	0.30
913	11/7/2002	5:55:46 AM	24.671	19.162	25.395	19.162	19.209	44.656	46.876	9.767	35.655	-1.279	-6.818	48.555	0.098	0.001	0	882.65	14.7109	45.3	11.9	40.2	2.769	0.015	0.000	0.360	0.31
914	11/7/2002	5:56:46 AM	24.641	19.162	25.28	19.212	19.204	45.039	46.979	9.413	35.57	-1.279	-6.839	47.653	0.1	0.001	0	883.65	14.7276	45.5	11.7	40.8	2.813	0.015	0.000	0.363	0.31
915	11/7/2002	5:57:46 AM	24.603	19.162	25.26	19.176	19.209	45.006	47.338	9.638	35.214	-1.282	-6.810	48.267	0.098	0.001	0	884.65	14.7442	45.8	11.9	40.6	2.788	0.015	0.000	0.363	0.31
916	11/7/2002	5:58:46 AM	24.57	19.151	25.269	19.166	19.183	45.164	47.469	9.561	35.263	-1.285	-6.821	47.491	0.097	0.001	0	885.65	14.7609	46.0	11.6	40.7	2.807	0.014	0.000	0.363	0.30
917	11/7/2002	5:59:46 AM	24.526	19.14	25.144	19.17	19.147	45.3	47.568	9.627	35.4	-1.286	-6.874	49.681	0.098	0.001	0	886.65	14.7776	45.1	12.2	40.9	2.816	0.015	0.000	0.366	0.30
918	11/7/2002	6:00:46 AM	24.478	19.139	25.163	19.124	19.121	44.776	46.896	9.706	35.136	-1.285	-6.835	47.923	0.099	0.001	0	887.65	14.7942	45.4	11.7	40.5	2.789	0.015	0.000	0.363	0.31
919	11/7/2002	6:01:46 AM	24.447	19.144	25.142	19.163	19.085	45.006	47.338	9.638	35.214	-1.282	-6.810	48.267	0.098	0.001	0	888.65	14.8109	45.9	11.8	40.6	2.807	0.015	0.000	0.368	0.30
920	11/7/2002	6:02:46 AM	24.406	19.132	25.055	19.172	19.088	44.733	47.171	9.438	35.7	-1.285	-6.821	48.225	0.099	0.001	0	889.65	14.8276	45.7	11.8	40.2	2.773	0.015	0.000	0.366	0.31
921	11/7/2002	6:03:46 AM	24.365	19.131	25.115	19.09	19.093	44.526	46.805	9.953	35.288	-1.282	-6.847	48.951	0.096	0.001	0	890.65	14.8442	45.3	12.0	39.9	2.751	0.014	0.000	0.367	0.30
922	11/7/2002	6:04:46 AM	24.36	19.136	25.064	19.146	19.129	44.814	47.274	9.865	35.503	-1.282	-6.863	48.195	0.096	0.001	0	891.65	14.8609	45.6	11.8	40.2	2.769	0.014	0.000	0.366	0.30
923	11/7/2002	6:05:46 AM	24.329	19.135	25.033	19.145	19.081	44.468	46.745	9.929	35.589	-1.282	-6.810	48.267	0.098	0.001	0	892.65	14.8776	45.3	11.8	39.9	2.752	0.014	0.000	0.363	0.30
924	11/7/2002	6:06:46 AM	24.309	19.11	25.093	19.104	19.086	44.283	46.565	10.094	34.916	-1.285	-6.881	49.505	0.096	0.001	0	893.65	14.8942	45.1	12.1	39.6	2.730	0.014	0.000	0.360	0.31
925	11/7/2002	6:07:46 AM	24.277	19.109	25.007	19.098	19.05	44.901	47.108	9.759	35.745	-1.286	-6.863	48.175	0.096	0.001	0	894.65	14.9109	45.9	11.8	39.6	2.780	0.014	0.000	0.365	0.30
926	11/7/2002	6:08:46 AM	24.272	19.104	25.032	19.073	19.06	44.462	46.811	9.967	35.464	-1.282	-6.863	49.217	0.096	0.001	0	895.65	14.9276	45.3	12.1	40.0	2.755	0.014	0.000	0.368	0.30
927	11/7/2002	6:09:46 AM	24.253	19.099	25.078	19.099	19.071	44.468	46.734	9.889	35.37	-1.282	-6.867	49.384	0.096	0.001	0	896.65	14.9442	45.3	12.1	39.9	2.753	0.014	0.000	0.368	0.30
928	11/7/2002	6:10:46 AM	24.227	19.098	24.977	19.144	19.09	44.489	47.404	9.903	35.204	-1.286	-6.812	48.983	0.096	0.001	0	897.65	14.9609	45.6	11.9	39.7	2.801	0.014	0.000	0.363	0.31
929	11/7/2002	6:11:46 AM	24.238	19.094	25.057	19.083	19.071	44.48	46.794	9.907	35.409	-1.279	-6.861	48.878	0.095	0.001	0	898.65	14.9776	45.3	12.0	39.9	2.754	0.014	0.000	0.364	0.30
930	11/7/2002	6:12:46 AM	24.248	19.1	25.083	19.104	19.066	44.362	46.465	9.889	35.209	-1.282	-6.867	47.993	0.095	0.001	0	899.65	14.9942	45.2	11.8	39.8	2.743	0.014	0.000	0.365	0.30
931	11/7/2002	6:13:46 AM	24.219	19.08	24.978	19.113	19.097	44.346	46.813	9.891	35.319	-1.285	-6.87	48.471	0.095	0.001	0	900.65	15.0109	45.3	11.9	39.8	2.746	0.014	0.000	0.366	0.30
932	11/7/2002	6:14:46 AM	24.209	19.08	25.058	19.095	19.062	43.973	46.201	10.111	34.774	-1.276	-6.831	49.22	0.094	0.001	0	901.65	15.0276	44.7	12.1	39.4	2.715	0.014	0.000	0.365	0.30
933	11/7/2002	6:15:46 AM	24.198	19.059	25.013	19.109	19.036	44.364	46.871	9.889	35.125	-1.285	-6.876	48.204	0.094	0.001	0	902.65	15.0442	45.4	11.8	39.7	2.740	0.014	0.000	0.362	0.30
934	11/7/2002	6:16:46 AM	24.178	19.064	24.983	19.099	19.061	43.944	46.443	10.051	34.707	-1.282	-6.572	49.429	0.093	0.001	0	903.65	15.0609	45.0	12.1	39.3	2.711	0.014	0.000	0.363	0.30
935	11/7/2002	6:17:46 AM	24.189	19.064	25.068	19.043	19.046	44.217	46.701	10.117	34.777	-1.285	-6.695	50.753	0.092	0.001	0	904.65	15.0776	45.2	12.4	39.5	2.723	0.014	0.000	0.347	0.29
936	11/7/2002	6:18:46 AM	24.189	19.069	25.008	19.099	19.026	44.221	46.773	10.051	34.932	-1.282	-6.678	49.429	0.092	0.001	0	905.65	15.0942	45.3	12.1	39.6	2.751	0.014	0.000	0.347	0.29
937	11/7/2002	6:19:46 AM	24.189	19.064	25.016	19.099	19.026	44.184	46.536	10.021	35.012	-1.282	-6.818	50.904	0.094	0.001	0	906.65	15.1109	45.1	12.5	39.6	2.730	0.014	0.000	0.354	0.30
938	11/7/2002	6:20:46 AM	24.163	19.049	25.078	19.099	19.005	44.319	46.401	10.076	34.924	-1.286	-6.868	48.207	0.094	0.001	0	907.65	15.1276	45.4	11.8	39.6	2.732	0.014	0.000	0.367	0.30
939	11/7/2002	6:21:46 AM	24.159	19.05	25.003	19.105	19.026	44.174	46.432	10.105	34.883	-1.285	-7.133	49.803	0.113	0.001	0	908.65	15.1442	45.0	12.2	39.5	2.725	0.017	0.000	0.426	0.36
940	11/7/2002	6:22:46 AM	24.155	19.05	25.059	19.024	19.027	44.437	46.45	10.145	34.969	-1.285	-7.243	50.084	0.09	0.001	0	909.65	15.1609	45.4	12.3	39.7	2.737	0.013	0.000	0.337	0.29
941	11/7/2002	6:23:46 AM	24.154	19.044	25.019	19.089	19.986	43.935	46.405	10.022	34.874	-1.282	-7.319	49.289	0.103	0.001	0	910.65	15.1776	45.9	12.1	39.3	2.710	0.015	0.000	0.344	0.29
942	11/7/2002	6:24:46 AM	24.193	19.034	25.093	19.038	19.005	44.433	46.958	9.606	35.464	-1.282	-7.099	49.557	0.095	0.001	0	911.65	15.1942	45.6	11.9	39.9	2.754	0.014	0.000	0.349	0.30
943	11/7/2002	6:25:46 AM	24.263	19.029	25.058	19.008	19.011	44.921	47.911	9.705	35.792	-1.285	-7.246	47.827	0.088	0.001	0	912.65	15.2109	46.0	11.7	40.4	2.782	0.013	0.000	0.320	0.27
944	11/7/2002	6:26:46 AM	24.354	19.034	25.479	19.054	19.036	44.414	46.895	9.647	35.491	-1.285	-7.787	48.219	0.095	0.001	0	913.65	15.2276	45.5	11.8	40.0	2.755	0.014	0.000	0.350	0.30
945	11/7/2002	6:27:46 AM	24.427	19.035	25.492	19.037	19.027	44.754	47.274	9.647	35.491	-1.285	-7.816	47.473	0.094	0.001	0	914.65	15.2442	45.6	12.1	40.4	2.764	0.014	0.000	0.349	0.30
946	11/7/2002	6:28:46 AM	24.395	19.025	25.369	19.014	19.027	45.257	47.525	9.515	36.793	-1.285	-7.167	47.363	0.097	0.001	0	915.65	15.2609	46.4	11.4	41.0	2.828	0.014	0.000	0.349	0.30
947	11/7/2002	6:29:46 AM	24.4	19.03	25.26	19.07	18.992	44.834	47.525	9.316	36.164	-1.286	-7.076	47.426	0.096	0.001	0	916.65	15.2776	46.1	11.6	40.5	2.792	0.014	0.000	0.351	0.30
948	11/7/2002	6:30:46 AM	24.39	19.02	25.204	19.044	18.966	45.059	47.677	9.323	36.332	-1.282	-7.122	45.639	0.097	0.001	0	917.65	15.2942	46.3	11.2	40.7	2.806	0.014	0.000	0.353	0.30
949	11/7/2002	6:31:46 AM	24.39	19.015	25.033	19.145	19.046	44.547	47.985	9.343	36.529	-1.282	-7.078	45.429	0.092	0.001	0	918.65	15.3109	45.4	11.5	40.1	2.824	0.014	0.000	0.351	0.29
950	11/7/2002	6:32:46 AM	24.37	19.01	25.12	19.07	18.941	44.768	47.312	9.494	35.98	-1.282	-7.078	46.956	0.094	0.001	0	919.65	15.3276	45.8	11.5	40.4	2.784	0.014	0.000	0.346	0.29
951	11/7/2002	6:33:46 AM	24.349	19.004	25.139	19.034	18.92	44.82	47.467	9.645	35.886	-1.279	-7.076	46.304	0.094	0.001	0	920.65	15.3442	46.0	11.8	40.4	2.782	0.014	0.000	0.360	0.30
952	11/7/2002	6:34:46 AM	24.319	18.998	25.108	18.963	19.909	45.067	47.303	9.406	36.271	-1.285	-7.248	47.768	0.096	0.001	0	921.65	15.3609	45.2	11.7	40.7	2.805	0.014	0.000	0.351	0.30
953																											

1041	11/7/2002	9:05:04 AM	24.562	18.991	25.366	19.254	19.453	45.331	47.27	10.079	36.281	-1.266	-6.748	49.536	0.101	0.001	0	1011.95	16.8659	45.8	12.1	40.8	2.813	0.015	0.015	0.000	0.365	0.31
1042	11/7/2002	9:06:04 AM	24.567	19.001	25.416	19.193	19.443	45.213	47.04	10.137	36.275	-1.262	-6.702	50.212	0.103	0.001	0	1012.95	16.8826	45.6	12.1	40.7	2.809	0.015	0.015	0.000	0.373	0.32
1043	11/7/2002	9:07:04 AM	24.573	19.007	25.432	19.29	19.454	45.537	47.463	9.99	36.574	-1.262	-6.728	48.427	0.101	0.001	0	1013.95	16.8992	46.0	11.9	41.1	2.831	0.015	0.015	0.000	0.362	0.31
1044	11/7/2002	9:08:04 AM	24.578	19.018	25.367	19.28	19.459	45.371	47.311	10.014	36.363	-1.263	-6.734	48.748	0.101	0.001	0	1014.95	16.9159	46.0	11.9	40.9	2.820	0.015	0.015	0.000	0.364	0.31
1045	11/7/2002	9:09:04 AM	24.574	19.025	25.433	19.27	19.459	45.213	47.111	10.044	36.191	-1.262	-6.719	49.316	0.106	0.009	0	1015.95	16.9326	45.6	11.9	40.7	2.805	0.015	0.015	0.000	0.368	0.30
1046	11/7/2002	9:10:04 AM	24.589	19.034	25.418	19.286	19.516	45.605	47.583	10.014	36.777	-1.279	-6.734	48.624	0.1	0.001	0	1016.95	16.9492	46.1	11.9	41.0	2.840	0.015	0.015	0.000	0.369	0.30
1047	11/7/2002	9:11:04 AM	24.6	19.029	25.404	19.246	19.551	45.151	47.072	10.087	36.216	-1.265	-6.688	47.472	0.099	0.001	0	1017.95	16.9659	45.6	11.9	40.7	2.805	0.015	0.015	0.000	0.369	0.31
1048	11/7/2002	9:12:04 AM	24.6	19.045	25.484	19.216	19.547	45.3	47.227	10.044	36.25	-1.262	-6.659	48.363	0.1	0.001	0	1018.95	16.9826	46.0	11.8	40.8	2.811	0.015	0.015	0.000	0.361	0.31
1049	11/7/2002	9:13:04 AM	24.586	19.061	25.41	19.296	19.578	45.245	47.101	10.132	36.23	-1.262	-6.708	49.316	0.099	0.001	0	1019.95	16.9992	45.7	11.8	40.7	2.808	0.015	0.015	0.000	0.368	0.30
1050	11/7/2002	9:14:04 AM	24.602	19.072	25.461	19.324	19.594	45.193	47.297	10.056	36.189	-1.262	-6.654	47.24	0.099	0.001	0	1020.95	17.0159	45.8	11.9	40.7	2.806	0.015	0.015	0.000	0.368	0.30
1051	11/7/2002	9:15:04 AM	24.608	19.083	25.487	19.401	19.605	45.081	47.400	10.169	36.038	-1.262	-6.74	49.327	0.098	0.001	0	1021.95	17.0326	45.6	12.1	40.6	2.796	0.015	0.015	0.000	0.365	0.30
1052	11/7/2002	9:16:04 AM	24.614	19.094	25.413	19.367	19.616	45.124	47.299	10.223	35.937	-1.262	-6.74	48.431	0.098	0.001	0	1022.95	17.0492	45.6	11.9	40.5	2.794	0.015	0.015	0.000	0.360	0.31
1053	11/7/2002	9:17:04 AM	24.625	19.105	25.479	19.262	19.630	45.108	47.026	9.986	36.295	-1.265	-6.788	47.688	0.098	0.001	0	1023.95	17.0659	45.5	11.9	40.7	2.806	0.015	0.015	0.000	0.364	0.30
1054	11/7/2002	9:18:04 AM	24.611	19.111	25.415	19.343	19.648	45.128	47.134	10.229	35.982	-1.262	-6.788	50.283	0.098	0.001	0	1024.95	17.0826	45.8	12.3	40.6	2.796	0.015	0.015	0.000	0.366	0.30
1055	11/7/2002	9:19:04 AM	24.602	19.112	25.366	19.334	19.67	45.093	47.136	10.02	36.256	-1.262	-6.728	49.285	0.098	0.001	0	1025.95	17.0992	45.7	12.1	40.7	2.804	0.015	0.015	0.000	0.366	0.30
1056	11/7/2002	9:20:04 AM	24.608	19.123	25.437	19.32	19.701	44.977	47.14	10.231	35.761	-1.262	-6.793	48.62	0.097	0.001	0	1026.95	17.1159	45.7	11.9	40.4	2.783	0.015	0.015	0.000	0.364	0.30
1057	11/7/2002	9:21:04 AM	24.584	19.129	25.263	19.351	19.692	45.127	47.146	10.087	36.295	-1.262	-6.74	48.178	0.097	0.001	0	1027.95	17.1326	45.7	12.1	40.7	2.806	0.015	0.015	0.000	0.363	0.30
1058	11/7/2002	9:22:04 AM	24.575	19.151	25.209	19.389	19.709	44.808	46.981	10.108	35.7	-1.279	-6.798	49.32	0.096	0.001	0	1028.95	17.1492	45.5	11.9	40.7	2.775	0.015	0.015	0.000	0.364	0.30
1059	11/7/2002	9:23:04 AM	24.546	19.141	25.174	19.388	19.719	44.634	46.84	9.959	35.833	-1.262	-6.746	48.186	0.094	0.001	0	1029.95	17.1659	45.4	12.1	40.2	2.774	0.015	0.015	0.000	0.347	0.29
1060	11/7/2002	9:24:04 AM	24.526	19.152	25.075	19.48	19.75	44.779	46.908	9.899	35.962	-1.265	-6.815	49.278	0.094	0.001	0	1030.95	17.1826	45.4	12.1	40.4	2.783	0.015	0.015	0.000	0.360	0.30
1061	11/7/2002	9:25:04 AM	24.495	19.151	25.094	19.448	19.753	44.675	46.949	10.014	35.636	-1.262	-6.812	48.341	0.095	0.001	0	1031.95	17.1992	45.5	12.1	40.2	2.769	0.015	0.015	0.000	0.362	0.30
1062	11/7/2002	9:26:04 AM	24.464	19.155	25.098	19.463	19.778	44.807	47.113	9.957	35.925	-1.262	-6.774	49.012	0.096	0.001	0	1032.95	17.2159	45.6	12.0	40.4	2.763	0.015	0.015	0.000	0.364	0.29
1063	11/7/2002	9:27:04 AM	24.453	19.164	25.022	19.644	19.818	44.613	46.678	9.896	35.869	-1.262	-6.821	48.264	0.094	0.001	0	1033.95	17.2326	45.2	12.1	40.2	2.774	0.015	0.015	0.000	0.348	0.30
1064	11/7/2002	9:28:04 AM	24.427	19.163	25.066	19.592	19.837	45.008	47.303	9.976	36.062	-1.265	-6.821	50.646	0.094	0.001	0	1034.95	17.2492	45.8	12.4	40.5	2.795	0.015	0.015	0.000	0.345	0.29
1065	11/7/2002	9:29:04 AM	24.391	19.167	25.045	19.47	19.866	44.693	46.945	9.953	35.91	-1.265	-6.815	49.073	0.094	0.001	0	1035.95	17.2659	45.5	12.0	40.2	2.775	0.015	0.015	0.000	0.348	0.30
1066	11/7/2002	9:30:04 AM	24.365	19.171	25.032	19.534	19.871	44.693	47.022	9.958	35.763	-1.279	-6.808	48.381	0.094	0.001	0	1036.95	17.2826	45.5	11.9	40.2	2.793	0.015	0.015	0.000	0.351	0.29
1067	11/7/2002	9:31:04 AM	24.366	19.193	25.065	19.394	19.866	45.126	47.512	9.983	36.107	-1.262	-6.76	48.525	0.094	0.001	0	1037.95	17.2992	46.0	11.9	40.6	2.800	0.015	0.015	0.000	0.344	0.29
1068	11/7/2002	9:32:04 AM	24.331	19.172	25.192	19.293	19.856	44.569	46.952	9.958	35.667	-1.265	-6.821	49.306	0.094	0.001	0	1038.95	17.3159	45.5	12.1	40.1	2.766	0.015	0.015	0.000	0.349	0.30
1069	11/7/2002	9:33:04 AM	24.322	19.194	24.991	19.4	19.877	44.571	46.871	9.979	35.61	-1.262	-6.824	49.28	0.093	0.001	0	1039.95	17.3326	45.4	12.1	40.1	2.764	0.015	0.015	0.000	0.346	0.29
1070	11/7/2002	9:34:04 AM	24.327	19.194	25.032	19.234	19.862	44.617	47.001	9.916	35.626	-1.268	-6.834	48.95	0.093	0.001	0	1040.95	17.3492	45.5	12.0	40.1	2.766	0.015	0.015	0.000	0.345	0.29
1071	11/7/2002	9:35:04 AM	24.328	19.201	24.978	19.301	19.874	44.942	47.351	9.931	36.109	-1.268	-6.798	47.972	0.091	0.001	0	1041.95	17.3659	45.5	11.8	40.5	2.794	0.015	0.015	0.000	0.356	0.29
1072	11/7/2002	9:36:04 AM	24.319	19.201	24.999	19.383	19.844	44.731	47.127	10.083	35.7	-1.262	-6.829	50.772	0.092	0.001	0	1042.95	17.3826	45.7	12.4	40.2	2.773	0.015	0.015	0.000	0.341	0.29
1073	11/7/2002	9:37:04 AM	24.32	19.212	25.055	19.364	19.84	44.439	46.881	10.142	35.323	-1.265	-6.838	49.993	0.092	0.001	0	1043.95	17.3992	45.4	12.3	39.9	2.750	0.015	0.015	0.000	0.343	0.29
1074	11/7/2002	9:38:04 AM	24.301	19.208	24.966	19.354	19.811	44.779	47.171	10.054	35.804	-1.265	-6.838	48.629	0.092	0.001	0	1044.95	17.4159	45.7	12.2	40.3	2.778	0.015	0.015	0.000	0.341	0.29
1075	11/7/2002	9:39:04 AM	24.328	19.212	25.055	19.364	19.811	44.538	47.078	10.048	35.466	-1.265	-6.798	48.652	0.091	0.001	0	1045.95	17.4326	45.5	11.9	40.2	2.768	0.015	0.015	0.000	0.346	0.29
1076	11/7/2002	9:40:04 AM	24.278	19.21	25.023	19.433	19.798	44.636	47.121	10.013	35.505	-1.265	-6.834	49.903	0.092	0.001	0	1046.95	17.4492	45.6	12.2	40.1	2.763	0.015	0.015	0.000	0.342	0.29
1077	11/7/2002	9:41:04 AM	24.347	19.23	25.012	19.431	19.827	44.811	47.148	10.174	35.432	-1.269	-															

1171	11/7/2002	10:18:41 AM	25.023	20.122	25.636	20.924	21.379	44.986	46.534	10.475	36.692	-1.288	-6.745	49.026	0.094	0.001	0	1145.57	19.0938	45.0	12.0	40.3	2.781	0.014	0.014	0.000	0.342	0.28
1172	11/7/2002	10:19:41 AM	25	20.155	25.499	21.002	21.387	45.106	46.563	10.524	36.755	-1.262	-6.751	49.696	0.094	0.001	0	1146.57	19.1095	45.1	12.2	40.4	2.788	0.014	0.014	0.000	0.342	0.28
1173	11/7/2002	10:20:41 AM	24.962	20.147	25.516	20.918	21.389	44.898	46.345	10.434	36.679	-1.265	-6.747	49.782	0.094	0.001	0	1147.57	19.1262	44.9	12.2	40.3	2.777	0.014	0.014	0.000	0.343	0.28
1174	11/7/2002	10:21:41 AM	24.95	20.16	25.449	20.982	21.397	45.059	46.556	10.495	36.691	-1.265	-6.745	50.474	0.094	0.001	0	1148.57	19.1428	45.1	12.4	40.4	2.783	0.014	0.014	0.000	0.343	0.29
1175	11/7/2002	10:22:41 AM	24.913	20.183	25.489	20.984	21.416	44.943	46.333	10.382	36.675	-1.265	-6.748	49.827	0.094	0.001	0	1149.57	19.1595	44.9	12.3	40.1	2.788	0.014	0.014	0.000	0.344	0.28
1176	11/7/2002	10:23:41 AM	24.92	20.196	25.494	21.088	21.433	44.903	46.405	10.537	36.797	-1.265	-6.749	49.505	0.094	0.001	0	1150.57	19.1762	44.9	12.1	40.2	2.788	0.014	0.014	0.000	0.344	0.28
1177	11/7/2002	10:24:41 AM	24.897	20.203	25.392	21.13	21.435	44.872	46.321	10.482	36.643	-1.265	-6.779	49.737	0.094	0.001	0	1151.57	19.1928	44.8	12.2	40.3	2.776	0.014	0.014	0.000	0.344	0.28
1178	11/7/2002	10:25:41 AM	24.885	20.2	25.419	20.966	21.437	45.112	46.685	10.515	36.808	-1.265	-6.780	49.84	0.094	0.001	0	1152.57	19.2095	45.2	12.2	40.5	2.790	0.014	0.014	0.000	0.342	0.29
1179	11/7/2002	10:26:41 AM	24.886	20.224	25.402	21.116	21.47	44.869	46.413	10.382	36.628	-1.265	-6.78	49.97	0.094	0.001	0	1153.57	19.2262	45.0	12.2	40.2	2.775	0.014	0.014	0.000	0.344	0.28
1180	11/7/2002	10:27:41 AM	24.87	20.216	25.334	21.103	21.452	45.565	47.288	10.18	36.999	-1.262	-6.726	50.13	0.094	0.001	0	1154.57	19.2428	45.7	12.3	41.1	2.832	0.014	0.014	0.000	0.338	0.29
1181	11/7/2002	10:28:41 AM	24.868	20.239	25.412	21.096	21.45	44.948	46.623	10.692	36.419	-1.262	-6.786	50.119	0.094	0.001	0	1155.57	19.2595	45.2	12.3	40.2	2.771	0.014	0.014	0.000	0.345	0.29
1182	11/7/2002	10:29:41 AM	24.866	20.252	25.365	21.149	21.458	45.093	46.778	10.474	36.91	-1.262	-6.786	49.981	0.094	0.001	0	1156.57	19.2762	45.2	12.2	40.5	2.789	0.014	0.014	0.000	0.343	0.29
1183	11/7/2002	10:30:41 AM	24.842	20.253	25.548	21.136	21.456	45.45	46.811	10.495	36.649	-1.265	-6.786	49.235	0.094	0.001	0	1157.57	19.2928	45.3	12.4	40.3	2.780	0.014	0.014	0.000	0.344	0.29
1184	11/7/2002	10:31:41 AM	24.844	20.261	25.384	21.188	21.497	44.7	46.244	10.51	36.44	-1.265	-6.792	50.612	0.094	0.001	0	1158.57	19.3095	44.8	12.4	40.1	2.783	0.014	0.014	0.000	0.346	0.29
1185	11/7/2002	10:32:41 AM	24.847	20.283	25.316	21.326	21.53	44.901	46.589	10.51	36.544	-1.265	-6.789	50.696	0.094	0.001	0	1159.57	19.3262	45.1	12.4	40.2	2.773	0.014	0.014	0.000	0.345	0.29
1186	11/7/2002	10:33:41 AM	24.813	20.29	25.362	21.242	21.526	45.033	46.503	10.482	36.831	-1.265	-6.777	50.312	0.094	0.001	0	1160.57	19.3428	45.0	12.3	40.4	2.788	0.014	0.014	0.000	0.347	0.30
1187	11/7/2002	10:34:41 AM	24.82	20.307	25.37	21.35	21.549	45.044	46.832	10.486	36.733	-1.265	-6.755	49.876	0.095	0.001	0	1161.57	19.3595	45.4	12.2	40.4	2.786	0.014	0.014	0.000	0.347	0.30
1188	11/7/2002	10:35:41 AM	24.823	20.319	25.307	21.418	21.601	44.824	46.561	10.368	36.462	-1.265	-6.798	50.111	0.095	0.001	0	1162.57	19.3762	45.0	12.2	40.1	2.788	0.014	0.014	0.000	0.350	0.30
1189	11/7/2002	10:36:41 AM	24.835	20.332	25.384	21.319	21.588	44.696	46.323	10.58	36.272	-1.268	-6.798	50.272	0.095	0.001	0	1163.57	19.3928	44.9	12.3	40.0	2.785	0.014	0.014	0.000	0.351	0.30
1190	11/7/2002	10:37:41 AM	24.833	20.355	25.337	21.393	21.601	44.834	46.688	10.669	36.254	-1.265	-6.792	50.639	0.095	0.001	0	1164.57	19.4095	45.2	12.4	40.0	2.761	0.014	0.014	0.000	0.350	0.30
1191	11/7/2002	10:38:41 AM	24.814	20.358	25.529	21.319	21.588	44.805	46.312	10.5	36.333	-1.265	-6.792	50.297	0.095	0.001	0	1165.57	19.4262	44.8	12.3	40.0	2.786	0.014	0.014	0.000	0.351	0.30
1192	11/7/2002	10:39:41 AM	24.796	20.384	25.368	21.346	21.55	44.844	46.259	10.488	36.464	-1.265	-6.719	50.742	0.095	0.001	0	1166.57	19.4428	44.9	12.4	40.1	2.762	0.014	0.014	0.000	0.350	0.30
1193	11/7/2002	10:40:41 AM	24.789	20.371	25.303	21.429	21.572	44.841	46.792	10.503	36.425	-1.268	-6.79	51.35	0.095	0.001	0	1167.57	19.4595	45.3	12.6	40.1	2.767	0.014	0.014	0.000	0.350	0.30
1194	11/7/2002	10:41:41 AM	24.79	20.388	25.365	21.355	21.539	44.532	46.244	10.543	36.229	-1.265	-6.821	50.994	0.095	0.001	0	1168.57	19.4762	44.8	12.5	39.9	2.750	0.014	0.014	0.000	0.352	0.30
1195	11/7/2002	10:42:41 AM	24.818	20.416	25.403	21.469	21.566	44.76	46.648	10.589	36.276	-1.262	-6.821	49.974	0.095	0.001	0	1169.57	19.4928	45.2	12.2	40.0	2.789	0.014	0.014	0.000	0.350	0.30
1196	11/7/2002	10:43:41 AM	24.82	20.432	25.514	21.471	21.548	44.843	46.743	10.596	36.461	-1.268	-6.819	49.861	0.095	0.001	0	1170.57	19.5095	45.3	12.2	40.2	2.767	0.014	0.014	0.000	0.350	0.30
1197	11/7/2002	10:44:41 AM	24.806	20.419	25.391	21.331	21.56	44.729	46.623	10.468	36.45	-1.265	-6.829	50.237	0.095	0.001	0	1171.57	19.5262	45.2	12.3	40.1	2.784	0.014	0.014	0.000	0.349	0.30
1198	11/7/2002	10:45:41 AM	24.818	20.431	25.343	21.444	21.597	44.7	46.753	10.561	36.182	-1.265	-6.821	50.53	0.095	0.001	0	1172.57	19.5428	45.3	12.4	39.9	2.754	0.014	0.014	0.000	0.351	0.30
1199	11/7/2002	10:46:41 AM	25.006	20.494	25.386	21.517	21.665	7.338	46.606	10.576	-2.364	33.341	80.099	50.746	0.001	0.001	0	1176.72	19.612	45.1	12.4	2.5	0.172	0.000	0.000	0.000	0.059	0.05
1200	11/7/2002	10:49:50 AM	24.362	20.512	25.453	21.519	21.678	7.226	46.778	10.597	-2.416	33.44	81.001	50.992	0.001	0.001	0	1177.72	19.6287	45.0	12.5	4.0	0.166	0.000	0.000	0.000	0.061	0.05
1201	11/7/2002	10:52:41 AM	25.546	20.514	25.38	21.617	21.714	38.294	46.372	10.642	38.711	-1.88	-1.978	50.113	0.112	0.001	0	1178.72	19.6453	45.1	12.3	33.5	2.017	0.017	0.017	0.000	0.463	0.42
1202	11/7/2002	10:53:41 AM	25.667	20.535	25.456	21.573	21.746	38.716	46.631	10.473	29.386	1.741	2.077	49.186	0.116	0.001	0	1179.25	19.6542	45.2	12.1	34.1	2.348	0.017	0.017	0.000	0.501	0.43
1203	11/7/2002	10:55:41 AM	25.784	20.547	25.392	21.71	21.768	38.503	46.664	10.666	28.737	1.837	2.17	51.921	0.112	0.001	0	1180.25	19.6709	45.2	12.2	33.6	2.318	0.017	0.017	0.000	0.491	0.42
1204	11/7/2002	10:56:41 AM	25.786	20.558	25.444	21.682	21.784	38.393	46.376	10.622	28.93	1.886	2.312	50.637	0.109	0.001	0	1181.25	19.6876	44.9	12.4	33.7	2.321	0.013	0.013	0.000	0.394	0.34
1205	11/7/2002	10:57:41 AM	25.699	20.569	25.386	21.727	21.812	38.282	46.511	10.608	28.929	1.838	2.407	49.251	0.109	0.001	0	1182.25	19.7042	45.0	11.9	33.5	2.307	0.017	0.017	0.000	0.392	0.34
1206	11/7/2002	10:58:41 AM	25.606	20.599	25.384	21.727	21.81	38.213	46.473	10.625	28.533	2.074	2.312	51.919	0.098	0.001	0	1183.25	19.7209	45.0	12.7	33.4	2.301	0.015	0.015	0.000	0.433	0.37
1207	11/7/2002	10:59:41 AM	25.608	20.601	25.446	21.719	21.801	38.072	46																			

1301	11/7/2002	12:33:01 PM	25.527	22.131	25.566	23.834	23.445	45.317	46.801	10.574	35.966	-1.286	-6.774	49.215	0.092	0.001	0	1279.90	21.3317	45.3	12.1	40.6	2.802	0.014	0.014	0.000	0.332	0.28
1302	11/7/2002	12:34:01 PM	25.542	22.152	25.642	23.885	23.465	45.305	47.03	10.465	36.07	-1.286	-6.776	50.123	0.092	0.001	0	1280.00	21.3484	45.6	12.3	40.7	2.805	0.014	0.014	0.000	0.331	0.28
1303	11/7/2002	12:35:01 PM	25.544	22.164	25.649	23.907	23.507	45.228	46.9	10.496	35.919	-1.291	-6.771	49.253	0.092	0.001	0	1281.90	21.3651	45.4	12.1	40.6	2.797	0.014	0.014	0.000	0.333	0.28
1304	11/7/2002	12:36:01 PM	25.545	22.175	25.657	23.908	23.509	45.307	46.895	10.473	36.132	-1.291	-6.776	48.848	0.092	0.001	0	1282.90	21.3817	45.4	12.0	40.7	2.807	0.014	0.014	0.000	0.330	0.28
1305	11/7/2002	12:37:01 PM	25.572	22.192	25.674	23.944	23.524	45.111	46.14	10.52	36.181	-1.286	-6.776	49.878	0.093	0.001	0	1283.90	21.3984	45.5	12.3	40.5	2.790	0.014	0.014	0.000	0.332	0.28
1306	11/7/2002	12:38:01 PM	25.594	22.204	25.678	23.997	23.547	45.238	46.952	10.584	35.753	-1.291	-6.751	49.878	0.093	0.001	0	1284.90	21.4151	45.5	12.2	40.5	2.792	0.014	0.014	0.000	0.334	0.28
1307	11/7/2002	12:39:01 PM	25.642	22.231	25.636	24.009	23.555	45.228	46.987	10.536	35.864	-1.291	-6.737	50.9	0.092	0.001	0	1285.90	21.4317	45.5	12.5	40.5	2.796	0.014	0.014	0.000	0.329	0.28
1308	11/7/2002	12:40:01 PM	25.684	22.244	25.983	24.067	23.577	45.062	46.931	10.583	35.491	-1.291	-6.751	50.939	0.092	0.001	0	1286.90	21.4484	45.5	12.5	40.3	2.777	0.014	0.014	0.000	0.331	0.28
1309	11/7/2002	12:41:01 PM	25.731	22.268	25.89	24.054	23.588	45.549	48.395	9.29	35.989	-1.286	-6.768	48.441	0.097	0.001	0	1287.90	21.4651	45.9	11.4	42.5	2.831	0.014	0.014	0.000	0.332	0.28
1310	11/7/2002	12:42:01 PM	25.753	22.278	25.762	24.111	23.621	46.698	48.274	9.291	35.515	-1.291	-6.702	47.013	0.097	0.001	0	1288.90	21.4817	47.1	11.5	42.6	2.939	0.014	0.014	0.000	0.332	0.28
1311	11/7/2002	12:43:01 PM	25.755	22.29	25.714	24.158	23.633	45.818	47.673	10.003	37.006	-1.288	-6.763	49.391	0.09	0.001	0	1289.90	21.4984	46.2	12.1	41.4	2.855	0.014	0.014	0.000	0.318	0.27
1312	11/7/2002	12:44:01 PM	25.752	22.312	25.727	24.135	23.621	45.901	47.721	9.549	37.526	-1.288	-6.716	48.878	0.094	0.001	0	1290.90	21.5151	46.2	12.0	41.7	2.876	0.014	0.014	0.000	0.329	0.28
1313	11/7/2002	12:45:01 PM	25.739	22.325	25.614	24.172	23.638	45.978	47.885	9.719	37.441	-1.288	-6.728	48.032	0.093	0.001	0	1291.90	21.5317	46.4	11.8	41.7	2.876	0.014	0.014	0.000	0.327	0.28
1314	11/7/2002	12:46:01 PM	25.745	22.355	25.639	24.218	23.683	46.191	48.199	9.732	37.53	-1.285	-6.728	47.955	0.093	0.001	0	1292.90	21.5484	46.7	11.8	41.9	2.886	0.014	0.014	0.000	0.325	0.28
1315	11/7/2002	12:47:01 PM	25.722	22.363	25.697	24.216	23.736	45.942	47.81	9.732	37.442	-1.288	-6.728	48.397	0.094	0.001	0	1293.90	21.5651	46.3	11.9	41.7	2.875	0.014	0.014	0.000	0.331	0.28
1316	11/7/2002	12:48:01 PM	25.725	22.391	25.634	24.269	23.769	45.708	47.814	9.81	37.098	-1.288	-6.763	48.487	0.092	0.001	0	1294.90	21.5817	46.1	11.9	41.4	2.865	0.014	0.014	0.000	0.326	0.28
1317	11/7/2002	12:49:01 PM	25.712	22.403	25.676	24.286	23.786	45.862	47.625	9.838	37.258	-1.288	-6.771	48.71	0.091	0.001	0	1295.90	21.5984	46.4	11.9	41.6	2.865	0.014	0.014	0.000	0.321	0.27
1318	11/7/2002	12:50:01 PM	25.671	22.426	25.484	24.293	23.789	46.021	47.967	9.697	37.493	-1.288	-6.763	47.791	0.092	0.001	0	1296.90	21.6151	46.5	11.9	41.6	2.865	0.014	0.014	0.000	0.328	0.28
1319	11/7/2002	12:51:01 PM	25.677	22.438	25.501	24.27	23.826	46.061	48.091	9.406	37.782	-1.288	-6.766	47.147	0.093	0.001	0	1297.90	21.6317	46.6	11.6	41.9	2.890	0.014	0.014	0.000	0.326	0.28
1320	11/7/2002	12:52:01 PM	25.664	22.44	25.488	24.317	23.843	45.905	47.829	9.65	37.493	-1.291	-6.776	48.854	0.092	0.001	0	1298.90	21.6484	46.4	12.0	41.7	2.875	0.014	0.014	0.000	0.324	0.28
1321	11/7/2002	12:53:01 PM	25.65	22.468	25.399	24.304	23.849	46.083	48.215	9.69	37.495	-1.294	-6.777	46.529	0.092	0.001	0	1299.90	21.6651	46.7	11.4	41.8	2.881	0.014	0.014	0.000	0.325	0.28
1322	11/7/2002	12:54:01 PM	25.642	22.478	25.471	24.281	23.831	45.853	47.781	9.697	37.34	-1.288	-6.774	47.46	0.092	0.001	0	1300.90	21.6817	46.3	11.6	41.6	2.888	0.014	0.014	0.000	0.325	0.28
1323	11/7/2002	12:55:01 PM	25.64	22.506	25.404	24.313	23.854	45.915	48.027	9.625	37.2	-1.291	-6.776	47.529	0.091	0.001	0	1301.90	21.6984	46.6	11.6	41.6	2.865	0.014	0.014	0.000	0.323	0.27
1324	11/7/2002	12:56:01 PM	25.627	22.523	25.416	24.31	23.871	45.988	48.036	9.661	37.606	-1.288	-6.777	46.441	0.091	0.001	0	1302.90	21.7151	46.6	11.4	41.8	2.882	0.014	0.014	0.000	0.321	0.27
1325	11/7/2002	12:57:01 PM	25.623	22.535	25.432	24.327	23.898	46.025	48.201	9.543	37.647	-1.285	-6.769	47.451	0.092	0.001	0	1303.90	21.7317	46.7	11.6	41.8	2.884	0.014	0.014	0.000	0.324	0.28
1326	11/7/2002	12:58:01 PM	25.626	22.545	25.434	24.332	23.915	46.255	48.345	9.491	37.666	-1.285	-6.776	47.455	0.092	0.001	0	1304.90	21.7484	46.9	11.6	41.9	2.886	0.014	0.014	0.000	0.325	0.28
1327	11/7/2002	12:59:01 PM	25.686	22.563	25.381	24.335	23.941	46.448	48.526	9.245	38.339	-1.291	-6.744	46.111	0.092	0.001	0	1305.90	21.7651	47.1	11.3	42.4	2.923	0.014	0.014	0.000	0.320	0.27
1328	11/7/2002	12:00:01 PM	25.607	22.628	25.541	23.367	23.073	38.586	46.784	10.368	29.362	2.004	-2.242	50.415	0.074	0.001	0	1246.90	20.7817	45.3	12.4	34.0	2.342	0.011	0.011	0.000	0.320	0.27
1329	11/7/2002	12:01:01 PM	25.606	22.641	25.549	23.355	23.126	38.737	46.964	10.375	29.378	-1.996	-2.436	49.815	0.082	0.001	0	1247.90	20.7984	45.5	12.2	34.1	2.346	0.012	0.012	0.000	0.353	0.30
1330	11/7/2002	12:02:01 PM	25.637	22.673	25.491	23.428	23.133	38.25	46.925	10.511	29.012	2.097	-2.48	49.972	0.081	0.001	0	1248.90	20.8151	45.0	12.2	33.6	2.319	0.012	0.012	0.000	0.354	0.30
1331	11/7/2002	12:03:01 PM	25.735	22.686	25.534	23.335	23.141	41.907	48.621	9.498	35.568	-1.288	-6.781	46.371	0.128	0.001	0	1249.90	20.8317	45.5	12.3	40.2	2.774	0.019	0.019	0.000	0.463	0.38
1332	11/7/2002	12:04:01 PM	25.576	22.672	25.44	23.316	23.097	45.522	46.988	10.348	36.515	-1.291	-6.781	50.446	0.109	0.001	0	1250.90	20.8484	45.4	12.4	41.0	2.828	0.016	0.016	0.000	0.391	0.33
1333	11/7/2002	12:05:01 PM	25.533	22.71	25.477	23.323	23.115	45.698	46.887	10.33	36.515	-1.288	-6.834	49.792	0.109	0.001	0	1251.90	20.8651	45.4	12.2	41.1	2.834	0.016	0.016	0.000	0.390	0.33
1334	11/7/2002	12:06:01 PM	25.501	22.722	25.51	23.401	23.117	45.878	47.011	10.245	36.826	-1.288	-6.558	50.709	0.102	0.001	0	1252.90	20.8817	45.5	12.4	41.4	2.851	0.015	0.015	0.000	0.363	0.31
1335	11/7/2002	12:07:01 PM	25.465	22.739	25.442	23.443	23.114	45.959	47.12	10.259	37.39	-1.288	-6.774	49.215	0.102	0.001	0	1253.90	20.8984	45.7	12.1	41.6	2.859	0.014	0.014	0.000	0.325	0.28
1336	11/7/2002	12:08:01 PM	25.474	22.766	25.514	23.455	23.114	45.878	47.011	10.245	36.707	-1.288	-6.558	50.26	0.102	0.001	0	1254.90	20.9151	45.4	12.3	41.2	2.840	0.015	0.015	0.000	0.364	0.31
1337	11/7/2002	12:09:01 PM	25.467	22.774	25.461	23.493	23.174	45.901	46.994	10.345	36.805	-1.288	-6.683	50.061	0.099	0.001	0	1255.90	20.9317	45.4	12.3	41.4	2.851	0.015	0.015	0.000	0.362	0.30
1338	11/7/2002	12:10:01 PM	25.448	22.779	25.447	23.489	23.195	45.592	46.753	10.198	36.521	-1.285	-6.693	50.111	0.099	0.001	0	1256.90	20.9484	45.3	12.3	41.1	2.831	0.015	0.015	0.000	0.355	0.30
1339	11/7/2002	12:11:01 PM	25.451	22.785	25.514	23.492	23.188	45.619	46.811	10.269	36.453	-1.288	-6.778	49.537	0.098	0.001	0	1257.90	20.9651	45.3	12.3	41.0	2.829	0.015	0.015	0.000	0.351	0.29
1340	11/7/2002	12:12:01 PM	25.448	22.813	25.427	23.459	23.184	45.936	47.229	10.278	36.875	-1.288	-6.693	49.312	0.099	0.001	0	1258.90	20.9817	45.8	12.1	41.4	2.855	0.015	0.015	0.000	0.352	0.30
1341	11/7/2002	12:13:01 PM	25.44																									

1431	11/7/2002	1:43:01 PM	25.862	23.252	25.526	25.167	24.568	44.93	47.562	10.307	35.769	-1.291	-6.888	50.094	0.083	0.001	0	1349.90	22.4984	46.3	12.3	40.3	2.782	0.012	0.002	0.000	0.302	0.26
1432	11/7/2002	1:44:01 PM	25.868	23.283	25.613	25.169	24.595	44.918	47.564	10.175	35.78	-1.286	-6.844	49.823	0.085	0.001	0	1350.90	22.5151	46.1	12.2	40.3	2.778	0.013	0.002	0.000	0.309	0.26
1433	11/7/2002	1:45:01 PM	25.865	23.275	25.639	25.227	24.626	44.954	47.444	10.264	35.645	-1.291	-6.853	49.182	0.084	0.001	0	1351.90	22.5317	46.0	12.1	40.1	2.768	0.013	0.002	0.000	0.307	0.26
1434	11/7/2002	1:46:01 PM	25.846	23.286	25.626	25.237	24.643	44.924	47.309	10.241	35.389	-1.291	-6.895	49.534	0.084	0.001	0	1352.90	22.5484	45.8	12.1	40.0	2.755	0.013	0.002	0.000	0.309	0.26
1435	11/7/2002	1:47:01 PM	25.865	23.319	25.626	25.246	24.665	44.963	47.171	10.264	35.362	-1.291	-6.884	49.219	0.084	0.001	0	1353.90	22.5651	45.9	12.1	39.9	2.746	0.013	0.002	0.000	0.309	0.26
1436	11/7/2002	1:48:01 PM	25.865	23.336	25.52	25.346	24.682	44.72	47.46	10.211	35.751	-1.291	-6.895	49.045	0.083	0.001	0	1354.90	22.5817	46.0	11.8	40.2	2.774	0.012	0.002	0.000	0.303	0.26
1437	11/7/2002	1:49:01 PM	25.866	23.341	25.581	25.317	24.688	44.633	47.479	10.271	35.499	-1.291	-6.899	49.264	0.083	0.001	0	1355.90	22.5984	46.0	12.1	40.1	2.762	0.012	0.002	0.000	0.304	0.26
1438	11/7/2002	1:50:01 PM	25.866	23.352	25.551	25.262	24.708	44.66	47.496	10.31	35.44	-1.288	-6.895	49.767	0.083	0.001	0	1356.90	22.6151	46.0	12.2	40.0	2.761	0.012	0.002	0.000	0.304	0.26
1439	11/7/2002	1:51:01 PM	25.867	23.372	25.538	25.252	24.733	44.668	47.491	10.284	35.252	-1.291	-6.895	49.349	0.083	0.001	0	1357.90	22.6317	45.9	12.1	39.9	2.746	0.012	0.002	0.000	0.306	0.26
1440	11/7/2002	1:52:01 PM	25.869	23.379	25.583	25.269	24.735	44.687	47.586	10.309	35.602	-1.291	-6.899	49.673	0.083	0.001	0	1358.90	22.6484	46.0	12.2	40.1	2.761	0.012	0.002	0.000	0.303	0.26
1441	11/7/2002	1:53:01 PM	25.868	23.405	25.534	25.305	24.741	44.683	47.508	10.291	35.485	-1.288	-6.895	49.043	0.083	0.001	0	1359.90	22.6651	46.0	12.0	40.1	2.764	0.012	0.002	0.000	0.304	0.26
1442	11/7/2002	1:54:01 PM	25.866	23.417	25.586	25.302	24.728	44.663	47.554	10.271	35.493	-1.288	-6.899	49.234	0.083	0.001	0	1360.90	22.6817	46.1	12.1	40.1	2.763	0.012	0.002	0.000	0.304	0.26
1443	11/7/2002	1:55:01 PM	25.896	23.432	25.596	25.402	24.738	44.49	47.364	10.265	35.321	-1.285	-6.8	49.251	0.083	0.001	0	1361.90	22.6984	45.8	12.3	39.9	2.751	0.012	0.002	0.000	0.305	0.26
1444	11/7/2002	1:56:01 PM	25.891	23.442	25.536	25.387	24.758	44.743	47.647	10.25	35.957	-1.288	-6.888	51.422	0.083	0.001	0	1362.90	22.7151	46.2	12.6	40.2	2.770	0.012	0.002	0.000	0.303	0.26
1445	11/7/2002	1:57:01 PM	25.886	23.457	25.601	25.387	24.758	44.451	47.101	10.237	35.329	-1.291	-6.855	50.017	0.083	0.001	0	1363.90	22.7317	45.9	12.3	39.9	2.750	0.012	0.002	0.000	0.305	0.26
1446	11/7/2002	1:58:01 PM	25.902	23.479	25.636	25.398	24.774	44.575	47.402	10.275	35.464	-1.288	-6.881	49.329	0.083	0.001	0	1364.90	22.7484	45.9	12.1	40.0	2.759	0.012	0.002	0.000	0.305	0.26
1447	11/7/2002	1:59:01 PM	25.907	23.494	25.592	25.383	24.811	44.263	47.2	10.242	35.245	-1.291	-6.951	48.578	0.082	0.001	0	1365.90	22.7651	45.8	11.9	39.8	2.742	0.012	0.002	0.000	0.302	0.26
1448	11/7/2002	2:00:01 PM	25.924	23.525	25.614	25.43	24.851	44.515	47.504	10.319	35.303	-1.288	-6.895	49.373	0.083	0.001	0	1366.90	22.7817	45.9	12.1	40.0	2.761	0.012	0.002	0.000	0.306	0.26
1449	11/7/2002	2:01:01 PM	25.93	23.521	25.619	25.425	24.857	44.704	47.477	10.306	35.575	-1.291	-6.899	49.266	0.082	0.001	0	1366.90	22.7823	46.2	12.1	40.1	2.767	0.012	0.002	0.000	0.299	0.26
1450	11/7/2002	2:02:01 PM	25.927	23.533	25.556	25.498	24.894	44.437	47.434	10.252	35.366	-1.291	-6.899	48.957	0.083	0.001	0	1367.90	22.7989	46.0	12.0	39.9	2.751	0.012	0.002	0.000	0.305	0.26
1451	11/7/2002	2:03:01 PM	25.933	23.55	25.628	25.424	24.92	44.6	47.481	10.303	35.45	-1.291	-6.899	49.115	0.083	0.001	0	1368.90	22.8156	46.0	12.0	40.0	2.760	0.012	0.002	0.000	0.304	0.26
1452	11/7/2002	2:04:01 PM	25.96	23.581	25.589	25.411	24.942	44.489	47.332	10.277	35.509	-1.291	-6.897	49.436	0.082	0.001	0	1369.90	22.8323	45.9	12.1	39.9	2.752	0.012	0.002	0.000	0.302	0.26
1453	11/7/2002	2:05:01 PM	25.94	23.587	25.6	25.431	24.922	44.321	47.305	10.246	35.245	-1.291	-6.909	49.343	0.083	0.001	0	1370.90	22.8489	45.8	12.1	39.8	2.743	0.012	0.002	0.000	0.306	0.26
1454	11/7/2002	2:06:01 PM	25.943	23.616	25.664	25.405	24.981	44.393	47.493	10.304	35.088	-1.288	-6.898	49.322	0.082	0.001	0	1371.90	22.8656	46.0	12.1	39.7	2.740	0.012	0.002	0.000	0.302	0.26
1455	11/7/2002	2:07:01 PM	25.963	23.634	25.592	25.458	25.02	44.598	47.643	10.412	35.251	-1.291	-6.909	49.306	0.082	0.001	0	1372.90	22.8823	46.2	12.1	39.9	2.762	0.012	0.002	0.000	0.301	0.26
1456	11/7/2002	2:08:01 PM	25.965	23.652	25.579	25.501	25.058	44.476	47.481	10.266	35.321	-1.291	-6.899	49.366	0.082	0.001	0	1373.90	22.8989	45.7	11.8	39.7	2.738	0.012	0.002	0.000	0.301	0.26
1457	11/7/2002	2:09:01 PM	25.979	23.676	25.629	25.5	25.071	44.522	47.533	10.373	35.251	-1.288	-6.895	48.484	0.082	0.001	0	1374.90	22.9156	46.1	11.4	39.9	2.750	0.012	0.002	0.000	0.301	0.26
1458	11/7/2002	2:10:01 PM	25.971	23.683	25.646	25.567	25.049	44.52	47.707	10.315	35.29	-1.291	-6.806	49.289	0.082	0.001	0	1375.90	22.9323	46.2	12.1	39.9	2.751	0.012	0.002	0.000	0.301	0.26
1459	11/7/2002	2:11:01 PM	25.96	23.687	25.69	25.576	25.052	44.418	47.485	10.273	35.299	-1.291	-6.803	49.668	0.082	0.001	0	1376.90	22.9489	46.0	12.2	39.9	2.746	0.012	0.002	0.000	0.301	0.26
1460	11/7/2002	2:12:01 PM	25.967	23.689	25.587	25.518	25.044	44.638	47.631	10.326	35.423	-1.284	-6.903	49.958	0.082	0.001	0	1377.90	22.9656	46.4	12.2	40.0	2.760	0.012	0.002	0.000	0.300	0.26
1461	11/7/2002	2:13:01 PM	25.985	23.722	25.669	25.541	25.037	44.517	47.456	10.319	35.382	-1.291	-6.899	49.217	0.082	0.001	0	1378.90	22.9823	46.1	12.1	39.9	2.754	0.012	0.002	0.000	0.300	0.26
1462	11/7/2002	2:14:01 PM	25.987	23.734	25.647	25.568	25.054	44.261	47.421	10.299	35.17	-1.291	-6.806	49.922	0.082	0.001	0	1379.90	22.9989	45.9	11.9	39.7	2.739	0.012	0.002	0.000	0.302	0.26
1463	11/7/2002	2:15:01 PM	25.989	23.751	25.669	25.525	25.072	44.677	47.882	10.367	35.372	-1.291	-6.796	48.578	0.082	0.001	0	1380.90	23.0156	46.4	11.9	40.0	2.760	0.012	0.002	0.000	0.300	0.26
1464	11/7/2002	2:16:01 PM	26.007	23.784	25.711	25.542	25.064	44.217	47.388	10.262	35.09	-1.291	-6.803	48.106	0.082	0.001	0	1381.90	23.0323	46.5	11.8	39.7	2.734	0.012	0.002	0.000	0.302	0.26
1465	11/7/2002	2:17:01 PM	26.000	23.777	25.734	25.675	25.096	44.244	47.401	10.295	35.082	-1.291	-6.803	48.303	0.082	0.001	0	1382.90	23.0489	46.3	11.9	39.8	2.748	0.012	0.002	0.000	0.302	0.26
1466	11/7/2002	2:18:01 PM	26.015	23.792	25.715	25.626	25.108	44.474	47.686	10.336	35.231	-1.288	-6.9	48.159	0.082	0.001	0	1383.90	23.0656	46.2	11.8	39.9	2.748	0.012	0.002	0.000	0.301	0.26
1467	11/7/2002	2:19:01 PM	26.016	23.793	25.666	25.587	25.123	44.339	47.444	10.3	35.17	-1.291	-6.8	48.93	0.082	0.001	0	1384.90	23.0823	46.0	12.0	39.8	2.741	0.012	0.002	0.000	0.302	0.26
1468	11/7/2002	2:20:01 PM	26.022	23.799	25.677	25.588	25.084	44.236	47.413	10.227	35.161	-1.291	-6.798	48.677	0.082	0.001	0	1385.90	23.0989	45.9	12.2	39.7	2.737	0.012	0.002	0.000	0.302	0.26
1469	11/7/2002	2:21:01 PM	26.025	23.802	25.679	25.591	25.058	44.498	47.589	10.307	35.278	-1.291	-6.803	49.366	0.082	0.001	0	1386.90	23.1156	46.2	12.1	39.9	2.749	0.012	0.002	0.000	0.301	0.26
1470	11/7/2002	2:22:01 PM	26.045	23.832	25.665	25.621	25.123	44.553	47.812	10.377	35.2	-1.291	-6.793	49.972	0.081	0.001	0	1387.90	23.1323	46.3	12.0	39.9	2.749	0.012	0.002	0.000	0.297	0.26
1471	11/7/2002	2:23:01 PM	26.046	23.848	25.736	25.631																						

1561	11/7/2002	3:52:03 PM	26.313	24.893	25.748	26.429	25.991	44.878	49.033	9.94	36.095	-1.286	-6.861	48.244	0.077	0.001	0	1478.94	24.6489	47.6	11.8	40.5	2.781	0.011	0.011	0.000	0.261	0.24
1562	11/7/2002	3:53:03 PM	26.299	24.889	25.674	26.44	25.992	44.832	49.138	10.024	37.796	-1.286	-6.867	48.412	0.077	0.001	0	1479.94	24.6666	47.7	11.9	40.5	2.780	0.011	0.011	0.000	0.279	0.24
1563	11/7/2002	3:54:03 PM	26.304	24.915	25.715	26.48	26.028	44.571	48.96	9.945	35.659	-1.286	-6.864	48.427	0.077	0.001	0	1480.94	24.6823	47.5	11.9	40.1	2.763	0.011	0.011	0.000	0.261	0.24
1564	11/7/2002	3:55:03 PM	26.322	24.933	25.798	26.484	26.051	44.646	48.799	9.9	35.78	-1.288	-6.861	48.379	0.078	0.001	0	1481.94	24.6989	47.3	11.9	40.2	2.773	0.012	0.011	0.000	0.263	0.24
1565	11/7/2002	3:56:03 PM	26.313	24.929	25.683	26.449	26.066	44.515	48.875	9.961	36.544	-1.291	-6.867	48.396	0.078	0.001	0	1482.94	24.7156	47.2	11.7	40.2	2.768	0.011	0.011	0.000	0.260	0.24
1566	11/7/2002	3:57:03 PM	26.319	24.939	25.754	26.455	26.052	44.648	48.82	10.019	36.616	-1.291	-6.867	48.502	0.077	0.001	0	1483.94	24.7323	47.3	12.3	40.1	2.767	0.011	0.011	0.000	0.260	0.24
1567	11/7/2002	3:58:03 PM	26.314	24.944	25.684	26.485	26.032	44.634	48.988	10.032	35.405	-1.291	-6.867	48.179	0.077	0.001	0	1484.94	24.7489	47.5	11.8	40.0	2.769	0.011	0.011	0.000	0.261	0.24
1568	11/7/2002	3:59:03 PM	26.315	24.95	25.715	26.436	26.043	44.861	48.958	10.02	35.849	-1.294	-6.815	47.869	0.078	0.001	0	1485.94	24.7656	47.6	11.7	40.4	2.782	0.012	0.011	0.000	0.262	0.24
1569	11/7/2002	4:00:03 PM	26.333	24.968	25.765	26.461	26.038	44.617	48.756	9.997	36.777	-1.291	-6.867	48.495	0.077	0.001	0	1486.94	24.7823	47.3	12.1	40.1	2.768	0.011	0.011	0.000	0.260	0.24
1570	11/7/2002	4:01:03 PM	26.321	24.966	25.746	26.447	26.049	44.614	48.901	10.009	36.751	-1.294	-6.815	47.682	0.077	0.001	0	1487.94	24.7989	47.6	11.7	40.3	2.772	0.011	0.011	0.000	0.279	0.24
1571	11/7/2002	4:02:03 PM	26.326	24.981	25.726	26.457	26.074	44.679	48.9	10.038	36.642	-1.291	-6.873	49.538	0.077	0.001	0	1488.94	24.8064	47.4	12.1	40.2	2.769	0.011	0.011	0.000	0.260	0.24
1572	11/7/2002	4:03:03 PM	26.332	24.993	25.727	26.488	26.045	45.247	48.995	10.026	36.267	-1.294	-6.877	48.955	0.078	0.001	0	1489.94	24.8231	48.1	11.9	40.8	2.810	0.012	0.011	0.000	0.260	0.24
1573	11/7/2002	4:03:30 PM	26.338	24.992	25.739	26.49	26.052	45.224	48.929	10.013	36.293	-1.294	-6.877	47.633	0.078	0.001	0	1490.94	24.8398	48.1	11.7	40.8	2.810	0.012	0.011	0.000	0.260	0.24
1574	11/7/2002	4:04:30 PM	26.361	25.022	25.631	26.522	26.089	45.017	49.208	10.015	36.027	-1.288	-6.847	48.71	0.077	0.001	0	1491.94	24.8564	47.7	11.9	40.5	2.794	0.011	0.011	0.000	0.278	0.24
1575	11/7/2002	4:05:30 PM	26.343	25.023	25.678	26.494	26.081	45.149	49.434	10.127	36.013	-1.291	-6.853	48.087	0.078	0.001	0	1492.94	24.8731	48.0	11.8	40.6	2.798	0.012	0.011	0.000	0.261	0.24
1576	11/7/2002	4:06:30 PM	26.323	25.019	25.689	26.53	26.072	45.292	49.699	10.179	35.015	-1.294	-6.864	47.919	0.078	0.001	0	1493.94	24.8898	48.2	11.7	40.7	2.803	0.012	0.011	0.000	0.261	0.24
1577	11/7/2002	4:07:30 PM	26.329	25.045	25.6	26.566	26.058	45.158	49.446	10.142	35.99	-1.291	-6.858	47.936	0.078	0.001	0	1494.94	24.9064	48.0	11.7	40.6	2.797	0.012	0.011	0.000	0.262	0.24
1578	11/7/2002	4:08:30 PM	26.319	25.05	25.63	26.55	26.068	45.143	49.451	10.225	36.892	-1.291	-6.818	48.909	0.078	0.001	0	1495.94	24.9231	47.9	11.7	40.5	2.788	0.011	0.011	0.000	0.260	0.24
1579	11/7/2002	4:09:30 PM	26.317	25.067	25.637	26.538	26.115	44.87	49.279	10.133	35.63	-1.291	-6.867	48.739	0.077	0.001	0	1496.94	24.9398	47.8	11.9	40.3	2.775	0.011	0.011	0.000	0.261	0.24
1580	11/7/2002	4:10:30 PM	26.298	25.074	25.589	26.509	26.126	45.392	49.422	10.142	36.236	-1.291	-6.867	48.414	0.077	0.001	0	1497.94	24.9564	48.2	11.9	40.8	2.814	0.011	0.011	0.000	0.277	0.24
1581	11/7/2002	4:11:30 PM	26.286	25.081	25.541	26.57	26.144	45.496	49.823	10.223	36.253	-1.291	-6.864	47.997	0.077	0.001	0	1498.94	24.9731	48.4	11.8	40.9	2.818	0.011	0.011	0.000	0.277	0.24
1582	11/7/2002	4:12:30 PM	26.299	25.084	25.538	26.579	26.176	45.056	49.333	10.126	35.909	-1.291	-6.873	47.636	0.077	0.001	0	1499.94	24.9898	47.9	11.7	40.5	2.774	0.011	0.011	0.000	0.260	0.24
1583	11/7/2002	4:13:30 PM	26.264	25.09	25.564	26.6	26.172	44.838	49.104	10.124	36.002	-1.297	-6.861	47.793	0.077	0.001	0	1500.94	25.0064	47.7	11.7	40.2	2.773	0.011	0.011	0.000	0.261	0.24
1584	11/7/2002	4:14:30 PM	26.265	25.086	25.486	26.626	26.194	44.959	49.598	10.125	36.747	-1.291	-6.867	47.953	0.077	0.001	0	1501.94	25.0231	47.9	11.8	40.4	2.782	0.011	0.011	0.000	0.261	0.24
1585	11/7/2002	4:15:30 PM	26.266	25.107	25.561	26.612	26.224	45.129	49.583	10.149	35.945	-1.288	-6.861	48.487	0.077	0.001	0	1502.94	25.0398	48.1	11.9	40.5	2.791	0.011	0.011	0.000	0.279	0.24
1586	11/7/2002	4:16:30 PM	26.262	25.113	25.502	26.308	26.25	45.075	49.577	10.145	36.023	-1.291	-6.867	48.687	0.077	0.001	0	1503.94	25.0564	48.1	12.0	40.6	2.780	0.011	0.011	0.000	0.261	0.24
1587	11/7/2002	4:17:30 PM	26.246	25.122	25.521	26.587	26.219	45.095	49.666	10.181	36.792	-1.291	-6.864	48.795	0.077	0.001	0	1504.94	25.0731	48.2	12.0	40.4	2.788	0.011	0.011	0.000	0.260	0.24
1588	11/7/2002	4:18:30 PM	26.266	25.137	25.561	26.627	26.234	45.269	49.746	10.183	36.003	-1.288	-6.861	47.212	0.077	0.001	0	1505.94	25.0898	48.3	11.6	40.6	2.802	0.011	0.011	0.000	0.278	0.24
1589	11/7/2002	4:19:30 PM	26.241	25.142	25.471	26.587	26.204	45.149	49.606	10.156	36.886	-1.291	-6.868	48.366	0.077	0.001	0	1506.94	25.1064	48.1	11.9	40.5	2.794	0.011	0.011	0.000	0.260	0.24
1590	11/7/2002	4:20:30 PM	26.24	25.146	25.596	26.576	26.219	45.197	49.585	10.088	36.122	-1.291	-6.858	48.279	0.077	0.001	0	1507.94	25.1231	48.1	11.3	40.7	2.803	0.011	0.011	0.000	0.278	0.24
1591	11/7/2002	4:21:30 PM	26.239	25.141	25.471	26.549	26.229	44.89	49.417	10.138	36.675	-1.291	-6.867	48.398	0.077	0.001	0	1508.94	25.1398	47.9	11.7	40.3	2.777	0.011	0.011	0.000	0.261	0.24
1592	11/7/2002	4:22:30 PM	26.231	25.162	25.526	26.557	26.204	45.162	49.484	10.103	36.06	-1.291	-6.861	47.69	0.077	0.001	0	1509.94	25.1564	48.0	11.7	40.6	2.800	0.011	0.011	0.000	0.279	0.24
1593	11/7/2002	4:23:30 PM	26.237	25.168	25.557	26.548	26.24	44.946	49.48	10.118	36.749	-1.291	-6.867	47.745	0.077	0.001	0	1510.94	25.1731	48.0	11.7	40.3	2.782	0.011	0.011	0.000	0.260	0.24
1594	11/7/2002	4:24:30 PM	26.212	25.163	25.472	26.503	26.17	45.122	49.647	10.193	35.623	-1.294	-6.867	47.984	0.077	0.001	0	1511.94	25.1898	48.2	11.7	40.5	2.790	0.011	0.011	0.000	0.260	0.24
1595	11/7/2002	4:25:30 PM	26.269	25.178	25.62	26.533	26.165	45.096	49.591	10.136	36.878	-1.291	-6.867	48.49	0.078	0.001	0	1512.94	25.2064	48.1	11.9	40.5	2.801	0.011	0.011	0.000	0.274	0.24
1596	11/7/2002	4:26:30 PM	26.239	25.194	25.529	26.55	26.182	45.06	49.562	10.154	36.868	-1.291	-6.861	47.784	0.077	0.001	0	1513.94	25.2231	48.1	11.7	40.5	2.790	0.011	0.011	0.000	0.260	0.24
1597	11/7/2002	4:27:30 PM	26.224	25.189	25.549	26.545	26.147	45.052	49.525	10.246	36.771	-1.291	-6.87	48.217	0.078	0.001	0	1514.94	25.2398	48.1	11.8	40.4	2.786	0.011	0.011	0.000	0.276	0.23
1598	11/7/2002	4:28:30 PM	26.223	25.206	25.586	26.596	26.153	44.942	49.329	10.15	35.906	-1.291	-6.864	48.196	0.078	0.001	0	1515.94	25.2564	47.9	11.8	40.4	2.784	0.011	0.011	0.000	0.276	0.23
1599	11/7/2002	4:29:30 PM	26.269	25.204	25.538	26.579	26.176	45.019	49.465	10.24	36.729	-1.294	-6.867	48.619	0.078	0.001	0	1516.94	25.2731	48.0	11.6	40.4	2.784	0.011	0.011	0.000	0.279	0.24
1600	11/7/2002	4:30:30 PM	26.245	25.221	25.562	26.546	26.198	45.162	49.719	10.188	36.878	-1.288	-6.795	48.016	0.073	0.001	0	1517.94	25.2898	48.2	11.8	40.5	2.794	0.011	0.011	0.000	0.264	0.24
1601	11/7/2002	4:31:30 PM	26.247	25.223	25.563	26.588																						

WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

1691	11/1/2002	9:45:25 AM	25.683	21.427	25.571	23.378	21.993	45.179	48.911	11.07	36.165	-1.288	-6.192	47.2	0.106	0.001	0.001	1608	39	26.8066	47.4	11.6	41.2	2.839	0.016	0.016	0.000	0.378	0.3
1692	11/1/2002	9:46:25 AM	25.679	21.424	25.583	23.299	22.044	45.682	48.42	11.806	34.906	-1.291	-6.326	50.287	0.102	0.001	0.001	1609	39	26.8222	46.9	12.3	40.3	2.778	0.015	0.015	0.000	0.371	0.32
1693	11/1/2002	9:47:25 AM	25.686	21.465	25.643	23.37	22.111	45.878	48.646	11.452	35.395	-1.291	-6.381	48.622	0.1	0.001	0.001	1610	39	26.8398	47.2	11.9	40.7	2.800	0.015	0.015	0.000	0.362	0.31
1694	11/1/2002	9:48:25 AM	25.73	21.616	25.704	23.686	22.488	45.781	48.65	11.652	35.345	-1.285	-6.488	45.978	0.1	0.001	0.001	1611	39	26.855	47.0	11.9	40.5	2.791	0.015	0.015	0.000	0.361	0.31
1695	11/1/2002	9:49:25 AM	25.627	21.507	25.646	23.583	22.249	46.046	48.712	11.689	35.348	-1.288	-6.418	47.464	0.101	0.001	0.001	1612	39	26.8732	47.2	11.6	40.7	2.806	0.015	0.015	0.000	0.363	0.31
1696	11/1/2002	9:50:25 AM	25.669	21.569	25.697	23.59	22.336	46.048	48.764	11.767	35.268	-1.288	-6.447	46.295	0.1	0.001	0.001	1613	39	26.8898	47.3	11.9	40.7	2.803	0.015	0.015	0.000	0.360	0.31
1697	11/1/2002	9:51:25 AM	25.688	21.689	25.777	23.61	22.396	45.558	48.767	11.624	35.026	-1.291	-6.447	49.457	0.102	0.001	0.001	1614	39	26.9056	46.9	12.1	40.3	2.778	0.015	0.015	0.000	0.369	0.31
1698	11/1/2002	9:52:25 AM	25.73	21.616	25.704	23.686	22.488	45.781	48.65	11.652	35.345	-1.285	-6.488	45.978	0.1	0.001	0.001	1615	39	26.9222	47.2	11.9	40.5	2.796	0.015	0.015	0.000	0.360	0.31
1699	11/1/2002	9:53:25 AM	25.745	21.621	25.783	23.646	22.533	46.126	48.727	11.679	35.307	-1.291	-6.473	48.429	0.1	0.001	0.001	1616	39	26.9398	47.5	11.9	40.9	2.821	0.015	0.015	0.000	0.356	0.30
1700	11/1/2002	9:54:25 AM	25.766	21.662	25.789	23.637	22.614	46.268	48.733	11.437	35.029	-1.294	-6.403	48.789	0.099	0.001	0.001	1617	39	26.9566	47.5	12.0	41.0	2.830	0.015	0.015	0.000	0.362	0.30
1701	11/1/2002	9:55:25 AM	25.811	21.692	25.784	23.737	22.679	46.118	48.902	11.493	35.665	-1.291	-6.502	49.362	0.098	0.001	0.001	1618	39	26.9732	47.4	12.1	40.9	2.819	0.015	0.015	0.000	0.350	0.30
1702	11/1/2002	9:56:25 AM	25.825	21.712	25.879	23.782	22.75	46.269	48.907	11.544	35.788	-1.291	-6.514	45.711	0.097	0.001	0.001	1619	39	26.9898	47.6	11.2	41.0	2.828	0.014	0.014	0.000	0.344	0.29
1703	11/1/2002	9:57:25 AM	25.866	21.798	25.83	23.828	22.821	46.62	49.436	11.574	36.802	-1.286	-6.538	49.207	0.096	0.001	0.001	1620	39	27.0066	48.0	11.8	41.3	2.848	0.014	0.014	0.000	0.338	0.28
1704	11/1/2002	9:58:25 AM	25.891	21.793	25.89	23.778	22.886	46.003	48.906	11.524	35.395	-1.288	-6.528	49.912	0.095	0.001	0.001	1621	39	27.0232	47.4	12.2	40.7	2.806	0.014	0.014	0.000	0.339	0.28
1705	11/1/2002	9:59:25 AM	25.917	21.819	25.961	23.693	22.962	46.348	49.163	11.687	36.714	-1.291	-6.536	47.962	0.094	0.001	0.001	1622	39	27.0398	47.7	11.7	41.0	2.829	0.014	0.014	0.000	0.332	0.28
1706	11/1/2002	10:00:25 AM	25.922	21.84	25.951	23.634	23.008	46.719	49.405	11.492	36.162	-1.288	-6.551	47.936	0.094	0.001	0.001	1623	39	27.0566	47.9	11.7	41.4	2.857	0.014	0.014	0.000	0.330	0.28
1707	11/1/2002	10:01:25 AM	25.947	21.88	25.981	23.523	23.058	46.558	49.522	11.428	36.105	-1.291	-6.588	49.062	0.093	0.001	0.001	1624	39	27.0732	47.9	11.8	41.3	2.860	0.014	0.014	0.000	0.323	0.27
1708	11/1/2002	10:02:25 AM	25.957	21.9	25.966	23.423	23.113	46.661	49.494	11.602	35.915	-1.291	-6.543	45.201	0.092	0.001	0.001	1625	39	27.0898	48.0	11.1	41.3	2.847	0.014	0.014	0.000	0.323	0.28
1709	11/1/2002	10:03:25 AM	25.962	21.93	25.926	23.352	23.199	46.454	49.196	11.565	35.872	-1.288	-6.554	47.068	0.09	0.001	0.001	1626	39	27.1066	47.7	11.5	41.2	2.838	0.013	0.013	0.000	0.318	0.27
1710	11/1/2002	10:04:25 AM	25.981	21.964	25.95	23.401	23.212	47.127	49.688	11.568	36.613	-1.288	-6.564	46.654	0.09	0.001	0.001	1627	39	27.1232	48.2	11.4	41.9	2.887	0.013	0.013	0.000	0.311	0.26
1711	11/1/2002	10:05:25 AM	25.92	21.983	25.984	23.431	23.272	46.978	49.744	11.449	36.807	-1.288	-6.575	45.838	0.088	0.001	0.001	1628	39	27.1398	48.2	11.7	41.6	2.861	0.013	0.013	0.000	0.309	0.26
1712	11/1/2002	10:06:25 AM	25.933	21.997	25.997	23.409	23.315	46.817	49.591	11.539	36.199	-1.288	-6.598	46.056	0.087	0.001	0.001	1629	39	27.1566	48.1	11.3	41.5	2.882	0.013	0.013	0.000	0.304	0.26
1713	11/1/2002	10:07:25 AM	25.957	22.021	26.116	23.32	23.304	46.284	49.269	12.054	35.149	-1.288	-6.608	46.705	0.086	0.001	0.001	1630	39	27.1732	47.8	11.4	40.7	2.807	0.013	0.013	0.000	0.302	0.26
1714	11/1/2002	10:08:25 AM	25.967	22.044	26.004	23.31	23.332	46.425	49.178	11.874	35.667	-1.291	-6.618	46.266	0.084	0.001	0.001	1631	39	27.1898	47.7	11.8	41.0	2.830	0.013	0.013	0.000	0.297	0.25
1715	11/1/2002	10:09:25 AM	25.928	22.006	26.102	23.227	23.049	46.069	48.982	12.257	34.729	-1.295	-6.659	46.009	0.081	0.001	0.001	1632	39	27.2066	47.4	11.8	40.4	2.795	0.012	0.012	0.000	0.290	0.25
1716	11/1/2002	10:10:25 AM	25.977	22.016	26.035	23.035	22.821	46.39	49.111	12.134	35.287	-1.288	-6.638	47.979	0.08	0.001	0.001	1633	39	27.2232	47.6	11.7	40.8	2.816	0.012	0.012	0.000	0.294	0.24
1717	11/1/2002	10:11:25 AM	26.076	21.924	25.83	22.889	22.6	46.276	49.01	12.101	35.186	-1.295	-6.685	47.388	0.08	0.001	0.001	1634	39	27.2398	47.5	11.6	40.7	2.808	0.012	0.012	0.000	0.286	0.24
1718	11/1/2002	10:12:25 AM	26.049	21.876	25.597	22.801	22.401	46.021	48.898	12.003	35.026	-1.288	-6.689	48.286	0.079	0.001	0.001	1635	39	27.2566	47.4	11.8	40.5	2.794	0.012	0.012	0.000	0.286	0.24
1719	11/1/2002	10:13:25 AM	26.009	21.821	25.538	22.721	22.236	45.896	48.986	12.49	34.216	-1.288	-6.711	48.444	0.078	0.001	0.001	1636	39	27.2732	47.5	11.9	40.7	2.800	0.012	0.012	0.000	0.286	0.24
1720	11/1/2002	10:14:25 AM	25.953	21.79	25.487	22.829	22.134	46.264	49.022	12.369	34.624	-1.291	-6.734	48.219	0.077	0.001	0.001	1637	39	27.2898	47.6	11.9	40.3	2.792	0.011	0.011	0.000	0.281	0.24
1721	11/1/2002	10:15:25 AM	25.899	21.721	25.297	22.749	21.919	46.411	49.117	12.268	35.078	-1.285	-6.718	48.244	0.077	0.001	0.001	1638	39	27.3066	47.7	11.8	40.7	2.800	0.011	0.011	0.000	0.279	0.24
1722	11/1/2002	10:16:25 AM	25.886	21.731	25.423	22.45	21.944	46.172	49.159	12.107	35.088	-1.288	-6.684	47.319	0.077	0.001	0.001	1639	39	27.3232	47.7	11.6	40.6	2.801	0.011	0.011	0.000	0.279	0.24
1723	11/1/2002	10:17:25 AM	25.826	21.713	25.37	22.502	21.881	46.127	48.997	12.077	35.161	-1.288	-6.74	47.831	0.075	0.001	0.001	1640	39	27.3398	47.6	11.7	40.6	2.802	0.011	0.011	0.000	0.273	0.23
1724	11/1/2002	10:18:25 AM	25.797	21.616	25.375	22.919	21.866	45.986	49.057	12.486	34.975	-1.285	-6.768	46.955	0.074	0.001	0.001	1641	39	27.3566	47.6	11.9	40.2	2.771	0.011	0.011	0.000	0.272	0.23
1725	11/1/2002	10:19:25 AM	25.78	21.691	25.428	22.611	21.899	46.686	48.386	12.618	35.047	-1.288	-6.76	49.246	0.074	0.001	0.001	1642	39	27.3732	47.9	12.1	40.9	2.818	0.011	0.011	0.000	0.267	0.23
1726	11/1/2002	10:20:25 AM	25.762	21.698	25.37	22.719	21.977	46.131	49.055	12.695	34.451	-1.288	-6.786	48.238	0.073	0.001	0.001	1643	39	27.3898	47.6	11.8	40.3	2.778	0.011	0.011	0.000	0.267	0.23
1727	11/1/2002	10:21:25 AM	25.739	21.695	25.507	22.796	22.059	46.686	49.523	12.61	35.151	-1.291	-6.76	48.848	0.073	0.001	0.001	1644	39	27.4066	48.1	12.0	40.9	2.821	0.011	0.011	0.000	0.262	0.22
1728	11/1/2002	10:22:25 AM	25.697	21.673	25.375	22.82	22.052	46.678	49.569	12.589	34.991	-1.288	-6.769	49.113	0.072	0.001	0.001	1645	39	27.4232	48.1	12.0	40.8	2.815	0.011	0.011	0.000	0.260	0.22
1729	11/1/2002	10:23:25 AM	25.676	21.662	25.444	22.788	22.127	46.264	49.302	12.791	34.424	-1.291	-6.74	48.219	0.071	0.001	0.001	1646	39	27.4398	47.8	11.9	40.3	2.782	0.011	0.011	0.000	0.259	0.22
1730	1																												

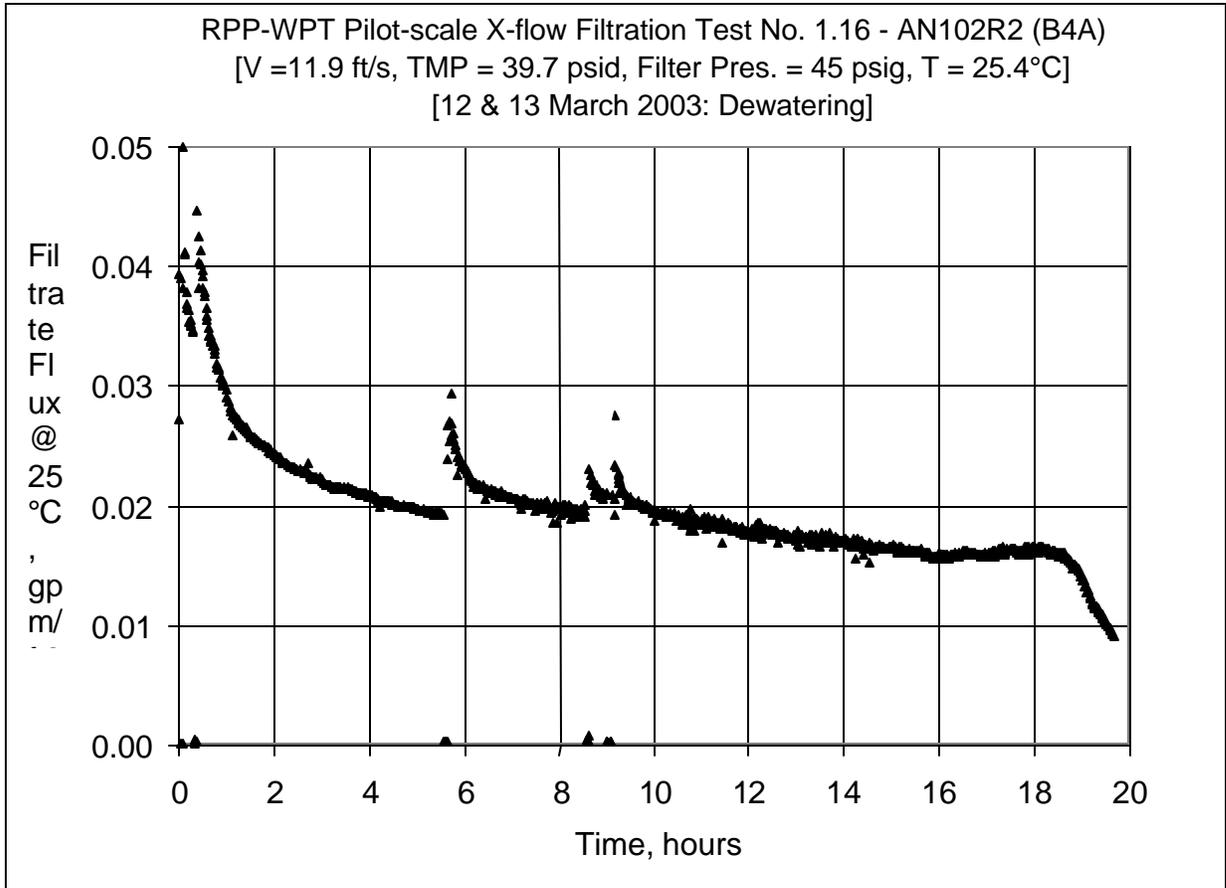


Figure D7: Dewatering of the AN-102R2, batch 4A, insoluble solids concentrations from 1.5 to 18 wt%

(Data from 10 Files)  
(1.16-4a-rpp-pxu-031203-0810, -1045, -1306, -1505, -1708, -1906, 2106, -2303)  
(1.16-3a-rpp-pxu-031303-77-0101, -0301)



131	3/12/2003	10:05:31 AM	25.115	22.112	25.218	23.89	23.923	44.003	45.552	8.814	36.067	-1.286	-5.328	48.726	0.167	0.001	0	114.00	1.9	44.1	11.9	40.0	2.760	0.025	0.001	0.618	0.53
132	3/12/2003	10:07:31 AM	25.148	22.135	25.306	23.907	23.96	43.701	45.153	8.736	35.908	-1.286	-5.328	48.935	0.166	0.001	0	115.00	1.91667	43.7	12.0	39.8	2.744	0.025	0.001	0.616	0.52
133	3/12/2003	10:07:31 AM	25.186	22.178	25.384	23.936	23.993	44.188	45.708	8.849	36.2	-1.284	-5.311	48.82	0.166	0.001	0	116.00	1.93333	44.2	12.0	40.0	2.771	0.025	0.001	0.619	0.52
134	3/12/2003	10:08:31 AM	25.209	22.201	25.392	23.943	24.036	43.914	45.41	8.78	36.036	-1.284	-5.311	48.814	0.166	0.001	0	117.00	1.95	43.9	12.0	40.0	2.756	0.025	0.001	0.612	0.52
135	3/12/2003	10:09:31 AM	25.222	22.219	25.365	24.001	24.074	44.07	45.569	8.73	36.276	-1.286	-5.312	48.762	0.164	0.001	0	118.00	1.96667	44.4	11.9	40.2	2.775	0.025	0.001	0.619	0.52
136	3/12/2003	10:10:31 AM	25.224	22.237	25.352	24.054	24.092	44.005	45.507	8.771	36.159	-1.289	-5.322	48.935	0.165	0.001	0	119.00	1.98333	44.0	12.0	40.1	2.764	0.025	0.001	0.608	0.52
137	3/12/2003	10:11:31 AM	25.222	22.265	25.325	24.112	24.145	44.285	45.877	8.844	36.27	-1.286	-5.322	48.661	0.165	0.001	0	120.00	2	44.4	11.9	40.3	2.777	0.025	0.001	0.605	0.52
138	3/12/2003	10:12:31 AM	25.222	22.283	25.278	24.12	24.178	44.007	45.643	8.864	36.008	-1.289	-5.317	48.738	0.164	0.001	0	121.00	2.01667	44.2	11.9	40.0	2.758	0.024	0.001	0.606	0.52
139	3/12/2003	10:13:31 AM	25.252	22.319	25.225	24.107	24.201	44.148	45.589	8.73	36.276	-1.286	-5.312	48.762	0.164	0.001	0	122.00	2.03333	44.1	11.9	40.2	2.770	0.024	0.001	0.609	0.52
140	3/12/2003	10:14:31 AM	25.266	22.334	25.259	24.156	24.218	44.109	45.759	8.835	36.065	-1.289	-5.322	48.633	0.163	0.001	0	123.00	2.05	44.3	11.9	40.1	2.764	0.024	0.001	0.602	0.51
141	3/12/2003	10:15:31 AM	25.288	22.356	25.236	24.198	24.281	43.954	45.577	8.858	35.961	-1.292	-5.32	48.608	0.163	0.001	0	124.00	2.06667	44.1	11.9	40.0	2.756	0.024	0.001	0.604	0.51
142	3/12/2003	10:16:31 AM	25.296	22.379	25.219	24.151	24.314	43.989	45.563	8.779	36.098	-1.286	-5.326	48.638	0.162	0.001	0	125.00	2.08333	44.1	11.9	40.0	2.761	0.024	0.001	0.601	0.51
143	3/12/2003	10:17:31 AM	25.263	22.385	25.195	24.17	24.316	44.148	45.734	8.849	36.149	-1.286	-5.322	48.81	0.162	0.001	0	126.00	2.1	44.3	12.0	40.1	2.768	0.024	0.001	0.598	0.51
144	3/12/2003	10:18:31 AM	25.297	22.423	25.203	24.18	24.358	44.148	45.703	8.807	36.167	-1.289	-5.331	48.935	0.161	0.001	0	127.00	2.11667	44.2	12.0	40.2	2.769	0.024	0.001	0.594	0.51
145	3/12/2003	10:19:31 AM	25.267	22.441	25.205	24.172	24.325	44.126	45.724	8.876	36.092	-1.289	-5.322	48.81	0.162	0.001	0	128.00	2.13333	44.3	12.0	40.1	2.765	0.024	0.001	0.599	0.51
146	3/12/2003	10:20:31 AM	25.295	22.464	25.223	24.245	24.399	43.962	45.61	8.86	35.973	-1.284	-5.338	48.206	0.161	0.001	0	129.00	2.15	44.1	12.0	40.0	2.758	0.024	0.001	0.597	0.51
147	3/12/2003	10:21:31 AM	25.293	22.497	25.171	24.288	24.396	43.964	45.505	8.828	36.071	-1.289	-5.327	48.896	0.161	0.001	0	130.00	2.16667	44.0	12.0	40.0	2.769	0.024	0.001	0.599	0.50
148	3/12/2003	10:22:31 AM	25.292	22.526	25.164	24.337	24.368	44.02	45.521	8.873	35.944	-1.296	-5.346	48.665	0.159	0.001	0	131.00	2.18333	44.1	11.9	40.0	2.757	0.024	0.001	0.595	0.50
149	3/12/2003	10:23:31 AM	25.304	22.559	25.202	24.435	24.388	43.979	45.655	8.776	36.153	-1.284	-5.343	48.678	0.159	0.001	0	132.00	2.2	44.2	11.9	40.1	2.762	0.024	0.001	0.588	0.50
150	3/12/2003	10:24:31 AM	25.296	22.571	25.174	24.447	24.375	44.119	45.716	8.807	36.131	-1.286	-5.343	48.606	0.159	0.001	0	133.00	2.21667	44.2	11.9	40.1	2.768	0.024	0.001	0.588	0.50
151	3/12/2003	10:25:31 AM	25.303	22.598	25.151	24.579	24.392	44.055	45.639	8.819	36.122	-1.286	-5.343	48.497	0.159	0.001	0	134.00	2.23333	44.2	11.9	40.1	2.764	0.024	0.001	0.589	0.50
152	3/12/2003	10:26:31 AM	25.305	22.62	25.158	24.646	24.399	44.03	45.64	8.773	36.11	-1.286	-5.343	48.717	0.159	0.001	0	135.00	2.25	44.1	11.9	40.1	2.763	0.024	0.001	0.589	0.50
153	3/12/2003	10:27:31 AM	25.302	22.642	25.16	24.678	24.405	44.115	45.692	8.82	36.08	-1.286	-5.34	48.573	0.159	0.001	0	136.00	2.26667	44.2	11.9	40.1	2.765	0.024	0.001	0.589	0.50
154	3/12/2003	10:28:31 AM	25.314	22.669	25.142	24.68	24.417	44.045	45.546	8.779	36.139	-1.289	-5.334	48.304	0.158	0.001	0	137.00	2.28333	44.1	11.8	40.1	2.764	0.024	0.001	0.585	0.50
155	3/12/2003	10:29:31 AM	25.31	22.69	25.128	24.711	24.404	44.275	45.936	8.888	36.215	-1.286	-5.334	48.566	0.158	0.001	0	138.00	2.3	44.5	11.9	40.2	2.775	0.024	0.001	0.583	0.50
156	3/12/2003	10:30:31 AM	25.312	22.717	25.15	24.703	24.411	44.196	45.78	8.856	36.188	-1.284	-5.334	48.243	0.158	0.001	0	139.00	2.31667	44.3	11.8	40.2	2.771	0.024	0.001	0.584	0.50
157	3/12/2003	10:31:31 AM	25.312	22.745	25.168	24.791	24.424	44.267	45.854	8.91	36.223	-1.286	-5.332	48.566	0.157	0.001	0	140.00	2.33333	44.1	12.0	39.9	2.763	0.023	0.001	0.583	0.50
158	3/12/2003	10:32:31 AM	25.332	22.773	25.145	24.864	24.466	44.879	45.498	8.76	35.905	-1.289	-5.334	48.74	0.157	0.001	0	141.00	2.35	44.0	11.9	39.9	2.760	0.023	0.001	0.584	0.50
159	3/12/2003	10:33:31 AM	25.336	22.79	25.143	24.897	24.499	44.132	45.704	8.781	36.229	-1.286	-5.34	48.063	0.157	0.001	0	142.00	2.36667	44.2	11.8	40.2	2.770	0.023	0.001	0.580	0.49
160	3/12/2003	10:34:31 AM	25.327	22.803	25.15	24.894	24.501	43.949	45.54	8.758	36.041	-1.286	-5.349	48.814	0.157	0.001	0	143.00	2.38333	44.1	12.0	40.0	2.768	0.023	0.001	0.583	0.50
161	3/12/2003	10:35:31 AM	25.34	22.836	25.158	24.957	24.515	43.954	45.515	8.781	36.2	-1.286	-5.367	48.579	0.157	0.001	0	144.00	2.4	44.0	11.9	39.9	2.750	0.023	0.001	0.584	0.50
162	3/12/2003	10:36:31 AM	25.357	22.863	25.14	25.019	24.568	43.886	45.468	8.73	36.153	-1.286	-5.367	48.452	0.156	0.001	0	145.00	2.41667	44.0	11.9	40.1	2.763	0.023	0.001	0.582	0.50
163	3/12/2003	10:37:31 AM	25.357	22.883	25.14	25.019	24.568	43.825	45.408	8.822	36.815	-1.289	-5.346	48.545	0.156	0.001	0	146.00	2.43333	43.9	11.9	39.8	2.745	0.023	0.001	0.582	0.50
164	3/12/2003	10:38:31 AM	25.361	22.912	25.158	25.032	24.605	44.026	45.718	8.794	36.051	-1.289	-5.363	48.655	0.156	0.001	0	147.00	2.45	44.2	11.9	40.0	2.761	0.023	0.001	0.578	0.49
165	3/12/2003	10:39:31 AM	25.369	22.935	25.167	25.086	24.613	43.947	45.466	8.827	36.951	-1.286	-5.364	48.592	0.156	0.001	0	148.00	2.46667	44.0	11.9	39.9	2.754	0.023	0.001	0.579	0.49
166	3/12/2003	10:40:31 AM	25.372	22.967	25.147	25.085	24.613	43.872	45.417	8.81	36.188	-1.286	-5.363	48.537	0.156	0.001	0	149.00	2.48333	44.1	11.9	40.1	2.765	0.023	0.001	0.578	0.49
167	3/12/2003	10:41:31 AM	25.38	23.001	25.163	25.142	24.634	44.291	45.968	8.89	36.253	-1.284	-5.34	48.483	0.155	0.001	0	150.00	2.5	44.5	11.9	40.3	2.777	0.023	0.001	0.571	0.49
168	3/12/2003	10:42:31 AM	25.388	23.02	25.176	25.17	24.712	43.995	45.629	8.863	36.967	-1.286	-5.337	48.948	0.155	0.001	0	151.00	2.51667	44.2	12.0	40.0	2.766	0.023	0.001	0.575	0.49
169	3/12/2003	10:43:31 AM	25.393	23.053	25.143	25.133	24.655	44.047	45.693	8.896	36.981	-1.289	-5.346	48.652	0.155	0.001	0	152.00	2.53333	44.3	12.0	40.0	2.759	0.023	0.001	0.576	0.49
170	3/12/2003	10:44:31 AM	25.392	23.089	25.174	25.138	24.668	44.043	45.755	8.88	36.946	-1.286	-5.346	48.594	0.155	0.001	0	153.00	2.55	44.3	11.9	40.0	2.767	0.023	0.001	0.575	0.49
171	3/12/2003	10:45:31 AM	25.398	23.085	25.141	25.165	24.681	43.911	45.546	8.87	36.754	-1.286	-5.342	48.779	0.154	0.001	0	154.00	2.56667	44.2	12.0	40.1	2.764	0.023	0.001	0.575	0.49
172	3/12/2003	10:46:31 AM	25.403	23.1	25.146	24.965	24.517	43.889	45.211	8.767	36.918	-1.289	-5.346	48.64	0.154	0.001	0.001	155.00	2.58333	43.7	11.9	39.8	2.744	0.023	0.001	0.574	0.49
173	3/12/2003	10:47																									

WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

261	3/12/2003	12:15:32 PM	25.697	23.365	25.309	24.462	23.944	44.235	46.061	8.784	36.237	-1.286	-6.408	48.235	0.141	0.001	0	244.02	4.06694	44.6	11.8	40.2	2.774	0.021	0.001	0.001	0.518	0.44
262	3/12/2003	12:16:32 PM	25.691	23.364	25.299	24.507	23.943	44.009	45.809	8.802	36.084	-1.289	-6.412	48.445	0.141	0.001	0	245.02	4.08361	44.3	11.9	40.2	2.781	0.021	0.001	0.001	0.521	0.44
263	3/12/2003	12:17:32 PM	25.677	23.365	25.299	24.502	23.934	44.188	45.881	8.903	36.28	-1.289	-6.621	48.132	0.14	0.001	0	246.02	4.10028	44.4	11.8	40.2	2.774	0.021	0.001	0.001	0.514	0.44
264	3/12/2003	12:18:32 PM	25.694	23.372	25.312	24.715	24.006	44.219	45.871	8.774	36.309	-1.286	-6.618	48.162	0.14	0.001	0	247.02	4.11694	44.4	11.8	40.3	2.776	0.021	0.001	0.001	0.514	0.44
265	3/12/2003	12:19:32 PM	25.682	23.369	25.284	24.814	24.144	44.171	45.923	8.797	36.276	-1.284	-6.543	48.16	0.14	0.001	0	248.02	4.13361	44.4	11.8	40.3	2.778	0.021	0.001	0.001	0.514	0.44
266	3/12/2003	12:20:32 PM	25.679	23.357	25.292	24.665	24.036	44.049	45.794	8.808	36.02	-1.286	-6.515	48.42	0.139	0.001	0	249.02	4.15028	44.3	11.9	40.2	2.780	0.021	0.001	0.001	0.513	0.44
267	3/12/2003	12:21:32 PM	25.686	23.369	25.304	25.037	24.073	44.186	45.977	8.834	36.17	-1.289	-6.606	48.361	0.139	0.001	0	250.02	4.16694	44.5	11.9	40.2	2.770	0.021	0.001	0.001	0.511	0.44
268	3/12/2003	12:22:32 PM	25.689	23.382	25.287	25.141	24.122	44.299	45.95	8.811	36.415	-1.289	-6.621	48.311	0.138	0.001	0	251.02	4.18361	44.5	11.8	40.4	2.782	0.021	0.001	0.001	0.506	0.43
269	3/12/2003	12:23:32 PM	25.671	23.414	25.264	24.414	24.144	44.111	46.073	8.829	36.363	-1.286	-6.543	48.255	0.135	0.001	0	252.02	4.20028	44.6	11.9	40.2	2.773	0.020	0.001	0.001	0.504	0.43
270	3/12/2003	12:24:32 PM	25.681	23.424	25.283	25.223	24.122	44.132	46.065	8.897	36.996	-1.286	-6.621	48.168	0.138	0.001	0	253.02	4.21694	44.6	11.8	40.1	2.782	0.021	0.001	0.001	0.509	0.43
271	3/12/2003	12:25:32 PM	25.6	23.448	25.297	25.377	24.252	44.297	46.092	8.841	36.333	-1.286	-6.667	48.004	0.138	0.001	0	254.02	4.23361	44.6	11.8	40.3	2.780	0.021	0.001	0.001	0.506	0.43
272	3/12/2003	12:26:32 PM	25.681	23.46	25.284	25.399	24.29	43.966	45.672	8.765	36.116	-1.289	-6.667	48.503	0.138	0.001	0	255.02	4.25028	44.2	11.9	40.2	2.781	0.021	0.001	0.001	0.510	0.43
273	3/12/2003	12:27:32 PM	25.695	23.478	25.283	25.332	24.298	44.128	45.941	8.764	36.28	-1.289	-6.667	48.315	0.138	0.001	0	256.02	4.26694	44.5	11.8	40.2	2.772	0.021	0.001	0.001	0.508	0.43
274	3/12/2003	12:28:32 PM	25.697	23.491	25.27	25.224	24.28	44.067	45.97	8.805	36.089	-1.289	-6.618	48.286	0.138	0.001	0	257.02	4.28361	44.5	11.8	40.1	2.784	0.021	0.001	0.001	0.509	0.43
275	3/12/2003	12:29:32 PM	25.699	23.497	25.287	25.116	24.277	44.101	45.908	8.827	36.08	-1.289	-6.661	48.26	0.138	0.001	0	258.02	4.30028	44.5	11.8	40.1	2.784	0.021	0.001	0.001	0.509	0.43
276	3/12/2003	12:30:32 PM	25.684	23.497	25.262	25.035	24.222	44.569	45.384	8.983	36.485	-1.286	-6.661	48.138	0.138	0.001	0	259.02	4.31694	44.9	11.8	40.5	2.794	0.021	0.001	0.001	0.504	0.43
277	3/12/2003	12:31:32 PM	25.684	23.503	25.242	25.011	24.257	43.968	45.726	8.81	36.069	-1.289	-6.661	48.447	0.138	0.001	0	260.02	4.33361	44.3	11.9	40.2	2.789	0.021	0.001	0.001	0.511	0.43
278	3/12/2003	12:32:32 PM	25.689	23.512	25.252	25.075	24.228	43.978	45.805	8.833	36.077	-1.286	-6.679	48.002	0.138	0.001	0	261.02	4.35028	44.5	11.8	40.2	2.780	0.021	0.001	0.001	0.509	0.43
279	3/12/2003	12:33:32 PM	25.683	23.512	25.256	24.95	24.176	44.045	45.974	8.835	36.016	-1.289	-6.668	48.262	0.138	0.001	0	262.02	4.36694	44.5	11.8	40.2	2.780	0.021	0.001	0.001	0.510	0.43
280	3/12/2003	12:34:32 PM	25.677	23.505	25.245	24.943	24.114	44.244	46.125	8.821	36.26	-1.286	-6.668	48.178	0.138	0.001	0	263.02	4.38361	44.7	11.8	40.3	2.775	0.021	0.001	0.001	0.508	0.43
281	3/12/2003	12:35:32 PM	25.675	23.498	25.223	24.936	24.112	44.252	46.126	8.821	36.397	-1.289	-6.668	48.269	0.138	0.001	0	264.02	4.40028	44.7	11.8	40.3	2.780	0.021	0.001	0.001	0.507	0.43
282	3/12/2003	12:36:32 PM	25.678	23.501	25.221	24.939	24.1	43.945	45.687	8.775	36.079	-1.286	-6.666	48.267	0.138	0.001	0	265.02	4.41694	44.2	11.8	40.2	2.789	0.021	0.001	0.001	0.511	0.43
283	3/12/2003	12:37:32 PM	25.691	23.51	25.259	24.957	24.078	44.237	46.169	8.88	36.196	-1.284	-6.663	48.201	0.137	0.001	0	266.02	4.43361	44.7	11.8	40.2	2.773	0.020	0.001	0.001	0.504	0.43
284	3/12/2003	12:38:32 PM	25.683	23.497	25.236	24.935	24.025	44.047	45.89	8.834	36.981	-1.284	-6.638	48.057	0.138	0.001	0	267.02	4.45028	44.4	11.8	40.2	2.789	0.021	0.001	0.001	0.511	0.43
285	3/12/2003	12:39:32 PM	25.681	23.499	25.213	24.922	23.978	44.154	46.057	8.875	36.086	-1.286	-6.638	48.097	0.137	0.001	0	268.02	4.46694	44.6	11.8	40.1	2.786	0.020	0.001	0.001	0.506	0.43
286	3/12/2003	12:40:32 PM	25.687	23.476	25.21	24.884	23.949	44.188	45.96	8.85	36.221	-1.289	-6.638	48.13	0.136	0.001	0	269.02	4.48361	44.5	11.8	40.2	2.782	0.020	0.001	0.001	0.501	0.43
287	3/12/2003	12:41:32 PM	25.697	23.485	25.262	24.917	24.011	44.297	46.063	8.829	36.363	-1.286	-6.618	48.252	0.136	0.001	0	270.02	4.50028	44.6	11.8	40.2	2.780	0.020	0.001	0.001	0.501	0.43
288	3/12/2003	12:42:32 PM	25.686	23.47	25.224	24.845	23.943	43.964	45.776	8.836	36.034	-1.286	-6.638	48.116	0.136	0.001	0	271.02	4.51694	44.3	11.8	40.2	2.778	0.020	0.001	0.001	0.504	0.43
289	3/12/2003	12:43:32 PM	25.679	23.457	25.222	24.87	23.835	43.829	45.617	8.874	36.777	-1.286	-6.621	48.222	0.136	0.001	0	272.02	4.53361	44.3	11.8	39.8	2.744	0.020	0.001	0.001	0.506	0.43
290	3/12/2003	12:44:32 PM	25.677	23.45	25.22	24.863	23.879	44.105	46.059	8.936	36.987	-1.286	-6.618	48.136	0.136	0.001	0	273.02	4.55028	44.6	11.8	40.2	2.781	0.020	0.001	0.001	0.503	0.43
291	3/12/2003	12:45:32 PM	25.686	23.455	25.264	24.883	23.933	43.947	45.852	8.863	36.867	-1.286	-6.603	48.288	0.136	0.001	0	274.02	4.56694	44.4	11.8	39.9	2.751	0.020	0.001	0.001	0.504	0.43
292	3/12/2003	12:46:32 PM	25.693	23.465	25.277	24.969	24.032	44.132	46.034	8.91	36.116	-1.284	-6.602	48.111	0.132	0.001	0	275.02	4.58361	44.4	11.8	40.2	2.786	0.020	0.001	0.001	0.502	0.43
293	3/12/2003	12:47:32 PM	25.682	23.465	25.265	25.069	24.039	43.964	45.868	8.911	36.01	-1.284	-6.603	48.097	0.135	0.001	0	276.02	4.60028	44.4	11.8	40.0	2.757	0.020	0.001	0.001	0.500	0.43
294	3/12/2003	12:48:32 PM	25.673	23.447	25.256	25.12	24.091	44.049	45.945	8.881	36.057	-1.289	-6.609	48.306	0.135	0.001	0	277.02	4.61694	44.5	11.8	40.1	2.782	0.020	0.001	0.001	0.499	0.42
295	3/12/2003	12:49:32 PM	25.681	23.464	25.289	25.253	24.143	44.01	45.89	8.869	36.01	-1.286	-6.618	48.067	0.135	0.001	0	278.02	4.63361	44.4	11.8	40.0	2.789	0.020	0.001	0.001	0.499	0.42
296	3/12/2003	12:50:32 PM	25.683	23.462	25.265	25.269	24.18	43.968	45.822	8.892	36.196	-1.284	-6.618	48.25	0.135	0.001	0	279.02	4.65028	44.5	11.8	39.7	2.756	0.020	0.001	0.001	0.497	0.42
297	3/12/2003	12:51:32 PM	25.687	23.48	25.274	25.484	24.245	44.096	46.126	8.912	36.006	-1.286	-6.609	48.199	0.135	0.001	0	280										

391	3/12/2003	2:24:36 PM	25.673	23.668	25.481	25.706	24.181	44.281	45.739	9.253	35.787	-1.292	-6.087	48.94	0.149	0.001	0	373.08	6.21806	44.3	12.0	40.0	2.760	0.022	0.002	0.001	0.547	0.47
392	3/12/2003	2:25:36 PM	25.887	23.676	25.475	25.704	24.185	44.387	45.749	9.118	36.182	-1.289	-6.089	48.887	0.149	0.001	0	374.08	6.23472	44.3	12.0	40.3	2.777	0.022	0.002	0.001	0.544	0.46
393	3/12/2003	2:26:36 PM	25.891	23.681	25.469	25.699	24.204	44.204	45.631	9.179	36.924	-1.289	-6.1	48.883	0.146	0.001	0	375.08	6.25139	44.2	12.0	40.1	2.762	0.022	0.002	0.001	0.536	0.46
394	3/12/2003	2:27:36 PM	25.886	23.685	25.473	25.698	24.173	44.304	45.654	9.043	36.282	-1.286	-6.096	48.888	0.146	0.001	0	376.08	6.26806	44.2	12.0	40.3	2.778	0.022	0.002	0.001	0.540	0.46
395	3/12/2003	2:28:36 PM	25.881	23.677	25.463	25.693	24.178	44.351	45.636	9.126	36.088	-1.284	-6.111	48.931	0.146	0.001	0	377.08	6.28472	44.4	12.0	40.2	2.773	0.022	0.002	0.001	0.534	0.46
396	3/12/2003	2:29:36 PM	25.869	23.664	25.437	25.607	24.157	44.264	45.652	9.033	36.178	-1.286	-6.096	48.827	0.148	0.001	0	378.08	6.30139	44.2	12.0	40.2	2.773	0.022	0.002	0.001	0.542	0.46
397	3/12/2003	2:30:36 PM	25.888	23.662	25.446	25.6	24.136	44.252	45.806	9.101	35.961	-1.289	-6.107	49.028	0.146	0.001	0	379.08	6.31806	44.3	12.0	40.1	2.765	0.022	0.002	0.001	0.536	0.46
398	3/12/2003	2:31:36 PM	25.888	23.667	25.455	25.64	24.111	44.219	45.897	9.095	35.951	-1.289	-6.098	48.887	0.147	0.001	0	380.08	6.33472	44.4	12.0	40.1	2.764	0.022	0.002	0.001	0.540	0.46
399	3/12/2003	2:32:36 PM	25.881	23.665	25.449	25.669	24.093	44.351	45.836	9.126	36.088	-1.284	-6.111	48.931	0.146	0.001	0	381.08	6.35139	44.4	12.0	40.2	2.773	0.022	0.002	0.001	0.534	0.46
400	3/12/2003	2:33:36 PM	25.861	23.666	25.428	25.683	24.123	44.335	45.854	9.136	36.065	-1.286	-6.104	49.959	0.147	0.001	0	382.08	6.36806	44.4	12.0	40.2	2.772	0.022	0.002	0.001	0.539	0.46
401	3/12/2003	2:34:36 PM	25.866	23.67	25.448	25.708	24.173	44.152	45.697	9.045	35.983	-1.286	-6.096	48.485	0.148	0.001	0	383.08	6.38472	44.2	11.9	40.1	2.763	0.022	0.002	0.001	0.544	0.46
402	3/12/2003	2:35:36 PM	25.869	23.662	25.44	25.745	24.25	44.115	45.701	9.08	35.94	-1.292	-6.127	48.686	0.145	0.001	0	384.08	6.40139	44.2	11.9	40.0	2.760	0.022	0.002	0.001	0.533	0.45
403	3/12/2003	2:36:36 PM	25.869	23.679	25.448	25.863	24.313	44.331	46.065	9.122	36.051	-1.286	-6.1	48.739	0.146	0.001	0	385.08	6.41806	44.6	11.9	40.2	2.771	0.022	0.002	0.001	0.535	0.46
404	3/12/2003	2:37:36 PM	25.869	23.689	25.457	26.002	24.388	44.358	46.086	9.115	36.133	-1.289	-6.098	48.857	0.144	0.001	0	386.08	6.43472	44.6	11.9	40.2	2.774	0.021	0.002	0.001	0.531	0.44
405	3/12/2003	2:38:36 PM	25.869	23.709	25.482	26.117	24.473	44.978	45.761	9.096	36.736	-1.286	-6.122	48.766	0.146	0.001	0	387.08	6.45139	44.2	11.9	39.9	2.748	0.022	0.002	0.001	0.539	0.46
406	3/12/2003	2:39:36 PM	25.865	23.724	25.477	26.242	24.533	44.159	45.924	9.182	36.796	-1.286	-6.136	48.749	0.145	0.001	0	388.08	6.46806	44.4	11.9	40.0	2.766	0.022	0.002	0.001	0.534	0.45
407	3/12/2003	2:40:36 PM	25.869	23.733	25.461	26.371	24.622	44.206	45.903	9.088	36.991	-1.284	-6.139	48.703	0.145	0.001	0	389.08	6.48472	44.5	11.9	40.1	2.765	0.022	0.002	0.001	0.532	0.45
408	3/12/2003	2:41:36 PM	25.883	23.753	25.476	26.391	24.652	44.352	45.823	9.13	36.457	-1.289	-6.145	48.898	0.144	0.001	0	390.08	6.50139	44.4	11.9	39.7	2.734	0.022	0.002	0.001	0.534	0.45
409	3/12/2003	2:42:36 PM	25.891	23.77	25.489	26.388	24.654	44.355	46.152	9.196	36.91	-1.289	-6.142	48.495	0.144	0.001	0	391.08	6.51806	44.7	11.9	40.1	2.767	0.021	0.002	0.001	0.528	0.45
410	3/12/2003	2:43:36 PM	25.878	23.77	25.451	26.305	24.645	44.057	45.675	9.128	36.774	-1.289	-6.148	48.573	0.144	0.001	0	392.08	6.53472	44.2	11.9	39.9	2.752	0.021	0.002	0.001	0.531	0.45
411	3/12/2003	2:44:36 PM	25.886	23.784	25.433	26.247	24.533	44.094	45.722	9.066	36.883	-1.289	-6.136	48.793	0.145	0.001	0	393.08	6.55139	44.3	12.0	40.0	2.767	0.022	0.002	0.001	0.534	0.45
412	3/12/2003	2:45:36 PM	25.891	23.785	25.438	26.153	24.599	44.225	46.001	9.111	36.087	-1.289	-6.154	48.701	0.144	0.001	0	394.08	6.56806	44.5	11.9	40.1	2.768	0.021	0.002	0.001	0.528	0.45
413	3/12/2003	2:46:36 PM	25.888	23.8	25.458	26.133	24.474	44.049	45.795	9.049	36.94	-1.289	-6.151	48.441	0.144	0.001	0	395.08	6.58472	44.3	11.9	39.9	2.754	0.021	0.002	0.001	0.531	0.45
414	3/12/2003	2:47:36 PM	25.891	23.795	25.428	26.078	24.444	44.034	45.881	9.068	36.875	-1.289	-6.136	48.592	0.144	0.001	0	396.08	6.60139	44.4	11.9	40.0	2.765	0.021	0.002	0.001	0.531	0.45
415	3/12/2003	2:48:36 PM	25.886	23.815	25.438	26.053	24.434	44.892	45.672	9.103	36.633	-1.289	-6.139	48.761	0.142	0.001	0	397.08	6.61806	44.2	11.9	39.8	2.741	0.021	0.002	0.001	0.526	0.45
416	3/12/2003	2:49:36 PM	25.901	23.825	25.453	26.018	24.499	44.07	45.747	9.041	36.977	-1.289	-6.142	48.803	0.143	0.001	0	398.08	6.63472	44.3	12.0	40.0	2.759	0.021	0.002	0.001	0.530	0.45
417	3/12/2003	2:50:36 PM	25.888	23.815	25.442	26.081	24.392	44.351	45.728	9.073	36.923	-1.289	-6.148	48.699	0.142	0.001	0	399.08	6.65139	44.3	11.9	39.9	2.752	0.021	0.002	0.001	0.534	0.45
418	3/12/2003	2:51:36 PM	25.888	23.818	25.436	25.945	24.361	43.878	45.373	9.086	36.506	-1.286	-6.142	48.682	0.143	0.001	0	400.08	6.66806	43.9	11.9	39.6	2.730	0.021	0.002	0.001	0.531	0.45
419	3/12/2003	2:52:36 PM	25.902	23.822	25.525	25.94	24.314	44.018	45.888	9.099	36.779	-1.286	-6.145	49.003	0.143	0.001	0	401.08	6.68472	44.4	12.0	39.9	2.751	0.021	0.002	0.001	0.527	0.45
420	3/12/2003	2:53:36 PM	25.917	23.821	25.524	25.904	24.319	44.088	46.034	9.183	36.584	-1.289	-6.139	48.757	0.143	0.001	0	402.08	6.70139	44.6	11.9	39.8	2.747	0.021	0.002	0.001	0.527	0.45
421	3/12/2003	2:54:36 PM	25.92	23.81	25.508	25.888	24.318	44.18	45.635	9.051	36.631	-1.289	-6.151	48.715	0.143	0.001	0	403.08	6.71806	44.2	11.9	39.7	2.730	0.021	0.002	0.001	0.523	0.45
422	3/12/2003	2:55:36 PM	25.93	23.817	25.492	25.881	24.322	44.148	45.808	9.074	36.643	-1.289	-6.151	48.734	0.141	0.001	0	404.08	6.73472	44.1	11.9	40.0	2.750	0.021	0.002	0.001	0.519	0.44
423	3/12/2003	2:56:36 PM	25.928	23.808	25.486	25.871	24.301	43.972	45.667	9.022	36.93	-1.286	-6.133	48.77	0.145	0.001	0	405.08	6.75139	44.4	12.0	39.9	2.744	0.022	0.002	0.001	0.534	0.45
424	3/12/2003	2:57:36 PM	25.932	23.807	25.505	25.839	24.27	44.039	45.875	9.152	36.781	-1.284	-6.154	48.761	0.142	0.001	0	406.08	6.76806	44.4	11.9	39.9	2.752	0.021	0.002	0.001	0.523	0.45
425	3/12/2003	2:58:36 PM	25.936	23.801	25.484	25.834	24.254	43.86	45.795	9.053	36.688	-1.286	-6.162	48.823	0.142	0.001	0	407.08	6.78472	44.3	12.0	39.8	2.742	0.021	0.002	0.001	0.525	0.45
426	3/12/2003	2:59:36 PM	25.936	23.819	25.497	25.827	24.242	43.841	45.865	9.074	36.903	-1.289	-6.168	48.876	0.142	0.001	0	408.08	6.80139	44.1	11.9	39.9	2.752	0.021	0.002	0.001	0.518	0.45
427	3/12/2003	3:00:36 PM	25.913	23.783	25.451	25.795	24.206	43.854	45.825	9.098	36.852	-1.286	-6.156	48.636	0.142	0.001	0	409.08	6.81806	44.4	11.9	39.8	2.748	0.021	0.002	0.001	0.525	0.45
428	3/12/2003	3:01:36 PM	25.912	23.776	25.464	25.759	24.194	43.933	45.886	9.059	36.715	-1.286	-6.162	48.522	0.142	0.001	0	410.08	6.83472	44.4	11.9	39.8	2.746	0.021	0.002	0.001	0.525	0.45
429	3/12/2003	3:02:36 PM	25.93	23.789	25.447	25.717	24.187	43.927	45.979	9.107	36.623	-1.284	-6.161	48.562	0.142	0.001	0	411.08	6.85139	44.5	11.9	39.8	2.742	0.021	0.002	0.001	0.526	0.45
430	3/12/2003	3:03:36 PM	25.889	23.788	25.421	25.61	24.188	43.85	45.895	9.052	36.627	-1.289	-6.168	48.554	0.141	0.001	0	412.08	6.86806	44.4	11.9	39.7	2.730	0.021	0.002	0.001	0.523	0.44
431	3/12/2003	3:04:36 PM	25.889	23.787	25.448	25.614	24.188	44.282	45.848	9.174	36.714	-1.289	-6.171	48.594	0.141	0.001												

521	3/12/2003	4:33:39 PM	25.99	23.88	25.548	25.992	24.303	43.809	46.262	9.145	35.576	-1.289	-1.97	48.189	0.132	0.001	0	502.13	8.38899	44.8	11.8	39.7	2.737	0.020	0.019	0.000	0.000	0.468	0.42
522	3/12/2003	4:34:39 PM	26.08	23.898	25.565	26.09	24.306	43.796	46.266	9.129	35.639	-1.286	-1.322	48.18	0.133	0.001	0	503.13	8.38556	44.8	11.8	39.7	2.738	0.020	0.020	0.000	0.000	0.491	0.42
523	3/12/2003	4:35:39 PM	25.99	23.89	25.588	26.128	24.312	43.889	46.245	9.105	35.776	-1.292	-1.6	48.243	0.13	0.001	0	504.13	8.40222	44.8	11.8	39.8	2.745	0.019	0.019	0.000	0.000	0.479	0.41
524	3/12/2003	4:36:39 PM	25.999	23.909	25.657	26.262	24.318	43.963	46.247	9.236	35.633	-1.289	-2.006	48.181	0.135	0.001	0	505.13	8.41889	44.8	11.8	39.8	2.745	0.020	0.020	0.000	0.000	0.496	0.42
525	3/12/2003	4:37:39 PM	26.019	23.924	25.702	26.381	24.327	44.037	46.208	9.151	35.439	-1.298	-1.913	48.271	0.133	0.001	0	506.13	8.39563	44.7	11.8	39.6	2.730	0.020	0.019	0.000	0.000	0.491	0.42
526	3/12/2003	4:38:39 PM	26.068	23.948	25.776	26.53	24.302	43.664	46.117	9.114	35.4	-1.289	-1.648	48.216	0.134	0.001	0	507.13	8.45222	44.6	11.8	39.5	2.726	0.020	0.020	0.000	0.000	0.494	0.42
527	3/12/2003	4:39:39 PM	26.067	23.947	25.795	26.569	24.303	43.652	46.37	9.198	35.514	-1.289	-1.148	48.434	0.133	0.001	0	508.13	8.46889	44.9	11.8	39.7	2.738	0.020	0.019	0.000	0.000	0.489	0.42
528	3/12/2003	4:40:39 PM	26.066	23.955	25.743	26.537	24.308	44.024	46.454	9.036	35.925	-1.289	-1.674	48.573	0.133	0.001	0	509.13	8.49556	45.0	11.8	40.0	2.756	0.020	0.019	0.000	0.000	0.486	0.41
529	3/12/2003	4:41:39 PM	26.102	23.97	25.696	26.519	24.3	43.593	46.022	9.164	35.442	-1.299	-1.17	48.302	0.134	0.001	0	510.13	8.50222	44.5	12.0	39.5	2.724	0.020	0.020	0.000	0.000	0.491	0.42
530	3/12/2003	4:42:39 PM	26.082	23.978	25.7	26.49	24.578	43.778	46.169	9.038	35.723	-1.289	-1.614	48.55	0.138	0.001	0	511.13	8.51889	44.7	11.8	39.8	2.741	0.021	0.020	0.000	0.000	0.508	0.43
531	3/12/2003	4:43:39 PM	26.126	23.963	25.666	26.445	24.582	43.452	45.875	9.077	35.226	-1.292	-1.6	48.271	0.13	0.001	0	512.13	8.53556	44.4	11.8	39.3	2.712	0.019	0.019	0.000	0.000	0.484	0.41
532	3/12/2003	4:44:39 PM	26.126	23.968	25.626	26.396	24.582	43.452	45.875	9.077	35.226	-1.292	-1.6	48.271	0.13	0.001	0	513.13	8.55222	44.4	11.8	39.3	2.712	0.019	0.019	0.000	0.000	0.484	0.41
533	3/12/2003	4:45:39 PM	26.142	24.013	25.65	26.355	24.579	43.466	45.897	9.056	35.364	-1.292	-1.972	48.202	0.002	0.001	0	514.13	8.56889	44.8	11.8	39.4	2.734	0.020	0.020	0.000	0.000	0.493	0.42
534	3/12/2003	4:46:39 PM	26.181	24.013	25.615	26.245	24.577	43.466	45.897	9.056	35.364	-1.292	-1.972	48.202	0.002	0.001	0	515.13	8.58556	44.8	11.8	39.4	2.734	0.020	0.020	0.000	0.000	0.493	0.42
535	3/12/2003	4:47:39 PM	26.141	24.031	25.324	26.168	24.595	44.21	46.32	8.895	36.202	-1.284	-0.791	47.337	0.002	0.001	0	516.13	8.60222	44.8	11.6	40.2	2.772	0.020	0.000	0.000	0.000	0.007	0.01
536	3/12/2003	4:48:39 PM	26.082	24.033	25.36	26.036	24.594	43.626	46.256	8.84	35.686	-1.286	-0.754	47.883	0.156	0.001	0	517.13	8.61889	44.8	11.7	39.7	2.734	0.023	0.023	0.001	0.001	0.581	0.49
537	3/12/2003	4:49:39 PM	26.021	24.031	25.339	25.893	24.526	44.067	46.336	9.023	35.899	-1.286	-0.852	47.803	0.153	0.001	0	518.13	8.63556	45.2	11.7	40.0	2.757	0.023	0.023	0.001	0.001	0.566	0.49
538	3/12/2003	4:50:39 PM	25.985	24.036	25.343	25.833	24.468	45.184	46.217	9.124	35.788	-1.286	-0.844	47.956	0.148	0.001	0	519.13	8.65222	44.7	11.8	39.7	2.742	0.020	0.020	0.000	0.000	0.574	0.47
539	3/12/2003	4:51:39 PM	25.949	24.024	25.327	25.816	24.437	44.036	46.49	8.949	35.951	-1.286	-0.835	47.937	0.147	0.001	0	520.13	8.66889	45.0	11.7	40.0	2.757	0.022	0.022	0.002	0.001	0.543	0.46
540	3/12/2003	4:52:39 PM	25.928	24.013	25.34	25.845	24.416	43.802	46.206	8.96	35.648	-1.289	-0.977	47.797	0.15	0.001	0	521.13	8.68556	44.7	11.7	39.7	2.739	0.022	0.022	0.001	0.001	0.558	0.47
541	3/12/2003	4:53:39 PM	25.936	24.022	25.354	25.879	24.404	43.896	46.306	9.02	35.668	-1.286	-0.974	47.922	0.15	0.001	0	522.13	8.70222	44.8	11.7	39.8	2.742	0.022	0.022	0.001	0.001	0.557	0.47
542	3/12/2003	4:54:39 PM	25.909	24.011	25.337	25.857	24.387	43.889	46.341	9.067	35.547	-1.286	-0.974	48.099	0.142	0.001	0	523.13	8.71889	44.9	11.8	39.7	2.738	0.021	0.021	0.001	0.001	0.538	0.45
543	3/12/2003	4:55:39 PM	26.007	24.008	25.36	25.89	24.38	43.8	46.221	9.014	35.521	-1.286	-0.987	47.95	0.144	0.001	0	524.13	8.73556	44.8	11.8	39.7	2.734	0.021	0.021	0.001	0.001	0.536	0.46
544	3/12/2003	4:56:39 PM	25.802	24.007	25.394	25.874	24.345	43.858	46.287	9.013	35.633	-1.286	-0.997	47.793	0.146	0.001	0	525.13	8.75222	44.8	11.7	39.7	2.740	0.022	0.022	0.001	0.001	0.542	0.46
545	3/12/2003	4:57:39 PM	25.88	23.99	25.382	25.782	24.322	44.363	46.808	9.04	36.157	-1.284	-0.617	48.126	0.143	0.001	0	526.13	8.76889	45.3	11.8	40.3	2.775	0.021	0.021	0.001	0.001	0.524	0.45
546	3/12/2003	4:58:39 PM	25.878	23.989	25.381	25.736	24.296	44.875	47.104	9.079	36.681	-1.289	-0.941	48.021	0.145	0.001	0	527.13	8.78556	45.7	11.8	40.6	2.912	0.022	0.022	0.002	0.001	0.536	0.46
547	3/12/2003	4:59:39 PM	25.859	23.982	25.369	25.693	24.292	44.46	46.826	9.124	36.448	-1.286	-0.974	48.099	0.142	0.001	0	528.13	8.80222	45.1	11.8	40.7	2.834	0.021	0.021	0.001	0.001	0.498	0.47
548	3/12/2003	5:00:39 PM	25.849	23.959	25.416	25.661	24.236	44.73	47.044	9.109	36.434	-1.286	-0.942	48.317	0.144	0.001	0	529.13	8.81889	45.6	11.8	40.6	2.968	0.021	0.021	0.001	0.001	0.523	0.44
549	3/12/2003	5:01:39 PM	25.852	23.967	25.444	25.619	24.199	44.844	47.352	9.122	36.554	-1.284	-0.988	48.296	0.141	0.001	0	530.13	8.83556	45.9	11.8	40.7	2.806	0.021	0.021	0.001	0.001	0.510	0.43
550	3/12/2003	5:02:39 PM	25.845	23.951	25.429	25.558	24.178	44.687	47.197	9.184	36.296	-1.289	-0.968	48.202	0.144	0.001	0	531.13	8.85222	45.7	11.8	40.5	2.792	0.021	0.021	0.001	0.001	0.524	0.45
551	3/12/2003	5:03:39 PM	25.851	23.951	25.444	25.528	24.198	44.645	47.044	9.227	36.235	-1.286	-0.977	48.218	0.143	0.001	0	532.13	8.86889	45.6	11.8	40.6	2.788	0.021	0.021	0.001	0.001	0.521	0.44
552	3/12/2003	5:04:39 PM	25.861	23.949	25.421	25.491	24.188	44.668	46.992	9.184	36.296	-1.286	-0.977	48.131	0.143	0.001	0	533.13	8.88556	45.7	11.8	40.6	2.792	0.021	0.021	0.001	0.001	0.519	0.44
553	3/12/2003	5:05:39 PM	25.865	23.935	25.498	25.547	24.198	44.869	47.299	9.192	36.421	-1.286	-0.977	48.311	0.143	0.001	0	534.13	8.90222	45.8	11.8	40.6	2.802	0.021	0.021	0.001	0.001	0.517	0.44
554	3/12/2003	5:06:39 PM	25.839	23.909	25.462	25.471	24.076	44.881	47.154	9.129	36.395	-1.289	-1.07	48.434	0.14	0.001	0	535.13	8.91889	45.7	11.9	40.5	2.795	0.021	0.021	0.001	0.001	0.508	0.43
555	3/12/2003	5:07:39 PM	25.817	23.882	25.445	25.319	24.049	44.648	47.265	9.124	36.698	-1.286	-1.004	48.426	0.142	0.001	0	536.13	8.93556	45.8	11.9	40.8	2.811	0.021	0.021	0.001	0.001	0.513	0.44
556	3/12/2003	5:08:39 PM	25.826	23.882	25.468	25.363	24.052	44.657	47.47	9.124	36.698	-1.286	-1.004	48.426	0.142	0.001	0	537.13	8.95222	45.7	11.9	40.7	2.802	0.021	0.021	0.001	0.001	0.511	0.44
557	3/12/2003	5:09:39 PM	25.834	23.879	25.481	25.345	24.036	44.697	47.038	9.227	36.303	-1.286	-1.116	48.388	0.143	0.001	0	538.13	8.96889	45.6	11.9	40.5	2.792	0.021	0.021	0.001	0.001	0.519	0.44
558	3/12/2003	5:10:39 PM	25.851	23.876	25.474	25.428	24.038	44.697	47.056	9.129	36.389	-1.286	-1.133	48.405	0.142	0.001	0	539.13	8.98556	45.6	11.9	40.5	2.794	0.021	0.021	0.001	0.001	0.515	0.44
559	3/12/2003	5:11:39 PM	25.879	23.869	25.502	25.481	24.011	44.701	47.322	9.136	36.315	-1.286	-1.133	47.975	0.002	0.001	0	540.13	8.99917	45.8	11.8	40.3	2.814	0.020	0.020	0.001	0.001	0.513	0.44
560	3/12/2003	5:12:39 PM	25.878	23.866	25.504	25.473	23.988	44.697	47.322	9.088</																			

651	3/12/2003	6:43:01 PM	26.03	23.814	25.702	25.442	24.418	44.562	46.878	9.31	36.2	-1.289	-6.288	48.719	0.132	0.001	0	631.50	10.525	45.4	11.9	40.4	2.784	0.020	0.019	0.000	0.478	0.41
652	3/12/2003	6:44:01 PM	26.025	23.815	25.693	25.372	24.383	44.606	46.841	9.289	36.225	-1.289	-6.281	48.701	0.131	0.001	0	632.50	10.5417	45.4	11.9	40.4	2.787	0.019	0.019	0.000	0.470	0.40
653	3/12/2003	6:45:01 PM	26.036	23.82	25.708	25.277	24.338	44.645	47.04	9.363	36.063	-1.286	-6.282	48.673	0.126	0.001	0	633.50	10.5583	45.6	12.0	40.4	2.782	0.019	0.019	0.000	0.456	0.39
654	3/12/2003	6:46:01 PM	26.03	23.819	25.677	25.141	24.297	44.533	46.816	9.268	36.161	-1.286	-6.283	48.659	0.13	0.001	0	634.50	10.575	45.3	11.9	40.3	2.782	0.019	0.019	0.000	0.471	0.40
655	3/12/2003	6:47:01 PM	26.033	23.812	25.655	24.931	24.24	44.466	46.936	9.213	36.286	-1.286	-6.272	48.755	0.129	0.001	0	635.50	10.5917	45.5	11.9	40.5	2.794	0.019	0.019	0.000	0.457	0.40
656	3/12/2003	6:48:01 PM	26.03	23.81	25.673	24.926	24.213	44.707	47.077	9.39	36.981	-1.286	-6.292	48.845	0.13	0.001	0	636.50	10.6083	45.6	12.0	40.3	2.782	0.019	0.019	0.000	0.471	0.40
657	3/12/2003	6:49:01 PM	26.022	23.801	25.67	24.833	24.149	44.355	46.531	9.25	36.965	-1.284	-6.286	48.843	0.13	0.001	0	637.50	10.625	45.1	12.0	40.2	2.789	0.019	0.019	0.000	0.474	0.40
658	3/12/2003	6:50:01 PM	26.998	23.777	25.631	24.739	24.095	44.465	46.728	9.265	36.122	-1.289	-6.24	49.053	0.126	0.001	0	638.50	10.6417	45.3	12.0	40.3	2.778	0.019	0.019	0.000	0.458	0.39
659	3/12/2003	6:51:01 PM	26.033	23.788	25.627	24.671	24.054	44.609	47.15	9.412	36.253	-1.289	-6.24	49.022	0.131	0.001	0	639.50	10.6583	45.7	12.0	40.5	2.794	0.019	0.019	0.000	0.457	0.40
660	3/12/2003	6:52:01 PM	26.995	23.754	25.643	24.6	23.977	44.678	46.99	9.376	36.122	-1.289	-6.253	49.008	0.129	0.001	0	640.50	10.675	45.5	12.0	40.4	2.778	0.019	0.019	0.000	0.468	0.40
661	3/12/2003	6:53:01 PM	26.977	23.742	25.645	24.523	23.934	44.679	46.891	9.313	36.319	-1.286	-6.29	49.933	0.129	0.001	0	641.50	10.6917	45.4	12.0	40.5	2.792	0.019	0.019	0.000	0.466	0.40
662	3/12/2003	6:54:01 PM	26.964	23.723	25.637	24.389	23.916	44.503	46.831	9.317	36.969	-1.289	-6.262	49.831	0.127	0.001	0	642.50	10.7083	45.4	12.0	40.2	2.774	0.019	0.019	0.000	0.462	0.39
663	3/12/2003	6:55:01 PM	26.956	23.711	25.624	24.376	23.953	44.569	46.858	9.332	36.08	-1.286	-6.249	49.875	0.13	0.001	0	643.50	10.725	45.4	12.0	40.3	2.780	0.019	0.019	0.000	0.472	0.40
664	3/12/2003	6:56:01 PM	26.948	23.698	25.642	24.409	23.978	44.638	46.757	9.246	36.29	-1.284	-6.232	49.875	0.123	0.001	0	644.50	10.7417	45.3	12.0	40.4	2.786	0.019	0.019	0.000	0.446	0.38
665	3/12/2003	6:57:01 PM	26.948	23.693	25.661	24.478	24.025	44.675	46.982	9.357	36.016	-1.286	-6.289	49.751	0.13	0.001	0	645.50	10.7583	45.5	11.9	40.3	2.778	0.019	0.019	0.000	0.472	0.40
666	3/12/2003	6:58:01 PM	26.948	23.682	25.651	24.544	24.045	44.757	46.97	9.309	36.411	-1.286	-6.11	49.747	0.129	0.001	0	646.50	10.775	45.5	11.9	40.6	2.798	0.019	0.019	0.000	0.465	0.40
667	3/12/2003	6:59:01 PM	26.933	23.667	25.651	24.614	24.075	44.432	46.593	9.298	36.004	-1.284	-6.004	49.579	0.13	0.001	0	647.50	10.7917	45.1	11.9	40.2	2.773	0.020	0.020	0.000	0.491	0.42
668	3/12/2003	7:00:01 PM	26.93	23.659	25.672	24.711	24.102	44.807	47.052	9.351	36.254	-1.284	-6.235	49.256	0.128	0.001	0	648.50	10.8083	45.5	11.9	40.5	2.794	0.019	0.019	0.000	0.457	0.39
669	3/12/2003	7:01:01 PM	26.942	23.681	25.71	24.798	24.139	44.919	47.088	9.371	36.417	-1.284	-6.303	49.371	0.126	0.001	0	649.50	10.825	45.6	11.9	40.7	2.804	0.019	0.019	0.000	0.453	0.39
670	3/12/2003	7:02:01 PM	26.918	23.658	25.656	24.814	24.151	44.811	47.067	9.415	36.276	-1.286	-6.229	49.556	0.123	0.001	0	650.50	10.8417	45.6	11.9	40.5	2.796	0.019	0.019	0.000	0.444	0.38
671	3/12/2003	7:03:01 PM	26.932	23.661	25.684	24.903	24.194	44.803	47.096	9.439	36.12	-1.286	-6.182	49.898	0.131	0.001	0	651.50	10.8583	45.6	12.0	40.6	2.790	0.020	0.020	0.000	0.474	0.40
672	3/12/2003	7:04:01 PM	26.924	23.660	25.696	24.95	24.226	44.614	46.73	9.31	36.206	-1.284	-6.194	49.663	0.13	0.001	0	652.50	10.875	45.3	11.9	40.4	2.786	0.019	0.019	0.000	0.470	0.40
673	3/12/2003	7:05:01 PM	26.937	23.681	25.705	24.988	24.275	44.697	46.737	9.305	36.194	-1.289	-6.165	49.797	0.126	0.001	0	653.50	10.8917	45.3	12.0	40.4	2.786	0.019	0.019	0.000	0.456	0.39
674	3/12/2003	7:06:33 PM	26.928	23.672	25.701	25.03	24.288	44.915	47.174	9.343	36.348	-1.286	-6.281	49.793	0.13	0.001	0	654.03	10.9067	45.7	12.0	40.6	2.801	0.019	0.019	0.000	0.468	0.40
675	3/12/2003	7:06:33 PM	26.931	23.675	25.704	25.057	24.329	44.637	46.781	9.283	36.307	-1.286	-6.298	49.711	0.13	0.001	0	655.03	10.9172	45.3	11.9	40.5	2.790	0.019	0.019	0.000	0.470	0.40
676	3/12/2003	7:07:33 PM	26.934	23.678	25.692	25.096	24.377	44.902	47.121	9.389	36.364	-1.289	-6.316	49.828	0.128	0.001	0	656.03	10.9338	45.6	11.9	40.6	2.802	0.019	0.019	0.000	0.461	0.39
677	3/12/2003	7:08:33 PM	26.937	23.681	25.695	25.149	24.426	44.789	46.759	9.339	36.327	-1.286	-6.297	49.828	0.129	0.001	0	657.03	10.9504	45.7	11.9	40.7	2.808	0.019	0.019	0.000	0.453	0.39
678	3/12/2003	7:09:33 PM	26.946	23.7	25.733	25.182	24.479	44.997	47.056	9.374	36.548	-1.286	-6.304	49.774	0.126	0.001	0	658.03	10.9672	45.6	12.0	40.8	2.811	0.019	0.019	0.000	0.451	0.38
679	3/12/2003	7:10:33 PM	26.948	23.697	25.71	25.149	24.346	44.416	46.566	9.341	36.84	-1.289	-6.33	49.502	0.127	0.001	0	659.03	10.9839	45.1	11.9	40.1	2.767	0.019	0.019	0.000	0.463	0.39
680	3/12/2003	7:11:33 PM	26.963	23.698	25.651	25.115	24.311	44.722	47.013	9.352	36.217	-1.286	-6.221	49.501	0.127	0.001	0	660.03	11.0006	45.5	11.9	40.5	2.790	0.019	0.019	0.000	0.459	0.39
681	3/12/2003	7:12:33 PM	26.963	23.707	25.67	25.029	24.24	44.736	46.598	9.282	36.356	-1.286	-6.336	49.633	0.126	0.001	0	661.03	11.0172	45.5	12.0	40.5	2.786	0.019	0.019	0.000	0.455	0.39
682	3/12/2003	7:13:33 PM	26.94	23.674	25.698	24.908	24.288	44.684	46.914	9.31	36.043	-1.289	-6.241	49.743	0.129	0.001	0	662.03	11.0338	45.4	11.9	40.4	2.789	0.019	0.019	0.000	0.453	0.39
683	3/12/2003	7:14:33 PM	26.943	23.677	25.656	24.814	24.145	44.548	46.823	9.314	36.104	-1.289	-6.29	49.772	0.131	0.001	0	663.03	11.0504	45.3	12.0	40.3	2.780	0.020	0.020	0.000	0.475	0.40
684	3/12/2003	7:15:33 PM	26.954	23.678	25.622	24.705	24.098	44.589	46.808	9.319	36.168	-1.289	-6.304	49.931	0.128	0.001	0	664.03	11.0672	45.3	12.0	40.4	2.784	0.019	0.019	0.000	0.464	0.40
685	3/12/2003	7:16:33 PM	26.945	23.659	25.593	24.626	24.027	44.579	46.777	9.238	36.305	-1.286	-6.29	49.803	0.129	0.001	0	665.03	11.0839	45.3	12.0	40.4	2.788	0.019	0.019	0.000	0.468	0.40
686	3/12/2003	7:17:33 PM	26.958	23.679	25.668	24.753	24.068	44.684	46.914	9.31	36.043	-1.289	-6.241	49.828	0.129	0.001	0	666.03	11.1006	45.5	12.0	40.6	2.798	0.019	0.019	0.000	0.453	0.39
687	3/12/2003	7:18:33 PM	26.958	23.652	25.511	24.483	23.92	44.62	46.905	9.314	36.131	-1.286	-6.281	49.752	0.125	0.001	0	667.03	11.1172	45.4	11.9	40.4	2.7					

781	3/12/2003	8:52:33 PM	25.418	23.131	25.201	23.767	23.494	44.798	47.147	9.399	36.428	-1.286	-6.316	48.38	0.119	0.001	0	761.03	12.6899	45.7	11.9	40.6	2.800	0.018	0.018	0.000	0.434	0.37
782	3/12/2003	8:53:33 PM	25.418	23.126	25.221	23.827	23.514	44.548	47.059	9.363	36.065	-1.286	-6.321	48.107	0.119	0.001	0	762.03	12.7006	45.6	11.9	40.6	2.779	0.018	0.018	0.000	0.437	0.37
783	3/12/2003	8:54:33 PM	25.414	23.121	25.247	23.889	23.54	44.674	47.146	9.368	36.137	-1.284	-6.304	48.283	0.119	0.001	0	763.03	12.7172	45.7	11.9	40.6	2.786	0.018	0.018	0.000	0.436	0.37
784	3/12/2003	8:55:33 PM	25.414	23.117	25.252	23.954	23.555	44.625	47.069	9.416	36.045	-1.284	-6.304	48.294	0.119	0.001	0	764.03	12.7359	45.6	11.9	40.6	2.781	0.018	0.018	0.000	0.437	0.37
785	3/12/2003	8:56:33 PM	25.417	23.119	25.26	24.011	23.688	44.565	47.056	9.343	36.008	-1.286	-6.317	48.027	0.119	0.001	0	765.03	12.7506	45.7	11.9	40.6	2.786	0.018	0.018	0.000	0.440	0.37
786	3/12/2003	8:57:33 PM	25.414	23.111	25.247	24.083	23.605	44.944	47.478	9.404	36.458	-1.289	-6.307	48.092	0.119	0.001	0	766.03	12.7672	46.0	11.9	40.7	2.806	0.018	0.018	0.000	0.433	0.37
787	3/12/2003	8:58:33 PM	25.418	23.12	25.291	24.137	23.689	44.751	47.253	9.435	36.149	-1.286	-6.301	48.338	0.118	0.001	0	767.03	12.7839	45.8	11.9	40.5	2.789	0.018	0.017	0.000	0.431	0.37
788	3/12/2003	8:59:33 PM	25.417	23.119	25.279	24.196	23.655	44.416	47.007	9.413	36.84	-1.289	-6.298	48.225	0.118	0.001	0	768.03	12.8006	45.6	11.9	40.4	2.767	0.018	0.017	0.000	0.435	0.37
789	3/12/2003	9:00:33 PM	25.417	23.112	25.338	24.205	23.747	44.565	47.056	9.343	36.008	-1.286	-6.317	48.346	0.119	0.001	0	769.03	12.8172	45.6	11.9	40.5	2.780	0.018	0.018	0.000	0.440	0.37
790	3/12/2003	9:01:33 PM	25.434	23.131	25.436	24.264	23.655	44.513	47.112	9.322	36.055	-1.286	-6.298	48.386	0.117	0.001	0	770.03	12.8339	45.6	11.9	40.3	2.777	0.017	0.017	0.000	0.428	0.36
791	3/12/2003	9:02:33 PM	25.446	23.128	25.474	24.286	23.773	44.171	46.984	9.257	36.721	-1.286	-6.284	48.566	0.119	0.001	0	771.03	12.8506	45.2	11.9	39.9	2.754	0.018	0.018	0.000	0.438	0.37
792	3/12/2003	9:03:33 PM	25.479	23.137	25.507	24.345	23.776	44.562	47.179	9.303	36.169	-1.286	-6.264	48.713	0.118	0.001	0	772.03	12.8672	45.7	11.9	40.4	2.783	0.018	0.017	0.000	0.430	0.37
793	3/12/2003	9:04:33 PM	25.498	23.14	25.496	24.333	23.794	44.486	47.222	9.221	36.987	-1.289	-6.264	48.644	0.117	0.001	0	773.03	12.8839	45.7	12.0	40.2	2.774	0.017	0.017	0.000	0.428	0.36
794	3/12/2003	9:05:33 PM	25.515	23.142	25.463	24.395	23.822	44.384	47.005	9.191	36.143	-1.289	-6.269	48.612	0.117	0.001	0	774.03	12.9006	45.4	11.9	40.1	2.764	0.017	0.017	0.000	0.430	0.37
795	3/12/2003	9:06:33 PM	25.534	23.151	25.462	24.389	23.841	44.289	46.862	9.268	36.875	-1.286	-6.264	48.454	0.117	0.001	0	775.03	12.9172	45.5	11.9	40.0	2.755	0.018	0.018	0.000	0.443	0.36
796	3/12/2003	9:07:33 PM	25.548	23.165	25.416	24.233	23.88	44.246	46.998	9.309	36.674	-1.289	-6.264	48.713	0.12	0.001	0	776.03	12.9339	45.5	11.9	40.0	2.755	0.018	0.018	0.000	0.443	0.36
797	3/12/2003	9:08:33 PM	25.567	23.179	25.395	24.462	23.939	44.386	47.021	9.224	36.061	-1.289	-6.313	48.69	0.117	0.001	0	777.03	12.9506	45.5	11.9	40.0	2.773	0.017	0.017	0.000	0.429	0.36
798	3/12/2003	9:09:33 PM	25.545	23.187	25.388	24.461	23.942	44.14	47.95	9.348	36.785	-1.289	-6.327	48.026	0.118	0.001	0	778.03	12.9672	45.7	12.0	39.9	2.751	0.018	0.017	0.000	0.436	0.37
799	3/12/2003	9:10:33 PM	25.523	23.184	25.38	24.437	23.964	44.155	46.742	9.374	36.637	-1.284	-6.31	49.072	0.118	0.001	0	779.03	12.9839	45.3	12.0	39.9	2.751	0.018	0.017	0.000	0.436	0.37
800	3/12/2003	9:11:33 PM	25.524	23.181	25.327	24.409	23.956	44.016	46.68	9.365	36.445	-1.292	-6.327	49.961	0.116	0.001	0	779.88	12.9981	45.2	12.0	39.7	2.739	0.017	0.017	0.000	0.431	0.37
801	3/12/2003	9:12:33 PM	25.53	23.192	25.302	24.42	23.937	44.13	46.87	9.315	36.627	-1.286	-6.299	49.686	0.113	0.001	0	780.88	13.0147	45.4	11.9	39.9	2.749	0.017	0.017	0.000	0.419	0.36
802	3/12/2003	9:13:33 PM	25.523	23.195	25.306	24.343	23.856	44.248	46.841	9.352	36.709	-1.284	-6.266	48.573	0.121	0.001	0	781.88	13.0314	45.4	11.9	40.0	2.756	0.018	0.018	0.000	0.431	0.36
803	3/12/2003	9:14:33 PM	25.521	23.194	25.279	24.266	23.808	44.389	47.063	9.365	36.865	-1.286	-6.31	49.786	0.118	0.001	0	782.88	13.0481	45.6	12.0	40.1	2.767	0.018	0.017	0.000	0.428	0.36
804	3/12/2003	9:15:33 PM	25.514	23.195	25.252	24.153	23.755	44.184	46.777	9.308	36.74	-1.286	-6.272	48.707	0.112	0.001	0	783.88	13.0647	45.3	11.9	40.0	2.755	0.017	0.017	0.000	0.415	0.36
805	3/12/2003	9:16:33 PM	25.489	23.182	25.217	24.008	23.675	44.388	46.957	9.231	36.089	-1.286	-6.31	48.717	0.117	0.001	0	784.88	13.0814	45.5	11.9	40.0	2.773	0.017	0.017	0.000	0.431	0.37
806	3/12/2003	9:17:33 PM	25.495	23.188	25.238	23.939	23.631	44.54	47.083	9.338	36.151	-1.286	-6.298	48.684	0.114	0.001	0	785.88	13.0981	45.6	11.9	40.0	2.782	0.018	0.018	0.000	0.437	0.37
807	3/12/2003	9:18:33 PM	25.477	23.187	25.212	23.607	23.617	44.429	47.007	9.367	36.803	-1.284	-6.326	49.612	0.112	0.001	0	786.88	13.1147	45.6	11.9	40.0	2.781	0.017	0.017	0.000	0.436	0.37
808	3/12/2003	9:19:33 PM	25.479	23.181	25.186	23.722	23.639	44.478	47.294	9.368	36.854	-1.284	-6.347	48.545	0.117	0.001	0	787.88	13.1314	45.8	11.9	40.0	2.789	0.017	0.017	0.000	0.432	0.37
809	3/12/2003	9:20:33 PM	25.474	23.151	25.181	23.641	23.449	44.241	46.876	9.353	36.689	-1.286	-6.292	49.024	0.116	0.001	0	788.88	13.1481	45.4	12.0	40.0	2.761	0.017	0.017	0.000	0.430	0.37
810	3/12/2003	9:21:33 PM	25.458	23.13	25.186	23.675	23.423	44.291	46.938	9.279	36.891	-1.286	-6.307	48.648	0.116	0.001	0	789.88	13.1647	45.6	11.9	40.0	2.784	0.017	0.017	0.000	0.429	0.37
811	3/12/2003	9:22:33 PM	25.453	23.121	25.171	23.551	23.459	44.341	46.945	9.333	36.797	-1.286	-6.347	49.684	0.114	0.001	0	790.88	13.1814	45.5	11.9	40.1	2.783	0.017	0.017	0.000	0.433	0.37
812	3/12/2003	9:23:33 PM	25.447	23.107	25.222	23.603	23.447	44.401	46.992	9.291	36.907	-1.286	-6.311	49.612	0.117	0.001	0	791.88	13.1981	45.6	11.9	40.0	2.781	0.017	0.017	0.000	0.431	0.37
813	3/12/2003	9:24:33 PM	25.442	23.099	25.18	23.675	23.488	44.413	47.086	9.279	36.977	-1.284	-6.31	48.631	0.118	0.001	0	792.88	13.2147	45.6	11.9	40.0	2.771	0.018	0.018	0.000	0.435	0.37
814	3/12/2003	9:25:33 PM	25.413	23.092	25.203	23.743	23.541	44.363	47.027	9.31	36.942	-1.286	-6.307	48.289	0.117	0.001	0	793.88	13.2314	45.6	11.9	40.0	2.788	0.017	0.017	0.000	0.432	0.37
815	3/12/2003	9:26:33 PM	25.418	23.085	25.196	23.767	23.544	44.583	47.298	9.303	36.049	-1.286	-6.319	48.348	0.119	0.001	0	794.88	13.2481	45.8	11.9	40.0	2.780	0.017	0.017	0.000	0.419	0.36
816	3/12/2003	9:27:33 PM	25.413	23.078	25.212	23.607	23.467	44.434	47.059	9.186	36.112	-1.286	-6.311	48.717	0.119	0.001	0	795.88	13.2647	45.6	11.9	40.0	2.777	0.017	0.017	0.000	0.428	0.36
817	3/12/2003	9:28:33 PM	25.425	23.092	25.222	23.934	23.605	44.063	46.692	9.27	36.736	-1.284	-6.284	48.317	0.115	0.001	0	796.88	13.2814									

WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

911	3/12/2003	11:02:24 PM	25.325	23.047	25.198	24.19	23.842	44.451	47.408	9.442	35.803	-1.292	-6.296	46.709	0.111	0.001	0	690.88	14.8481	45.9	11.9	40.1	2.672	0.017	0.016	0.000	0.410	0.35
912	3/12/2003	11:03:16 PM	25.322	23.054	25.205	24.202	23.848	44.714	47.569	9.268	36.29	-1.292	-6.296	46.657	0.111	0.001	0	691.75	14.8626	46.1	11.9	40.5	2.767	0.017	0.016	0.000	0.406	0.35
913	3/12/2003	11:04:16 PM	25.324	23.066	25.232	24.26	23.877	43.933	46.572	9.327	35.398	-1.284	-6.29	46.956	0.111	0.001	0	692.75	14.8792	45.1	11.9	39.6	2.731	0.017	0.016	0.000	0.415	0.35
914	3/12/2003	11:05:16 PM	25.343	23.085	25.246	24.273	23.938	44.138	46.633	9.261	35.689	-1.294	-6.296	46.913	0.111	0.001	0	693.75	14.8958	45.5	11.9	39.9	2.752	0.017	0.016	0.000	0.422	0.35
915	3/12/2003	11:06:16 PM	25.323	23.087	25.213	24.295	23.936	44.43	47.429	9.373	35.826	-1.296	-6.297	46.449	0.111	0.001	0	694.75	14.9125	46.0	11.9	40.1	2.767	0.017	0.016	0.000	0.410	0.35
916	3/12/2003	11:07:16 PM	25.334	23.101	25.237	24.329	23.956	44.277	47.166	9.329	35.815	-1.286	-6.272	46.214	0.112	0.001	0	695.75	14.9292	45.7	11.8	40.0	2.761	0.017	0.017	0.000	0.414	0.35
917	3/12/2003	11:08:16 PM	25.338	23.105	25.246	24.338	23.98	44.239	47.094	9.315	35.83	-1.289	-6.284	46.405	0.111	0.001	0	696.75	14.9458	45.6	11.9	40.0	2.760	0.017	0.016	0.000	0.411	0.35
918	3/12/2003	11:09:16 PM	25.336	23.102	25.223	24.335	23.983	44.291	47.234	9.428	35.682	-1.296	-6.291	46.558	0.111	0.001	0	697.75	14.9625	45.8	11.9	40.0	2.757	0.017	0.016	0.000	0.411	0.35
919	3/12/2003	11:10:16 PM	25.331	23.104	25.204	24.346	23.988	44.372	47.344	9.443	35.623	-1.286	-6.291	46.336	0.112	0.001	0	698.75	14.9792	45.9	11.9	40.0	2.754	0.017	0.017	0.000	0.413	0.35
920	3/12/2003	11:11:16 PM	25.336	23.108	25.304	24.326	23.936	44.02	46.943	9.313	35.564	-1.286	-6.292	46.378	0.112	0.001	0	699.75	14.9958	45.9	11.9	39.8	2.744	0.017	0.017	0.000	0.416	0.35
921	3/12/2003	11:12:16 PM	25.344	23.111	25.347	24.224	23.888	44.387	47.402	9.321	35.881	-1.284	-6.292	46.447	0.111	0.001	0	700.75	15.0125	45.9	11.9	40.1	2.767	0.017	0.016	0.000	0.408	0.35
922	3/12/2003	11:13:16 PM	25.366	23.118	25.304	24.141	23.818	44.192	47.156	9.372	35.656	-1.286	-6.297	46.659	0.111	0.001	0	701.75	15.0292	45.7	11.9	39.9	2.753	0.017	0.016	0.000	0.411	0.35
923	3/12/2003	11:14:16 PM	25.383	23.12	25.296	24.042	23.74	43.941	47.065	9.352	35.521	-1.286	-6.281	46.611	0.113	0.001	0	702.75	15.0458	45.6	11.9	39.8	2.743	0.017	0.017	0.000	0.421	0.35
924	3/12/2003	11:15:16 PM	25.389	23.116	25.277	23.903	23.696	44.111	47.111	9.284	35.639	-1.284	-6.327	46.755	0.111	0.001	0	703.75	15.0625	45.6	11.9	39.9	2.749	0.017	0.016	0.000	0.412	0.35
925	3/12/2003	11:16:16 PM	25.399	23.111	25.247	23.792	23.63	44.146	47.067	9.351	35.688	-1.284	-6.324	46.55	0.112	0.001	0	704.75	15.0792	45.6	11.9	39.9	2.752	0.017	0.017	0.000	0.415	0.35
926	3/12/2003	11:17:16 PM	25.394	23.095	25.217	23.677	23.655	44.142	47.081	9.363	35.576	-1.286	-6.336	46.291	0.109	0.001	0	705.75	15.0958	45.6	11.8	39.9	2.748	0.016	0.016	0.000	0.405	0.34
927	3/12/2003	11:18:16 PM	25.394	23.085	25.211	23.591	23.659	44.331	47.387	9.365	35.641	-1.286	-6.378	46.327	0.110	0.001	0	706.75	15.1125	45.9	11.8	40.1	2.764	0.016	0.016	0.000	0.407	0.35
928	3/12/2003	11:19:16 PM	25.398	23.09	25.226	23.626	23.619	44.354	47.325	9.336	35.795	-1.294	-6.346	46.669	0.111	0.001	0	707.75	15.1292	45.9	11.9	40.0	2.760	0.016	0.016	0.000	0.411	0.35
929	3/12/2003	11:20:16 PM	25.368	23.045	25.166	23.436	23.408	44.262	47.238	9.321	35.84	-1.289	-6.36	46.353	0.111	0.001	0	708.75	15.1458	45.8	11.8	40.1	2.761	0.016	0.016	0.000	0.408	0.35
930	3/12/2003	11:21:16 PM	25.374	23.046	25.172	23.465	23.408	44.057	47.05	9.306	35.557	-1.286	-6.324	46.406	0.112	0.001	0	709.75	15.1625	45.6	11.9	39.8	2.745	0.017	0.017	0.000	0.417	0.35
931	3/12/2003	11:22:16 PM	25.362	23.027	25.178	23.459	23.446	44.548	47.854	9.375	35.922	-1.286	-6.336	46.464	0.112	0.001	0	710.75	15.1792	46.2	11.9	40.2	2.774	0.017	0.017	0.000	0.413	0.35
932	3/12/2003	11:23:16 PM	25.363	23.015	25.186	23.551	23.454	44.347	47.325	9.352	35.797	-1.286	-6.347	46.9	0.111	0.001	0	711.75	15.1958	45.9	11.9	40.1	2.763	0.016	0.016	0.000	0.411	0.35
933	3/12/2003	11:24:16 PM	25.352	23.004	25.17	23.658	23.503	44.175	47.128	9.27	35.793	-1.289	-6.321	46.514	0.111	0.001	0	712.75	15.2125	45.7	11.9	40.0	2.757	0.017	0.016	0.000	0.412	0.35
934	3/12/2003	11:25:16 PM	25.347	23.003	25.164	23.71	23.512	44.343	47.342	9.346	35.789	-1.289	-6.331	46.506	0.111	0.001	0	713.75	15.2292	45.9	11.9	40.1	2.762	0.017	0.016	0.000	0.411	0.35
935	3/12/2003	11:26:16 PM	25.338	22.995	25.186	23.761	23.549	44.125	47.272	9.347	35.486	-1.286	-6.303	46.52	0.109	0.001	0	714.75	15.2458	45.9	11.9	39.8	2.744	0.016	0.016	0.000	0.406	0.35
936	3/12/2003	11:27:16 PM	25.318	22.984	25.191	23.761	23.549	44.161	47.272	9.302	35.74	-1.286	-6.317	46.573	0.111	0.001	0	715.75	15.2625	45.7	11.9	40.0	2.762	0.016	0.016	0.000	0.408	0.35
937	3/12/2003	11:28:16 PM	25.32	22.991	25.188	23.833	23.586	44.335	47.501	9.4	35.766	-1.286	-6.347	46.373	0.111	0.001	0	716.75	15.2792	46.0	11.9	40.1	2.761	0.016	0.016	0.000	0.407	0.35
938	3/12/2003	11:29:16 PM	25.317	22.993	25.189	23.921	23.683	44.289	47.503	9.423	35.623	-1.286	-6.319	46.319	0.111	0.001	0	717.75	15.2958	46.0	11.8	40.0	2.756	0.016	0.016	0.000	0.408	0.35
939	3/12/2003	11:30:16 PM	25.324	22.996	25.217	23.958	23.635	43.906	46.994	9.306	35.343	-1.286	-6.313	46.25	0.111	0.001	0	718.75	15.3125	45.5	11.8	39.6	2.732	0.016	0.016	0.000	0.411	0.35
940	3/12/2003	11:31:16 PM	25.312	22.993	25.205	23.976	23.648	44.119	47.218	9.302	35.613	-1.286	-6.319	46.424	0.111	0.001	0	719.75	15.3292	45.7	11.9	39.9	2.749	0.016	0.016	0.000	0.409	0.35
941	3/12/2003	11:32:16 PM	25.354	22.942	25.317	24.04	23.687	44.186	47.498	9.343	35.684	-1.286	-6.347	46.289	0.111	0.001	0	720.75	15.3458	45.8	11.9	39.9	2.753	0.016	0.016	0.000	0.411	0.35
942	3/12/2003	11:33:16 PM	25.301	22.992	25.188	24.124	23.717	44.306	47.545	9.317	35.717	-1.289	-6.307	46.321	0.111	0.001	0	721.75	15.3625	46.1	11.8	40.0	2.759	0.017	0.016	0.000	0.411	0.35
943	3/12/2003	11:34:16 PM	25.319	23.016	25.232	24.124	23.75	44.036	47.063	9.297	35.598	-1.289	-6.31	46.457	0.111	0.001	0	722.75	15.3792	45.6	11.9	39.8	2.745	0.016	0.016	0.000	0.409	0.35
944	3/12/2003	11:35:16 PM	25.306	23.003	25.214	24.121	23.742	44.194	47.201	9.326	35.813	-1.289	-6.29	46.959	0.109	0.001	0	723.75	15.3958	45.7	11.9	40.0	2.758	0.016	0.016	0.000	0.404	0.34
945	3/12/2003	11:36:16 PM	25.318	23.018	25.247	24.189	23.748	44.196	47.363	9.343	35.684	-1.286	-6.347	46.289	0.111	0.001	0	724.75	15.4125	45.8	11.9	39.9	2.753	0.016	0.016	0.000	0.408	0.35
946	3/12/2003	11:37:16 PM	25.321	23.028	25.244	24.235	23.743	43.823	46.932	9.312	35.32	-1.286	-6.301	46.294	0.111	0.001	0	725.75	15.4292	45.4	11.8	39.6	2.728	0.016	0.016	0.000	0.412	0.35
947	3/12/2003	11:38:16 PM	25.314	23.025	25.312	24.214	23.77	44.393	47.507	9.357	35.8	-1.286	-6.287	46.306	0.111	0.001	0	726.75	15.4458	46.0	11.9	40.2	2.771	0.016	0.016	0.000	0.404	0.34
948	3/12/2003	11:39:16 PM	25.323	23.027	25.319	24.215	23.767	44.15	47.313	9.406	35.327	-1.286	-6.333	46.575	0.111	0.001	0	727.75	15.4625	45.9	11.9	39.8	2.747	0.016	0.016	0.000	0.408	0.35
949	3/12/2003	11:40:16 PM	25.337	23.039	25.311	24.212	23.799	44.21	47.498	9.353	35.709	-1.286	-6.342	46.59	0.109	0.001	0	728.75	15.4792	46.0	11.9	40.0	2.757	0.016	0.016	0.000	0.403	0.34
950	3/12/2003	11:41:16 PM	25.354	23.048	25.304	24.196	23.816	44.186	47.445	9.346	35.684	-1.286	-6.347	46.319	0.111	0.001	0	729.75	15.4958	45.8	11.9	39.8	2.746	0.016	0.016	0.000	0.408	0.35
951	3/12/2003	11:42:16 PM	25.373	23.07	25.286	24.228	23.835	43.999	47.158	9.332	35.308	-1.286	-6.342</															

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SRT-RPP-2003-00087, REV. 0

1041	3/13/2003	1:11:52 AM	25.645	23.137	25.633	23.939	23.726	43.904	47.869	9.761	34.798	-1.286	-6.278	46.409	0.108	0.001	0	1020.35	17.0058	46.4	11.9	39.4	2.713	0.016	0.016	0.000	0.000	0.402	0.34
1042	3/13/2003	1:12:52 AM	25.666	23.133	25.664	23.814	23.657	44.109	47.962	9.679	35.25	-1.289	-6.316	46.205	0.109	0.001	0	1021.35	17.0225	46.5	11.9	39.7	2.736	0.016	0.016	0.000	0.000	0.402	0.34
1043	3/13/2003	1:13:52 AM	25.67	23.117	25.633	23.703	23.591	43.925	47.752	9.779	34.841	-1.284	-6.267	46.317	0.111	0.001	0	1022.35	17.0392	46.3	11.9	39.3	2.712	0.016	0.016	0.000	0.000	0.410	0.35
1044	3/13/2003	1:14:52 AM	25.681	23.113	25.654	23.644	23.441	43.966	47.962	9.766	35.037	-1.284	-6.307	46.503	0.108	0.001	0	1023.35	17.0559	46.5	11.9	39.5	2.734	0.016	0.016	0.000	0.000	0.407	0.34
1045	3/13/2003	1:15:52 AM	25.676	23.088	25.669	23.528	23.466	44.132	48.059	9.801	35.142	-1.284	-6.304	46.195	0.111	0.001	0	1024.35	17.0725	46.4	11.9	39.6	2.733	0.016	0.016	0.000	0.000	0.406	0.35
1046	3/13/2003	1:16:52 AM	25.676	23.088	25.664	23.468	23.457	44.21	48.12	9.625	35.371	-1.284	-6.301	47.948	0.109	0.001	0	1025.35	17.0892	46.6	11.9	39.8	2.743	0.016	0.016	0.000	0.000	0.401	0.34
1047	3/13/2003	1:17:52 AM	25.703	23.074	25.67	23.475	23.483	43.966	48.047	9.668	35.015	-1.286	-6.268	48.088	0.111	0.001	0	1026.35	17.1058	46.6	11.9	39.5	2.733	0.016	0.016	0.000	0.000	0.411	0.35
1048	3/13/2003	1:18:52 AM	25.674	23.025	25.636	23.446	23.459	44.285	48.333	9.677	35.254	-1.289	-6.272	47.918	0.108	0.001	0	1027.35	17.1225	46.9	11.9	39.8	2.742	0.016	0.016	0.000	0.000	0.405	0.34
1049	3/13/2003	1:19:52 AM	25.691	23.025	25.668	23.459	23.442	44.529	48.292	9.644	35.293	-1.289	-6.271	47.815	0.108	0.001	0	1028.35	17.1392	46.8	11.9	39.9	2.748	0.016	0.016	0.000	0.000	0.407	0.34
1050	3/13/2003	1:20:52 AM	25.674	23.027	25.686	23.628	23.481	44.248	48.303	9.688	35.386	-1.286	-6.281	47.86	0.108	0.001	0	1029.35	17.1558	46.8	11.9	39.8	2.745	0.016	0.016	0.000	0.000	0.397	0.34
1051	3/13/2003	1:21:52 AM	25.696	23.017	25.713	23.698	23.571	44.217	48.25	9.676	35.277	-1.284	-6.288	47.656	0.111	0.001	0	1030.35	17.1725	46.8	11.9	39.7	2.740	0.016	0.016	0.000	0.000	0.408	0.35
1052	3/13/2003	1:22:52 AM	25.701	23.002	25.713	23.734	23.581	43.989	47.838	9.678	35.355	-1.289	-6.278	47.802	0.109	0.001	0	1031.35	17.1892	46.4	11.9	39.7	2.736	0.016	0.016	0.000	0.000	0.401	0.34
1053	3/13/2003	1:23:52 AM	25.711	23.007	25.758	23.659	23.618	43.928	47.872	9.624	35.166	-1.286	-6.272	47.969	0.109	0.001	0	1032.35	17.2058	46.4	11.9	39.5	2.725	0.016	0.016	0.000	0.000	0.402	0.34
1054	3/13/2003	1:24:52 AM	25.701	22.997	25.758	23.904	23.621	45.376	49.369	9.725	35.559	-1.286	-6.261	47.602	0.109	0.001	0	1033.35	17.2225	47.9	11.9	41.0	2.825	0.016	0.016	0.000	0.000	0.388	0.33
1055	3/13/2003	1:25:52 AM	25.707	22.999	25.777	23.976	23.638	45.145	49.251	9.775	36.143	-1.286	-6.182	46.552	0.113	0.001	0	1034.35	17.2392	47.8	11.9	40.6	2.802	0.016	0.016	0.000	0.000	0.406	0.35
1056	3/13/2003	1:26:52 AM	25.714	23.005	25.812	24.009	23.655	45.074	49.105	9.816	36.167	-1.289	-6.229	46.648	0.112	0.001	0	1035.35	17.2558	47.6	11.9	40.6	2.801	0.016	0.016	0.000	0.000	0.402	0.34
1057	3/13/2003	1:27:52 AM	25.743	23.065	25.858	24.047	23.668	45.41	49.597	9.899	36.241	-1.289	-6.165	46.459	0.113	0.001	0	1036.35	17.2725	48.1	11.9	40.9	2.818	0.016	0.016	0.000	0.000	0.402	0.34
1058	3/13/2003	1:28:52 AM	25.743	23.004	25.826	24.047	23.659	45.161	49.287	9.868	36.159	-1.289	-6.225	46.715	0.113	0.001	0	1037.35	17.2892	47.8	11.9	40.7	2.803	0.016	0.016	0.000	0.000	0.405	0.34
1059	3/13/2003	1:29:52 AM	25.76	23.022	25.816	24.139	23.741	45.602	49.735	9.888	36.452	-1.286	-6.114	46.292	0.112	0.001	0	1038.35	17.3058	48.3	11.9	41.0	2.829	0.016	0.016	0.000	0.000	0.398	0.34
1060	3/13/2003	1:30:52 AM	25.768	23.019	25.8	24.197	23.759	45.124	49.204	9.782	36.157	-1.286	-6.214	46.562	0.114	0.001	0	1039.35	17.3225	47.7	11.9	40.6	2.802	0.016	0.016	0.000	0.000	0.409	0.35
1061	3/13/2003	1:31:52 AM	25.776	23.027	25.813	24.21	23.762	44.969	49.2	9.861	36.983	-1.286	-6.203	46.388	0.113	0.001	0	1040.35	17.3392	47.7	11.9	40.4	2.787	0.016	0.016	0.000	0.000	0.407	0.35
1062	3/13/2003	1:32:52 AM	25.783	23.03	25.806	24.213	23.81	45.072	49.123	9.828	36.092	-1.286	-6.114	46.938	0.111	0.001	0	1041.35	17.3558	47.7	11.9	40.6	2.798	0.016	0.016	0.000	0.000	0.399	0.34
1063	3/13/2003	1:33:52 AM	25.776	23.033	25.774	24.241	23.827	45.435	49.545	9.851	36.438	-1.289	-6.177	46.627	0.109	0.001	0	1042.35	17.3725	48.1	11.9	40.9	2.822	0.016	0.016	0.000	0.000	0.388	0.33
1064	3/13/2003	1:34:52 AM	25.783	23.044	25.776	24.298	23.844	45.376	49.518	9.868	36.321	-1.286	-6.211	46.557	0.111	0.001	0	1043.35	17.3892	48.0	11.9	40.8	2.816	0.016	0.016	0.000	0.000	0.396	0.34
1065	3/13/2003	1:35:52 AM	25.796	23.063	25.789	24.276	23.868	45.263	49.527	9.844	36.041	-1.286	-6.174	46.522	0.113	0.001	0	1044.35	17.4058	48.1	11.9	40.7	2.804	0.016	0.016	0.000	0.000	0.405	0.34
1066	3/13/2003	1:36:52 AM	25.783	23.065	25.812	24.303	23.875	45.24	49.589	9.878	36.032	-1.284	-6.181	46.429	0.112	0.001	0	1045.35	17.4225	48.0	11.9	40.6	2.802	0.016	0.016	0.000	0.000	0.402	0.34
1067	3/13/2003	1:37:52 AM	25.796	23.072	25.778	24.33	23.912	45.449	49.657	9.932	36.296	-1.286	-6.121	46.29	0.112	0.001	0	1046.35	17.4392	48.2	11.9	40.9	2.818	0.016	0.016	0.000	0.000	0.401	0.34
1068	3/13/2003	1:38:52 AM	25.787	23.074	25.74	24.427	23.934	45.362	49.624	9.896	36.264	-1.286	-6.188	46.407	0.112	0.001	0	1047.35	17.4558	48.1	11.9	40.8	2.814	0.016	0.016	0.000	0.000	0.401	0.34
1069	3/13/2003	1:39:52 AM	25.809	23.096	25.732	24.444	23.965	45.368	49.588	9.828	36.294	-1.286	-6.174	46.493	0.112	0.001	0	1048.35	17.4725	48.1	11.9	40.8	2.815	0.016	0.016	0.000	0.000	0.401	0.34
1070	3/13/2003	1:40:52 AM	25.796	23.088	25.664	24.411	23.968	45.434	49.812	9.963	36.227	-1.289	-6.165	46.371	0.111	0.001	0	1049.35	17.4892	48.3	11.9	40.8	2.815	0.016	0.016	0.000	0.000	0.401	0.34
1071	3/13/2003	1:41:52 AM	25.787	23.097	25.742	24.422	23.981	45.47	49.764	9.931	36.249	-1.286	-6.171	46.336	0.112	0.001	0	1050.35	17.5058	48.1	11.9	40.6	2.807	0.016	0.016	0.000	0.000	0.403	0.34
1072	3/13/2003	1:42:52 AM	25.775	23.112	25.628	24.436	24.002	45.128	49.515	9.862	36.053	-1.289	-6.162	46.56	0.112	0.001	0	1051.35	17.5225	47.8	11.9	40.6	2.799	0.016	0.016	0.000	0.000	0.404	0.34
1073	3/13/2003	1:43:52 AM	25.762	23.119	25.695	24.457	24.014	45.397	49.647	9.863	36.378	-1.286	-6.112	46.032	0.112	0.001	0	1052.35	17.5392	48.2	11.9	40.9	2.819	0.016	0.016	0.000	0.000	0.402	0.34
1074	3/13/2003	1:44:52 AM	25.759	23.126	25.597	24.474	24.016	45.772	49.988	9.969	36.2	-1.286	-6.182	46.233	0.112	0.001	0	1053.35	17.5558	48.5	11.9	40.9	2.840	0.016	0.016	0.000	0.000	0.399	0.34
1075	3/13/2003	1:45:52 AM	25.743	23.138	25.689	24.421	24.033	45.157	49.369	9.839	36.27	-1.286	-6.191	47.929	0.112	0.001	0	1054.35	17.5725	47.9	11.9	40.6	2.802	0.016	0.016	0.000	0.000	0.402	0.34
1076	3/13/2003	1:46:52 AM	25.729	23.14	25.661	24.442	24.047	45.412																					

1171	3/13/2003	3:21:33 AM	25.494	23.211	25.247	24.133	23.916	46.118	50.848	10.688	36.237	-1.286	-6.566	47.841	0.084	0.001	0	1150.03	19.1672	49.4	11.7	41.2	2.839	0.013	0.012	0.000	0.302	0.26	
1172	3/13/2003	3:22:33 AM	25.488	23.2	25.236	24.022	23.845	46.489	51.361	10.8	36.352	-1.286	-6.566	47.57	0.084	0.001	0	1151.03	19.1839	49.9	11.7	41.4	2.866	0.013	0.012	0.000	0.300	0.26	
1173	3/13/2003	3:23:33 AM	25.486	23.194	25.209	23.925	23.788	46.309	51.117	10.666	36.419	-1.286	-6.538	47.526	0.081	0.001	0	1152.03	19.2006	49.6	11.6	41.4	2.862	0.012	0.012	0.000	0.290	0.25	
1174	3/13/2003	3:24:33 AM	25.49	23.193	25.223	23.834	23.727	45.316	50.111	11.491	34.546	-1.289	-6.603	49.002	0.08	0.001	0	1153.03	19.2172	48.6	12.2	39.9	2.753	0.012	0.012	0.000	0.297	0.25	
1175	3/13/2003	3:25:33 AM	25.47	23.167	25.217	23.713	23.696	45.822	50.451	11.472	35.132	-1.286	-6.625	49.621	0.079	0.001	0	1154.03	19.2339	49.0	12.2	40.5	2.791	0.012	0.012	0.000	0.289	0.25	
1176	3/13/2003	3:26:33 AM	25.463	23.155	25.281	23.661	23.629	45.395	50.215	11.41	34.722	-1.286	-6.625	49.399	0.079	0.001	0	1155.03	19.2506	48.7	12.1	40.1	2.762	0.012	0.012	0.000	0.292	0.25	
1177	3/13/2003	3:27:33 AM	25.496	23.145	25.321	23.696	23.664	45.669	50.257	11.352	35.001	-1.289	-6.602	49.326	0.078	0.001	0	1156.03	19.2672	48.8	12.1	40.3	2.777	0.012	0.012	0.000	0.286	0.24	
1178	3/13/2003	3:28:33 AM	25.473	23.135	25.351	23.61	23.609	45.625	50.325	11.22	35.277	-1.284	-6.623	48.005	0.079	0.001	0	1157.03	19.2839	48.9	12.0	40.5	2.789	0.012	0.012	0.000	0.280	0.25	
1179	3/13/2003	3:29:33 AM	25.466	23.137	25.377	23.672	23.62	45.266	49.988	11.391	34.646	-1.284	-6.617	49.295	0.079	0.001	0	1158.03	19.3006	48.5	12.1	40.0	2.754	0.012	0.012	0.000	0.292	0.25	
1180	3/13/2003	3:30:33 AM	25.478	23.115	25.375	23.66	23.644	45.524	50.373	11.285	35.037	-1.286	-6.634	49.141	0.078	0.001	0	1159.03	19.3172	48.9	12.0	40.3	2.777	0.012	0.012	0.000	0.286	0.24	
1181	3/13/2003	3:31:33 AM	25.481	23.108	25.399	23.724	23.672	45.505	50.288	11.303	34.99	-1.284	-6.614	48.87	0.075	0.001	0	1160.03	19.3339	48.8	12.0	40.2	2.775	0.011	0.011	0.000	0.275	0.23	
1182	3/13/2003	3:32:33 AM	25.47	23.087	25.403	23.789	23.671	45.704	50.546	11.255	35.134	-1.286	-6.654	48.772	0.077	0.001	0	1161.03	19.3506	49.1	12.0	40.4	2.787	0.011	0.011	0.000	0.281	0.24	
1183	3/13/2003	3:33:33 AM	25.481	23.088	25.444	23.659	23.682	45.457	50.335	11.190	34.972	-1.289	-6.664	48.678	0.076	0.001	0	1162.03	19.3672	48.9	11.9	40.2	2.773	0.011	0.011	0.000	0.278	0.24	
1184	3/13/2003	3:34:33 AM	25.491	23.078	25.489	23.904	23.707	45.472	50.288	11.312	34.89	-1.284	-6.663	48.829	0.075	0.001	0	1163.03	19.3839	48.8	12.0	40.2	2.770	0.011	0.011	0.000	0.274	0.23	
1185	3/13/2003	3:35:33 AM	25.517	23.084	25.53	23.946	23.726	45.522	50.439	11.207	35.003	-1.286	-6.686	48.382	0.075	0.001	0	1164.03	19.4006	49.0	11.9	40.3	2.776	0.011	0.011	0.000	0.274	0.23	
1186	3/13/2003	3:36:33 AM	25.513	23.08	25.526	24.002	23.764	45.49	50.429	11.211	34.966	-1.246	-6.631	48.139	0.072	0.001	0	1165.03	19.4172	49.0	11.8	40.2	2.773	0.011	0.011	0.000	0.263	0.22	
1187	3/13/2003	3:37:33 AM	25.523	23.075	25.526	24.073	23.77	45.664	50.565	11.136	35.3	-1.217	-6.662	48.201	0.073	0.001	0	1166.03	19.4339	49.1	11.8	40.5	2.791	0.011	0.011	0.000	0.265	0.23	
1188	3/13/2003	3:38:33 AM	25.536	23.076	25.517	24.144	23.781	45.71	50.573	11.077	35.443	-1.229	-6.696	47.839	0.072	0.001	0	1167.03	19.4506	49.1	11.7	40.6	2.798	0.011	0.011	0.000	0.261	0.22	
1189	3/13/2003	3:39:33 AM	25.537	23.083	25.544	24.091	23.823	45.393	50.251	11.615	34.583	-1.284	-6.727	48.954	0.071	0.001	0	1168.03	19.4672	48.8	12.0	40.0	2.767	0.011	0.010	0.000	0.261	0.22	
1190	3/13/2003	3:40:33 AM	25.553	23.08	25.591	24.163	23.845	44.971	49.8	11.483	34.19	-1.229	-6.683	49.279	0.07	0.001	0	1169.03	19.4839	48.3	12.1	39.6	2.729	0.010	0.010	0.000	0.259	0.22	
1191	3/13/2003	3:41:33 AM	25.555	23.077	25.633	24.224	23.867	45.097	49.953	11.544	34.274	-1.286	-6.759	48.891	0.069	0.001	0	1170.03	19.5006	48.5	12.0	39.7	2.736	0.010	0.010	0.000	0.256	0.22	
1192	3/13/2003	3:42:33 AM	25.577	23.094	25.675	24.262	23.889	44.954	49.837	11.441	34.256	-1.286	-6.744	49.855	0.069	0.001	0	1171.03	19.5172	48.4	12.2	39.6	2.731	0.010	0.010	0.000	0.255	0.22	
1193	3/13/2003	3:43:33 AM	25.6	23.107	25.693	24.265	23.922	44.848	49.68	11.373	34.221	-1.22	-6.767	46.735	0.068	0.001	0	1172.03	19.5339	48.2	11.5	39.5	2.726	0.010	0.010	0.000	0.251	0.21	
1194	3/13/2003	3:44:33 AM	25.601	23.098	25.664	24.261	23.923	45.306	50.319	11.485	34.438	-1.223	-6.77	44.865	0.068	0.001	0	1173.03	19.5506	48.8	11.0	39.9	2.749	0.010	0.010	0.000	0.249	0.21	
1195	3/13/2003	3:45:33 AM	25.618	23.105	25.691	24.308	23.93	44.877	49.791	11.389	34.233	-1.229	-6.779	48.776	0.067	0.001	0	1174.03	19.5672	48.3	12.0	39.6	2.727	0.010	0.010	0.000	0.248	0.21	
1196	3/13/2003	3:46:33 AM	25.636	23.113	25.714	24.341	23.948	45.014	49.963	11.413	34.278	-1.223	-6.747	48.273	0.066	0.001	0	1175.03	19.5839	48.5	11.8	39.6	2.733	0.010	0.010	0.000	0.243	0.21	
1197	3/13/2003	3:47:33 AM	25.649	23.126	25.747	24.374	23.971	44.973	49.789	11.346	34.448	-1.223	-6.854	48.269	0.067	0.001	0	1176.03	19.6006	48.3	11.8	39.7	2.738	0.010	0.010	0.000	0.246	0.21	
1198	3/13/2003	3:48:33 AM	25.667	23.139	25.81	24.427	23.974	44.946	49.775	11.448	34.331	-1.217	-6.837	48.571	0.065	0.001	0	1177.03	19.6172	48.3	11.9	39.6	2.733	0.010	0.009	0.000	0.239	0.20	
1199	3/13/2003	3:49:33 AM	25.668	23.12	25.796	24.388	23.965	44.913	49.858	11.476	34.118	-1.223	-6.872	48.443	0.064	0.001	0	1178.03	19.6339	48.4	11.9	39.5	2.724	0.010	0.009	0.000	0.236	0.20	
1200	3/13/2003	3:50:33 AM	25.696	23.143	25.759	24.416	23.993	44.674	49.659	11.315	34.157	-1.223	-6.828	48.606	0.063	0.001	0	1179.03	19.6506	48.2	11.9	39.4	2.718	0.009	0.009	0.000	0.233	0.20	
1201																													
1202	Averages		25.6	23.2	25.4	24.6	23.9	44.0	46.9	9.3	35.5	-1.0	-5.5	48.4	0.1	0.0	0.0	601.0	10.0	45.4	11.9	39.7	2.7	0.0	0.0	0.0	0.5	0.4	
1203	Maximum		26.1	24.0	25.9	26.6	24.7	46.8	51.4	11.5	37.8	35.5	87.1	50.0	0.4	0.0	0.0	1179.0	19.7	50.0	12.2	42.0	2.9	0.1	0.1	0.0	1.7	1.4	
1204	Median		25.6	23.2	25.3	24.5	24.0	44.3	46.8	9.3	36.0	-1.3	-6.2	48.5	0.1	0.0	0.0	600.5	10.0	45.3	11.9	40.1	2.8	0.0	0.0	0.0	0.5	0.4	
1205	Minimum		24.7	19.6	24.8	21.6	20.8	3.5	1.5	1.1	3.6	-1.3	-6.0	0.2	0.0	0.0	0.0	25.0	0.4	3.0	0.1	3.5	0.2	0.0	0.0	0.0	0.3	0.3	
1206	2 x Std Dev		0.610	1.560	0.407	1.894	1.102	8.184	5.652	1.388	7.631	6.097	10.298	4.430	0.065	0.000	0.000	667.621	11.127	5.652	1.086	7.879	0.543	0.010	0.010	0.000	0.248	0.211	
1207	Number of Points Used*		1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161	1161
1208																													

Figure D8-10: Dewatering of the AN-102R2, batch 4A, insoluble solids concentrations from 1.5 to 81 wt% - Raw & Calculated Data

## Appendix E: Steady-state Filtering, Test Runs 1.17 – 1.29 – AN-102R2

After each dewatering test run (run 1.16 of Batches 3 and 4) the filter was to be operated under steady state insoluble solids concentrations. During dewatering the insoluble solids concentration of the test slurry is increased to above 20 wt%, then while maintaining the high concentration constant 13 test runs were carried out. Those thirteen test runs were to vary the slurry axial velocity,  $V$ , and transmembrane pressure, TMP, in order to determine the combination that would give the best filtrate flux.

Initially there were to be just two tests using an organic based slurry: Batch 3 and Batch 4. However, problems with filtering Batch 3 led to reformulating the slurry; therefore it was followed with a Batch 3B and a Batch 3A. The first batch was named Batch 3C. Instead of having two batch it turned out to be four: Batches 3C, 3B, 3A, and 4). The Batch 3C dewatering test was not completed because of poor filterability, therefore no steady-state runs were made. The next batch, Batch 3B, went as planned, therefore all the high solids concentration steady-state runs were completed. Batch 3A did not filter as well, therefore the RPP customer did not required steady-state test, but gave permission to carry out some to quantify the filtrate flux. The customer also did not require the steady-state runs for Batch 4.

This Appendix includes the following test runs:

Steady-state test runs with simulant slurry AN-102R2 Batch 3B at insoluble solids of 22 wt%:

1.17, 1.18, 1.19, 1.20	done on 24 October 2002
1.21, 1.22, 1.23, 1.24	done on 28 October 2002
1.25, 1.26, 1.27, 1.28, 1.29	done on 29 October 2002

Steady-state test runs with simulant slurry AN-102R2 Batch 3A\* at insoluble solids of 25 wt%:

1.17, 1.20	done on 11 November 2002
1.23, 1.25, 1.28, 1.29	done on 12 November 2002

\*Because the dewatering of Batch 3A did not filter as good as Batch 3B steady state runs were not going to be done for this last Batch 3 slurry, except for a few to establish filtrate fluxes. Eight runs were eventually done due to available time and slurry.

Each dewatering test in this Appendix contains a graph of the filtrate flux with time and tables of the data taken and calculated. To better understand the presented information important aspects of the graphs and tables are explained below:

Graphs – Each graph contains time averages of some of the important parameters taken during the run at the top of the figures, i.e. Slurry velocity in the filter tube,  $V$ ; transmembrane pressure, TMP; slurry pressure at the entrance of the filter tube, Filter Pres; and the slurry temperature,  $T$ .

Tables – Each table is divided into raw data (the first 17 columns) and calculations (the last 10 columns) which are based on the raw data. The raw data section is divided into three parts:

Individual Entries – Raw Data

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used, except for tests Clean 1 & 2) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid with has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column and corrected for a 40.9-inch water column that exists from the transducer to the point where P1 is measured.)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.  
Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.87 ft<sup>2</sup>)  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T))-(1/298)] \text{ as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0}$$

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)  
Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing  
Permiability – Same as Permiability but in metric units, meter/day/bar

Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 x Std Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not included the points taken during the backpulse sequence of each test. This is explained below.

Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is were the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

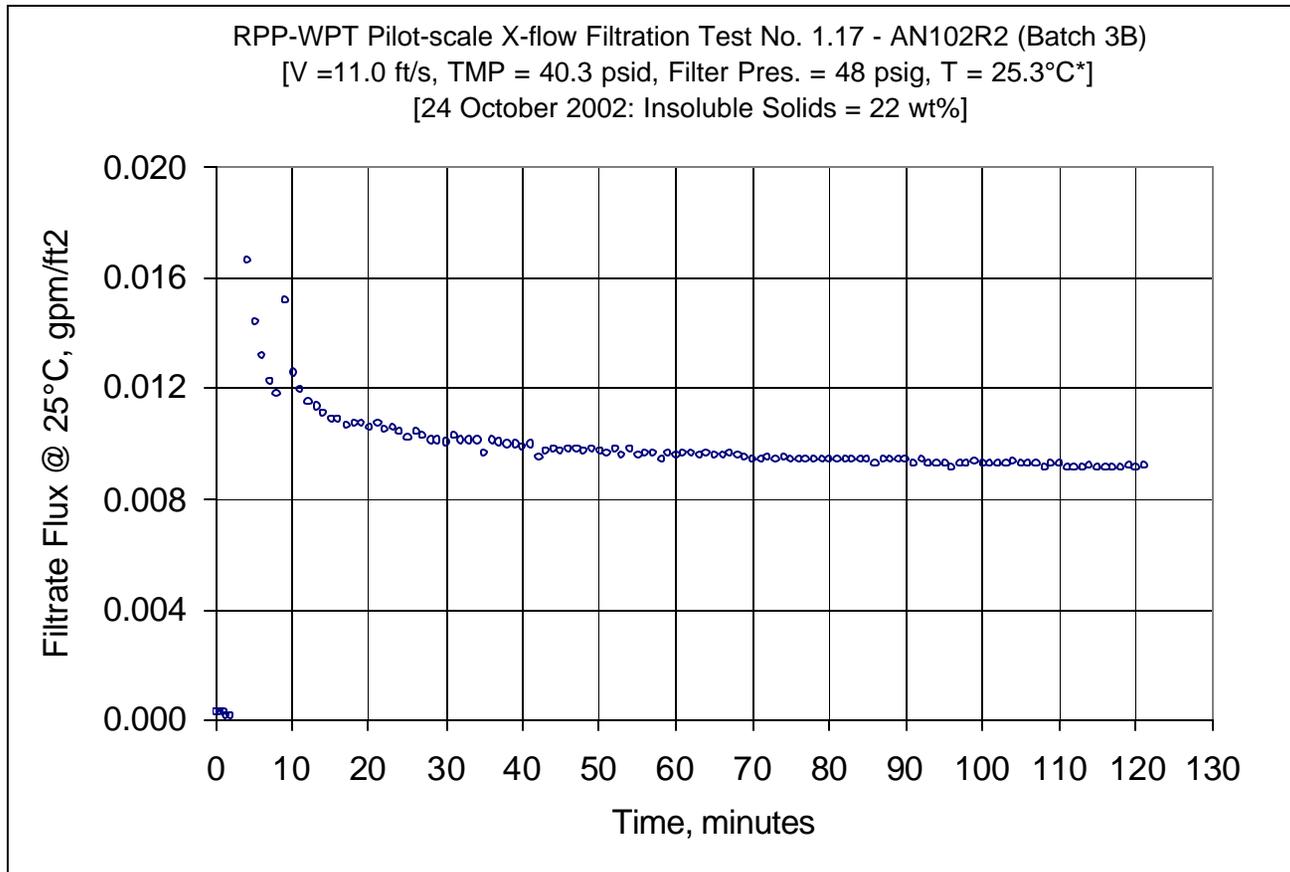


Figure E1: Steady state test run 1.17 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



10/24/2002	9:32:30 AM	25.248	22.774	25.262	24.153	23.8	49.363	50.232	18.188	32.014	-1.286	-6.411	44.424	0.065	0.001	0	57.12	0.95194	48.8	10.9	40.7	2.805	0.010	0.010	0.0002	0.236	0.20
10/24/2002	9:33:30 AM	25.257	22.792	25.365	24.126	23.799	49.231	50.135	18.326	31.754	-1.284	-6.394	44.969	0.064	0.001	0	58.12	0.96861	48.7	11.0	40.5	2.792	0.010	0.009	0.0002	0.233	0.20
10/24/2002	9:34:30 AM	25.26	22.801	25.194	24.16	23.837	48.893	49.68	18.204	31.713	-1.289	-6.405	44.6	0.065	0.001	0	59.12	0.98528	48.2	11.0	40.3	2.779	0.010	0.010	0.0002	0.239	0.20
10/24/2002	9:35:30 AM	25.279	22.819	25.332	24.139	23.821	49.318	50.298	18.315	31.877	-1.286	-6.406	43.537	0.065	0.001	0	60.12	1.00194	48.8	10.7	40.6	2.799	0.010	0.010	0.0002	0.236	0.20
10/24/2002	9:36:30 AM	25.288	22.834	25.267	24.208	23.88	49.219	50.137	18.273	31.877	-1.286	-6.411	45.146	0.065	0.001	0	61.12	1.01861	48.7	11.1	40.5	2.796	0.010	0.010	0.0002	0.237	0.20
10/24/2002	9:37:30 AM	25.302	22.873	25.271	24.247	23.955	49.392	50.3	18.223	32.145	-1.286	-6.406	45.257	0.065	0.001	0	62.12	1.03528	48.8	11.1	40.8	2.811	0.010	0.010	0.0002	0.236	0.20
10/24/2002	9:38:30 AM	25.311	22.882	25.37	24.256	23.954	49.993	49.889	18.267	31.553	-1.286	-6.406	44.762	0.065	0.001	0	63.12	1.05194	48.4	11.0	40.3	2.777	0.010	0.010	0.0002	0.238	0.20
10/24/2002	9:39:30 AM	25.315	22.901	25.209	24.316	23.973	49.022	50.083	18.165	31.721	-1.289	-6.388	44.907	0.065	0.001	0	64.12	1.06861	48.6	11.0	40.4	2.783	0.010	0.010	0.0002	0.239	0.20
10/24/2002	9:40:30 AM	25.319	22.9	25.318	24.249	24.007	49.949	50.083	18.204	31.549	-1.292	-6.411	44.8	0.065	0.001	0	65.12	1.08528	48.6	11.0	40.2	2.775	0.010	0.010	0.0002	0.239	0.20
10/24/2002	9:41:30 AM	25.343	22.934	25.282	24.318	24.021	49.09	49.928	18.208	31.897	-1.286	-6.406	45.167	0.065	0.001	0	66.12	1.10194	48.5	11.1	40.5	2.792	0.010	0.010	0.0002	0.237	0.20
10/24/2002	9:42:30 AM	25.336	22.947	25.27	24.321	24.064	49.16	50.29	18.257	31.803	-1.286	-6.371	44.938	0.065	0.001	0	67.12	1.11861	48.8	11.0	40.5	2.791	0.010	0.010	0.0002	0.238	0.20
10/24/2002	9:43:30 AM	25.345	22.966	25.348	24.315	24.073	48.991	49.884	18.242	31.752	-1.289	-6.423	45.114	0.065	0.001	0	68.12	1.13528	48.4	11.1	40.4	2.783	0.010	0.010	0.0002	0.238	0.20
10/24/2002	9:44:30 AM	25.358	22.985	25.207	24.369	24.137	49.069	50.164	18.326	31.463	-1.286	-6.417	44.951	0.064	0.001	0	69.12	1.15194	48.7	11.0	40.3	2.776	0.010	0.009	0.0002	0.236	0.20
10/24/2002	9:45:30 AM	25.371	23.003	25.345	24.332	24.104	49.005	50.209	18.176	31.695	-1.289	-6.417	44.888	0.064	0.001	0	70.12	1.16861	48.7	11.0	40.4	2.782	0.010	0.009	0.0002	0.234	0.20
10/24/2002	9:46:30 AM	25.379	23.026	25.313	24.395	24.127	49.076	50.1	18.33	31.566	-1.286	-6.417	44.854	0.064	0.001	0	71.12	1.18528	48.6	11.0	40.3	2.780	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:47:30 AM	25.373	23.035	25.287	24.383	24.191	48.926	50.011	18.244	31.557	-1.286	-6.417	44.839	0.064	0.001	0	72.12	1.20194	48.5	11.0	40.2	2.775	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:48:30 AM	25.397	23.053	25.43	24.382	24.195	49.198	50.36	18.257	31.783	-1.289	-6.417	45.19	0.064	0.001	0	73.12	1.21861	48.9	11.1	40.5	2.792	0.010	0.009	0.0002	0.233	0.20
10/24/2002	9:49:30 AM	25.415	23.086	25.288	24.47	24.218	49.014	50.104	18.245	31.654	-1.289	-6.397	45.85	0.064	0.001	0	74.12	1.23528	48.6	11.2	40.3	2.781	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:50:30 AM	25.417	23.094	25.401	24.483	24.251	48.846	49.994	18.198	31.379	-1.286	-6.403	45.043	0.064	0.001	0	75.12	1.25194	48.5	11.0	40.1	2.766	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:51:30 AM	25.444	23.128	25.425	24.517	24.343	49.208	50.452	18.367	31.662	-1.286	-6.405	45.699	0.064	0.001	0	76.12	1.26861	49.0	11.2	40.4	2.788	0.010	0.009	0.0002	0.233	0.20
10/24/2002	9:52:30 AM	25.429	23.126	25.338	24.47	24.363	48.842	49.812	18.104	31.725	-1.286	-6.405	45.028	0.064	0.001	0	77.12	1.28528	48.3	11.0	40.3	2.777	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:53:30 AM	25.458	23.155	25.482	24.544	24.332	48.96	50.236	18.158	31.625	-1.286	-6.42	45.2	0.064	0.001	0	78.12	1.30194	48.8	11.1	40.3	2.778	0.010	0.009	0.0002	0.234	0.20
10/24/2002	9:54:30 AM	25.47	23.177	25.349	24.601	24.344	49.04	50.176	18.2	31.787	-1.286	-6.42	44.793	0.064	0.001	0	79.12	1.31861	48.7	11.0	40.4	2.786	0.010	0.009	0.0002	0.234	0.20
10/24/2002	9:55:30 AM	25.484	23.196	25.453	24.545	24.343	49.15	50.373	18.372	31.594	-1.284	-6.395	44.948	0.064	0.001	0	80.12	1.33528	48.9	11.0	40.4	2.784	0.010	0.009	0.0002	0.233	0.20
10/24/2002	9:56:30 AM	25.471	23.198	25.42	24.547	24.4	48.935	50.251	18.162	31.578	-1.289	-6.417	45.347	0.064	0.001	0	81.12	1.35194	48.8	11.1	40.3	2.776	0.010	0.009	0.0002	0.234	0.20
10/24/2002	9:57:30 AM	25.489	23.221	25.368	24.59	24.388	48.949	50.205	18.263	31.561	-1.289	-6.417	44.99	0.064	0.001	0	82.12	1.36861	48.7	11.0	40.3	2.775	0.010	0.009	0.0002	0.235	0.20
10/24/2002	9:58:30 AM	25.493	23.235	25.482	24.569	24.427	48.529	49.646	18.112	31.25	-1.289	-6.412	45.047	0.064	0.001	0	83.12	1.38528	48.2	11.0	39.9	2.750	0.010	0.009	0.0002	0.236	0.20
10/24/2002	9:59:30 AM	25.525	23.268	25.369	24.606	24.504	49.08	50.346	18.248	31.654	-1.284	-6.414	45.062	0.064	0.001	0	84.12	1.40194	48.9	11.0	40.4	2.783	0.010	0.009	0.0002	0.234	0.20
10/24/2002	10:00:30 AM	25.532	23.285	25.461	24.628	24.486	48.871	50.023	18.064	31.744	-1.284	-6.417	44.695	0.064	0.001	0	85.12	1.41861	48.6	11.0	40.3	2.779	0.010	0.009	0.0002	0.234	0.20
10/24/2002	10:01:30 AM	25.524	23.276	25.428	24.595	24.488	48.995	50.23	18.072	31.821	-1.292	-6.394	44.965	0.063	0.001	0	86.12	1.43528	48.8	11.0	40.4	2.786	0.009	0.009	0.0002	0.230	0.20
10/24/2002	10:02:30 AM	25.537	23.3	25.351	24.653	24.516	48.891	50.218	18.032	31.68	-1.289	-6.423	44.586	0.064	0.001	0	87.12	1.45194	48.7	10.9	40.3	2.778	0.010	0.009	0.0002	0.235	0.20
10/24/2002	10:03:30 AM	25.554	23.322	25.488	24.636	24.508	48.81	50.052	17.974	31.666	-1.286	-6.426	44.516	0.064	0.001	0	88.12	1.46861	48.5	10.9	40.2	2.775	0.010	0.009	0.0002	0.234	0.20
10/24/2002	10:04:30 AM	25.551	23.334	25.33	24.672	24.566	48.939	50.246	17.963	31.883	-1.286	-6.429	43.843	0.064	0.001	0	89.12	1.48528	48.9	10.7	40.4	2.786	0.010	0.009	0.0002	0.234	0.20
10/24/2002	10:05:30 AM	25.559	23.357	25.423	24.655	24.574	48.889	50.106	18.025	31.67	-1.286	-6.426	44.669	0.064	0.001	0	90.12	1.50194	48.6	10.9	40.3	2.777	0.010	0.009	0.0002	0.234	0.20
10/24/2002	10:06:30 AM	25.571	23.379	25.42	24.677	24.605	48.96	50.375	18.041	31.68	-1.289	-6.429	44.69	0.063	0.001	0	91.12	1.51861	48.9	11.0	40.3	2.780	0.009	0.009	0.0002	0.230	0.20
10/24/2002	10:07:30 AM	25.578	23.396	25.347	24.694	24.663	48.734	50.091	17.975	31.613	-1.286	-6.391	44.793	0.064	0.001	0	92.12	1.53528	48.6	11.0	40.2	2.770	0.010	0.009	0.0002	0.235	0.20
10/24/2002	10:08:30 AM	25.586	23.404	25.464	24.686	24.66	48.577	49.758	18.003	31.428	-1.289	-6.411	44.869	0.063	0.001	0	93.12	1.55194	48.3	11.0	40.0	2.758	0.009	0.009	0.0002	0.232	0.20
10/24/2002	10:09:30 AM	25.593	23.431	25.332	24.734	24.697	49.016	50.379	18.064	31.74	-1.286	-6.426	44.825	0.063	0.001	0	94.12	1.56861	48.9	11.0	40.4	2.784	0.009	0.009	0.0002	0.230	0.20
10/24/2002	10:10:30 AM	25.584	23.438	25.413	24.705	24.689	48.939	50.085	18.024	31.807	-1.289	-6.423	44.657	0.063	0.001	0	95.12	1.58528	48.6	10.9	40.4	2.784	0.009	0.009	0.0002	0.230	0.20
10/24/2002	10:11:30 AM	25.596	23.454	25.405	24.707	24.65	49.026	50.368	18.135	31.805	-1.289	-6.426	44.831	0.062	0.001	0	96.12	1.60194	48.9	11.0	40.4	2.787	0.009	0.009	0.0002	0.226	0.19
10/24/2002	10:12:30 AM	25.604	23.472	25.338	24.73	24.718	48.984	50.387	18.027	31.789	-1.289	-6.426	44.662	0.063	0.001	0	97.12	1.61861	48.9	11.0	40.4	2.785	0.009	0.009	0.0002	0.230	0.20
10/24/2002	10:13:30 AM	25.6	23.488	25.464	24.701	24.684	49.152</																				

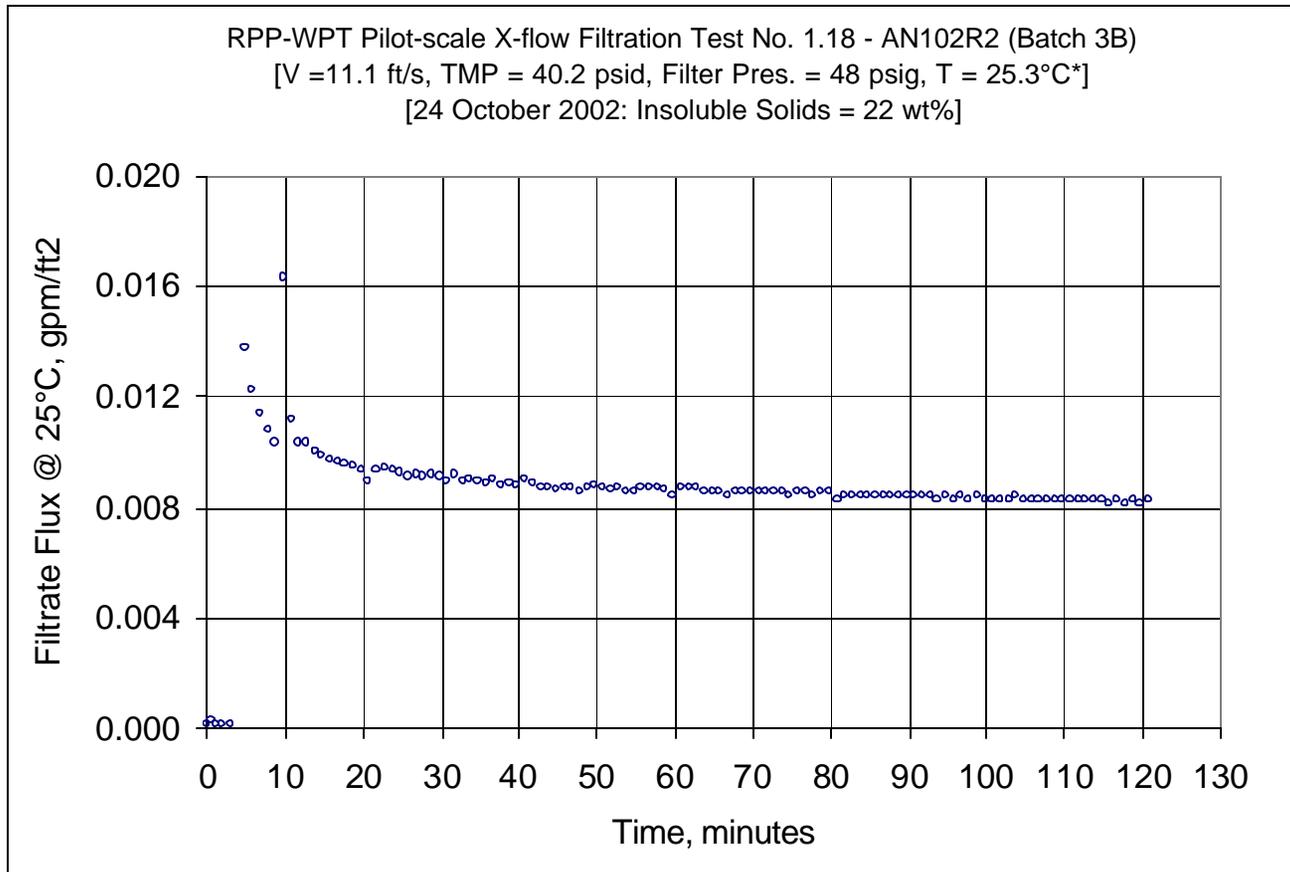


Figure E3: Steady state test run 1.18 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



10/24/2002 11:39:32 AM	25.989	24.967	25.258	26.307	26.2	48.581	50.06	17.055	32.305	-1.289	-6.458	45.164	0.057	0.001	0	59.75	0.99583	48.6	11.1	40.4	2.788	0.008	0.008	0.0002	0.209	0.18
10/24/2002 11:40:32 AM	26.001	24.989	25.365	26.343	26.227	48.365	49.814	16.909	32.384	-1.289	-6.44	45.46	0.059	0.001	0	60.75	1.0125	48.3	11.1	40.4	2.784	0.009	0.009	0.0002	0.216	0.18
10/24/2002 11:41:32 AM	25.998	25	25.332	26.38	26.243	48.492	49.86	17.055	32.331	-1.289	-6.458	45.363	0.059	0.001	0	61.75	1.02917	48.4	11.1	40.4	2.786	0.009	0.009	0.0002	0.216	0.18
10/24/2002 11:42:32 AM	25.999	25.012	25.294	26.362	26.26	48.626	49.932	17.024	32.456	-1.292	-6.486	45.395	0.059	0.001	-0.001	62.75	1.04583	48.5	11.1	40.5	2.795	0.009	0.009	0.0002	0.215	0.18
10/24/2002 11:43:32 AM	25.998	25.025	25.387	26.355	26.334	48.272	49.773	16.867	32.315	-1.292	-6.484	45.494	0.058	0.001	0	63.75	1.0625	48.3	11.1	40.3	2.778	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:44:32 AM	26.026	25.059	25.26	26.399	26.347	48.063	49.51	16.847	32.198	-1.289	-6.484	45.441	0.058	0.001	0	64.75	1.07917	48.0	11.1	40.1	2.767	0.009	0.009	0.0002	0.214	0.18
10/24/2002 11:45:32 AM	26.024	25.067	25.408	26.376	26.35	48.4	49.862	17.075	32.215	-1.289	-6.484	45.307	0.058	0.001	0	65.75	1.09583	48.4	11.1	40.3	2.779	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:46:32 AM	26.027	25.09	25.296	26.425	26.363	48.218	49.607	16.968	32.225	-1.289	-6.484	45.262	0.057	0.001	0	66.75	1.1125	48.1	11.1	40.2	2.773	0.008	0.008	0.0002	0.210	0.18
10/24/2002 11:47:32 AM	26.041	25.119	25.375	26.433	26.362	48.519	50.029	16.998	32.376	-1.289	-6.484	45.367	0.058	0.001	0	67.75	1.12917	48.6	11.1	40.4	2.789	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:48:32 AM	26.037	25.13	25.342	26.455	26.363	48.226	49.816	16.995	32.055	-1.289	-6.489	45.393	0.059	0.001	0	68.75	1.14583	48.3	11.1	40.1	2.788	0.009	0.009	0.0002	0.213	0.18
10/24/2002 11:49:32 AM	26.045	25.146	25.324	26.472	26.401	48.446	49.992	16.963	32.329	-1.286	-6.489	45.494	0.059	0.001	0	69.75	1.1625	48.5	11.1	40.4	2.795	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:50:32 AM	26.047	25.155	25.421	26.439	26.469	48.344	49.793	17.024	32.266	-1.286	-6.458	44.11	0.059	0.001	0	70.75	1.17917	48.3	10.8	40.3	2.779	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:51:32 AM	26.059	25.182	25.369	26.522	26.47	48.26	49.893	16.969	32.278	-1.292	-6.469	45.36	0.059	0.001	0	71.75	1.19583	48.4	11.1	40.3	2.776	0.009	0.009	0.0002	0.213	0.18
10/24/2002 11:52:32 AM	26.057	25.19	25.406	26.524	26.448	48.222	49.721	17.009	32.086	-1.292	-6.472	45.603	0.059	0.001	0	72.75	1.2125	48.2	11.2	40.2	2.788	0.009	0.009	0.0002	0.213	0.18
10/24/2002 11:53:32 AM	26.054	25.202	25.368	26.546	26.475	48.411	49.88	16.998	32.327	-1.292	-6.472	45.278	0.058	0.001	0	73.75	1.22917	48.4	11.1	40.4	2.783	0.009	0.009	0.0002	0.213	0.18
10/24/2002 11:54:32 AM	26.071	25.224	25.361	26.599	26.492	48.146	49.845	17.025	31.914	-1.289	-6.469	45.23	0.057	0.001	0	74.75	1.24583	48.4	11.1	40.0	2.760	0.008	0.008	0.0002	0.210	0.18
10/24/2002 11:55:32 AM	26.074	25.242	25.373	26.626	26.525	48.22	49.891	17.011	31.991	-1.289	-6.475	44.38	0.058	0.001	0	75.75	1.2625	48.4	10.9	40.1	2.765	0.009	0.009	0.0002	0.213	0.18
10/24/2002 11:56:32 AM	26.087	25.26	25.306	26.614	26.512	48.45	50.091	17.011	32.325	-1.289	-6.472	45.366	0.058	0.001	0	76.75	1.27917	48.6	11.1	40.4	2.785	0.009	0.009	0.0002	0.212	0.18
10/24/2002 11:57:32 AM	26.083	25.272	25.408	26.561	26.544	47.947	49.483	16.936	31.905	-1.292	-6.475	45.341	0.057	0.001	0	77.75	1.29583	48.0	11.1	39.9	2.753	0.008	0.008	0.0002	0.210	0.18
10/24/2002 11:58:32 AM	26.105	25.298	25.269	26.642	26.556	48.193	49.74	16.975	32.129	-1.289	-6.475	45.343	0.058	0.001	0	78.75	1.3125	48.3	11.1	40.2	2.769	0.009	0.009	0.0002	0.214	0.18
10/24/2002 11:59:32 AM	26.111	25.309	25.4	26.633	26.562	48.057	49.415	16.97	32.075	-1.289	-6.472	45.599	0.058	0.001	0	79.75	1.32917	47.9	11.2	40.1	2.762	0.009	0.009	0.0002	0.213	0.18
10/24/2002 12:00:32 PM	26.113	25.331	25.312	26.73	26.624	48.048	49.556	16.864	32.092	-1.286	-6.472	45.339	0.056	0.001	0	80.75	1.34583	48.1	11.1	40.1	2.763	0.008	0.008	0.0002	0.207	0.18
10/24/2002 12:01:32 PM	26.125	25.348	25.349	26.677	26.595	48.38	50.149	17.091	32.059	-1.289	-6.472	45.363	0.057	0.001	0	81.75	1.3625	48.7	11.1	40.2	2.773	0.008	0.008	0.0002	0.209	0.18
10/24/2002 12:02:32 PM	26.126	25.365	25.396	26.654	26.632	48.293	49.957	17.06	32.043	-1.289	-6.475	45.446	0.057	0.001	0	82.75	1.37917	48.5	11.1	40.2	2.769	0.008	0.008	0.0002	0.209	0.18
10/24/2002 12:03:32 PM	26.138	25.381	25.292	26.64	26.629	48.03	49.7	16.867	32.104	-1.289	-6.472	45.097	0.057	0.001	0	83.75	1.39583	48.2	11.1	40.1	2.762	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:04:32 PM	26.134	25.387	25.423	26.636	26.635	48.189	49.907	17.089	31.988	-1.289	-6.478	45.991	0.057	0.001	0	84.75	1.4125	48.4	11.3	40.1	2.762	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:05:32 PM	26.141	25.409	25.26	26.633	26.646	48.094	50.037	16.983	31.85	-1.289	-6.478	45.473	0.057	0.001	0	85.75	1.42917	48.6	11.1	40.0	2.766	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:06:32 PM	26.137	25.425	25.396	26.659	26.667	48.038	49.731	16.974	31.862	-1.289	-6.478	44.55	0.057	0.001	0	86.75	1.44583	48.3	10.9	40.0	2.754	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:07:32 PM	26.139	25.443	25.299	26.737	26.67	47.926	49.951	16.944	31.83	-1.289	-6.486	45.913	0.057	0.001	0	87.75	1.4625	48.5	11.3	39.9	2.749	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:08:32 PM	26.152	25.465	25.341	26.774	26.708	48.262	50.071	17.044	31.961	-1.292	-6.486	45.309	0.057	0.001	0	88.75	1.47917	48.6	11.1	40.1	2.766	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:09:32 PM	26.16	25.478	25.384	26.802	26.735	48.218	50.164	16.995	32.022	-1.292	-6.486	45.309	0.057	0.001	0	89.75	1.49583	48.7	11.1	40.1	2.766	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:10:32 PM	26.161	25.5	25.306	26.829	26.717	47.711	49.541	16.82	31.772	-1.292	-6.486	45.295	0.057	0.001	0	90.75	1.5125	48.1	11.1	39.7	2.740	0.008	0.008	0.0002	0.212	0.18
10/24/2002 12:11:32 PM	26.163	25.507	25.423	26.785	26.719	47.994	49.75	16.965	31.93	-1.289	-6.486	45.599	0.057	0.001	0	91.75	1.52917	48.3	11.2	40.0	2.755	0.008	0.008	0.0002	0.210	0.18
10/24/2002 12:12:32 PM	26.177	25.54	25.271	26.889	26.772	48.125	49.953	17.072	31.836	-1.289	-6.489	46.371	0.057	0.001	0	92.75	1.54583	48.5	11.4	40.0	2.757	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:13:32 PM	26.194	25.557	25.423	26.881	26.764	47.937	49.87	16.939	31.869	-1.292	-6.486	45.513	0.056	0.001	0	93.75	1.5625	48.4	11.2	39.9	2.751	0.008	0.008	0.0002	0.207	0.18
10/24/2002 12:14:32 PM	26.185	25.559	25.275	26.842	26.776	48.04	49.899	17.018	31.823	-1.292	-6.492	45.607	0.057	0.001	0	94.75	1.57917	48.4	11.2	39.9	2.753	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:15:32 PM	26.193	25.582	25.358	26.88	26.794	48.357	50.16	17.074	32.092	-1.289	-6.489	45.303	0.056	0.001	0	95.75	1.59583	48.7	11.1	40.2	2.773	0.008	0.008	0.0002	0.205	0.17
10/24/2002 12:16:32 PM	26.204	25.597	25.369	26.896	26.829	48.009	49.835	17.019	31.92	-1.289	-6.489	45.381	0.057	0.001	0	96.75	1.6125	48.4	11.1	40.0	2.755	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:17:32 PM	26.206	25.614	25.32	26.863	26.841	47.552	49.406	16.845	31.637	-1.289	-6.489	46.779	0.056	0.001	0	97.75	1.62917	47.9	11.5	39.6	2.730	0.008	0.008	0.0002	0.209	0.18
10/24/2002 12:18:32 PM	26.216	25.639	25.43	26.968	26.851	47.949	50.015	16.941	31.758	-1.289	-6.486	45.504	0.057	0.001	0	98.75	1.64583	48.5	11.2	39.9	2.748	0.008	0.008	0.0002	0.211	0.18
10/24/2002 12:19:32 PM	26.202	25.64	25.236	27.158	26.877	47.719	49.644	16.948	31.65	-1.295	-6.492	45.355	0.056	0.001	0	99.75	1.6625	48.2	11.1	39.7	2.736	0.008	0.008	0.0002	0.209	0.18
10/24/2002 12:20:32 PM	26.217	25.67	25.416	27.203	26.907	48.17	50.106	17.123	31.866	-1.289	-6.489	45.492	0.056	0.001	0	100.75	1.67917	48.6	11.1	40.0	2.759					

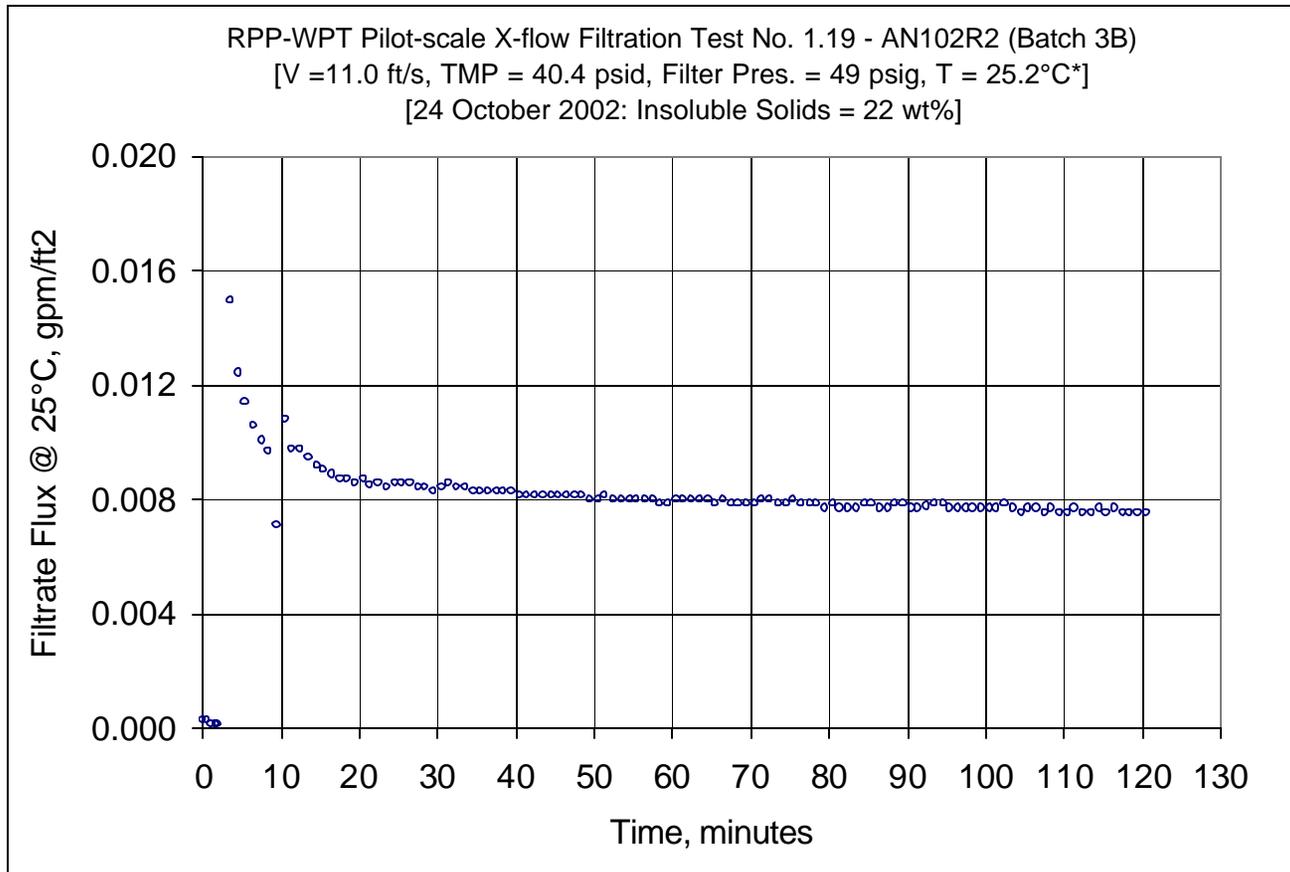


Figure E5: Steady state test run 1.19 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



WSRC-TR-2003-00204, REV. 0  
SRT-RPP-2003-00087, REV. 0

10/24/2002	1:42.40 PM	26.187	26.461	25.182	27.004	27.352	48.587	50.029	16.409	32.794	-1.292	-6.524	45.867	0.054	0.001	0	57.47	0.95778	48.6	11.2	40.7	2.805	0.008	0.008	0.0002	0.197	0.17
10/24/2002	1:43.40 PM	26.177	26.451	25.292	26.959	27.362	48.581	50.05	16.378	33.021	-1.295	-6.527	44.747	0.053	0.001	-0.001	58.47	0.97444	48.6	11.0	40.8	2.813	0.008	0.008	0.0002	0.192	0.16
10/24/2002	1:44.40 PM	26.183	26.452	25.143	27.02	27.328	48.489	50.052	16.334	32.962	-1.292	-6.524	44.382	0.053	0.001	0	59.47	0.99111	48.6	10.9	40.7	2.808	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:45.40 PM	26.174	26.448	25.284	26.981	27.304	48.374	49.878	16.319	32.839	-1.289	-6.501	44.693	0.054	0.001	0	60.47	1.00778	48.4	11.0	40.6	2.800	0.008	0.008	0.0002	0.197	0.17
10/24/2002	1:46.40 PM	26.175	26.454	25.125	27.022	27.34	48.106	49.537	16.312	32.61	-1.289	-6.501	44.766	0.054	0.001	0	61.47	1.02444	48.1	11.0	40.4	2.783	0.008	0.008	0.0002	0.199	0.17
10/24/2002	1:47.40 PM	26.171	26.435	25.221	26.928	27.326	48.651	50.253	16.404	32.97	-1.292	-6.504	44.663	0.054	0.001	0	62.47	1.04111	48.8	10.9	40.8	2.814	0.008	0.008	0.0002	0.196	0.17
10/24/2002	1:48.40 PM	26.176	26.445	25.171	26.938	27.301	48.498	50.166	16.425	32.761	-1.295	-6.507	44.921	0.054	0.001	-0.001	63.47	1.05778	48.7	11.0	40.6	2.801	0.008	0.008	0.0002	0.197	0.17
10/24/2002	1:49.40 PM	26.183	26.452	25.213	26.95	27.313	48.21	49.638	16.236	32.898	-1.289	-6.495	44.732	0.054	0.001	0	64.47	1.07444	48.2	11.0	40.6	2.796	0.008	0.008	0.0002	0.197	0.17
10/24/2002	1:50.40 PM	26.172	26.426	25.237	26.914	27.297	48.295	49.822	16.331	32.737	-1.295	-6.507	44.365	0.053	0.001	0	65.47	1.09111	48.9	10.9	40.5	2.793	0.008	0.008	0.0002	0.194	0.16
10/24/2002	1:51.40 PM	26.198	26.452	25.162	26.935	27.298	48.643	50.317	16.421	32.98	-1.286	-6.501	45.146	0.054	0.001	0	66.47	1.10778	48.8	11.1	40.8	2.814	0.008	0.008	0.0002	0.196	0.17
10/24/2002	1:52.40 PM	26.2	26.449	25.279	26.927	27.28	48.431	50.025	16.214	32.915	-1.289	-6.501	44.596	0.053	0.001	0	67.47	1.12444	48.6	10.9	40.7	2.804	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:53.40 PM	26.195	26.439	25.099	26.947	27.27	48.601	50.296	16.333	33.013	-1.295	-6.507	44.667	0.053	0.001	0	68.47	1.14111	48.8	10.9	40.8	2.813	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:54.40 PM	26.199	26.453	25.254	26.896	27.274	48.409	50.066	16.284	32.925	-1.289	-6.501	44.728	0.053	0.001	0	69.47	1.15778	48.6	11.0	40.7	2.804	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:55.40 PM	26.189	26.438	25.138	26.986	27.219	48.425	50.158	16.229	33.033	-1.289	-6.501	44.787	0.053	0.001	0	70.47	1.17444	48.7	11.0	40.7	2.808	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:56.40 PM	26.198	26.457	25.213	26.935	27.213	48.612	50.379	16.3	33.035	-1.286	-6.501	44.47	0.054	0.001	0	71.47	1.19111	48.9	10.9	40.8	2.815	0.008	0.008	0.0002	0.196	0.17
10/24/2002	1:57.40 PM	26.181	26.45	25.226	26.963	27.211	48.396	50.031	16.209	32.931	-1.289	-6.504	44.655	0.054	0.001	0	72.47	1.20778	48.6	10.9	40.7	2.804	0.008	0.008	0.0002	0.197	0.17
10/24/2002	1:58.40 PM	26.167	26.441	25.102	26.994	27.163	48.643	50.29	16.316	33.019	-1.289	-6.501	44.422	0.053	0.001	0	73.47	1.22444	48.8	10.9	40.8	2.815	0.008	0.008	0.0002	0.193	0.16
10/24/2002	1:59.40 PM	26.164	26.437	25.243	26.946	27.124	48.634	50.489	16.276	33.007	-1.289	-6.504	44.258	0.053	0.001	0	74.47	1.24111	49.0	10.8	40.8	2.814	0.008	0.008	0.0002	0.192	0.16
10/24/2002	2:00.40 PM	26.154	26.433	25.083	27.001	27.109	48.164	49.88	16.17	32.927	-1.292	-6.501	44.541	0.054	0.001	0	75.47	1.25778	48.4	10.9	40.5	2.795	0.008	0.008	0.0002	0.196	0.17
10/24/2002	2:01.40 PM	26.154	26.448	25.184	26.951	27.08	48.239	49.94	16.163	32.81	-1.289	-6.504	44.523	0.053	0.001	0	76.47	1.27444	48.5	10.9	40.5	2.794	0.008	0.008	0.0002	0.194	0.17
10/24/2002	2:02.40 PM	26.148	26.442	25.172	26.94	27.038	48.388	50.222	16.324	32.812	-1.289	-6.501	44.405	0.053	0.001	0	77.47	1.29111	48.7	10.9	40.6	2.798	0.008	0.008	0.0002	0.194	0.16
10/24/2002	2:03.40 PM	26.141	26.434	25.09	26.908	27.031	48.547	50.412	16.298	32.911	-1.289	-6.501	44.428	0.053	0.001	0	78.47	1.30778	48.9	10.9	40.7	2.808	0.008	0.008	0.0002	0.194	0.16
10/24/2002	2:04.40 PM	26.138	26.438	25.219	26.851	27.036	48.519	50.327	16.312	32.893	-1.289	-6.501	44.172	0.052	0.001	0	79.47	1.32444	48.9	10.8	40.8	2.810	0.008	0.008	0.0002	0.189	0.16
10/24/2002	2:05.40 PM	26.147	26.451	25.066	26.849	26.992	48.498	50.197	16.324	32.945	-1.289	-6.501	44.737	0.053	0.001	0	80.47	1.34111	48.7	11.0	40.7	2.808	0.008	0.008	0.0002	0.194	0.16
10/24/2002	2:06.40 PM	26.138	26.452	25.172	26.78	26.983	48.251	49.965	16.224	32.941	-1.292	-6.507	44.581	0.052	0.001	0	81.47	1.35778	48.5	10.9	40.6	2.799	0.008	0.008	0.0002	0.190	0.16
10/24/2002	2:07.40 PM	26.159	26.463	25.178	26.801	26.939	48.21	50.038	16.236	32.777	-1.286	-6.501	44.625	0.052	0.001	0	82.47	1.37444	48.6	10.9	40.5	2.792	0.008	0.008	0.0002	0.191	0.16
10/24/2002	2:08.40 PM	26.162	26.47	25.126	26.809	26.897	48.411	50.371	16.242	32.953	-1.289	-6.501	44.974	0.052	0.001	0	83.47	1.39111	48.9	11.0	40.7	2.805	0.008	0.008	0.0002	0.190	0.16
10/24/2002	2:09.40 PM	26.164	26.457	25.233	26.726	26.839	48.218	50.095	16.228	32.796	-1.292	-6.507	44.659	0.053	0.001	0	84.47	1.40778	48.6	10.9	40.5	2.793	0.008	0.008	0.0002	0.194	0.16
10/24/2002	2:10.40 PM	26.153	26.442	25.062	26.65	26.768	48.245	50.002	16.186	32.923	-1.289	-6.501	44.888	0.053	0.001	0	85.47	1.42444	48.5	11.0	40.6	2.798	0.008	0.008	0.0002	0.194	0.17
10/24/2002	2:11.40 PM	26.146	26.44	25.2	26.588	26.711	48.334	50.178	16.251	32.866	-1.292	-6.507	45.89	0.052	0.001	0	86.47	1.44111	48.7	11.2	40.6	2.799	0.008	0.008	0.0002	0.190	0.16
10/24/2002	2:12.40 PM	26.148	26.422	25.077	26.525	26.639	48.11	50.112	16.159	32.64	-1.292	-6.51	44.722	0.052	0.001	0	87.47	1.45778	48.6	11.0	40.4	2.784	0.008	0.008	0.0002	0.192	0.16
10/24/2002	2:13.40 PM	26.114	26.393	25.138	26.446	26.575	48.055	50.002	16.228	32.56	-1.289	-6.504	44.651	0.053	0.001	0	88.47	1.47444	48.5	10.9	40.3	2.779	0.008	0.008	0.0002	0.195	0.17
10/24/2002	2:14.40 PM	26.127	26.391	25.176	26.444	26.548	48.295	50.015	16.308	32.818	-1.289	-6.501	44.636	0.053	0.001	0	89.47	1.49111	48.5	10.9	40.6	2.796	0.008	0.008	0.0002	0.194	0.16
10/24/2002	2:15.40 PM	26.11	26.364	25.089	26.412	26.471	48.429	50.468	16.263	32.806	-1.289	-6.504	44.539	0.052	0.001	0	90.47	1.50778	49.0	10.9	40.6	2.800	0.008	0.008	0.0002	0.190	0.16
10/24/2002	2:16.40 PM	26.109	26.348	25.226	26.351	26.45	47.943	49.946	16.196	32.497	-1.289	-6.484	45.061	0.052	0.001	0	91.47	1.52444	48.5	11.0	40.2	2.773	0.008	0.008	0.0002	0.192	0.16
10/24/2002	2:17.40 PM	26.093	26.322	25.042	26.31	26.414	48.305	50.271	16.297	32.706	-1.289	-6.489	44.705	0.052	0.001	0	92.47	1.54111	48.8	11.0	40.5	2.793	0.008	0.008	0.0002	0.191	0.16
10/24/2002	2:18.40 PM	26.09	26.313	25.199	26.307	26.395	48.278	50.246	16.309	32.597	-1.289	-6.486	44.686	0.053	0.001	0	93.47	1.55778	48.8	11.0	40.4	2.788	0.008	0.008	0.0002	0.194	0.17
10/24/2002	2:19.40 PM	26.076	26.29	25.105	26.349	26.327	48.456	50.458	16.419	32.719	-1.289	-6.486	44.667	0.053	0.001	0	94.47	1.57444	49.0	10.9	40.6	2.801	0.008	0.008	0.0002	0.194	0.17
10/24/2002	2:20.40 PM	26.083	26.287	25.157	26.4	26.403	48.202	50.319	16.279	32.475	-1.286	-6.481	44.405	0.052	0.001	0	95.47	1.59111	48.9	10.9	40.3	2.781	0.008	0.008	0.0002	0.191	0.16
10/24/2002	2:21.40 PM	26.08	26.259	25.239	26.412	26.391	47.997	49.88	16.17	32.567	-1.284	-6.486	44.2	0.052	0.001	0	96.47	1.60778	48.4	10.8	40.3	2.777	0.008	0.008	0.0002	0.191	0.16
10/24/2002	2:22.40 PM	26.074	26.238	25.088	26.437	26.455	48.038	49.992	16.171	32.747	-1.286	-6.486	44.607	0.052	0.002	0	97.47	1.62444	48.5	10.9	40.4	2.785	0.008	0.008	0.0002	0.191	0.16
10/24/2002	2:23.40 PM	26.073	26.232	25.237	26.466	26.459																					

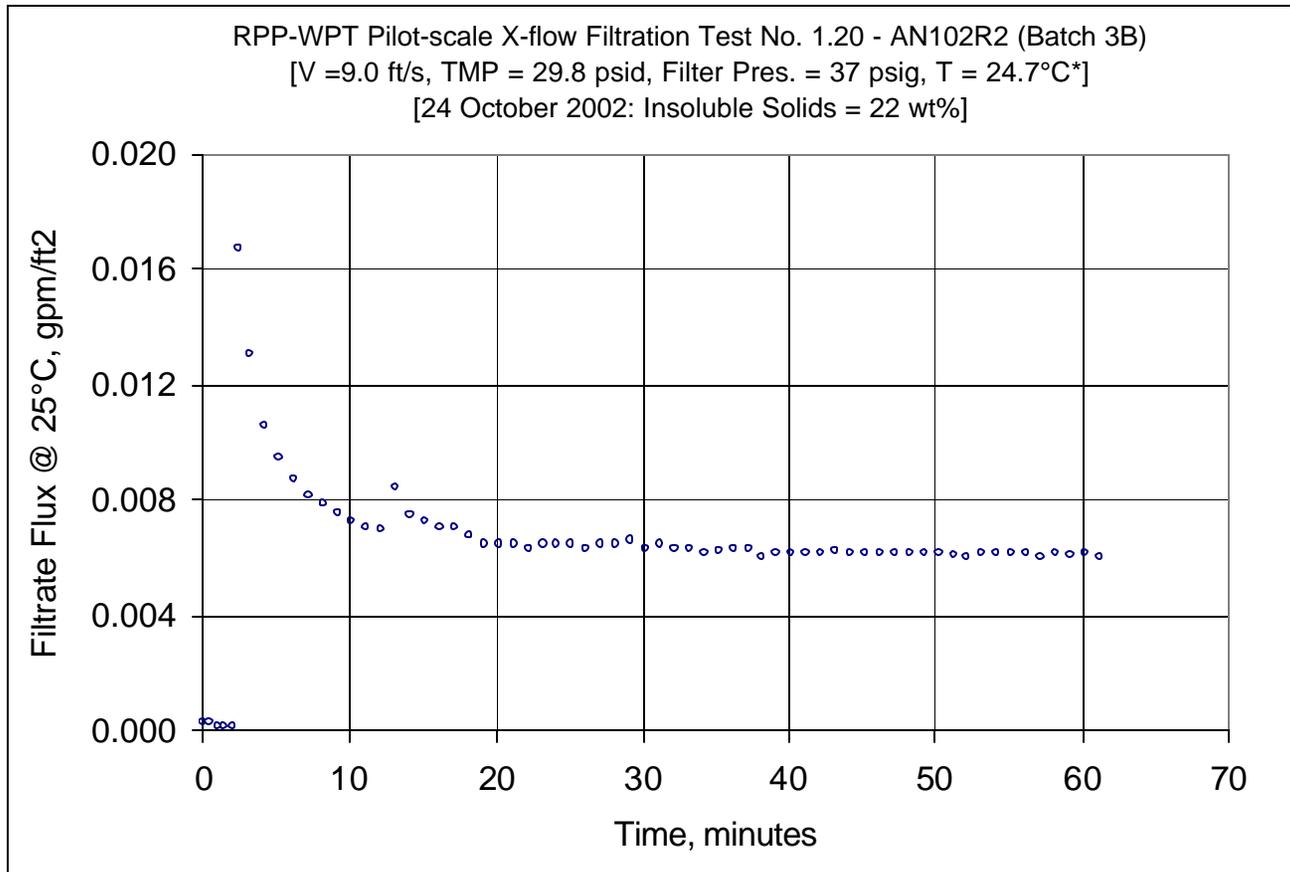


Figure E7: Steady state test run 1.20 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



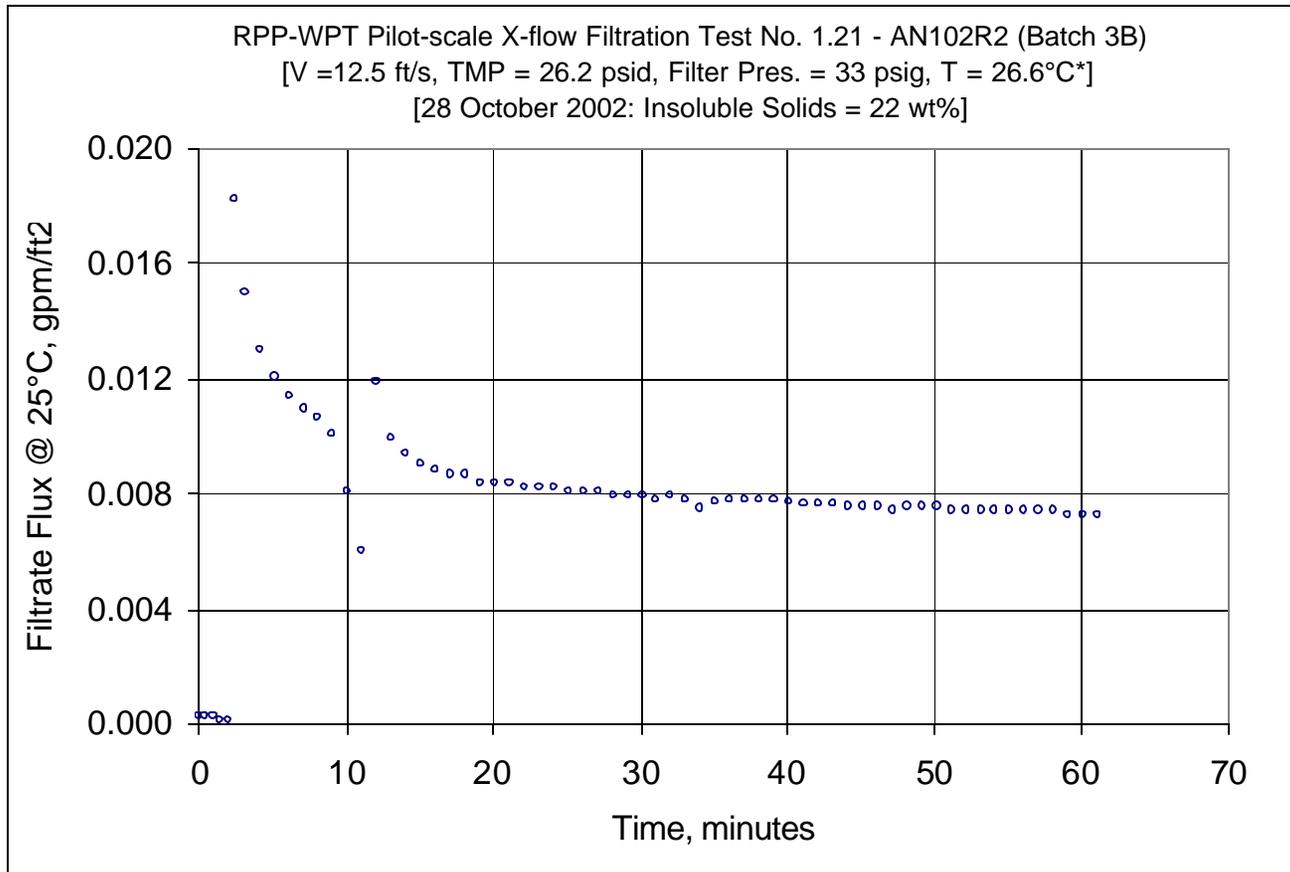


Figure E9: Steady state test run 1.21 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



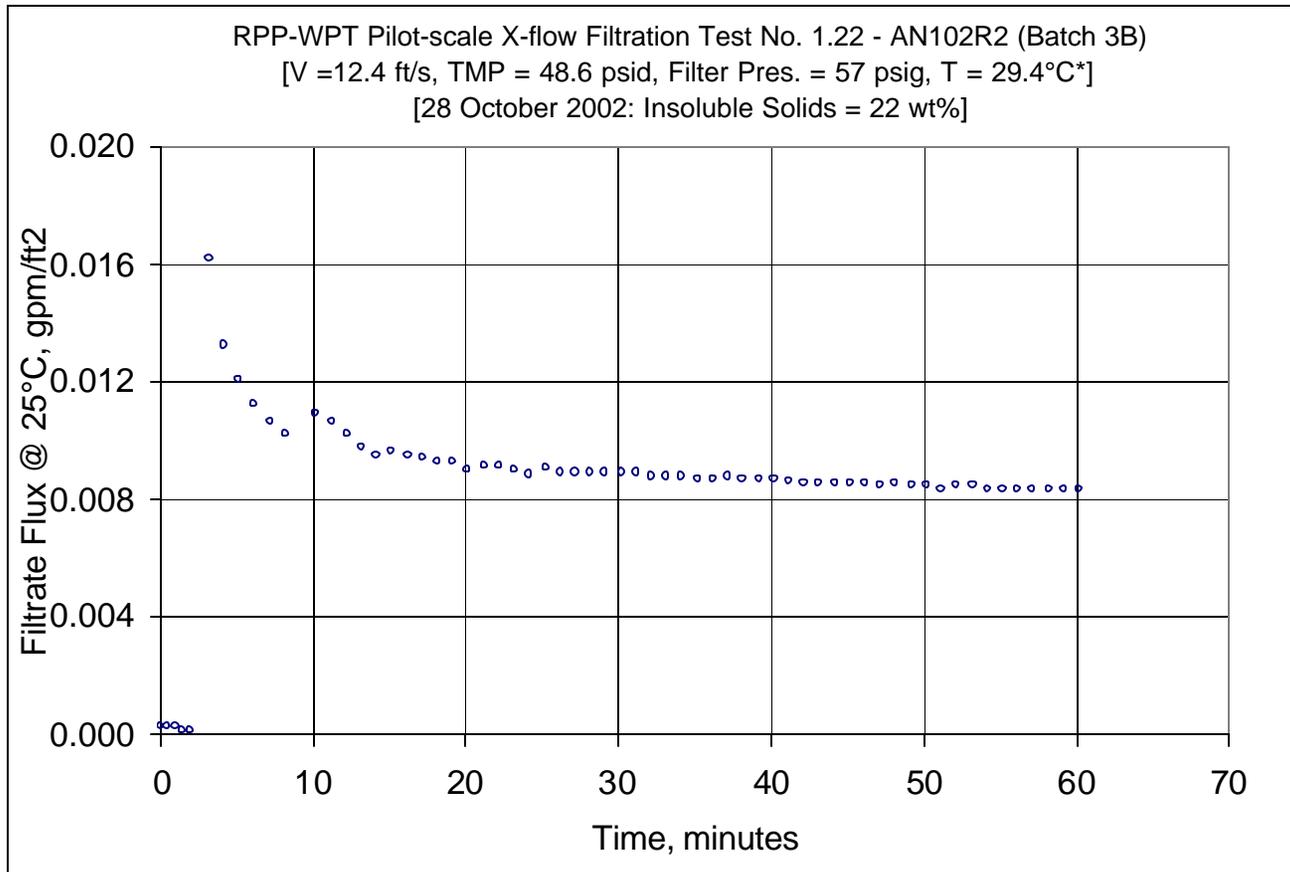


Figure E11: Steady state test run 1.22 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



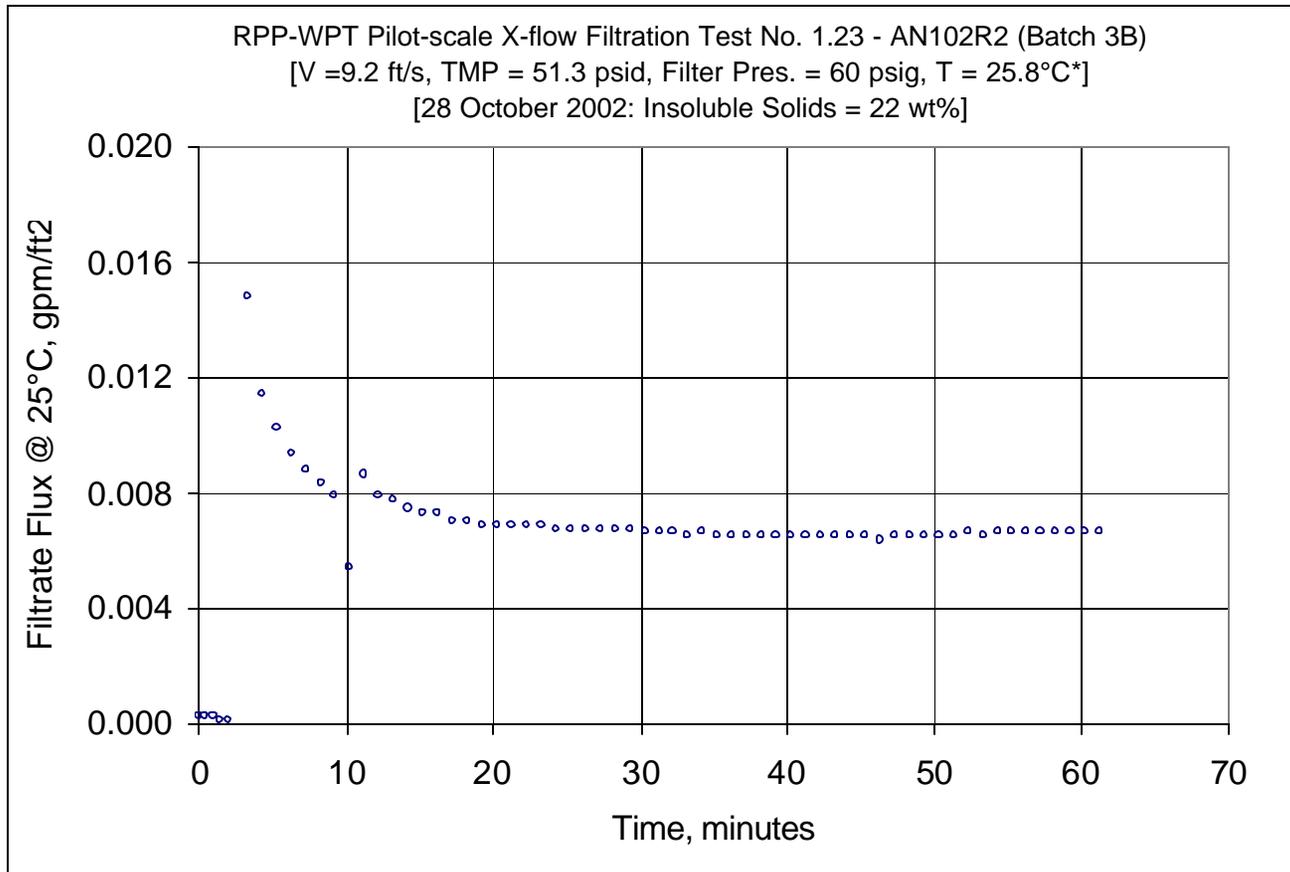


Figure E13: Steady state test run 1.23 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



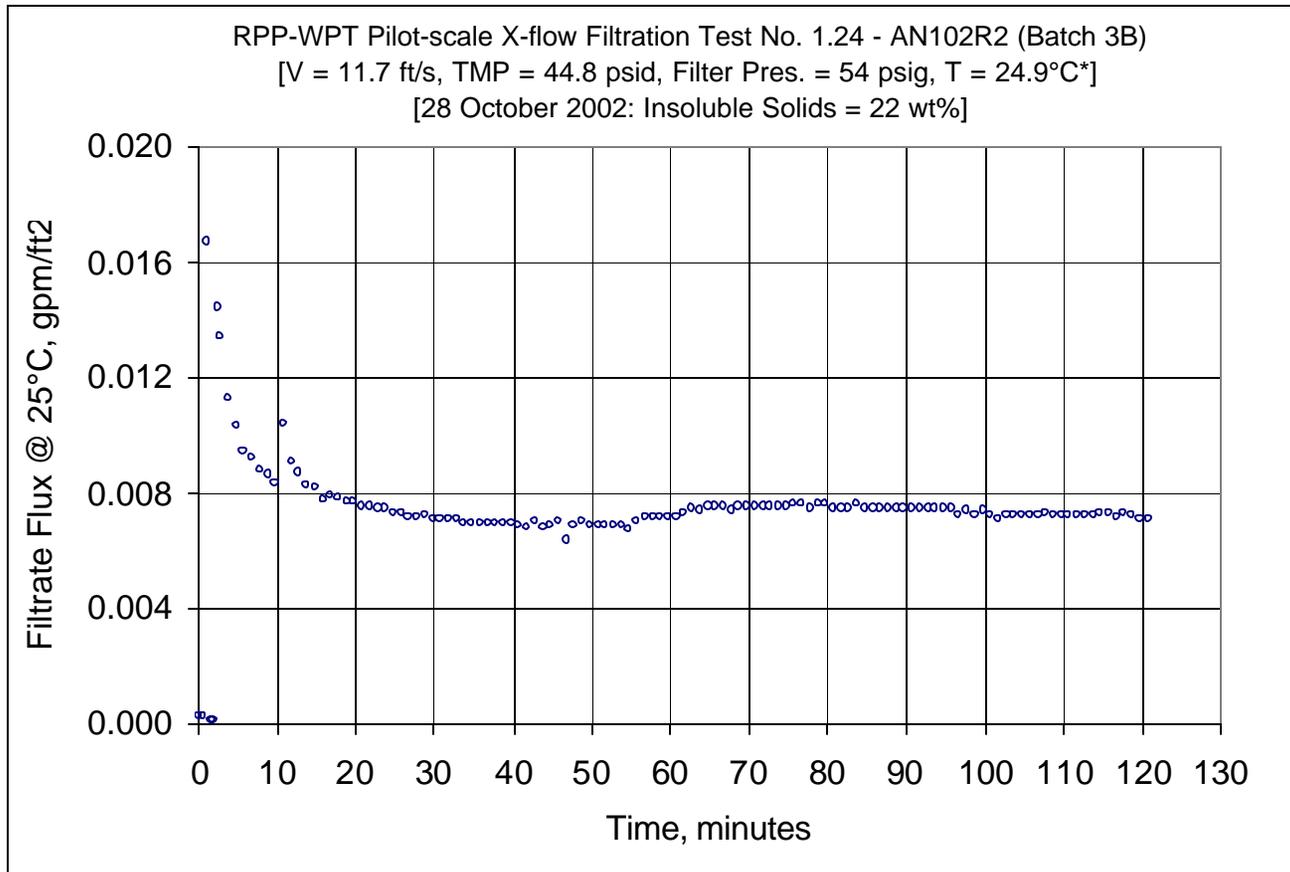


Figure E15: Steady state test run 1.24 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



10/28/2002	3:16-53 PM	25.924	26.297	24.191	27.45	26.515	51.368	53.815	15.531	36.827	-1.292	-6.524	46.253	0.047	0.001	0	56.75	0.94583	52.3	11.3	44.1	3.040	0.007	0.007	0.0002	0.163	0.14
10/28/2002	3:17-53 PM	25.944	26.343	24.242	27.416	26.555	52.437	55.019	15.966	37.183	-1.289	-6.521	46.664	0.047	0.001	0	57.75	0.9625	53.5	11.4	44.8	3.089	0.007	0.007	0.0002	0.160	0.14
10/28/2002	3:18-53 PM	25.933	26.357	24.246	27.434	26.574	51.959	54.603	15.76	36.798	-1.292	-6.524	47.226	0.047	0.001	0	56.75	0.97917	53.1	11.6	44.4	3.060	0.007	0.007	0.0002	0.161	0.14
10/28/2002	3:19-53 PM	25.927	26.36	24.265	27.423	26.583	52.607	55.156	16.022	37.4	-1.292	-6.524	46.996	0.047	0.001	0	59.75	0.99583	53.7	11.5	45.0	3.103	0.007	0.007	0.0002	0.159	0.14
10/28/2002	3:20-53 PM	25.93	26.379	24.283	27.422	26.586	53.172	55.739	16.105	37.973	-1.289	-6.524	47.174	0.047	0.001	0	60.75	1.0125	54.3	11.6	45.6	3.142	0.007	0.007	0.0002	0.157	0.13
10/28/2002	3:21-53 PM	25.921	26.375	24.294	27.433	26.572	54.241	56.951	16.503	38.471	-1.292	-6.518	47.276	0.048	0.001	0	61.75	1.02917	55.5	11.8	46.4	3.196	0.007	0.007	0.0002	0.157	0.13
10/28/2002	3:22-53 PM	25.933	26.392	24.336	27.42	26.584	54.78	57.448	16.538	39.07	-1.289	-6.513	48.115	0.049	0.001	0	62.75	1.04583	56.0	11.8	46.9	3.235	0.007	0.007	0.0002	0.159	0.13
10/28/2002	3:23-53 PM	25.938	26.412	24.376	27.444	26.594	54.974	57.706	16.734	38.917	-1.289	-6.515	48.588	0.049	0.001	0	63.75	1.0625	56.2	11.9	46.9	3.237	0.007	0.007	0.0002	0.158	0.13
10/28/2002	3:24-53 PM	25.945	26.414	24.398	27.371	26.621	55.457	58.124	16.917	39.349	-1.289	-6.513	48.376	0.05	0.001	0	64.75	1.07917	56.7	11.9	47.4	3.268	0.007	0.008	0.0002	0.160	0.14
10/28/2002	3:25-53 PM	25.948	26.412	24.407	27.395	26.639	56.033	58.702	17.052	39.758	-1.292	-6.518	48.667	0.05	0.001	0	65.75	1.09583	57.2	11.9	47.9	3.302	0.007	0.008	0.0002	0.158	0.13
10/28/2002	3:26-53 PM	25.96	26.439	24.454	27.431	26.656	56.848	58.889	16.967	39.447	-1.292	-6.515	49.319	0.05	0.001	0	66.75	1.1125	57.2	12.1	47.6	3.295	0.007	0.008	0.0002	0.159	0.14
10/28/2002	3:27-53 PM	25.975	26.454	24.494	27.436	26.656	56.397	59.064	17.209	39.799	-1.286	-6.513	48.678	0.049	0.001	0	67.75	1.12917	57.6	11.9	48.1	3.316	0.007	0.007	0.0002	0.154	0.13
10/28/2002	3:28-53 PM	25.975	26.464	24.519	27.381	26.666	56.265	59.09	17.15	39.748	-1.292	-6.51	48.894	0.05	0.001	0	68.75	1.14583	57.6	12.0	48.0	3.310	0.007	0.008	0.0002	0.157	0.13
10/28/2002	3:29-53 PM	25.986	26.47	24.545	27.397	26.662	56.348	59.2	17.025	40.059	-1.289	-6.51	48.902	0.05	0.001	0	69.75	1.1625	57.7	12.0	48.2	3.323	0.007	0.008	0.0002	0.157	0.13
10/28/2002	3:30-53 PM	26.005	26.484	24.584	27.391	26.676	56.7	59.603	17.157	40.231	-1.289	-6.51	49.259	0.05	0.001	0	70.75	1.17917	58.1	12.1	48.5	3.342	0.007	0.008	0.0002	0.156	0.13
10/28/2002	3:31-53 PM	26.03	26.499	24.614	27.426	26.676	56.654	59.454	17.234	40.143	-1.292	-6.513	49.263	0.05	0.001	0	71.75	1.19583	58.0	12.1	48.4	3.337	0.007	0.008	0.0002	0.156	0.13
10/28/2002	3:32-53 PM	26.036	26.5	24.63	27.457	26.702	57.004	59.815	17.38	40.405	-1.295	-6.513	49.491	0.05	0.001	0	72.75	1.2125	58.3	12.1	48.7	3.358	0.007	0.008	0.0002	0.155	0.13
10/28/2002	3:33-53 PM	26.055	26.519	24.664	27.466	26.696	57.17	60.187	17.426	40.303	-1.292	-6.513	49.519	0.05	0.001	0	73.75	1.22917	58.7	12.1	48.7	3.360	0.007	0.008	0.0002	0.154	0.13
10/28/2002	3:34-53 PM	26.076	26.53	24.71	27.442	26.702	57.079	59.899	17.33	40.608	-1.292	-6.513	49.475	0.05	0.001	0	74.75	1.24583	58.4	12.1	48.8	3.368	0.007	0.008	0.0002	0.154	0.13
10/28/2002	3:35-53 PM	26.114	26.553	24.763	27.415	26.715	57.25	60.073	17.375	40.683	-1.289	-6.507	48.967	0.051	0.001	0	75.75	1.2625	58.6	12.0	49.0	3.376	0.008	0.008	0.0002	0.156	0.13
10/28/2002	3:36-53 PM	26.121	26.549	24.765	27.457	26.707	57.12	60.098	17.402	40.313	-1.289	-6.478	49.376	0.051	0.001	0	76.75	1.27917	58.6	12.1	48.7	3.359	0.008	0.008	0.0002	0.157	0.13
10/28/2002	3:37-53 PM	26.127	26.54	24.781	27.408	26.703	57.155	60.176	17.434	40.327	-1.289	-6.478	49.41	0.05	0.001	0	77.75	1.29583	58.7	12.1	48.7	3.361	0.007	0.008	0.0002	0.154	0.13
10/28/2002	3:38-53 PM	26.149	26.557	24.808	27.4	26.724	57.567	60.427	17.541	40.858	-1.289	-6.472	49.777	0.051	0.001	0	78.75	1.3125	59.0	12.2	49.2	3.393	0.008	0.008	0.0002	0.155	0.13
10/28/2002	3:39-53 PM	26.155	26.554	24.815	27.247	26.731	57.236	60.29	17.368	40.507	-1.290	-6.478	49.904	0.051	0.001	0	79.75	1.32917	58.8	12.2	48.9	3.370	0.008	0.008	0.0002	0.156	0.13
10/28/2002	3:40-53 PM	26.178	26.582	24.862	27.34	26.729	57.174	59.976	17.425	40.507	-1.292	-6.478	49.638	0.05	0.001	0	80.75	1.34583	58.5	12.2	48.8	3.367	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:41-53 PM	26.179	26.578	24.863	27.416	26.715	57.402	60.567	17.602	40.352	-1.292	-6.475	49.529	0.05	0.001	0	81.75	1.3625	59.1	12.1	48.9	3.370	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:42-53 PM	26.195	26.574	24.879	27.406	26.711	57.516	60.648	17.451	40.737	-1.292	-6.475	49.533	0.05	0.001	0	82.75	1.37917	59.2	12.2	49.1	3.387	0.007	0.007	0.0002	0.152	0.13
10/28/2002	3:43-53 PM	26.211	26.59	24.905	27.402	26.707	57.238	60.315	17.417	40.481	-1.289	-6.472	48.858	0.051	0.001	0	83.75	1.39583	58.8	12.0	48.9	3.369	0.008	0.008	0.0002	0.156	0.13
10/28/2002	3:44-53 PM	26.232	26.586	24.921	27.423	26.703	57.493	60.51	17.504	40.622	-1.292	-6.478	49.248	0.05	0.001	0	84.75	1.4125	59.0	12.1	49.1	3.382	0.007	0.007	0.0002	0.152	0.13
10/28/2002	3:45-53 PM	26.231	26.585	24.925	27.432	26.712	57.029	60.081	17.276	40.507	-1.292	-6.478	49.848	0.05	0.001	0	85.75	1.42917	58.6	12.2	48.8	3.362	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:46-53 PM	26.251	26.59	24.95	27.372	26.717	57.319	60.313	17.442	40.675	-1.289	-6.475	50.045	0.05	0.001	0	86.75	1.44583	58.8	12.3	49.0	3.378	0.007	0.007	0.0002	0.152	0.13
10/28/2002	3:47-53 PM	26.263	26.602	24.977	27.389	26.734	57.414	60.402	17.539	40.814	-1.292	-6.478	49.877	0.05	0.001	0	87.75	1.4625	58.9	12.2	48.8	3.379	0.007	0.007	0.0002	0.152	0.13
10/28/2002	3:48-53 PM	26.306	26.615	25.005	27.377	26.737	56.948	60.154	17.788	39.873	-1.292	-6.478	50.248	0.05	0.001	0	88.75	1.47917	58.7	12.3	48.4	3.338	0.007	0.007	0.0002	0.154	0.13
10/28/2002	3:49-53 PM	26.335	26.633	25.059	27.421	26.73	57.205	60.377	17.683	40.264	-1.286	-6.475	49.034	0.05	0.001	0	89.75	1.49583	58.9	12.0	48.7	3.360	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:50-53 PM	26.327	26.621	25.052	27.404	26.713	56.88	60.007	17.517	40.139	-1.289	-6.478	49.93	0.05	0.001	0	90.75	1.5125	58.5	12.2	48.5	3.345	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:51-53 PM	26.333	26.612	25.048	27.35	26.714	57.143	60.282	17.526	40.348	-1.292	-6.475	49.942	0.05	0.001	0	91.75	1.52917	58.8	12.2	48.7	3.361	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:52-53 PM	26.354	26.623	25.064	27.361	26.7	57.159	60.172	17.569	40.393	-1.289	-6.475	50.393	0.05	0.001	0	92.75	1.54583	58.7	12.3	48.8	3.363	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:53-53 PM	26.359	26.618	25.059	27.266	26.695	57.07	60.181	17.661	40.159	-1.292	-6.478	51.326	0.05	0.001	0	93.75	1.5625	58.7	12.6	48.6	3.352	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:54-53 PM	26.369	26.618	25.069	27.316	26.715	57.333	60.555	17.723	40.342	-1.289	-6.481	51.283	0.05	0.001	0	94.75	1.57917	59.1	12.6	48.8	3.367	0.007	0.007	0.0002	0.152	0.13
10/28/2002	3:55-53 PM	26.38	26.619	25.075	27.307	26.706	57.248	60.41	17.60	40.266	-1.295	-6.484	50.091	0.05	0.001	-0.001	95.75	1.59583	58.9	12.3	48.8	3.362	0.007	0.007	0.0002	0.153	0.13
10/28/2002	3:56-53 PM	26.386	26.62	25.091	27.313	26.707	56.969	60.228	17.533	40.11	-1.292	-6.481	50.116	0.049	0.001	0	96.75	1.6125	58.8	12.3	48.5	3.347	0.007	0.007	0.0002	0.150	0.13
10/28/2002	3:57-53 PM	26.393	26.622	25.103	27.27	26.684	57.495	60.872	17.707	40.473	-1.289																

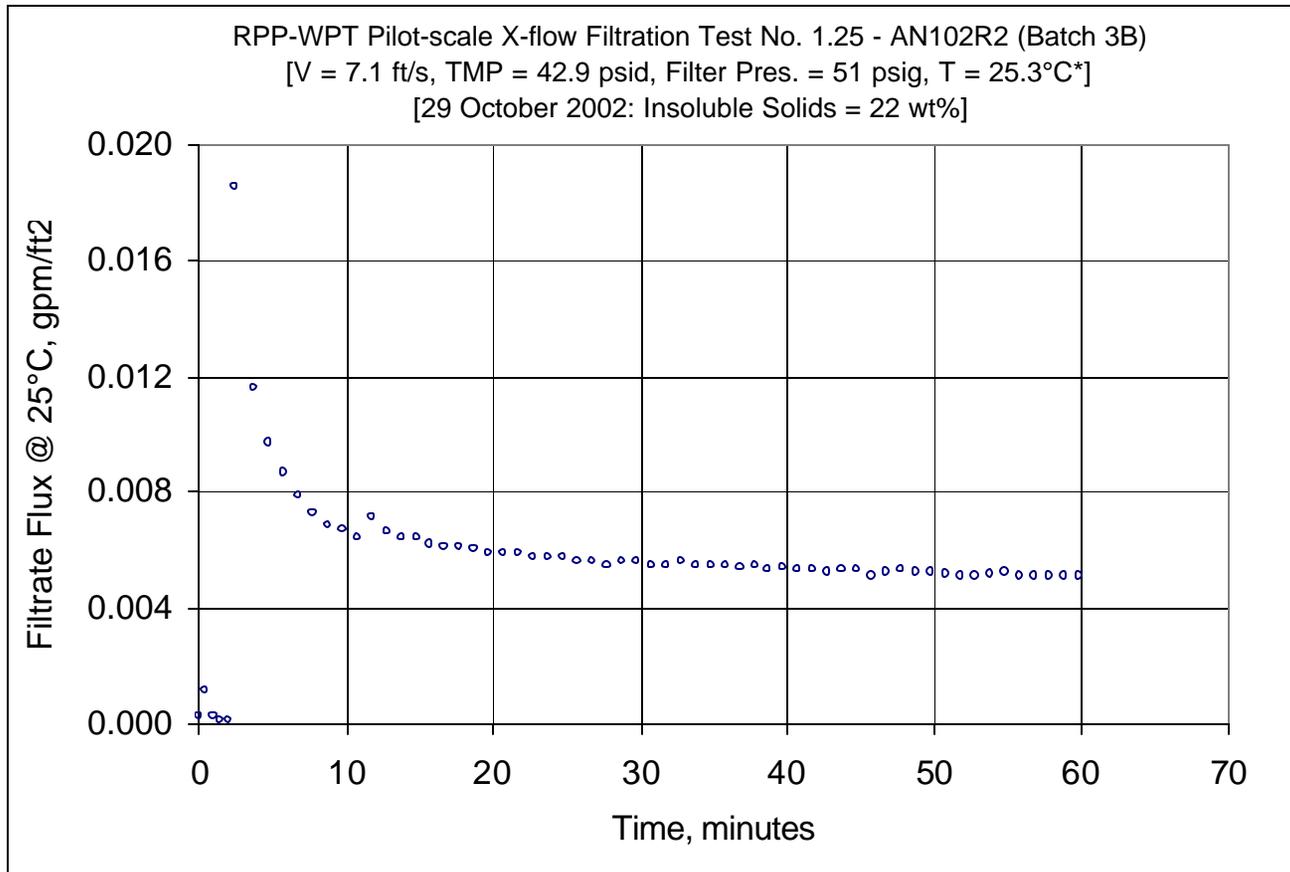


Figure E17: Steady state test run 1.25 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



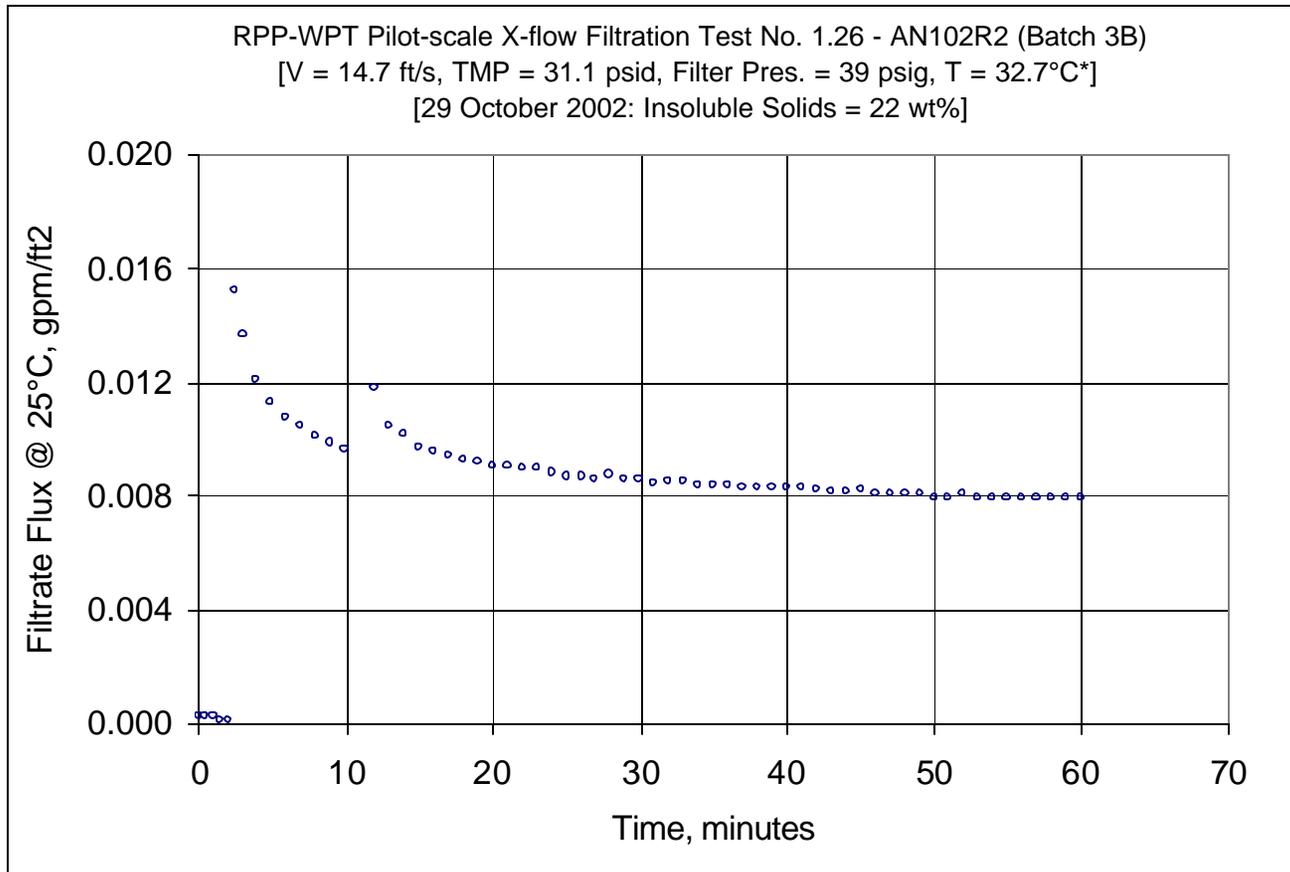


Figure E19: Steady state test run 1.26 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



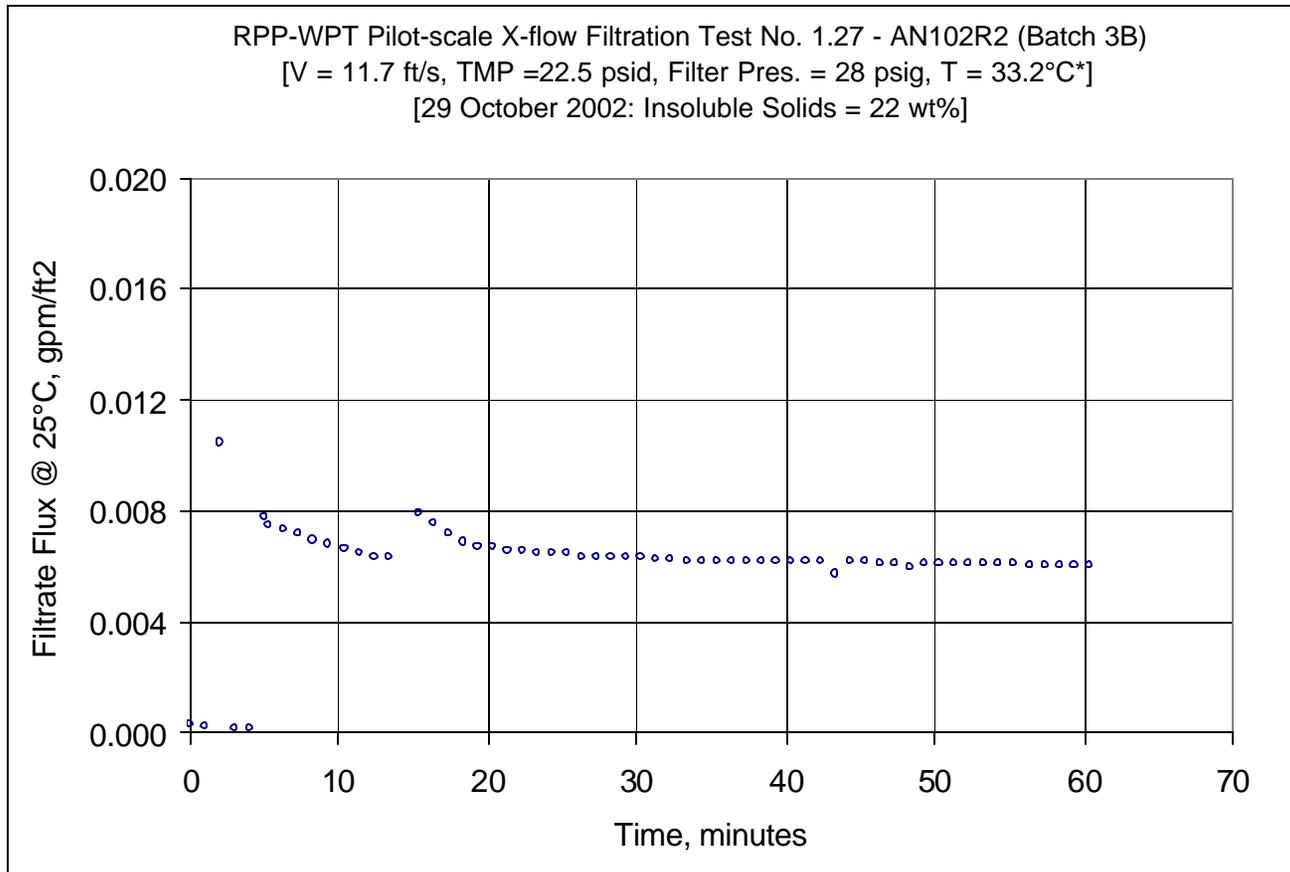


Figure E21: Steady state test run 1.27 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



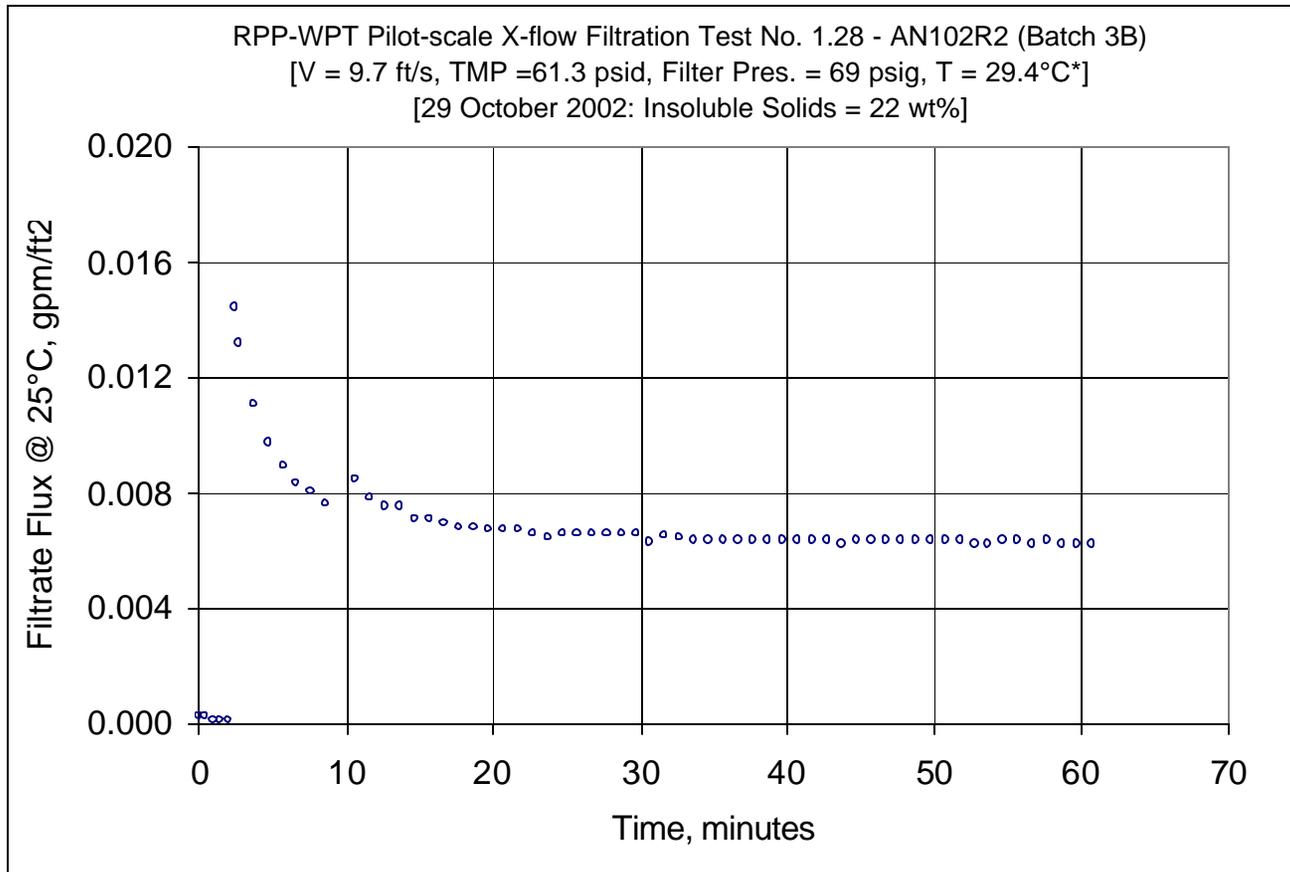


Figure E23: Steady state test run 1.28 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%

DATE	Temperature Measurements >					Pressure Measurements >>>>>					Flow Measurements >>>				
	Filtrate deg C	Cleaning deg C	Slurry deg C	Hi Amb deg C	Lo Amb deg C	BotTMP psid	Filter deg C	Filter deg C	Filter deg C	TopTMP psid	Filtrate deg C	Pulsopot psid	Slurry deg C	Filtrate deg C	Backpulse deg C
TIME	T2	T3	T1	T4	T5	dP2	dP1	dP3	F2	F3	F3	Q1	Q2	Q3	Obp
Zeros															
10/29/2002 7:44:20 AM	22.171	22.452	21.341	22.224	22.268	-0.129	0.071	-0.054	0.054	-0.395	0.395	-0.216	0.001	0.001	0.002
10/29/2002 7:44:33 AM	22.171	22.452	21.341	22.224	22.268	-0.129	0.071	-0.054	0.054	-0.395	0.395	-0.216	0.001	0.001	0.002
10/29/2002 7:44:34 AM	22.171	22.447	21.351	22.244	22.283	-0.129	0.073	-0.053	0.058	-0.384	0.384	-0.212	0.002	0.001	0.002
10/29/2002 7:44:35 AM	22.171	22.447	21.356	22.239	22.283	-0.127	0.071	-0.053	0.058	-0.382	0.361	-0.212	0.002	0.001	0.002
10/29/2002 7:44:36 AM	22.171	22.452	21.351	22.239	22.273	-0.129	0.071	-0.053	0.056	-0.344	0.361	-0.21	0.002	0.001	0.003
10/29/2002 7:44:37 AM	22.171	22.447	21.346	22.229	22.263	-0.127	0.071	-0.053	0.056	-0.347	0.361	-0.214	0.002	0.001	0.003
10/29/2002 7:44:38 AM	22.176	22.452	21.346	22.239	22.283	-0.129	0.073	-0.053	0.056	-0.37	0.364	-0.212	0.002	0.001	0.003
10/29/2002 7:44:39 AM	22.176	22.447	21.351	22.234	22.283	-0.129	0.073	-0.053	0.056	-0.382	0.361	-0.214	0.001	0.001	0.002
Data - Per Minute															
10/29/2002 2:44:06 PM	29.38	23.677	27.071	23.018	23.71	49.345	69.333	15.693	34.212	13.633	109.348	40.525	0.002	0.001	0
10/29/2002 2:44:36 PM	26.651	23.66	27.168	22.99	23.677	-7.461	67.39	7.818	-18.557	81.44	83.404	41.775	0.002	0.001	1.083
10/29/2002 2:45:06 PM	27.894	23.655	27.343	22.895	23.667	6.086	67.742	9.118	-2.136	55.952	6.969	43.638	0.001	0.001	0
10/29/2002 2:45:36 PM	28.546	23.659	27.402	22.894	23.651	80.179	68.141	10.757	50.194	1.902	0.576	43.006	0.36	0.001	0
10/29/2002 2:46:06 PM	28.665	23.644	27.487	22.974	23.636	62.375	68.763	11.782	51.331	0.404	0.599	42.933	0.129	0.001	0
10/29/2002 2:46:36 PM	28.71	23.643	27.561	22.959	23.695	62.186	68.481	12.34	50.723	0.292	0.622	42.963	0.104	0.001	0
10/29/2002 2:46:47 PM	28.744	23.643	27.591	22.969	23.685	62.027	68.549	12.52	50.207	0.292	0.654	41.57	0.095	0.001	0
10/29/2002 2:47:17 PM	28.85	23.629	27.731	23.08	23.651	62.261	68.611	12.991	50.053	0.251	0.68	41.085	0.08	0.001	0
10/29/2002 2:48:07 PM	28.93	23.609	27.876	23.136	23.647	62.404	68.759	13.432	49.638	0.251	0.699	40.622	0.071	0.001	0
10/29/2002 2:49:47 PM	29.021	23.601	28.032	23.183	23.663	62.791	69.109	13.879	49.754	0.251	0.709	40.463	0.065	0.001	0
10/29/2002 2:50:47 PM	29.122	23.582	28.164	23.24	23.67	62.333	68.743	13.943	49.247	0.257	0.730	40.225	0.061	0.001	0
10/29/2002 2:51:47 PM	29.205	23.585	28.271	23.559	23.603	62.805	69.147	14.122	49.165	0.283	0.755	39.764	0.059	0.001	0
10/29/2002 2:52:47 PM	29.307	23.585	28.744	23.517	23.614	62.716	69.267	14.21	49.385	0.291	0.755	39.491	0.059	0.001	0
10/29/2002 2:53:47 PM	29.274	23.565	28.48	23.418	23.688	65.759	69.42	14.315	52.197	-1.289	-3.552	39.363	0.311	0.001	0
10/29/2002 2:54:47 PM	28.654	23.577	28.682	23.285	23.695	68.744	69.265	14.505	55.079	-1.289	-6.301	39.428	0.063	0.001	0
10/29/2002 2:55:47 PM	28.501	23.574	28.648	23.166	23.722	68.207	69.052	14.463	54.5	-1.289	-6.481	39.199	0.059	0.001	0
10/29/2002 2:56:47 PM	28.433	23.595	28.744	23.157	23.718	69.143	70.094	14.587	54.939	-1.284	-6.456	39.308	0.059	0.001	0
10/29/2002 2:57:47 PM	28.423	23.58	28.784	23.032	23.708	68.973	69.008	14.738	54.518	-1.286	-6.595	39.25	0.056	0.001	0
10/29/2002 2:58:47 PM	28.447	23.569	28.808	22.95	23.707	68.425	69.389	14.839	54.287	-1.289	-6.562	39.313	0.053	0.001	0
10/29/2002 2:59:47 PM	28.461	23.568	28.857	22.858	23.731	68.891	69.552	14.934	54.911	-1.289	-6.595	39.225	0.053	0.001	0
10/29/2002 3:00:47 PM	28.5	23.587	28.93	23.963	23.755	68.416	69.147	14.89	54.408	-1.289	-6.553	39.252	0.052	0.001	0
10/29/2002 3:01:47 PM	28.540	23.603	28.986	24.01	23.864	68.371	69.469	14.981	54.021	-1.289	-6.595	39.154	0.051	0.001	0
10/29/2002 3:02:47 PM	28.603	23.631	29.103	23.168	23.875	69.164	69.838	15.137	54.891	-1.289	-6.568	39.304	0.051	0.001	0
10/29/2002 3:03:47 PM	28.641	23.639	29.166	23.176	23.908	68.36	69.316	14.934	54.184	-1.286	-6.576	39.336	0.051	0.001	0
10/29/2002 3:04:47 PM	28.681	23.639	29.211	23.196	23.943	69.079	70.119	15.148	54.721	-1.289	-6.595	39.362	0.051	0.001	0
10/29/2002 3:05:47 PM	28.724	23.652	29.273	23.146	23.866	68.744	69.789	15.273	54.481	-1.289	-6.595	39.428	0.049	0.001	0
10/29/2002 3:06:47 PM	28.757	23.66	29.316	23.157	23.974	69.122	70.27	15.265	54.51	-1.289	-6.582	39.573	0.05	0.001	0
10/29/2002 3:07:47 PM	28.793	23.657	29.338	23.088	23.94	68.859	70.144	15.18	54.364	-1.289	-6.541	39.443	0.049	0.001	0
10/29/2002 3:08:47 PM	28.839	23.688	29.399	23.07	23.922	68.714	70.007	15.054	54.322	-1.292	-6.599	39.487	0.05	0.001	0
10/29/2002 3:09:47 PM	28.891	23.691	29.456	23.07	23.884	68.891	70.104	15.21	54.688	-1.286	-6.632	39.444	0.049	0.001	0
10/29/2002 3:10:47 PM	28.909	23.653	29.498	23.124	23.895	69.031	70.113	15.162	54.655	-1.289	-6.623	39.585	0.05	0.001	0
10/29/2002 3:11:47 PM	28.931	23.655	29.53	23.097	23.823	69.023	69.811	15.245	54.846	-1.289	-6.625	39.657	0.05	0.001	0
10/29/2002 3:12:47 PM	28.982	23.656	29.571	23.037	23.789	69.325	70.526	15.243	54.821	-1.286	-6.625	39.623	0.05	0.001	0
10/29/2002 3:13:47 PM	29.006	23.641	29.598	23.047	23.729	69.166	70.555	15.101	54.852	-1.286	-6.625	39.548	0.05	0.001	0
10/29/2002 3:14:47 PM	29.031	23.63	29.63	23.046	23.683	68.897	70.115	15.236	54.536	-1.286	-6.591	39.768	0.048	0.001	0
10/29/2002 3:15:47 PM	29.05	23.625	29.674	22.991	23.653	69.226	70.589	15.342	54.608	-1.289	-6.594	39.558	0.05	0.001	0
10/29/2002 3:16:47 PM	29.06	23.605	29.689	22.946	23.638	69.441	70.845	15.238	54.796	-1.286	-6.597	39.749	0.049	0.001	0
10/29/2002 3:17:47 PM	29.07	23.589	29.723	22.895	23.627	69.559	70.827	15.343	55.075	-1.289	-6.617	39.707	0.049	0.001	0
10/29/2002 3:18:47 PM	29.099	23.584	29.758	22.825	23.607	68.907	70.212	15.202	54.551	-1.292	-6.599	39.772	0.049	0.001	0
10/29/2002 3:19:47 PM	29.124	23.574	29.793	22.835	23.567	69.477	71.017	15.3	54.831	-1.286	-6.597	39.812	0.049	0.001	0
10/29/2002 3:20:47 PM	29.138	23.558	29.812	22.774	23.551	69.122	70.634	15.181	54.667	-1.286	-6.597	39.797	0.049	0.001	0
10/29/2002 3:21:47 PM	29.163	23.543	29.842	22.804	23.531	68.563	71.309	15.457	54.657	-1.286	-6.597	39.6	0.049	0.001	0
10/29/2002 3:22:47 PM	29.204	23.544	29.863	22.835	23.537	69.305	70.789	15.34	54.786	-1.286	-6.597	39.77	0.049	0.001	0
10/29/2002 3:23:47 PM	29.21	23.525	29.868	22.85	23.542	68.837	70.357	15.281	54.283	-1.289	-6.597	39.862	0.049	0.001	0
10/29/2002 3:24:47 PM	29.236	23.526	29.895	22.852	23.549	68.915	70.427	15.277	54.416	-1.286	-6.597	39.407	0.049	0.001	0
10/29/2002 3:25:47 PM	29.256	23.511	29.89	22.736	23.539	69.444	71.052	15.409	54.766	-1.289	-6.597	39.904	0.049	0.001	0
10/29/2002 3:26:47 PM	29.262	23.512	29.91	22.672	23.555	69.433	70.715	15.389	55.048	-1.289	-6.597	39.879	0.049	0.001	0
10/29/2002 3:27:47 PM	29.278	23.503	29.906	22.597	23.566	69.398	70.795	15.38	54.864	-1.289	-6.599	39.974	0.048	0.001	0
10/29/2002 3:28:47 PM	29.288	23.509	29.927	22.648	23.592	69.56	71.151	15.47	54.778	-1.284	-6.594	40.124	0.049	0.001	0
10/29/2002 3:29:47 PM	29.289	23.499	29.923	22.709	23.607	69.705	71.267	15.325	55.103	-1.289	-6.599	40.363	0.049	0.001	0
10/29/2002 3:30:47 PM	29.295	23.505	29.973	22.725	23.603	69.663	71.455	15.388	54.923	-1.286	-6.597	39.523	0.049	0.001	0
10/29/2002 3:31:47 PM	29.311	23.497	29.975	22.611	23.625	69.226	70.787	15.039	55.073	-1.289	-6.597	39.806	0.049	0.001	0
10/29/2002 3:32:47 PM	29.293	23.508	29.996	22.588	23.626	69.864	71.431	15.388	55.449	-1.289	-6.599	40.135	0.049	0.001	0
10/29/2002 3:33:47 PM	29.293	23.488	29.971	22.477	23.621	69.599	71.402	15.415	54.87	-1.289	-6.597	39.862	0.049	0.001	

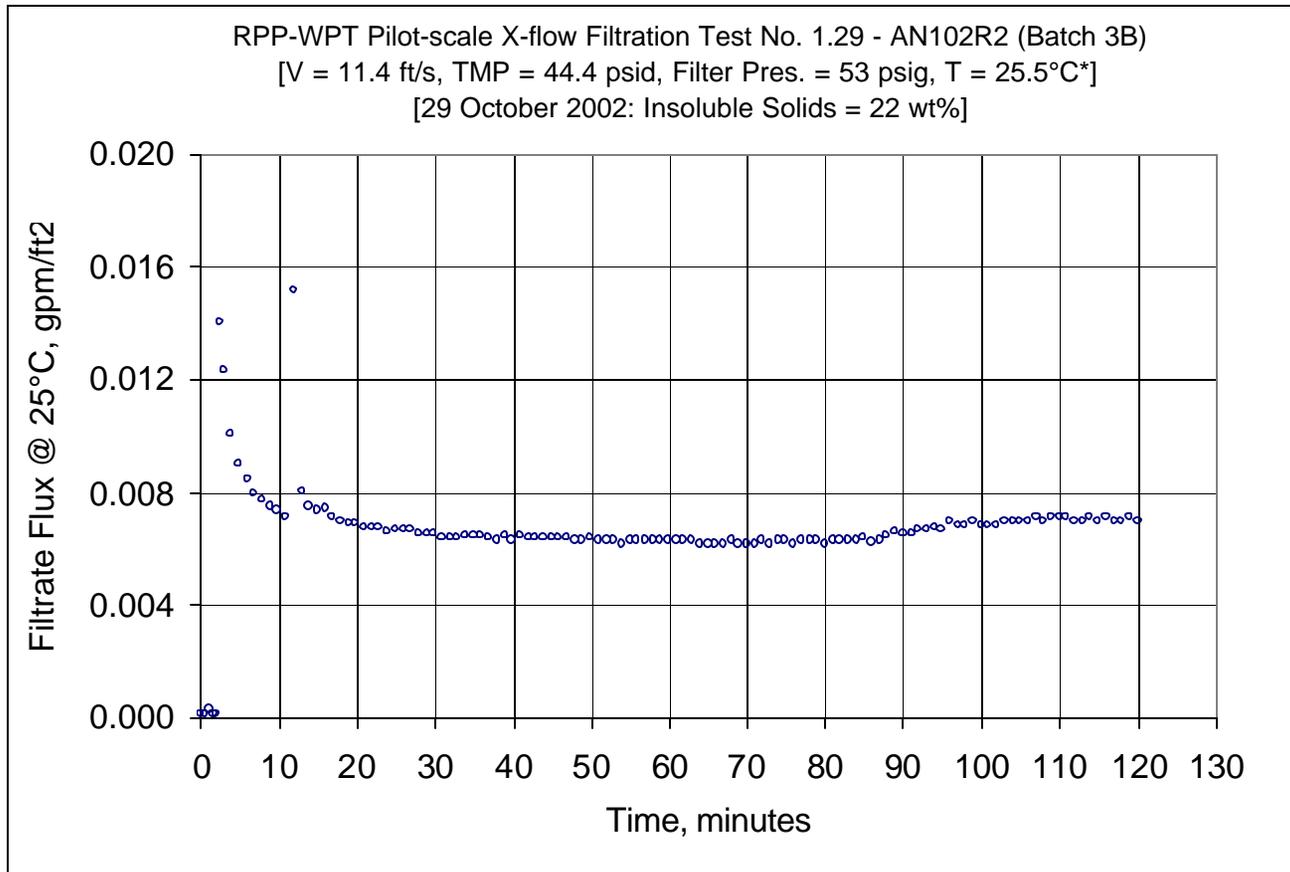


Figure E25: Steady state test run 1.29 of AN-102R2, batch 3B, insoluble solids concentration of 22 wt%



10/29/2002	4:50:20 PM	25.653	23.567	25.527	22.968	23.75	50.745	53.054	15.23	36.245	-1.289	-6.515	45.647	0.043	0.001	0	56.87	0.94776	51.6	11.2	43.5	2.999	0.006	0.006	0.0001	0.145	0.12
10/29/2002	4:51:20 PM	25.681	23.575	25.445	23.091	23.763	49.939	52.278	14.989	35.798	-1.296	-6.613	45.33	0.043	0.001	0	57.87	0.96444	50.8	11.1	42.8	2.964	0.006	0.006	0.0001	0.148	0.13
10/29/2002	4:52:20 PM	25.671	23.56	25.63	22.961	23.753	49.769	53.265	15.012	36.451	-1.289	-6.516	45.683	0.043	0.001	0	58.87	0.98111	50.6	11.2	43.6	2.938	0.006	0.006	0.0001	0.146	0.13
10/29/2002	4:53:20 PM	25.682	23.566	25.6	22.836	23.749	50.236	52.532	14.965	36.147	-1.292	-6.515	45.492	0.043	0.001	0	59.87	0.99776	51.1	11.1	43.2	2.978	0.006	0.006	0.0001	0.146	0.12
10/29/2002	4:54:20 PM	25.698	23.572	25.562	22.802	23.75	50.896	53.163	15.217	36.593	-1.289	-6.515	45.458	0.043	0.001	0	60.87	1.01444	51.7	11.1	43.7	3.016	0.006	0.006	0.0001	0.144	0.12
10/29/2002	4:55:20 PM	25.719	23.583	25.478	22.773	23.756	50.3	52.828	15.171	35.717	-1.286	-6.513	45.488	0.043	0.001	0	61.87	1.03111	51.4	11.1	43.0	2.965	0.006	0.006	0.0001	0.147	0.13
10/29/2002	4:56:20 PM	25.738	23.602	25.662	22.736	23.765	50.648	52.977	15.387	36.102	-1.286	-6.513	45.37	0.043	0.001	0	62.87	1.04776	51.5	11.1	43.4	2.991	0.006	0.006	0.0001	0.145	0.12
10/29/2002	4:57:20 PM	25.719	23.588	25.638	22.632	23.756	50.881	53.297	15.402	36.178	-1.289	-6.486	45.678	0.042	0.001	-0.001	63.87	1.06444	51.9	11.2	43.5	3.001	0.006	0.006	0.0001	0.141	0.12
10/29/2002	4:58:20 PM	25.715	23.589	25.604	22.819	23.762	50.876	53.161	15.345	36.364	-1.286	-6.489	45.267	0.042	0.001	0	64.87	1.08111	51.7	11.1	43.6	3.007	0.006	0.006	0.0001	0.141	0.12
10/29/2002	4:59:20 PM	25.727	23.586	25.516	22.967	23.779	50.892	53.345	15.418	36.237	-1.286	-6.489	46.435	0.042	0.001	0	65.87	1.09776	51.9	11.4	43.6	3.004	0.006	0.006	0.0001	0.142	0.12
10/29/2002	5:00:20 PM	25.733	23.602	25.477	22.973	23.785	51.491	53.925	15.653	36.901	-1.289	-6.547	44.72	0.042	0.001	0	66.87	1.11444	52.5	11.0	44.0	3.033	0.006	0.006	0.0001	0.140	0.12
10/29/2002	5:01:20 PM	25.745	23.613	25.688	22.889	23.786	50.757	53.226	15.361	36.073	-1.286	-6.544	45.684	0.043	0.001	0	67.87	1.13111	51.9	11.2	43.4	2.993	0.006	0.006	0.0001	0.145	0.12
10/29/2002	5:02:20 PM	25.74	23.608	25.643	22.758	23.796	50.374	52.756	15.262	35.91	-1.286	-6.553	45.747	0.042	0.001	0	68.87	1.14776	51.3	11.2	43.1	2.974	0.006	0.006	0.0001	0.143	0.12
10/29/2002	5:03:20 PM	25.745	23.609	25.574	22.744	23.787	51.116	53.557	15.413	36.395	-1.289	-6.553	45.666	0.042	0.001	0	69.87	1.16444	52.1	11.2	43.8	3.017	0.006	0.006	0.0001	0.141	0.12
10/29/2002	5:04:20 PM	25.756	23.615	25.485	22.765	23.798	50.548	53.031	15.333	35.948	-1.289	-6.566	45.802	0.042	0.001	0	70.87	1.18111	51.6	11.2	43.2	2.982	0.006	0.006	0.0001	0.143	0.12
10/29/2002	5:05:20 PM	25.772	23.631	25.726	22.971	23.809	50.96	53.515	15.396	36.206	-1.286	-6.547	46.048	0.043	0.001	0	71.87	1.19776	52.0	11.3	43.6	3.006	0.006	0.006	0.0001	0.144	0.12
10/29/2002	5:06:20 PM	25.762	23.621	25.691	22.871	23.809	50.784	53.226	15.454	36.051	-1.289	-6.553	46.943	0.042	0.001	0	72.87	1.21444	51.8	11.5	43.4	2.993	0.006	0.006	0.0001	0.142	0.12
10/29/2002	5:07:20 PM	25.744	23.603	25.607	22.883	23.796	50.826	53.186	15.397	36.387	-1.289	-6.553	46.444	0.043	0.001	0	73.87	1.23111	51.7	11.4	43.6	3.007	0.006	0.006	0.0001	0.145	0.12
10/29/2002	5:08:20 PM	25.752	23.61	25.52	22.866	23.763	50.935	53.627	15.502	35.989	-1.289	-6.566	46.221	0.043	0.001	0	74.87	1.24776	52.2	11.3	43.5	2.997	0.006	0.006	0.0001	0.145	0.12
10/29/2002	5:09:20 PM	25.765	23.614	25.694	22.789	23.772	51.226	53.832	15.672	36.403	-1.286	-6.56	46.815	0.042	0.001	0	75.87	1.26444	52.4	11.2	43.8	3.021	0.006	0.006	0.0001	0.141	0.12
10/29/2002	5:10:20 PM	25.769	23.617	25.702	22.817	23.785	51.628	54.028	15.805	36.892	-1.289	-6.55	46.477	0.043	0.001	0	76.87	1.28111	52.6	11.4	44.3	3.052	0.006	0.006	0.0001	0.142	0.12
10/29/2002	5:11:20 PM	25.769	23.622	25.672	22.908	23.79	51.271	53.886	15.576	36.477	-1.286	-6.55	46.387	0.043	0.001	0	77.87	1.29776	52.4	11.4	43.9	3.026	0.006	0.006	0.0001	0.143	0.12
10/29/2002	5:12:20 PM	25.757	23.611	25.691	22.891	23.809	51.366	54.086	15.634	36.413	-1.289	-6.55	46.716	0.043	0.001	0	78.87	1.31444	52.6	11.4	43.9	3.026	0.006	0.006	0.0001	0.144	0.12
10/29/2002	5:13:20 PM	25.748	23.602	25.487	22.832	23.806	51.662	54.125	15.803	36.739	-1.289	-6.553	46.112	0.042	0.001	0	79.87	1.33111	52.7	11.3	44.2	3.047	0.006	0.006	0.0001	0.140	0.12
10/29/2002	5:14:20 PM	25.767	23.616	25.711	22.755	23.799	51.621	54.2	15.801	36.532	-1.289	-6.553	46.57	0.043	0.001	0	80.87	1.34776	52.7	11.4	44.1	3.039	0.006	0.006	0.0001	0.143	0.12
10/29/2002	5:15:20 PM	25.772	23.626	25.734	22.739	23.787	51.737	54.541	15.752	36.887	-1.292	-6.566	46.712	0.043	0.001	0	81.87	1.36444	53.1	11.4	44.3	3.045	0.006	0.006	0.0001	0.142	0.12
10/29/2002	5:16:20 PM	25.778	23.647	25.686	22.716	23.804	50.95	53.59	15.437	36.278	-1.286	-6.55	46.23	0.043	0.001	0	82.87	1.38111	52.1	11.3	43.6	3.007	0.006	0.006	0.0001	0.144	0.12
10/29/2002	5:17:20 PM	25.805	23.654	25.628	22.723	23.832	51.404	54.107	15.717	36.36	-1.289	-6.55	46.5	0.043	0.001	0	83.87	1.39776	52.6	11.4	43.9	3.026	0.006	0.006	0.0001	0.144	0.12
10/29/2002	5:18:20 PM	25.801	23.65	25.74	22.72	23.803	53.793	56.577	16.353	38.082	-1.286	-6.541	48.032	0.044	0.001	0	84.87	1.41444	56.1	11.8	45.9	3.167	0.007	0.006	0.0001	0.140	0.12
10/29/2002	5:19:20 PM	25.803	23.642	25.797	22.726	23.805	52.648	55.152	16.074	37.427	-1.289	-6.544	46.979	0.043	0.001	0	85.87	1.43111	53.7	11.5	45.0	3.106	0.006	0.006	0.0001	0.139	0.12
10/29/2002	5:20:20 PM	25.786	23.629	25.734	22.739	23.787	51.52	54.276	15.786	36.488	-1.289	-6.55	46.624	0.043	0.001	0	86.87	1.44776	52.8	11.5	44.0	3.034	0.006	0.006	0.0001	0.143	0.12
10/29/2002	5:21:20 PM	25.8	23.634	25.684	22.748	23.762	53.806	56.368	16.379	38.383	-1.289	-6.541	47.977	0.044	0.001	0	87.87	1.46444	54.9	11.8	46.1	3.178	0.007	0.006	0.0001	0.140	0.12
10/29/2002	5:22:20 PM	25.809	23.632	25.622	22.742	23.77	54.065	56.776	16.542	38.321	-1.286	-6.539	48.128	0.045	0.001	0	88.87	1.48111	56.3	11.8	46.2	3.185	0.007	0.007	0.0001	0.143	0.12
10/29/2002	5:23:20 PM	25.827	23.631	25.651	22.726	23.779	54.698	57.257	16.711	38.905	-1.289	-6.539	48.195	0.045	0.001	0	89.87	1.49776	56.8	11.8	46.8	3.226	0.007	0.007	0.0001	0.140	0.12
10/29/2002	5:24:20 PM	25.768	23.622	25.627	22.737	23.775	54.898	57.675	16.822	39.629	-1.286	-6.539	48.728	0.045	0.001	0	90.87	1.51444	56.2	11.9	46.3	3.231	0.007	0.007	0.0001	0.140	0.12
10/29/2002	5:25:20 PM	25.782	23.6	25.745	22.755	23.748	55.478	58.207	16.959	39.271	-1.286	-6.539	48.547	0.046	0.001	0	91.87	1.53111	56.7	11.9	47.4	3.265	0.007	0.007	0.0001	0.142	0.12
10/29/2002	5:26:20 PM	25.817	23.611	25.691	22.776	23.744	55.577	58.364	17.017	39.253	-1.289	-6.536	46.408	0.046	0.001	0	92.87	1.54776	56.9	11.4	47.4	3.269	0.007	0.007	0.0001	0.142	0.12
10/29/2002	5:27:20 PM	25.801	23.63	25.655	22.815	23.773	55.638	58.526	16.979	39.347	-1.286	-6.53	48.623	0.046	0.001	0	93.87	1.56444	57.1	11.9	47.5	3.274	0.007	0.007	0.0001	0.142	0.12
10/29/2002	5:28:20 PM	25.767	23.641	25.671	22.841	23.764	56.261	59.099	17.268	39.732	-1.289	-6.53	49.221	0.046	0.001	0	94.87	1.58111	57.6	12.1	48.0	3.309	0.007	0.007	0.0001	0.139	0.12
10/29/2002	5:29:20 PM	25.778	23.643	25.682	22.817	23.755	57.368	60.139	17.507	40.722	-1.286	-6.534	49.793	0.046	0.001	0	95.87	1.59776	58.7	12.2	48.0	3.381	0.007	0.007	0.0001	0.142	0.12
10/29/2002	5:30:20 PM	25.819	23.643	25.678	22.773	23.751	57.574	60.439	17.655	40.626	-1.286	-6.527	49.676	0.047	0.001	0	96.87	1.61444	59.0	12.2	49.1	3.365	0.007	0.007	0.0001	0.139	0.12
10/29/2002	5:31:20 PM	25.836	23.635	25.814	22.729	23.747	5																				

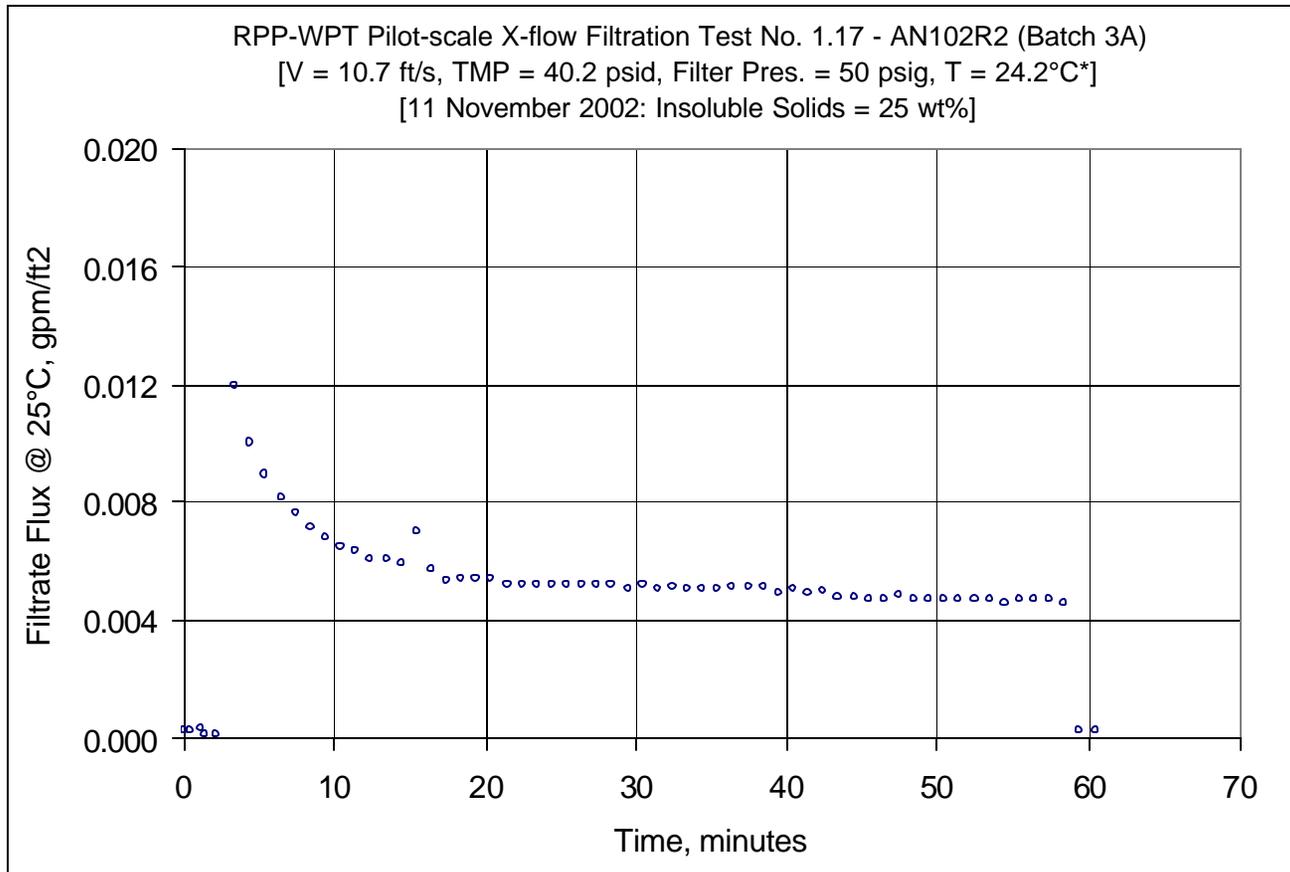


Figure E27: Steady state test run 1.17 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%



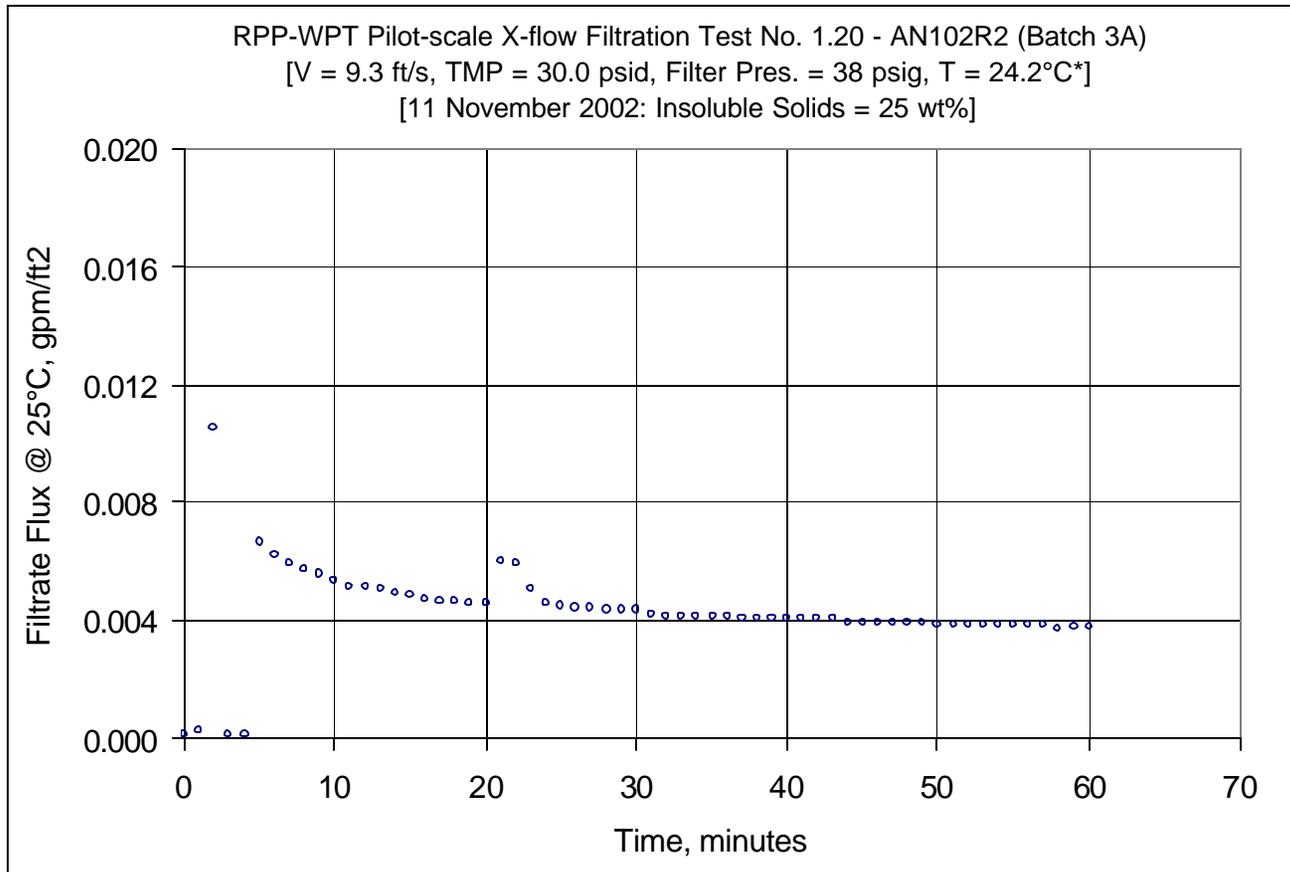


Figure E29: Steady state test run 1.20 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%



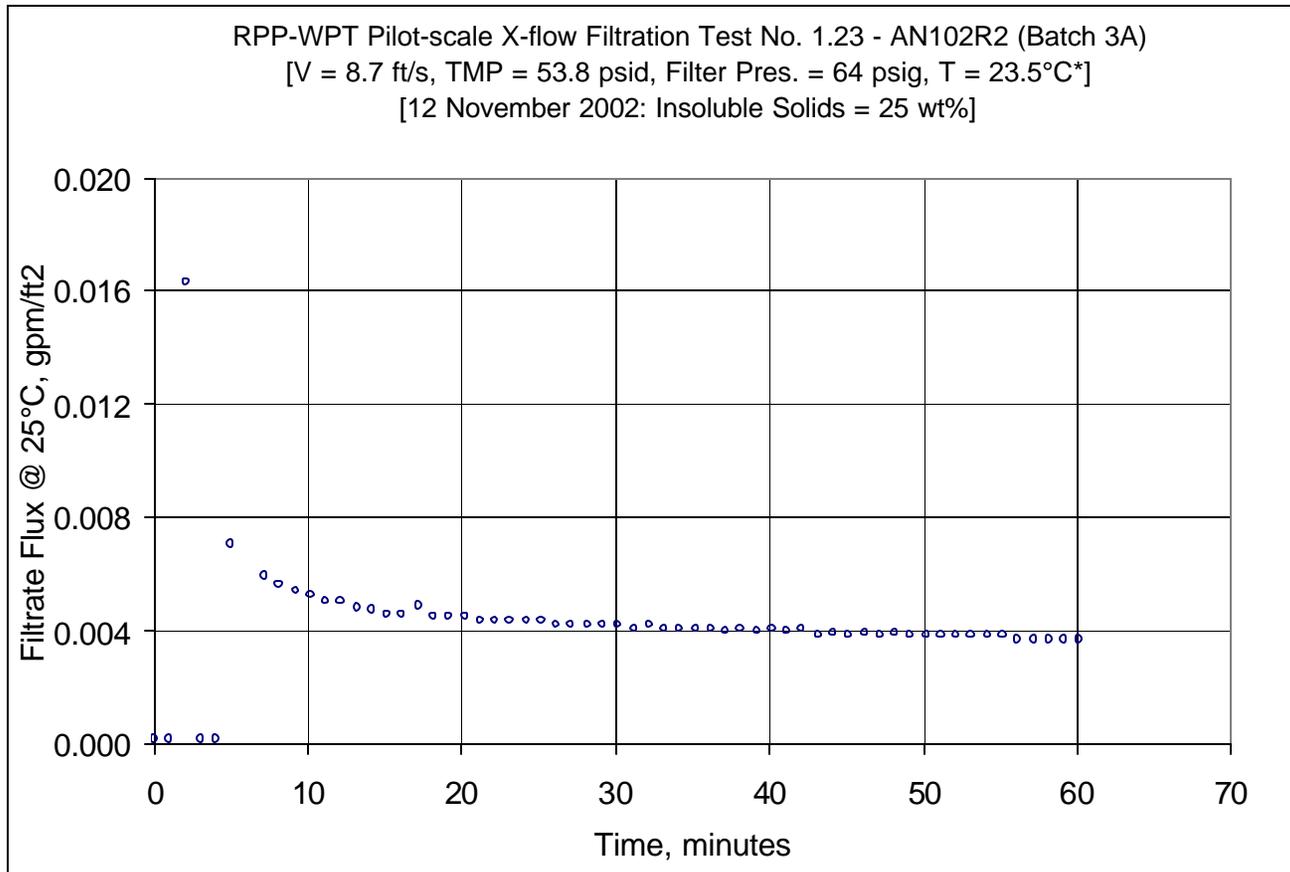


Figure E31: Steady state test run 1.23 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%



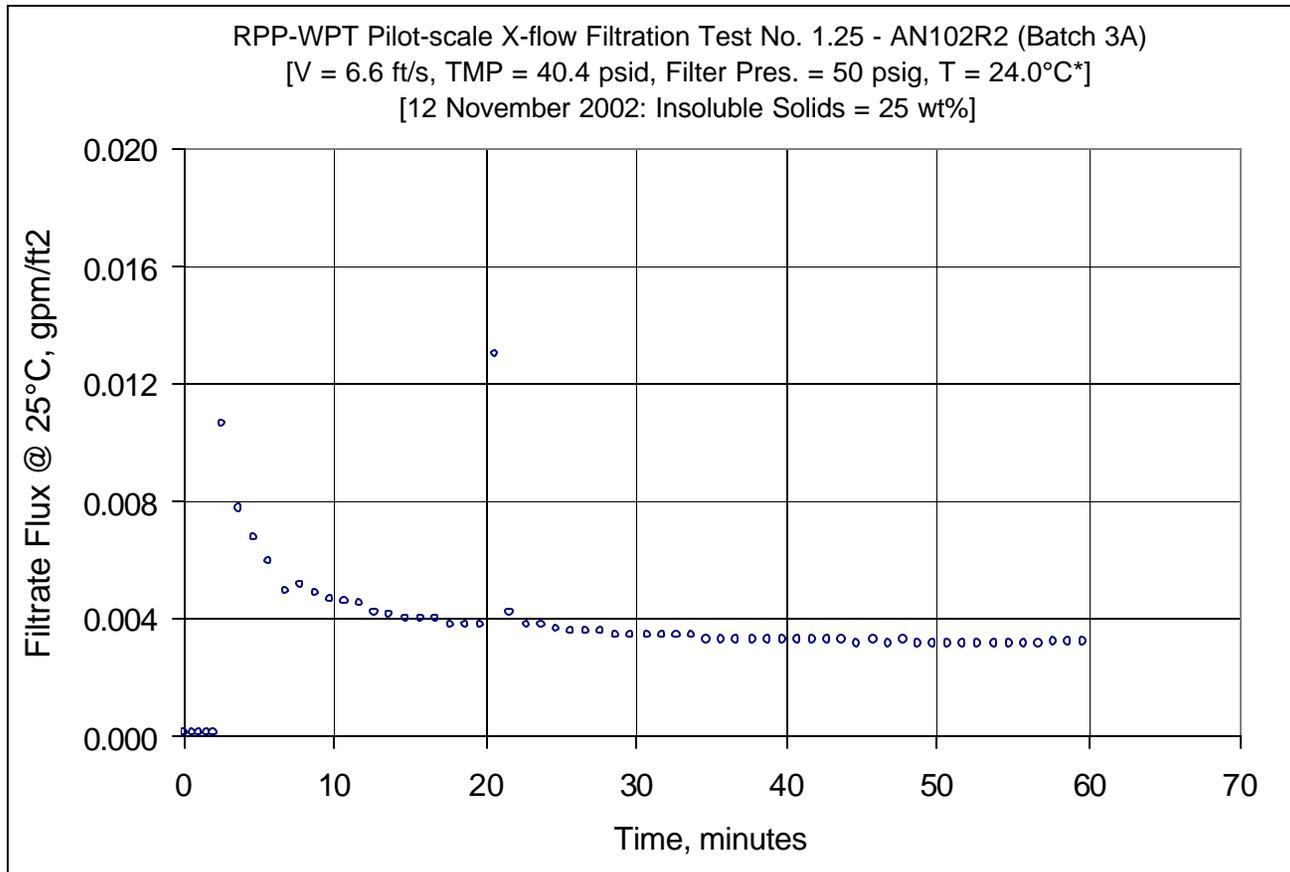


Figure E33: Steady state test run 1.25 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%



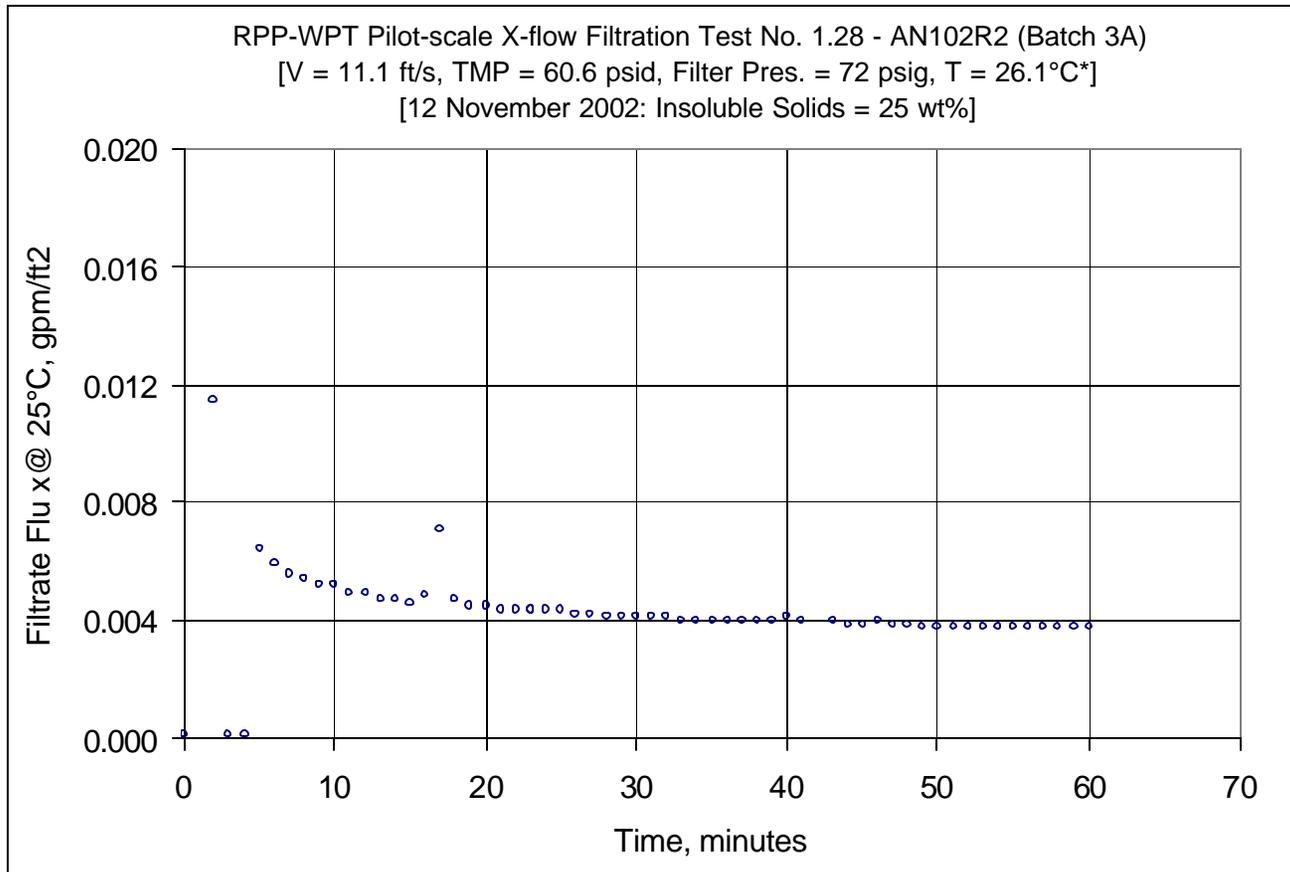


Figure E35: Steady state test run 1.28 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%



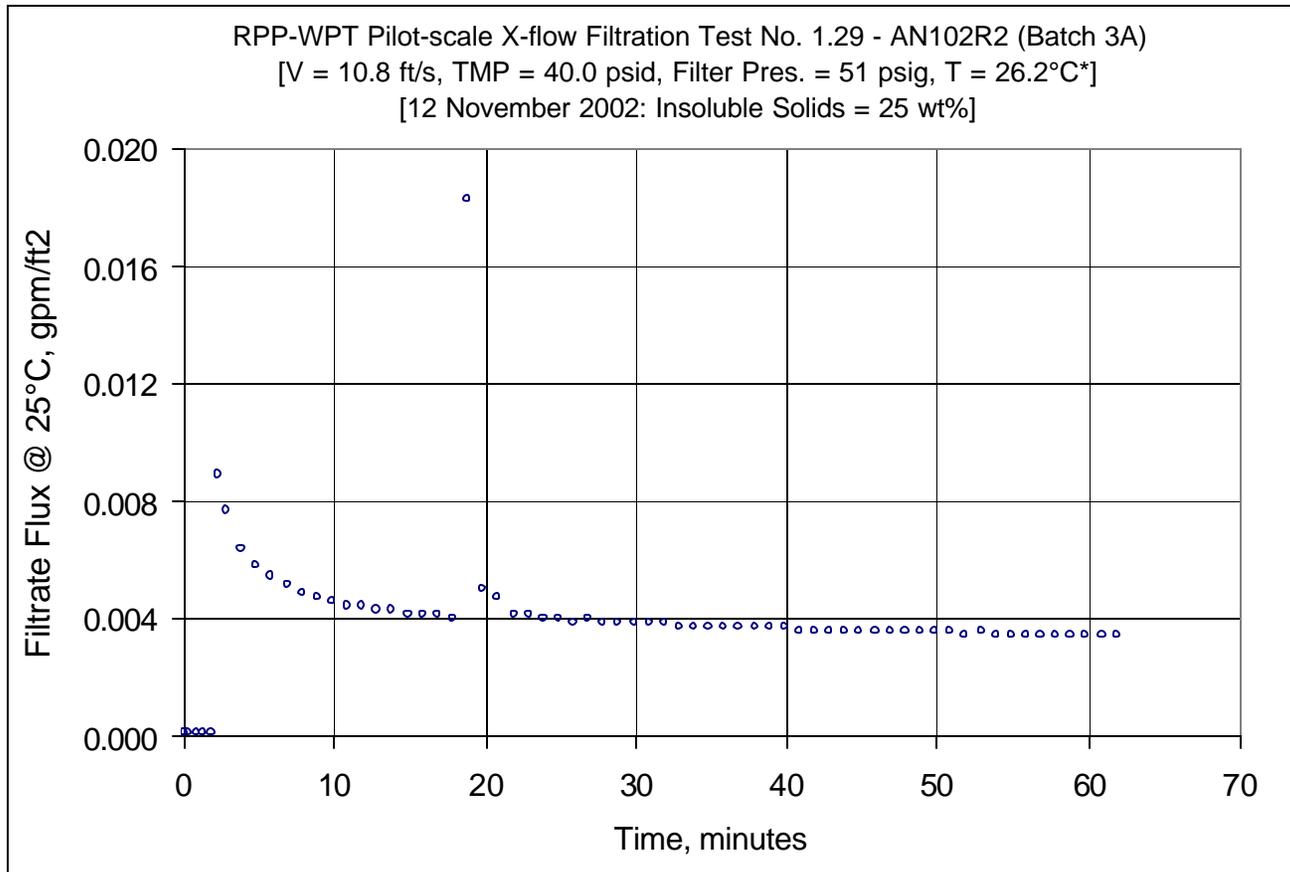


Figure E37: Steady state test run 1.29 of AN-102R2, batch 3A, insoluble solids concentration of 25 wt%

DATE	TIME	Temperature Measurements					Pressure Measurements					Flow Measurements					Calculated From Raw Data												
		Filtrate deg C	Cleaning deg C	Slurry deg C	H2 Amb deg C	Lo Amb deg C	BotTMP psid	Filtrate psig	Filtrate psid	TopTMP psid	Filtrate psig	Filtrate psid	PulsPos	Slurry gpm	Filtrate gpm	H2 Filtrate gpm	Backpulse gpm	Temp psi	Temp psi	Temp psi	Temp psi								
Zeros																													
11/12/2002	8:11:47 AM	21.54	21.663	20.804	21.275	21.296	-0.129	0.016	-0.042	0.049	-0.377	0.334	-0.211	0.001	0.001	0.001													
11/12/2002	8:12:06 AM	21.54	21.663	20.804	21.275	21.296	-0.129	0.016	-0.042	0.049	-0.377	0.334	-0.211	0.001	0.001	0.001													
11/12/2002	8:12:06 AM	21.541	21.644	20.79	21.271	21.267	-0.131	0.015	-0.043	0.049	-0.389	0.331	-0.213	0.001	0.001	0.001													
11/12/2002	8:12:07 AM	21.541	21.644	20.79	21.271	21.257	-0.129	0.016	-0.043	0.049	-0.377	0.331	-0.213	0.001	0.001	0.002													
11/12/2002	8:12:08 AM	21.542	21.65	20.791	21.271	21.263	-0.129	0.015	-0.042	0.049	-0.377	0.328	-0.213	0.001	0.001	0.002													
11/12/2002	8:12:09 AM	21.531	21.644	20.795	21.271	21.267	-0.129	0.015	-0.042	0.049	-0.418	0.334	-0.215	0.001	0.001	0.001													
11/12/2002	8:12:10 AM	21.541	21.644	20.795	21.271	21.257	-0.129	0.016	-0.042	0.049	-0.38	0.331	-0.211	0.001	0.001	0.002													
11/12/2002	8:12:11 AM	21.536	21.644	20.79	21.271	21.247	-0.129	0.015	-0.042	0.051	-0.377	0.334	-0.215	0.001	0.001	0.001													
Data - Per Minute																													
11/12/2002	3:30:50 PM	25.897	20.378	26.815	21.97	21.448	44.219	51.904	15.495	29.991	1.498	92.506	46.539	0.001	0.001	0.001	0	0	50.4	11.4	36.8	2.538	0.000	0.000	0.000	0.004	0.00		
11/12/2002	3:31:07 PM	25.897	20.378	26.815	21.97	21.448	44.219	51.904	15.495	29.991	1.498	92.506	46.539	0.001	0.001	0.001	0	0	0.26	0.00472	50.4	11.4	36.8	2.538	0.000	0.000	0.000	0.004	0.00
11/12/2002	3:31:37 PM	24.071	20.405	26.767	22.158	21.496	3.912	50.859	12.201	-7.306	41.192	54.221	48.691	0.001	0.001	0.001	0.001	0	0.78	0.01306	49.4	11.9	-1.7	-0.117	0.000	0.000	0.000	-0.064	-0.07
11/12/2002	3:32:07 PM	25.866	20.417	26.769	22.2	21.533	22.692	50.834	12.65	10.932	22.228	0.657	48.078	0.245	0.001	0	0	0	1.26	0.02139	49.2	11.8	16.8	1.959	0.000	0.000	0.000	0.006	0.01
11/12/2002	3:32:37 PM	25.476	20.428	26.72	22.256	21.559	42.707	50.543	13.132	30.498	1.944	0.6	47.992	0.081	0.001	0	0	0	1.78	0.02972	49.1	11.8	36.6	2.524	0.000	0.000	0.000	0.004	0.00
11/12/2002	3:33:07 PM	25.368	20.445	26.791	22.268	21.591	43.088	50.928	13.48	30.5	1.834	0.612	47.839	0.063	0.001	0	0	0	2.28	0.03806	49.5	11.7	36.8	2.537	0.009	0.009	0.002	0.243	0.21
11/12/2002	3:33:39 PM	25.389	20.456	26.708	22.39	21.637	43.138	51.178	13.718	30.22	1.718	0.65	47.55	0.054	0.001	0	0	0	2.82	0.04694	49.7	11.7	36.7	2.529	0.008	0.008	0.002	0.209	0.18
11/12/2002	3:34:39 PM	25.512	20.484	26.705	22.423	21.691	43.029	50.92	14.051	29.78	1.675	0.636	47.799	0.045	0.001	0	0	0	3.82	0.06361	49.3	11.7	36.4	2.510	0.007	0.005	0.002	0.175	0.16
11/12/2002	3:35:39 PM	25.634	20.516	26.583	22.626	21.743	43.586	51.403	14.266	30.107	1.654	0.668	47.084	0.041	0.001	0	0	0	4.82	0.08028	49.9	11.5	36.8	2.540	0.006	0.005	0.002	0.159	0.14
11/12/2002	3:36:39 PM	25.722	20.524	26.47	22.623	21.796	44.145	51.997	14.495	30.379	1.649	0.687	46.415	0.038	0.001	0	0	0	5.82	0.09694	50.5	11.4	37.3	2.569	0.006	0.005	0.001	0.146	0.12
11/12/2002	3:37:39 PM	25.798	20.551	26.322	22.68	21.848	44.236	51.948	14.612	30.564	1.64	0.682	46.25	0.036	0.001	0	0	0	6.82	0.11361	50.5	11.3	37.4	2.579	0.005	0.005	0.001	0.138	0.12
11/12/2002	3:38:39 PM	25.874	20.58	26.163	22.693	21.914	44.167	51.948	14.712	30.749	1.637	0.686	45.1	0.033	0.001	0	0	0	7.82	0.13028	50.4	11.2	37.3	2.570	0.005	0.005	0.001	0.130	0.10
11/12/2002	3:39:39 PM	25.883	20.61	26.261	22.7	21.972	44.644	52.27	14.798	30.453	1.64	0.705	45.941	0.033	0.001	0	0	0	8.82	0.14694	50.8	11.3	37.5	2.583	0.005	0.005	0.001	0.127	0.11
11/12/2002	3:40:39 PM	25.885	20.638	26.259	22.712	22.03	44.054	51.726	14.833	30.103	1.64	0.716	45.766	0.032	0.001	0	0	0	9.82	0.16361	50.3	11.2	37.1	2.566	0.005	0.005	0.001	0.124	0.11
11/12/2002	3:41:39 PM	25.902	20.665	26.2	22.744	22.072	44.211	51.877	14.986	30.056	1.64	0.728	45.534	0.031	0.001	0	0	0	10.82	0.18028	50.4	11.2	37.1	2.560	0.005	0.005	0.001	0.120	0.10
11/12/2002	3:42:39 PM	25.938	20.682	26.13	22.766	22.124	44.059	51.683	15.129	30.044	1.64	0.741	45.323	0.029	0.001	0	0	0	11.82	0.19694	50.4	11.2	37.2	2.563	0.005	0.005	0.001	0.117	0.10
11/12/2002	3:43:39 PM	25.915	20.714	26.173	22.757	22.171	44.665	52.361	15.071	30.4	1.637	0.745	45.264	0.03	0.001	0	0	0	12.82	0.21361	50.9	11.1	37.5	2.584	0.004	0.004	0.001	0.115	0.10
11/12/2002	3:44:39 PM	25.916	20.725	26.19	22.753	22.217	44.743	52.57	15.169	30.367	1.637	0.754	44.79	0.03	0.001	0	0	0	13.82	0.23028	51.1	11.0	37.6	2.589	0.004	0.004	0.001	0.115	0.10
11/12/2002	3:45:39 PM	25.923	20.772	26.226	22.8	22.269	44.617	52.206	15.192	30.17	1.64	0.771	44.739	0.029	0.001	0	0	0	14.82	0.24694	50.8	11.0	37.3	2.575	0.004	0.004	0.001	0.112	0.10
11/12/2002	3:46:39 PM	25.925	20.785	26.153	22.817	22.324	44.426	52.089	15.3	30.158	1.64	0.784	44.582	0.028	0.001	0	0	0	15.82	0.26361	50.7	10.9	37.4	2.577	0.004	0.004	0.001	0.110	0.09
11/12/2002	3:47:39 PM	25.901	20.816	26.11	22.728	22.323	45.039	52.73	15.383	30.514	1.634	0.779	44.116	0.029	0.001	0	0	0	16.82	0.28028	51.3	10.8	37.6	2.605	0.004	0.004	0.001	0.111	0.09
11/12/2002	3:48:39 PM	25.908	20.848	26.192	22.781	22.37	44.609	52.305	15.429	30.019	1.62	0.8	44.049	0.028	0.001	0	0	0	17.82	0.29694	50.8	10.8	37.3	2.573	0.004	0.004	0.001	0.108	0.09
11/12/2002	3:49:39 PM	25.891	20.876	26.229	22.858	22.423	47.647	52.818	15.537	33.008	-0.967	-0.089	43.907	0.127	0.001	0	0	0	18.82	0.31361	51.3	10.8	40.3	2.780	0.019	0.018	0.005	0.454	0.39
11/12/2002	3:50:39 PM	25.817	20.903	26.163	22.923	22.465	47.637	52.874	15.567	33.008	-0.967	-0.089	43.907	0.127	0.001	0	0	0	19.82	0.33028	51.6	10.7	40.2	2.773	0.020	0.019	0.005	0.454	0.39
11/12/2002	3:51:39 PM	25.83	20.915	26.188	22.853	22.498	47.941	52.794	15.602	33.167	-1.291	-0.691	44.123	0.033	0.001	0	0	0	20.82	0.34694	51.3	10.8	40.6	2.796	0.005	0.005	0.001	0.117	0.10
11/12/2002	3:52:39 PM	25.862	20.953	26.176	22.905	22.536	48.198	52.988	15.626	33.337	-1.288	-0.691	43.705	0.029	0.001	0	0	0	21.82	0.36361	51.5	10.7	40.8	2.811	0.004	0.004	0.001	0.103	0.09
11/12/2002	3:53:39 PM	25.874	20.975	26.218	22.947	22.562	47.989	52.655	15.391	33.43	-1.288	-0.697	43.909	0.029	0.001	0	0	0	22.82	0.38028	51.2	10.8	40.7	2.807	0.004	0.004	0.001	0.103	0.09
11/12/2002	3:54:39 PM	25.881	20.989	26.2	22.923	22.585	48.289	52.899	15.415	33.603	-1.288	-0.697	43.909	0.029	0.001	0	0	0	23.82	0.39694	51.1	10.7	40.9	2.821	0.004	0.004	0.001	0.099	0.08
11/12/2002	3:55:39 PM	25.91	21.026	26.243	22.973	22.633	47.751	52.577	15.446	32.996	-1.288	-0.7	43.921	0.029	0.001	0	0	0	24.82	0.41361	51.1	10.6	40.4	2.784	0.004	0.004	0.001	0.100	0.08
11/12/2002	3:56:39 PM	25.911	21.047	26.174	22.954	22.645	48.045	52.829	15.488	33.264	-1.288	-0.712	43.722	0.027	0.001	0	0	0	25.82	0.43028	51.4	10.7	40.7	2.804	0.004	0.004	0.001	0.096	0.08
11/12/2002	3:57:39 PM	25.933	21.07	26.152	22.967	22.677	48.299	53.23	15.546	33.552	-1.285	-0.689	43.523	0.028	0.001	0	0	0	26.82	0.44694	51.8	10.7	40.9	2.822	0.004	0.004	0.001	0.099	0.08
11/12/2002	3:58:39 PM	25.941	21.087	26.174	22.984	22.705	48.168	52.943	15.522	33.653	-1.285	-0.697	43.705	0.027	0.001	0	0	0	27.82	0.46361	51.5	10.7	40.9	2.821	0.004	0.004	0.001	0.095	0.08

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Individual Entries – Raw Data

Temperature	Filtrate – from the filtrate loop at the exit of the filter bundle Cleaning – from the cleaning loop (this loop was not used, except for tests Clean 1 & 2) Slurry – from the slurry loop in the slurry reservoir Hi Amb. – outside ambient temperature at the top of the test rig Lo Amb. – inside ambient temperature at the bottom of the test rig
Pressure	BotTMP – differential pressure across the filter tube at the bottom of the vertical tube Filter – gauge pressure of the slurry at the entrance of the filter tube bundle Filter dP – differential pressure of the slurry along the height of the vertical 90-inch tube TopTMP – differential pressure across the filter tube at the top the vertical 90-inch tube Filtrate – gauge pressure of the filtrate at the exit of the filter tube housing Pulsepot – gauge pressure of the filtrate at the bottom of the pulsepot
Flow	Slurry – rate of slurry just before entering the seven-filter-tube bundle Filtrate – rate of slurry filtrate under normal flow (max. is 1.2 gpm) Hi Filtrate – rate of any liquid with has a high flowrate (water, acid, etc.) (max. 5 gpm) Backpulse – rate of filtrate in opposite direction from normal flow, i.e., backpulse

Individual Entries – Calculated Data

Time – Minutes after start of test, including the backpulse (based on raw data TIME column)  
Press. – Internal filter pressure of slurry at the filter bundle entrance (based on raw data P1 column and corrected for a 40.9-inch water column that exists from the transducer to the point where P1 is measured.)  
Vel. – Slurry velocity in filter tube (based on raw data Q1 column and i.d. of the tubes of 0.488 inches)  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in psi.  
TMP – Filter transmembrane pressure (based on average of raw data columns dP2 and dP3) in bar.  
Filtrate Flux – Filtrate flow rate (raw data columns Q2/Q3) divided by inside filter surface area (6.87 ft<sup>2</sup>)  
Filtrate Flux @ 25°C – Same as Filtrate flux, but correct for temperature with the following multiplier:

$$T(\text{corrected}) = T \times \text{Exp}[2500/((1/273+T))-(1/298)] \text{ as per Test Spec 24590-WTP-TSP-RT-01-029, Rev. 0}$$

Permiability – Filtrate flow rate per TMP (based on calculated columns Filtrate Flux @ 25°C and TMP)  
Permiability x 1000 – Same as the above Permiability, but increase by 1000 to facilitate graphing  
Permiability – Same as Permiability but in metric units, meter/day/bar

Statistics

At the bottom of the last individual entry there are six rows with some data statistics to better understand the data and their fluctuations. The columns are self explained with titles of Averages, Maximum, Median, and Minimum. The next row 2 x Std Dev, is two times the population standard deviation based on the number of data points used, which is the last row. The Number of Points used generally do not included the points taken during the backpulse sequence of each test. This is explained below.

Raw Data Table Layout

The raw data is generally made up of three sections:

Zeros – These eight rows include approximately 15 to 20 seconds of data taken with the pressure transducers placed in the “zero” mode to determine if any zero drift occurred from one test to the next.

Data-Per Minute – On most of the tables the first six rows of these data are contained in a box which indicate data taken during the backpulse. This is were the filtrate flow is reversed temporarily to knock the filtrate cake of the filter surface. During these first few minutes the filtrate flow is stopped, then reversed, then stopped again, then it is finally returned to normal operation. The data during the backpulse operation were taken with a separate log, therefore those data are marked with a box to note this fact. Most or all of those data points are not counted in the statistics at the bottom of the table. The tables of some of the later tests do not show the boxed data because separate logs of data were not taken, however since a backpulse for each run still occurred only those data were not included in the statistics at the bottom of the page.

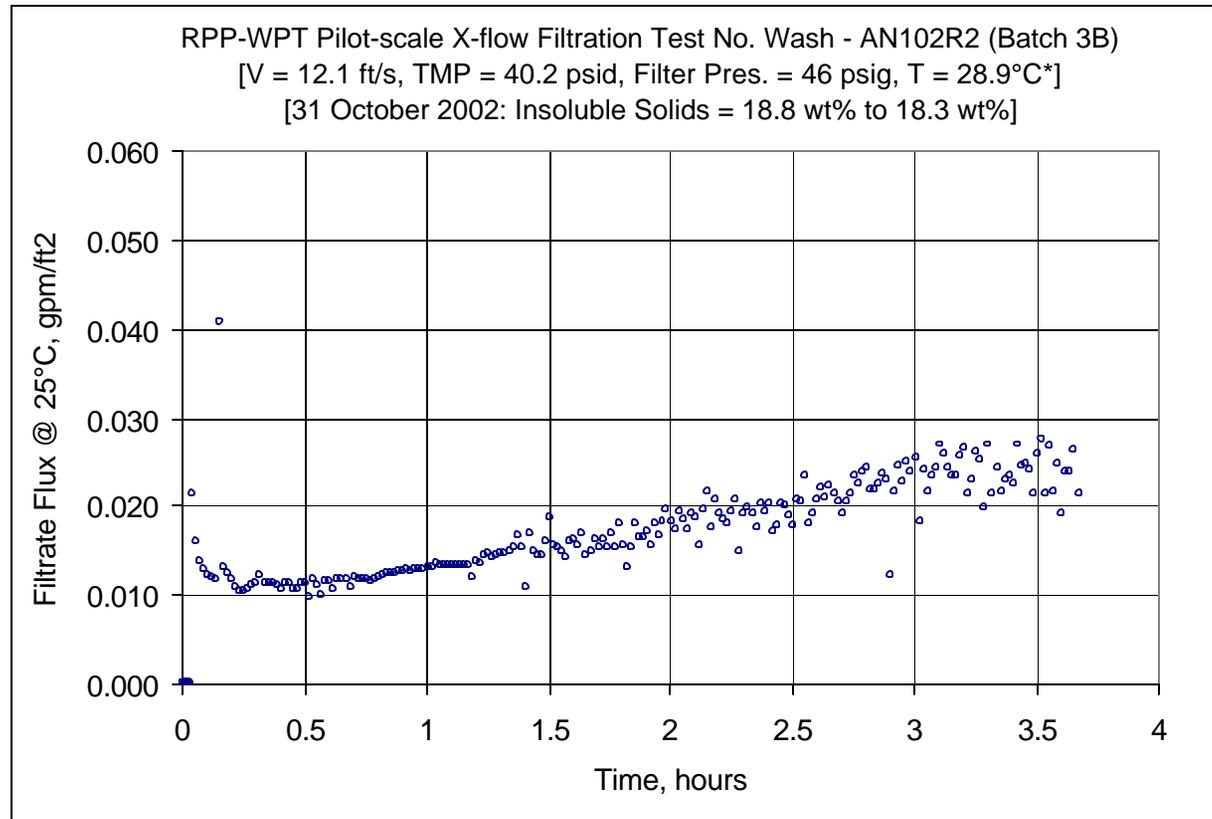


Figure F1. Complete washing cycle – 21 mini-batches of inhibited/filtered water with a Volume = Total Slurry Volume x (21/18)/21 were added and removed. At an average filtrate flux of 0.0175 gpm/ft<sup>2</sup> the mini-batch additions occurred approximately, on the average, every 10 minutes



10/31/2002	8:37-59 AM	25.866	20.675	27.762	22.054	21.777	45.671	47.216	12.433	34.259	-1.285	-6.404	49.737	0.086	0.001	0	47.27	0.78778	45.7	12.2	40.0	2.755	0.013	0.012	0.0003	0.297	0.25
10/31/2002	8:38-59 AM	26.025	20.699	27.905	21.973	21.809	45.41	47.208	12.368	33.89	-1.288	-6.386	49.727	0.087	0.001	0	48.27	0.80444	45.7	12.2	39.7	2.734	0.013	0.012	0.0003	0.302	0.26
10/31/2002	8:39-59 AM	26.154	20.717	27.744	22.107	21.837	45.361	47.303	12.44	33.645	-1.288	-6.395	50.331	0.089	0.001	0	49.27	0.82111	45.8	12.3	39.5	2.724	0.013	0.012	0.0003	0.311	0.26
10/31/2002	8:40-59 AM	26.258	20.737	27.763	22.071	21.882	44.959	46.898	12.387	33.147	-1.285	-6.386	50.314	0.09	0.001	0	50.27	0.83778	45.4	12.3	39.1	2.693	0.013	0.012	0.0003	0.318	0.27
10/31/2002	8:41-59 AM	26.341	20.76	28.016	22.084	21.931	45.137	46.964	12.394	33.651	-1.285	-6.357	50.448	0.091	0.001	0	51.27	0.85444	45.5	12.4	39.4	2.716	0.014	0.012	0.0003	0.317	0.27
10/31/2002	8:42-59 AM	26.44	20.779	28.07	22.209	21.975	45.381	47.251	11.803	34.427	-1.288	-6.369	48.983	0.092	0.001	0	52.27	0.87111	45.8	12.0	39.9	2.751	0.014	0.013	0.0003	0.316	0.27
10/31/2002	8:43-59 AM	26.534	20.803	28.088	22.298	22.014	45.827	47.81	11.886	34.762	-1.285	-6.346	48.917	0.093	0.001	0	53.27	0.88778	46.3	12.0	40.3	2.778	0.014	0.013	0.0003	0.316	0.27
10/31/2002	8:44-59 AM	26.607	20.827	28.291	22.312	22.052	45.462	47.539	11.693	34.47	-1.285	-6.363	47.852	0.094	0.001	0	54.27	0.90444	46.1	11.7	40.0	2.756	0.014	0.013	0.0003	0.320	0.27
10/31/2002	8:45-59 AM	26.691	20.851	28.31	22.437	22.102	45.845	47.798	11.763	34.875	-1.285	-6.352	48.781	0.095	0.001	0	55.27	0.92111	46.3	12.0	40.4	2.783	0.014	0.013	0.0003	0.320	0.27
10/31/2002	8:46-59 AM	26.775	20.88	28.284	22.471	22.161	45.559	47.543	11.551	34.84	-1.285	-6.349	48.095	0.094	0.001	0	56.27	0.93778	46.1	11.8	40.2	2.772	0.014	0.013	0.0003	0.318	0.27
10/31/2002	8:47-59 AM	26.863	20.904	28.472	22.49	22.185	45.681	47.793	11.638	34.775	-1.285	-6.343	48.594	0.095	0.001	0	57.27	0.95444	46.3	11.9	40.2	2.774	0.014	0.013	0.0003	0.320	0.27
10/31/2002	8:48-59 AM	26.937	20.923	28.486	22.523	22.224	46.054	48.509	11.727	34.944	-1.288	-6.346	50.323	0.095	0.001	0	58.27	0.97111	47.0	12.3	40.5	2.792	0.014	0.013	0.0003	0.317	0.27
10/31/2002	8:49-59 AM	26.98	20.946	28.3	22.456	22.242	45.812	48.106	11.623	34.899	-1.285	-6.34	48.532	0.095	0.001	0	59.27	0.98778	46.6	11.9	40.4	2.782	0.014	0.013	0.0003	0.320	0.27
10/31/2002	8:50-59 AM	27.064	20.965	28.189	22.485	22.286	45.539	47.692	11.593	34.903	-1.288	-6.337	49.234	0.096	0.001	0	60.27	1.00444	46.2	12.1	40.2	2.770	0.014	0.013	0.0003	0.326	0.28
10/31/2002	8:51-59 AM	27.122	21.009	28.182	22.554	22.345	45.325	47.614	11.593	34.439	-1.282	-6.323	50.545	0.097	0.001	0	61.27	1.02111	46.1	12.4	39.9	2.750	0.014	0.013	0.0003	0.323	0.28
10/31/2002	8:52-59 AM	27.105	21.012	28.111	22.607	22.368	45.12	47.614	11.57	34.197	-1.288	-6.317	49.198	0.099	0.001	0	62.27	1.03778	46.1	12.1	39.7	2.734	0.015	0.014	0.0003	0.341	0.29
10/31/2002	8:53-59 AM	27.109	21.046	28.309	22.596	22.417	45.087	47.45	11.536	34.271	-1.285	-6.308	48.995	0.099	0.001	0	63.27	1.05444	46.0	12.0	39.7	2.736	0.015	0.013	0.0003	0.339	0.29
10/31/2002	8:54-59 AM	27.133	21.07	28.407	22.665	22.451	45.176	47.651	11.654	34.185	-1.285	-6.308	49.243	0.099	0.001	0	64.27	1.07111	46.2	12.1	39.7	2.736	0.015	0.013	0.0003	0.338	0.29
10/31/2002	8:55-59 AM	27.172	21.084	28.341	22.719	22.485	45.209	47.673	11.554	34.42	-1.285	-6.288	50.499	0.098	0.001	0	65.27	1.08778	46.2	12.4	39.8	2.745	0.015	0.013	0.0003	0.334	0.28
10/31/2002	8:56-59 AM	27.206	21.118	28.48	22.628	22.514	45.106	47.601	11.527	34.246	-1.288	-6.285	49.117	0.099	0.001	0	66.27	1.10444	46.1	12.0	39.7	2.736	0.015	0.013	0.0003	0.338	0.29
10/31/2002	8:57-59 AM	27.249	21.142	28.588	22.646	22.538	45.255	47.862	11.597	34.345	-1.285	-6.308	48.683	0.099	0.001	0	67.27	1.12111	46.4	11.9	39.8	2.744	0.015	0.013	0.0003	0.336	0.29
10/31/2002	8:58-59 AM	27.277	21.16	28.471	22.694	22.561	44.867	47.543	11.512	34.068	-1.285	-6.276	48.311	0.099	0.001	0	68.27	1.13778	46.1	11.8	39.5	2.721	0.015	0.013	0.0003	0.340	0.29
10/31/2002	8:59-59 AM	27.305	21.178	28.544	22.677	22.604	45.199	47.87	11.6	34.349	-1.288	-6.294	48.737	0.099	0.001	0	69.27	1.15444	46.4	11.9	39.8	2.742	0.015	0.013	0.0003	0.338	0.29
10/31/2002	9:00-59 AM	27.372	21.206	28.507	22.645	22.647	44.888	47.63	11.429	34.242	-1.288	-6.286	48.733	0.099	0.001	0	70.27	1.17111	46.2	11.9	39.6	2.728	0.015	0.013	0.0003	0.336	0.29
10/31/2002	9:01-59 AM	27.416	21.245	28.271	22.795	22.691	44.787	47.614	11.449	33.978	-1.285	-6.172	48.311	0.099	0.001	0	71.27	1.18778	46.1	11.8	39.4	2.715	0.013	0.012	0.0003	0.308	0.26
10/31/2002	9:02-59 AM	27.414	21.273	28.195	22.833	22.729	44.799	47.642	11.487	34.011	-1.288	-6.268	50.095	0.102	0.001	0	72.27	1.20444	46.2	12.3	39.4	2.717	0.015	0.014	0.0004	0.353	0.30
10/31/2002	9:03-59 AM	27.417	21.286	28.337	22.816	22.758	45.423	48.24	11.521	34.623	-1.285	-6.187	49.626	0.1	0.001	0	73.27	1.22111	46.8	12.2	40.0	2.759	0.015	0.014	0.0003	0.339	0.29
10/31/2002	9:04-59 AM	27.41	21.315	28.306	22.924	22.796	45.524	48.408	11.589	34.557	-1.288	-6.236	49.786	0.106	0.001	0	74.27	1.23778	46.9	12.2	40.0	2.761	0.016	0.014	0.0004	0.360	0.31
10/31/2002	9:05-59 AM	27.403	21.338	28.383	22.862	22.834	45.609	48.414	11.589	34.625	-1.288	-6.204	49.67	0.108	0.001	0	75.27	1.25444	46.9	12.2	40.1	2.766	0.016	0.015	0.0004	0.365	0.31
10/31/2002	9:06-59 AM	27.462	21.367	28.561	22.926	22.878	45.688	48.857	11.687	34.633	-1.291	-5.118	49.74	0.105	0.001	0	76.27	1.27111	47.4	12.2	40.2	2.769	0.016	0.014	0.0004	0.363	0.30
10/31/2002	9:07-59 AM	27.484	21.4	28.534	23.044	22.901	45.557	48.305	11.546	34.635	-1.285	-6.169	49.526	0.107	0.001	0	77.27	1.28778	46.8	12.1	40.1	2.764	0.016	0.014	0.0004	0.361	0.31
10/31/2002	9:08-59 AM	27.517	21.408	28.552	23.007	22.924	45.847	48.567	11.616	34.971	-1.285	-5.961	49.777	0.109	0.001	0	78.27	1.30444	47.1	12.2	40.4	2.786	0.016	0.015	0.0004	0.364	0.31
10/31/2002	9:09-59 AM	27.55	21.431	28.729	22.869	22.937	45.628	48.358	11.622	34.811	-1.285	-6.132	49.366	0.11	0.001	0	79.27	1.32111	46.9	12.1	40.2	2.773	0.016	0.015	0.0004	0.368	0.31
10/31/2002	9:10-59 AM	27.603	21.459	28.608	23.048	22.965	45.916	48.662	11.521	34.926	-1.288	-6.189	49.576	0.11	0.001	0	80.27	1.33778	47.2	12.1	40.4	2.787	0.016	0.015	0.0004	0.367	0.31
10/31/2002	9:11-59 AM	27.652	21.488	28.781	22.896	22.994	45.644	48.462	11.46	34.871	-1.288	-5.998	49.673	0.115	0.001	0	81.27	1.35444	47.0	12.2	40.3	2.776	0.017	0.015	0.0004	0.383	0.33
10/31/2002	9:12-59 AM	27.704	21.516	28.749	22.899	23.022	45.561	48.544	11.465	34.758	-1.285	-5.961	49.345	0.124	0.001	0	82.27	1.37111	47.1	12.1	40.2	2.769	0.018	0.017	0.0004	0.415	0.35
10/31/2002	9:13-59 AM	27.732	21.534	28.756	22.901	23.034	45.487	48.166	11.439	34.705	-1.288	-6.161	49.656	0.114	0.001	0	83.27	1.38778	46.7	12.2	40.1	2.764	0.017	0.015	0.0004	0.382	0.32
10/31/2002	9:14-59 AM	27.795	21.557	29.058	22.854	23.052	45.752	48.424	11.471	34.916	-1.291	-5.466	50.161	0.082	0.001	0	84.27	1.40444	47.0	12.3	40.3	2.781	0.012	0.011	0.0003	0.271	0.23
10/31/2002	9:15-59 AM	27.848	21.575	29.141	22.953	23.096	45.69	48.228	11.467	34.844	-1.291	-5.943	49.23	0.128	0.001	0	85.27	1.42111	46.8	12.1	40.3	2.776	0.019	0.017	0.0004	0.422	0.36
10/31/2002	9:16-59 AM	27.926	21.629	29.233	23.057	23.129	45.478	48.133	11.371	34.815	-1.285	-5.998	49.651	0.113	0.001	0	86.27	1.43778	46.7	12.2	40.1	2.768	0.017	0.015	0.0004	0.373	0.32
10/31/2002	9:17-59 AM	28.004	21.637	29.455	23.02	23.157	45.599	48.16	11.434	34.856	-1.285	-5.975	50.144	0.11	0.001	0	87.27	1.45444	46.7	12.3	40.2	2.774	0.016	0.014	0.0004	0.360	0.31
10/31/2002	9:18-59 AM	28.081	21.664	29.517	23.178	23.18	45.43																				

10/31/2002	9:42:59 AM	29.437	22.25	30.781	23.701	23.864	45.321	47.589	10.799	35.028	-1.288	-5.891	50.214	0.13	0.001	0	112.27	1.87111	46.1	12.3	40.2	2.770	0.019	0.017	0.0004	0.411	0.35
10/31/2002	9:43:59 AM	29.494	22.262	30.857	23.578	23.876	45.331	47.465	10.744	35.292	-1.288	-5.869	48.982	0.13	0.001	0	113.27	1.88778	46.0	12.0	40.3	2.779	0.019	0.016	0.0004	0.409	0.35
10/31/2002	9:44:59 AM	29.576	22.285	30.9	23.596	23.914	45.274	47.529	10.802	34.922	-1.291	-5.804	49.553	0.135	0.001	0	114.27	1.90444	46.1	12.1	40.1	2.765	0.020	0.017	0.0004	0.427	0.36
10/31/2002	9:45:59 AM	29.633	22.317	30.659	23.708	23.961	44.772	47.398	10.695	34.695	-1.288	-4.991	50.425	0.122	0.001	0	115.27	1.92111	45.9	12.4	39.7	2.739	0.018	0.016	0.0004	0.392	0.33
10/31/2002	9:46:59 AM	29.67	22.34	30.557	23.691	23.944	45.073	47.098	10.634	35.022	-1.288	-5.857	50.541	0.142	0.001	0	116.27	1.93778	45.6	12.4	40.0	2.761	0.021	0.018	0.0005	0.453	0.39
10/31/2002	9:47:59 AM	29.682	22.362	30.748	23.617	23.951	44.845	47.469	10.703	34.774	-1.288	-4.721	50.461	0.132	0.001	0	117.27	1.95444	46.0	12.4	39.8	2.745	0.020	0.017	0.0004	0.422	0.36
10/31/2002	9:48:59 AM	29.679	22.389	30.72	23.68	23.993	45.653	47.789	10.461	35.737	-1.288	-5.781	49.586	0.143	0.001	0	118.27	1.97111	46.3	12.2	40.7	2.806	0.021	0.018	0.0004	0.447	0.38
10/31/2002	9:49:59 AM	29.701	22.401	30.752	23.631	23.995	45.727	48.056	10.475	35.708	-1.288	-5.515	49.119	0.154	0.001	0	119.27	1.98778	46.6	12.0	40.7	2.807	0.023	0.020	0.0005	0.481	0.41
10/31/2002	9:50:59 AM	29.762	22.422	30.981	23.618	23.996	45.802	47.765	10.312	35.964	-1.285	-5.764	47.5	0.145	0.001	0	120.27	2.00444	46.3	11.6	40.9	2.819	0.022	0.018	0.0004	0.448	0.38
10/31/2002	9:51:59 AM	29.804	22.455	30.795	23.671	24.009	45.891	47.75	10.41	36.044	-1.288	-5.634	49.073	0.137	0.001	0	121.27	2.02111	46.3	12.0	41.0	2.825	0.020	0.017	0.0004	0.425	0.36
10/31/2002	9:52:59 AM	29.831	22.477	30.623	23.767	24.015	45.98	48.24	10.405	36.06	-1.285	-5.602	49.337	0.152	0.001	0	122.27	2.03778	46.8	12.1	41.0	2.828	0.023	0.019	0.0005	0.473	0.40
10/31/2002	9:53:59 AM	29.828	22.474	30.65	23.629	24.022	45.458	47.547	10.279	35.888	-1.291	-5.706	49.232	0.145	0.001	0	123.27	2.05444	46.1	12.1	40.6	2.797	0.022	0.018	0.0005	0.456	0.39
10/31/2002	9:54:59 AM	29.85	22.506	30.488	23.801	24.039	45.329	47.322	10.066	35.933	-1.285	-5.665	49.289	0.136	0.001	0	124.27	2.07111	45.9	12.1	40.6	2.801	0.020	0.017	0.0004	0.429	0.36
10/31/2002	9:55:59 AM	29.826	22.527	30.454	23.908	24.056	45.495	47.398	10.271	35.821	-1.288	-5.822	49.268	0.15	0.001	0	125.27	2.08778	45.9	12.1	40.7	2.803	0.022	0.019	0.0005	0.473	0.40
10/31/2002	9:56:59 AM	29.808	22.549	30.585	23.794	24.057	45.681	47.825	10.319	35.971	-1.288	-5.463	49.056	0.146	0.001	0	126.27	2.10444	46.4	12.0	40.8	2.815	0.022	0.019	0.0005	0.457	0.39
10/31/2002	9:57:59 AM	29.789	22.565	30.502	23.906	24.079	45.814	47.653	10.225	36.197	-1.291	-5.729	48.831	0.122	0.001	0	127.27	2.12111	46.2	12.0	41.0	2.827	0.018	0.016	0.0004	0.381	0.32
10/31/2002	9:58:59 AM	29.786	22.582	30.419	23.953	24.096	45.671	47.638	10.217	36.077	-1.288	-5.732	48.617	0.153	0.001	0	128.27	2.13778	46.2	11.9	40.9	2.818	0.023	0.020	0.0005	0.480	0.41
10/31/2002	9:59:59 AM	29.743	22.605	30.347	23.81	24.103	45.578	47.634	10.248	35.847	-1.288	-5.474	49.542	0.169	0.001	0	129.27	2.15444	46.2	12.1	40.7	2.807	0.025	0.022	0.0005	0.534	0.45
10/31/2002	10:00:59 AM	29.705	22.606	30.169	23.791	24.134	45.561	47.487	10.227	35.739	-1.288	-5.619	49.467	0.137	0.001	0	130.27	2.17111	46.0	12.1	40.7	2.803	0.020	0.018	0.0004	0.436	0.37
10/31/2002	10:01:59 AM	29.662	22.638	29.948	23.853	24.151	45.441	47.328	10.166	35.704	-1.288	-5.715	46.646	0.16	0.001	0	131.27	2.18778	45.9	11.4	40.6	2.797	0.024	0.021	0.0005	0.513	0.44
10/31/2002	10:02:59 AM	29.614	22.665	30.129	23.89	24.168	45.603	47.62	10.222	35.722	-1.285	-5.663	49.27	0.149	0.001	0	132.27	2.20444	46.1	12.1	40.7	2.804	0.022	0.019	0.0005	0.474	0.40
10/31/2002	10:03:59 AM	29.577	22.677	30.22	23.938	24.185	45.205	47.241	10.039	35.688	-1.285	-5.332	48.502	0.144	0.001	0	133.27	2.22111	45.8	11.9	40.4	2.789	0.021	0.019	0.0005	0.459	0.39
10/31/2002	10:04:59 AM	29.563	22.694	30.117	23.959	24.197	45.483	47.493	10.069	35.841	-1.291	-5.72	49.123	0.139	0.001	0	134.27	2.23778	46.0	12.0	40.7	2.804	0.021	0.018	0.0004	0.442	0.38
10/31/2002	10:05:59 AM	29.566	22.722	30.229	24.022	24.22	45.323	47.336	10.043	35.741	-1.288	-5.687	48.238	0.15	0.001	0	135.27	2.25444	45.9	11.8	40.5	2.795	0.022	0.019	0.0005	0.477	0.41
10/31/2002	10:06:59 AM	29.562	22.733	30.236	24.093	24.251	45.296	47.094	10.468	36.43	-1.288	-5.608	49.427	0.16	0.001	0	136.27	2.27111	45.6	12.1	40.4	2.783	0.024	0.021	0.0005	0.511	0.44
10/31/2002	10:07:59 AM	29.58	22.761	29.975	24.156	24.269	44.847	47.011	10.428	34.766	-1.288	-5.425	49.909	0.115	0.001	0	137.27	2.28778	45.5	12.2	39.8	2.745	0.017	0.015	0.0004	0.375	0.32
10/31/2002	10:08:59 AM	29.531	22.762	29.891	24.107	24.29	44.884	46.784	10.465	34.871	-1.288	-5.596	50.134	0.147	0.001	0	138.27	2.30444	45.3	12.3	39.9	2.749	0.022	0.019	0.0005	0.480	0.41
10/31/2002	10:09:59 AM	29.518	22.799	30.042	24.154	24.317	44.578	46.664	10.494	34.568	-1.285	-5.492	50.874	0.153	0.001	0	139.27	2.32111	45.2	12.5	39.6	2.728	0.023	0.020	0.0005	0.501	0.43
10/31/2002	10:10:59 AM	29.5	22.816	29.965	24.216	24.329	44.874	46.815	10.067	35.401	-1.288	-5.451	49.406	0.147	0.001	0	140.27	2.33778	45.3	12.1	40.1	2.767	0.022	0.019	0.0005	0.476	0.40
10/31/2002	10:11:59 AM	29.456	22.827	30.021	24.137	24.345	44.95	47.212	10.172	35.204	-1.288	-5.101	49.589	0.136	0.001	0	141.27	2.35444	45.7	12.2	40.1	2.763	0.020	0.018	0.0004	0.440	0.37
10/31/2002	10:12:59 AM	29.464	22.855	30.212	24.18	24.357	45.29	46.9	10.026	35.859	-1.288	-5.616	48.03	0.157	0.001	0	142.27	2.37111	45.4	11.8	40.6	2.797	0.023	0.020	0.0005	0.498	0.43
10/31/2002	10:13:59 AM	29.499	22.875	30.133	24.306	24.393	45.317	47.216	10.043	35.868	-1.288	-5.529	49.06	0.15	0.001	0	143.27	2.38778	45.7	12.0	40.6	2.799	0.022	0.020	0.0005	0.479	0.41
10/31/2002	10:14:59 AM	29.49	22.877	30.095	24.302	24.414	45.352	47.425	9.99	35.859	-1.288	-5.379	48.601	0.156	0.001	0	144.27	2.40444	46.0	11.9	40.6	2.800	0.023	0.020	0.0005	0.497	0.42
10/31/2002	10:15:59 AM	29.528	22.91	30.266	24.19	24.467	45.224	47.545	9.936	35.643	-1.291	-5.214	48.324	0.134	0.001	0	145.27	2.42111	46.1	11.8	40.4	2.788	0.020	0.017	0.0004	0.427	0.36
10/31/2002	10:16:59 AM	29.569	22.941	30.203	24.366	24.484	45.421	47.473	9.974	35.921	-1.285	-5.5	48.706	0.138	0.001	0	146.27	2.43778	46.0	11.9	40.7	2.804	0.021	0.018	0.0004	0.438	0.37
10/31/2002	10:17:59 AM	29.561	22.958	30.16	24.413	24.515	45.487	47.545	10.04	35.847	-1.291	-5.526	49.356	0.157	0.001	0	147.27	2.45444	46.1	12.1	40.7	2.804	0.023	0.020	0.0005	0.499	0.42
10/31/2002	10:18:59 AM	29.588	22.98	30.246	24.31	24.542	45.507	47.539	10.043	35.921	-1.291	-5.532	49.083	0.155	0.001	0	148.27	2.47111	46.1	12.0	40.7	2.807	0.023	0.020	0.0005	0.491	0.42
10/31/2002	10:19:59 AM	29.595	23.012	30.05	24.387	24.574	45.439	47.566	9.963																		

10/31/2002	10:47:59 AM	29.574	23.599	29.781	25.128	25.18	44.344	46.592	9.532	35.141	-1.288	-5.405	49.532	0.174	0.001	0	177.27	2.95444	45.1	12.1	39.7	2.740	0.026	0.023	0.0006	0.572	0.49
10/31/2002	10:48:59 AM	29.602	23.617	29.823	25.076	25.213	44.623	46.629	9.455	35.667	-1.291	-5.321	48.985	0.191	0.001	0	178.27	2.97111	45.2	12.0	40.1	2.768	0.028	0.025	0.0006	0.621	0.53
10/31/2002	10:49:59 AM	29.619	23.629	30.044	25.008	25.23	44.89	46.96	9.532	35.776	-1.294	-5.234	48.827	0.184	0.001	0	179.27	2.98778	45.5	12.0	40.3	2.781	0.027	0.024	0.0006	0.592	0.50
10/31/2002	10:50:59 AM	29.676	23.667	30.052	25.136	25.273	44.818	47.136	9.559	35.624	-1.291	-5.17	49.068	0.197	0.001	0	180.27	3.00444	45.7	12.0	40.2	2.773	0.029	0.026	0.0006	0.635	0.54
10/31/2002	10:51:59 AM	29.718	23.674	29.939	25.122	25.295	44.961	47.063	9.513	35.915	-1.294	-5.107	48.876	0.141	0.001	0	181.27	3.02111	45.6	12.0	40.4	2.788	0.021	0.018	0.0005	0.453	0.39
10/31/2002	10:52:59 AM	29.76	23.707	30.022	25.18	25.303	44.766	47.163	9.488	35.64	-1.288	-5.005	48.148	0.185	0.001	0	182.27	3.03778	45.7	11.8	40.2	2.772	0.028	0.024	0.0006	0.597	0.51
10/31/2002	10:53:59 AM	29.767	23.724	29.865	25.288	25.325	44.544	46.86	9.498	35.475	-1.288	-4.927	50.002	0.166	0.001	0	183.27	3.05444	45.4	12.3	40.0	2.759	0.025	0.022	0.0005	0.541	0.46
10/31/2002	10:54:59 AM	29.745	23.746	29.797	25.325	25.347	44.544	47.074	9.569	35.295	-1.291	-4.915	49.224	0.179	0.001	0	184.27	3.07111	45.6	12.1	39.9	2.752	0.027	0.023	0.0006	0.586	0.50
10/31/2002	10:55:59 AM	29.743	23.769	30.039	25.333	25.375	44.876	47.094	9.504	35.733	-1.291	-5.315	49.146	0.188	0.001	0	185.27	3.08778	45.6	12.0	40.3	2.779	0.028	0.024	0.0006	0.605	0.51
10/31/2002	10:56:59 AM	29.715	23.787	30.071	25.37	25.412	44.75	46.771	9.451	35.71	-1.288	-5.199	48.595	0.208	0.001	0	186.27	3.10444	45.3	11.9	40.2	2.774	0.031	0.027	0.0007	0.670	0.57
10/31/2002	10:57:59 AM	29.733	23.815	30.044	25.433	25.465	45.157	47.243	9.561	35.982	-1.291	-5.208	48.638	0.2	0.001	0	187.27	3.12111	45.8	11.9	40.5	2.794	0.030	0.026	0.0006	0.640	0.54
10/31/2002	10:58:59 AM	29.71	23.832	30.22	25.385	25.462	44.863	47.15	9.475	35.862	-1.291	-5.295	48.584	0.189	0.001	0	188.27	3.13778	45.7	11.9	40.4	2.783	0.028	0.024	0.0006	0.604	0.51
10/31/2002	10:59:59 AM	29.797	23.854	30.237	25.412	25.475	44.604	47.187	9.557	35.272	-1.288	-4.826	49.091	0.182	0.001	0	189.27	3.15444	45.7	12.0	39.9	2.754	0.027	0.023	0.0006	0.588	0.50
10/31/2002	11:00:59 AM	29.873	23.871	30.015	25.489	25.461	44.095	46.629	9.47	34.854	-1.288	-4.71	48.746	0.18	0.001	0	190.27	3.17111	45.2	11.9	39.5	2.722	0.027	0.023	0.0006	0.592	0.50
10/31/2002	11:01:59 AM	29.871	23.894	30.018	25.507	25.479	44.592	46.898	9.557	35.319	-1.291	-5.06	48.985	0.197	0.001	0	191.27	3.18778	45.4	12.0	40.0	2.755	0.029	0.026	0.0006	0.640	0.54
10/31/2002	11:02:59 AM	29.863	23.91	29.965	25.564	25.48	44.081	46.44	9.396	35.041	-1.288	-4.994	49.511	0.204	0.001	0	192.27	3.20444	45.0	12.1	39.6	2.728	0.030	0.027	0.0007	0.670	0.57
10/31/2002	11:03:59 AM	29.86	23.933	29.907	25.621	25.493	44.565	46.968	9.496	35.208	-1.291	-5.26	49.339	0.164	0.001	0	193.27	3.22111	45.5	12.1	39.9	2.750	0.024	0.021	0.0005	0.535	0.46
10/31/2002	11:04:59 AM	29.862	23.955	30.069	25.623	25.53	44.634	46.854	9.42	35.593	-1.288	-5.167	49.014	0.177	0.001	0	194.27	3.23778	45.4	12.0	40.1	2.766	0.026	0.023	0.0006	0.572	0.49
10/31/2002	11:05:59 AM	29.869	23.962	30.195	25.72	25.527	44.689	46.989	9.432	35.532	-1.288	-5.162	48.966	0.202	0.001	0	195.27	3.25444	45.5	12.0	40.1	2.765	0.030	0.026	0.0007	0.650	0.55
10/31/2002	11:06:59 AM	29.861	23.989	30.062	25.717	25.534	45	47.072	9.477	35.817	-1.291	-5.188	49.211	0.195	0.001	0	196.27	3.27111	45.6	12.0	40.4	2.786	0.029	0.025	0.0006	0.625	0.53
10/31/2002	11:07:59 AM	29.829	24.027	30.011	25.655	25.562	44.53	46.753	9.365	35.542	-1.291	-5.309	48.936	0.153	0.001	0	197.27	3.28778	45.3	12.0	40.0	2.760	0.023	0.020	0.0005	0.496	0.57
10/31/2002	11:08:59 AM	29.862	24.045	30.039	25.723	25.585	44.766	46.62	9.353	35.796	-1.291	-5.118	49.031	0.208	0.001	0	198.27	3.30444	45.1	12.0	40.3	2.777	0.031	0.027	0.0007	0.670	0.57
10/31/2002	11:09:59 AM	29.829	24.067	29.852	25.73	25.602	44.254	46.438	9.317	35.165	-1.291	-4.901	48.775	0.165	0.001	0	199.27	3.32111	45.0	12.0	39.7	2.738	0.025	0.022	0.0005	0.542	0.46
10/31/2002	11:10:59 AM	29.797	24.095	30.004	25.813	25.605	44.283	46.751	9.35	35.268	-1.288	-5.072	47.714	0.188	0.001	0	200.27	3.33778	45.3	11.7	39.8	2.742	0.028	0.024	0.0006	0.614	0.52
10/31/2002	11:11:59 AM	29.875	24.103	30.171	25.811	25.628	44.209	46.838	9.342	35.057	-1.291	-4.522	48.768	0.167	0.001	0	201.27	3.35444	45.4	12.0	39.6	2.733	0.025	0.022	0.0005	0.544	0.46
10/31/2002	11:12:59 AM	29.882	24.116	30.039	25.818	25.63	44.393	46.771	9.362	35.358	-1.291	-5.211	48.024	0.178	0.001	0	202.27	3.37111	45.3	11.8	39.9	2.749	0.027	0.023	0.0006	0.579	0.49
10/31/2002	11:13:59 AM	29.925	24.144	29.977	25.856	25.638	44.48	46.811	9.312	35.477	-1.288	-5.315	47.856	0.181	0.001	0	203.27	3.38778	45.3	11.7	40.0	2.756	0.027	0.024	0.0006	0.588	0.50
10/31/2002	11:14:59 AM	29.907	24.161	30.034	25.874	25.675	43.782	46.871	9.384	34.631	-1.291	-4.001	49.517	0.173	0.001	0	204.27	3.40444	45.4	12.1	39.2	2.703	0.026	0.022	0.0006	0.572	0.49
10/31/2002	11:15:59 AM	29.83	24.178	29.858	25.926	25.683	44.136	46.552	9.256	35.221	-1.291	-4.852	50.319	0.207	0.001	0	205.27	3.42111	45.1	12.3	39.7	2.736	0.031	0.027	0.0007	0.680	0.58
10/31/2002	11:16:59 AM	29.833	24.211	30.02	25.979	25.701	44.132	46.569	9.149	35.278	-1.285	-5.303	48.59	0.189	0.001	0	206.27	3.43778	45.1	11.9	39.7	2.738	0.028	0.025	0.0006	0.618	0.53
10/31/2002	11:17:59 AM	29.926	24.245	30.257	25.993	25.725	44.178	46.912	9.235	35.317	-1.288	-4.166	48.15	0.192	0.001	0	207.27	3.45444	45.4	11.8	39.7	2.740	0.029	0.025	0.0006	0.623	0.53
10/31/2002	11:18:59 AM	29.941	24.24	30.158	25.943	25.665	44.083	46.848	9.304	34.983	-1.291	-4.38	48.492	0.186	0.001	0	208.27	3.47111	45.4	11.9	39.5	2.726	0.028	0.024	0.0006	0.608	0.52
10/31/2002	11:19:59 AM	29.95	24.25	30.177	25.902	25.619	44.402	46.941	9.375	35.307	-1.288	-4.756	48.162	0.166	0.001	0	209.27	3.48778	45.5	11.8	39.9	2.748	0.025	0.021	0.0005	0.538	0.46
10/31/2002	11:20:59 AM	29.979	24.274	30.39	25.806	25.588	44.718	47.088	9.588	35.362	-1.288	-4.803	48.66	0.201	0.001	0	210.27	3.50444	45.6	11.9	40.0	2.761	0.030	0.026	0.0006	0.645	0.55
10/31/2002	11:21:59 AM	29.966	24.271	30.272	25.733	25.495	44.733	47.028	9.572	35.395	-1.291	-4.968	48.336	0.215	0.001	0	211.27	3.52111	45.6	11.8	40.1	2.762	0.032	0.028	0.0007	0.692	0.59
10/31/2002	11:22:59 AM	29.938	24.277	30.249	25.634	25.426	44.482	46.86	9.554	35.147	-1.288	-5.043	48.29	0.166	0.001	0	212.27	3.53778	45.4	11.8	39.8	2.745	0.025	0.021	0.0005	0.538	0.46
10/31/2002	11:23:59 AM	29.982	24.267	30.402	25.494	25.366	44.745	46.838	9.566	35.497	-1.294	-5.057	48.473	0.209	0.001	0	213.27	3.55444	45.4	11.9	40.1	2.766	0.031	0.027	0.0007	0.669	0.57
10/31/2002	11:24:59 AM	30.061	24.276	30.342	25.443	25.285	44.863	47.26	9.615	35.393	-1.288	-4.869	48.391	0.168	0.001	0	214.27	3.57111	45.8	11.9	40.1	2.767	0.025	0.022	0.0005	0.538	0.46
10/31/2002	11:25:59 AM	30.075	24.281	30.277	25.317	25.234	44.812	46.867	9.625	35.432	-1.288	-5.182	48.36	0.193	0.001	0	215.27	3.58778	45.4	11.9	40.1	2.766	0.029	0.025	0.0006	0.620	0.53
10/31/2002	11:26:59 AM	30.071	24.281	30.456	25.268	25.23	44.704	46.952	9.674	35.245	-1.288	-5.182	48.943	0.149	0.001	0	216.27	3.60444	45.5	12.0	40.0	2.756	0.022	0.019	0.0005	0.478	0.41
10/31/2002	11:27:59 AM	30.108	24.284	30.409	25.376	25.258	44.335	46.786	9.567	35.065	-1.291	-5.153	47.93	0.186	0.001	0	217.27	3.62111	45.3	11.7	39.7	2.737	0.028	0.024	0.0006	0.601	0.51
10/31/2002	11:28:59 AM	30.152	24.283	30.33																							

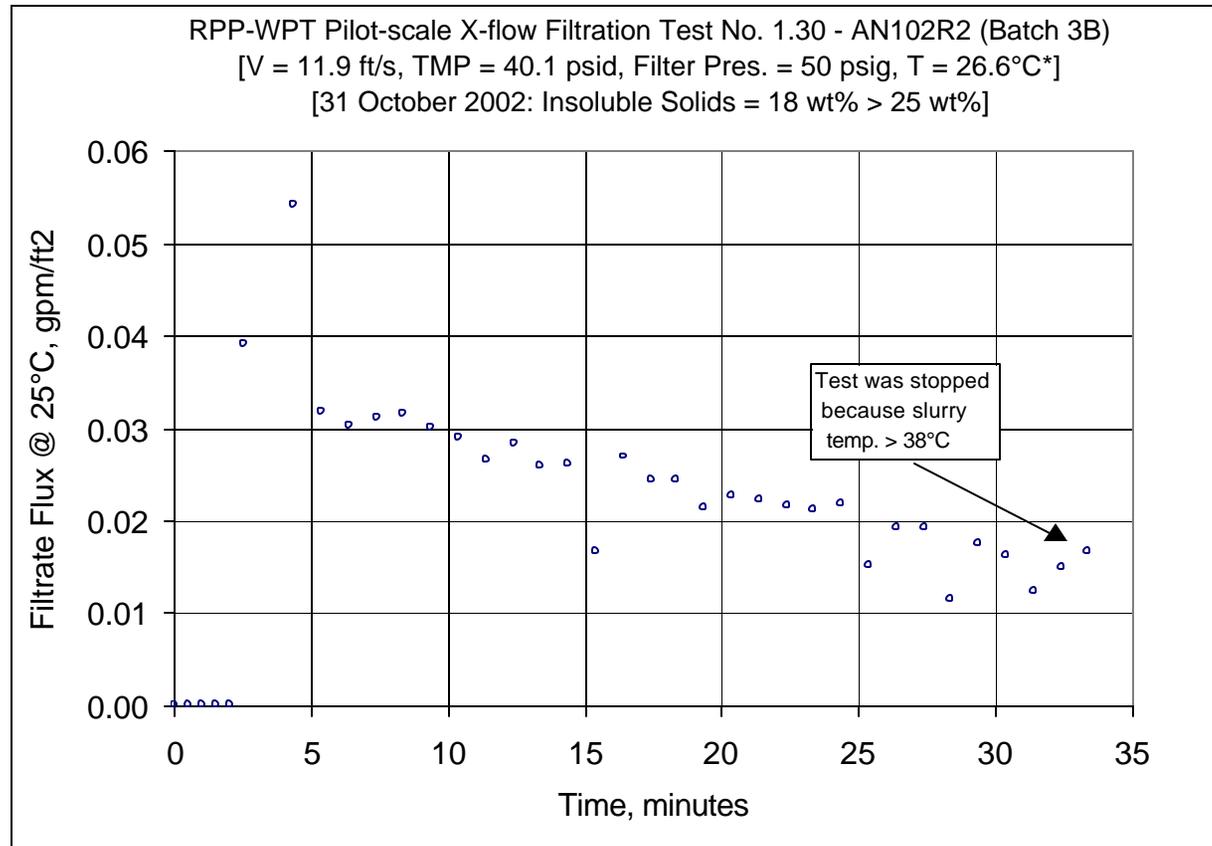


Figure F3: Concentrating washed slurry to maximum possible. It turned out that neither the slurry volume, nor a filter pluggage limited concentration. It was the slurry temperature. After the 26<sup>th</sup> minute to slurry properties changed such that the active cooling was less and less effective. The exponential temperature increase forced termination. When the temperature passed 38°C, and increasing at 2.2°C/min, the test was stopped to avoid pump damage. The thermal momentum caused the temperature to reach 46°C before it could be controlled. Approximately 20 liters of the approximate 75 liters of washed slurry were removed. The insoluble solids concentration increased from 19 to 25 wt%.



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## APPENDIX G

### ANALYTICAL, RHEOLOGICAL, AND PARTICAL-SIZE DATA

#### Appendix Contents

1. List of all samples taken during test: Table G1.
2. Notes to Table G2.
3. Table G2 contains all of the analytical data as well as some rheological and particle-size data.
4. Slurry Rheology
5. Particle-size Distribution data

#### Note on measurement uncertainties of the included data:

There are no measurement uncertainties listed because the measurement uncertainties for analytical data are beyond the scope and control of this task. There is reason to believe that all analytical data can be at least 15% accurate but no quantitative data are given to this effect. Density, filtrate viscosity, turbidity are the only simulatn property data that were obtained at the test rig location and the uncertainty of those data can be stated as:

Density:  $\pm 0.5\%$  of reading by calibration

Viscosity:  $\pm 0.34\%$  of reading by manufacturer's statement.

Turbidity:  $\pm 0.04$  NTU

**WSRC-TR-2003-00204, REV. 0**  
**SRT-RPP-2003-00087, REV. 0**

Related Test	When Sample was Taken		Sample Size (mL)	EDL	ADS or ITS	Analysis Requested
	Date	Time		Sample #	Sample #	
<b>AN-102 Batch 3C</b>						
1.16-3C	1-Oct-02	before test	250	rpp-pxu-filtrate-pre1.16-turbidity	none-by EDL/EDS/SRTC	turb, dens, visc
1.16-3C	1-Oct-02	before test	250	rpp-pxu-filtrate-pre1.16-archive	none	none-archive
1.16-3C	1-Oct-02	before test	15	rpp-pxu-filtrate-pre1.16-archive	none	none-archive
1.16-3C	1-Oct-02	before test	15	rpp-pxu-filtrate-pre1.16-table1	300188154	ICPES, IC An, TIC/TOC
1.16-3C	1-Oct-02	before test	15	rpp-pxu-filtrate-pre1.16-solids	300186654	TS, dens
1.16-3C	1-Oct-02	before test	250	rpp-pxu-slurry-pre1.16-rheology	none-by PDH/ITS/SRTC	rheology
1.16-3C	1-Oct-02	before test	250	rpp-pxu-slurry-pre1.16-archive	none	none-archive
1.16-3C	1-Oct-02	before test	15	rpp-pxu-slurry-pre1.16-solids1	300186655	TS, SS, dens
1.16-3C	1-Oct-02	before test	15	rpp-pxu-slurry-pre1.16-solids2	300186656	TS, SS, dens
1.16-3C	1-Oct-02	before test	15	rpp-pxu-slurry-pre1.16-psd	300188111	microtrac
1.16-3C	1-Oct-02	before test	15	rpp-pxu-slurry-pre1.16-archive	none	none-archive
1.16-3C	3-Oct-02	test end	15	rpp-pxu-filtrate-mid1.16-table1	300188155	ICPES, IC An, TIC/TOC, turb
1.16-3C	3-Oct-02	test end	15	rpp-pxu-filtrate-mid1.16-solids	no number, used for >	acqeous for next 2 samples
1.16-3C	3-Oct-02	test end	15	rpp-pxu-slurry-mid1.16-solids1	300186909	TS, SS, dens
1.16-3C	3-Oct-02	test end	15	rpp-pxu-slurry-mid1.16-solids2	300186910	TS, SS, dens
1.16-3C	3-Oct-02	test end	15	rpp-pxu-slurry-mid1.16-psd	300188112	microtrac
1.16-3C	3-Oct-02	test end	250	rpp-pxu-slurry-mid1.16-archive	none	none-archive
<b>AN-102 Batch 3B</b>						
1.16-3B	22-Oct-02	before test	250	Pre1.16-batch 3B - P. Townson	sent to Hanford	none
1.16-3B	22-Oct-02	before test	250	rpp-pxu-slu-pre1.16-3b-rheology	none-by PDH/ITS/SRTC	rheology
1.16-3B	22-Oct-02	before test	250	rpp-pxu-slu-pre1.16-3b-archive	none	none-archive
1.16-3B	22-Oct-02	before test	15	rpp-pxu-slu-pre1.16-3b-solids1	300187815	TS, SS, dens
1.16-3B	22-Oct-02	before test	15	rpp-pxu-slu-pre1.16-3b-solids2	300187816	TS, SS, dens
1.16-3B	22-Oct-02	before test	15	rpp-pxu-slu-pre1.16-3b-psd	300188109	microtrac
1.16-3B	22-Oct-02	before test	15	rpp-pxu-slu-pre1.16-3b-archive	none	none-archive
1.16-3B	22-Oct-02	1 hr into test	250	rpp-pxu-filt-pre1.16-3b-turbidity	none-by EDL/EDS/SRTC	turb, dens, visc
1.16-3B	22-Oct-02	1 hr into test	15	rpp-pxu-filt-pre1.16-3b-archive	none	none-archive
1.16-3B	22-Oct-02	1 hr into test	15	rpp-pxu-filt-pre1.16-3b-table1	300188150	ICPES, IC An, TIC/TOC
1.16-3B	23-Oct-02	test end/02:56	250	rpp-pxu-filt-end1.16-3b-solids	for archive	none
1.16-3B	23-Oct-02	test end/02:56	15	rpp-pxu-filt-end1.16-3b-solids	no number	none
1.16-3B	23-Oct-02	test end/02:56	15	rpp-pxu-slu-end1.16-3b-solids1	300187825	TS, SS, dens
1.16-3B	23-Oct-02	test end/02:56	15	rpp-pxu-slu-end1.16-3b-solids2	300187826	TS, SS, dens
1.16-3B	23-Oct-02	test end/19:00	250	rpp-pxu-filt-final1.16-3b-archive	none	none-archive
1.16-3B	23-Oct-02	test end/19:00	15	rpp-pxu-filt-final1.16-3b-solids	no number, used for >	acqeous for next solids1&2
1.16-3B	23-Oct-02	test end/19:00	15	rpp-pxu-filt-final1.16-3b-table1	300188152	ICPES, IC An, TIC/TOC, turb
1.16-3B	23-Oct-02	test end/19:00	250	Final1.16-batch 3B - P. Townson	sent to Hanford	none
1.16-3B	23-Oct-02	test end/19:00	250	rpp-pxu-slu-final1.16-3b-rheology	none-by PDH/ITS/SRTC	rheology
1.16-3B	23-Oct-02	test end/19:00	250	rpp-pxu-slu-final1.16-3b-archive	none	none-archive
1.16-3B	23-Oct-02	test end/19:00	15	rpp-pxu-slu-final1.16-3b-solids1	300187857	TS, SS, dens
1.16-3B	23-Oct-02	test end/19:00	15	rpp-pxu-slu-final1.16-3b-solids2	300187858	TS, SS, dens
1.16-3B	23-Oct-02	test end/19:00	15	rpp-pxu-slu-final1.16-3b-psd	300188110	microtrac
Wash-3B	30-Oct-02	PreWash22wt%	250	rpp-pxu-filt22%-prewash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PreWash22wt%	250	rpp-pxu-slu22%-prewash-3b-rheology	none-by PDH/ITS/SRTC	rheology
Wash-3B	30-Oct-02	PreWash22wt%	250	rpp-pxu-slu22%-prewash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PreWash20wt%	250	rpp-pxu-filt20%-prewash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PreWash20wt%	250	rpp-pxu-slu20%-prewash-3b-rheology	none-by PDH/ITS/SRTC	rheology
Wash-3B	30-Oct-02	PreWash20wt%	250	rpp-pxu-slu20%-prewash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PreWash20wt%	15	rpp-pxu-filt20%-prewash-3b-table1	300189078	ICPES, IC An, TIC/TOC
Wash-3B	30-Oct-02	PreWash20wt%	15	rpp-pxu-filt20%-prewash-3b-solids	300189087	TS, dens
Wash-3B	30-Oct-02	PreWash20wt%	15	rpp-pxu-slu20%-prewash-3b-solids	300189088	TS, SS, dens
Wash-3B	30-Oct-02	PreWash20wt%	15	rpp-pxu-slu20%-prewash-3b-psd	300189271	microtrac
Wash-3B	30-Oct-02	Wash	15	rpp-pxu-filt-wash-5-3b	300189083	ICPES
Wash-3B	30-Oct-02	Wash	15	rpp-pxu-filt-wash-10-3b	300189084	ICPES
Wash-3B	30-Oct-02	Wash	15	rpp-pxu-filt-wash-15-3b	300189085	ICPES
Wash-3B	30-Oct-02	PostWash	250	rpp-pxu-filt-postwash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PostWash	250	rpp-pxu-slu-postwash-3b-rheology	none-by PDH/ITS/SRTC	rheology
Wash-3B	30-Oct-02	PostWash	250	rpp-pxu-slu-postwash-3b-archive	none	none-archive
Wash-3B	30-Oct-02	PostWash	15	rpp-pxu-filt-postwash-3b-table1	300189079	ICPES, IC An, TIC/TOC
Wash-3B	30-Oct-02	PostWash	15	rpp-pxu-filt-postwash-3b-solids	300189089	TS, dens
Wash-3B	30-Oct-02	PostWash	15	rpp-pxu-slu-postwash-3b-solids	300189090	TS, SS, dens
Wash-3B	30-Oct-02	PostWash	15	rpp-pxu-slu-postwash-3b-psd	300189272	microtrac
130-3B	31-Oct-02	Test End	250	rpp-pxu-filt-end1.30-3b-archive	none	none-archive
130-3B	31-Oct-02	Test End	15	rpp-pxu-filt-end1.30-3b-solids	300189091	TS, dens
130-3B	31-Oct-02	Test End	15	rpp-pxu-filt-end1.30-3b-table1	300189080	TS, SS, dens
130-3B	31-Oct-02	Test End	250	rpp-pxu-slu-end1.30-3b-rheology	none-by PDH/ITS/SRTC	rheology
130-3B	31-Oct-02	Test End	250	rpp-pxu-slu-end1.30-3b-archive	none	none-archive
130-3B	31-Oct-02	Test End	15	rpp-pxu-slu-end1.30-3b-table1	300189086	ICPES, IC An, TIC/TOC
130-3B	31-Oct-02	Test End	-50 in 125	rpp-pxu-slu-end1.30-3b-solids	300189092	TS, SS, dens

Table G1:All Samples taken during AN-102 Testing, Page 1



Notes to Table G2

2. The units listed are used for the data in each row except where otherwise noted.
3. See the sample page, which precedes this table for the nomenclature.
4. Turbidity was checked periodically: on 10/2/02 it was 0.28 NTU, on 10/3/02 it was 0.28 NTU on 10/9/02 it was 1.01 NTU. This turbidity increase may be due to exposure to light because another sample was taken from a filtrate batch that was created on 10/1/02, but it was kept from light. Its turbidity was 0.16 NTU; the same as the original sample taken on 10/1/02.
5. Testing with batch 3C was stopped because of poor filterability and a dedicated slurry sample was not taken for rheological measurements as part of the filtration task. However, sample was not taken as part of the precipitation task. The results of sample RPP-WTP-PREC3C-3SL are in memo: SRTC-PDH-2002-00005 of 8-Oct-2002: 9.68cP and 9.50 cP; Yield=1.47 Pa and 1.79 Pa
6. The slurry sample was taken AFTER the filtrate sample was taken. Approximately 0.75 liters of filtrate was removed from the slurry and the remaining slurry was approximately 60 liters. Therefore the solids concentration of 18.71 wt% of the slurry sample was slightly higher than the slurry at the end of the experiment and the actual insoluble solids contents was approximately 18.3 wt%.

	A	B	C	D	E	F	G	H
1	Test Run ----->>>			1.16-3C	1.16-3C	1.16-3C	1.16-3C	1.16-3C
2	Sample Taken Date ----->>>			October 1, 2002	October 1, 2002	October 1, 2002	October 1, 2002	October 1, 2002
3	Sample Taken Time ----->>>			before test	before test	before test	before test	before test
4	Sample ID (Prefix = rpp-pxu-) -->>			filtrate-pre1.16-turbidity	filtrate-pre1.16-table1	filtrate-pre1.16-solids	slurry-pre1.16-rheology	slurry-pre1.16-solids1
5	ADS Sample ID ----->>>			none	300188154	300186654	none	300186655
6	Type Sample ----->>>			filtrate	filtrate	filtrate	slurry	slurry
7	Sample Size (mL) ----->>>			250	15	15	250	15
8	Item Measured	Units*	Method/Analyst Org					
9	Al	ug/mL	ICP-ES / ADS		7840			
10	B	ug/mL	ICP-ES / ADS		24.9			
11	Ba	ug/mL	ICP-ES / ADS		<0.024			
12	Ca	ug/mL	ICP-ES / ADS		78.8			
13	Cd	ug/mL	ICP-ES / ADS		35.2			
14	Ce	ug/mL	ICP-ES / ADS		6.9			
15	Cf	ug/mL	IC Anions / ADS		3410			
16	Co	ug/mL	ICP-ES / ADS		<1.0			
17	Cr	ug/mL	ICP-ES / ADS		146			
18	Cu	ug/mL	ICP-ES / ADS		<0.25			
19	Fe	ug/mL	ICP-ES / ADS		1.5			
20	K	ug/mL	ICP-ES / ADS		1740			
21	La	ug/mL	ICP-ES / ADS		4.2			
22	Mg	ug/mL	ICP-ES / ADS		<0.168			
23	Mn	ug/mL	ICP-ES / ADS		4.7			
24	Mo	ug/mL	ICP-ES / ADS		29.6			
25	Na	ug/mL	ICP-ES / ADS		123000			
26	Nd	ug/mL	ICP-ES / ADS		11.4			
27	Ni	ug/mL	ICP-ES / ADS		240			
28	NO3 (Nitrate)	ug/mL	IC Anions / ADS		135000			
29	P	ug/mL	ICP-ES / ADS		681			
30	PO4 (Phosphate)	ug/mL	IC Anions / ADS		3140			
31	Pb	ug/mL	ICP-ES / ADS		20.3			
32	S	ug/mL	ICP-ES / ADS		2840			
33	Si	ug/mL	ICP-ES / ADS		21.6			
34	Sn	ug/mL	ICP-ES / ADS		0.7			
35	SO4 (Sulfate)	ug/mL	IC Anions / ADS		8890			
36	Sr	ug/mL	ICP-ES / ADS		30.5			
37	W	ug/mL	ICP-ES / ADS		107			
38	Zn	ug/mL	ICP-ES / ADS		1.2			
39	Zr	ug/mL	ICP-ES / ADS		2.4			
40	Total Organic Carbon	ug/mL	TIC-TOC / ADS		10000			
41	Total Inorganic Carbon	ug/mL	TIC-TOC / ADS		6990			
42	Suspended Solids	wt%	Gravimetric / ADS					1.00
43	Total Solids	wt%	Gravimetric / ADS			33.08		33.70
44	Particle Size by Volume	micron	Microtrac / ADS					
45	Particle Size by Number	micron	Microtrac / ADS					
46	Kin. Viscosity	cSt	CONE/ITS-CAPILLARY/EDL	2.16			2.8	
47	Dyn. Visc./Consistency	cP	Kin. Visc. x Density	2.67			3.6	
48	Yield Stress	Pa					0.0	
49	Density	g/mL	Gravimetric / EDL	1.238			1.279	
50	Density	g/mL	Gravimetric / ADS			1.250		1.330
51	Turbidity	NTU	/ EDL	0.18 (on 10/1)				
52	Comment - Note (1)	Note (2)	Note (3)	Note (4)			Note (5)	
53	Note (1) - See notes on page preceding this table.							

Table G2:AN-102 simulant analytical and other data, Page 1

	I	J	K	L	M	N	O	P	Q
1	Test Run ----->>		1.16-3C	1.16-3C	1.16-3C	1.16-3C	1.16-3C	1.16-3C	
2	Sample Taken Date ----->>		October 1, 2002	October 1, 2002	October 3, 2002	October 3, 2002	October 3, 2002	October 3, 2002	
3	Sample Taken Time ----->>		before test	before test	test end	test end	test end	test end	
4	Sample ID (Prefix = rpp-pxu-) ->>		slurry-pre1.16-solids2	slurry-pre1.16-psd	filtrate-mid1.16-table1	slurry-mid1.16-solids1	slurry-mid1.16-solids2	slurry-mid1.16-psd	
5	ADS Sample ID ----->>		300186656	300188111	300188155	300186909	300186910	300188112	
6	Type Sample ----->>		slurry	slurry	filtrate	slurry	slurry	slurry	
7	Sample Size (mL) ----->>		15	15	15	15	15	15	
8	Item Measured	Units*							
9	Al	ug/mL			8480				
10	B	ug/mL			27.5				
11	Ba	ug/mL			<0.024				
12	Ca	ug/mL			102.0				
13	Cd	ug/mL			38.4				
14	Ce	ug/mL			5.6				
15	Cl	ug/mL			3610				
16	Co	ug/mL			<1.0				
17	Cr	ug/mL			160				
18	Cu	ug/mL			<0.25				
19	Fe	ug/mL			0.9				
20	K	ug/mL			1940				
21	La	ug/mL			2.5				
22	Mg	ug/mL			<0.168				
23	Mn	ug/mL			5.4				
24	Mo	ug/mL			31.8				
25	Na	ug/mL			133000				
26	Nd	ug/mL			6.9				
27	Ni	ug/mL			254				
28	NO3 (Nitrate)	ug/mL			132000				
29	P	ug/mL			669				
30	PO4 (Phosphate)	ug/mL			3220				
31	Pb	ug/mL			35.2				
32	S	ug/mL			3120				
33	Si	ug/mL			24.4				
34	Sn	ug/mL			0.8				
35	SO4 (Sulfate)	ug/mL			9380				
36	Sr	ug/mL			10.9				
37	W	ug/mL			120				
38	Zn	ug/mL			1.4				
39	Zr	ug/mL			2.4				
40	Total Organic Carbon	ug/mL			10900				
41	Total Inorganic Carbon	ug/mL			7820				
42	Suspended Solids	wt%	0.68			8.51	8.30		
43	Total Solids	wt%	33.49			38.71	38.56		
44	Particle Size by Volume	micron		2.56(32%), 8.59(68%)				2.47(49%), 6.75(51%)	
45	Particle Size by Number	micron		2.08 (100%)				1.91	
46	Kin. Viscosity	cSt						7.5	
47	Dyn. Visc./Consistency	cP						9.8	
48	Yield Stress	Pa						1.7	
49	Density	g/mL							
50	Density	g/mL	1.310			1.276	1.306		
51	Turbidity	NTU			0.14				
52	Comment - Note (1)	Note (2)		bimodal by volume					bimodal by volume
53	Note(1)-Notes precede this table								

Table G2:AN-102 simulant analytical and other data, Page 2

	R	S	T	U	V	W	X	Y
1	Test Run ----->>		1.16-3B	1.16-3B	1.16-3B	1.16-3B	1.16-3B	1.16-3B
2	Sample Taken Date ----->>		October 22, 2002	October 22, 2002	October 22, 2002	October 22, 2002	October 22, 2002	October 22, 2002
3	Sample Taken Time ----->>		before test	before test	before test	before test	1 hr into test	1 hr into test
4	Sample ID (Prefix = rpp-pxu-) ->>		slu-pre1.16-3b-rheology	slu-pre1.16-3b-solids1	slu-pre1.16-3b-solids2	slu-pre1.16-3b-psd	filt-pre1.16-3b-turbidity	filt-pre1.16-3b-table1
5	ADS Sample ID ----->>		none	300187815	300187816	300188109	none	300188150
6	Type Sample ----->>		slurry	slurry	slurry	slurry	filtrate	filtrate
7	Sample Size (mL) ----->>		250	15	15	15	250	15
8	Item Measured	Units*						
9	Al	ug/mL						7970
10	B	ug/mL						25.2
11	Ba	ug/mL						<0.024
12	Ca	ug/mL						56.2
13	Cd	ug/mL						36.1
14	Ce	ug/mL						2.3
15	Cf	ug/mL						3510
16	Co	ug/mL						<1.0
17	Cr	ug/mL						134
18	Cu	ug/mL						<0.25
19	Fe	ug/mL						1.1
20	K	ug/mL						1790
21	La	ug/mL						<1.4
22	Mg	ug/mL						<0.168
23	Mn	ug/mL						8.3
24	Mo	ug/mL						31.4
25	Na	ug/mL						140000
26	Nd	ug/mL						3.9
27	Ni	ug/mL						229
28	NO3 (Nitrate)	ug/mL						135000
29	P	ug/mL						1130
30	PO4 (Phosphate)	ug/mL						4090
31	Pb	ug/mL						36.4
32	S	ug/mL						2900
33	Si	ug/mL						23.2
34	Sn	ug/mL						0.6
35	SO4 (Sulfate)	ug/mL						8680
36	Sr	ug/mL						40.6
37	W	ug/mL						115
38	Zn	ug/mL						3.2
39	Zr	ug/mL						1.0
40	Total Organic Carbon	ug/mL						9620
41	Total Inorganic Carbon	ug/mL						6480
42	Suspended Solids	wt%		1.30	1.12			
43	Total Solids	wt%		32.72	32.71			
44	Particle Size by Volume	micron				2.25(52%), 8.55(48%)		
45	Particle Size by Number	micron				1.94		
46	Kin. Viscosity	cSt	3.1				2.8	
47	Dyn. Visc./Consistency	cP	4.0				3.6	
48	Yield Stress	Pa	0.0					
49	Density	g/mL	1.285				1.279	
50	Density	g/mL		1.314	1.265			
51	Turbidity	NTU					0.13	
52	Comment - Note (1)	Note (2)				bimodal by volume		
53	Note(1)-Notes precede this table							

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	Z	AA	AB	AC	AD	AE	AF	AG
1	Test Run ----->>		1.16-3B	1.16-3B	1.16-3B	1.16-3B	1.16-3B	1.16-3B
2	Sample Taken Date ----->>		October 23, 2002	October 23, 2002	October 23, 2002	October 23, 2002	October 23, 2002	October 23, 2002
3	Sample Taken Time ----->>		test end / 02:56 A.M.	test end / 02:56 A.M.	test end / 02:56 A.M.	test end / 19:00	test end / 19:00	test end / 19:00
4	Sample ID (Prefix = rpp-pxu-) ->>		filt-end1.16-3b-solids	slu-end1.16-3b-solids1	slu-end1.16-3b-solids2	filt-final1.16-3b-solids	filt-final1.16-3b-table1	slu-final1.16-3b-rheology
5	ADS Sample ID ----->>		none	300187825	300187826	none	300188152	none
6	Type Sample ----->>		filtrate	slurry	slurry	filtrate	filtrate	slurry
7	Sample Size (mL) ----->>		15	15	15	15	15	250
8	Item Measured	Units*						
9	Al	ug/mL					8150	
10	B	ug/mL					25.6	
11	Ba	ug/mL					<0.024	
12	Ca	ug/mL					69.3	
13	Cd	ug/mL					36.3	
14	Ce	ug/mL					1.8	
15	Cl <sup>-</sup>	ug/mL					3360	
16	Co	ug/mL					<1.0	
17	Cr	ug/mL					134	
18	Cu	ug/mL					<0.25	
19	Fe	ug/mL					1.2	
20	K	ug/mL					1840	
21	La	ug/mL					<1.4	
22	Mg	ug/mL					<0.168	
23	Mn	ug/mL					6.2	
24	Mo	ug/mL					31.4	
25	Na	ug/mL					141000	
26	Nd	ug/mL					2.8	
27	Ni	ug/mL					228	
28	NO3 (Nitrate)	ug/mL					122000	
29	P	ug/mL					716	
30	PO4 (Phosphate)	ug/mL					2570	
31	Pb	ug/mL					32.0	
32	S	ug/mL					2910	
33	Si	ug/mL					24.0	
34	Sn	ug/mL					0.9	
35	SO4 (Sulfate)	ug/mL					7900	
36	Sr	ug/mL					35.5	
37	W	ug/mL					112	
38	Zn	ug/mL					3.2	
39	Zr	ug/mL					1.0	
40	Total Organic Carbon	ug/mL					9830	
41	Total Inorganic Carbon	ug/mL					6470	
42	Suspended Solids	wt%		14.44	14.47			
43	Total Solids	wt%		41.83	41.85			
44	Particle Size by Volume	micron						
45	Particle Size by Number	micron						
46	Kin. Viscosity	cSt				2.9		15
47	Dyn. Visc./Consistency	cP				3.7		21
48	Yield Stress	Pa						8.8
49	Density	g/mL				1.283		1.423
50	Density	g/mL	1.277	1.345	1.404	1.288		
51	Turbidity	NTU					0.28	
52	Comment - Note (1)	Note (2)						
53	Note(1)-Notes precede this table							

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	AH	AI	AJ	AK	AL	AM	AN	AO
1	Test Run ----->>		1.16-3B	1.16-3B	1.16-3B	Wash-3B	Wash-3B	Wash-3B
2	Sample Taken Date ----->		October 23, 2002	October 23, 2002	October 23, 2002	October 30, 2002	October 30, 2002	October 30, 2002
3	Sample Taken Time ----->>		test end / 19:00	test end / 19:00	test end / 19:00	prewash 22 wt%	prewash 20 wt%	prewash 20 wt%
4	Sample ID (Prefix = rpp-pxu-) ->>		slu-final1.16-3b-solids1	slu-final1.16-3b-solids2	slu-final1.16-3b-psd	slu22%-prewash-3b-rheology	slu20%-prewash-3b-rheology	fil20%-prewash-3b-table1
5	ADS Sample ID ----->>		300187857	300187858	300188110	none	none	300189078
6	Type Sample ----->>		slurry	slurry	slurry	slurry	slurry	filtrate
7	Sample Size (mL) ----->>		15	15	15	250	250	15
8	Item Measured	Units*						
9	Al	ug/mL						7950
10	B	ug/mL						n/a
11	Ba	ug/mL						n/a
12	Ca	ug/mL						82.3
13	Cd	ug/mL						38
14	Ce	ug/mL						n/a
15	Cl	ug/mL						3260
16	Co	ug/mL						n/a
17	Cr	ug/mL						84.6
18	Cu	ug/mL						4
19	Fe	ug/mL						1.2
20	K	ug/mL						1640
21	La	ug/mL						n/a
22	Mg	ug/mL						n/a
23	Mn	ug/mL						5.5
24	Mo	ug/mL						n/a
25	Na	ug/mL						146000
26	Nd	ug/mL						2.6
27	Ni	ug/mL						222
28	NO3 (Nitrate)	ug/mL						130000
29	P	ug/mL						590
30	PO4 (Phosphate)	ug/mL						2280
31	Pb	ug/mL						29.1
32	S	ug/mL						2960
33	Si	ug/mL						n/a
34	Sn	ug/mL						n/a
35	SO4 (Sulfate)	ug/mL						9030
36	Sr	ug/mL						19.2
37	W	ug/mL						n/a
38	Zn	ug/mL						2.9
39	Zr	ug/mL						n/a
40	Total Organic Carbon	ug/mL						9380
41	Total Inorganic Carbon	ug/mL						6820
42	Suspended Solids	wt%	21.69	21.65				
43	Total Solids	wt%	47.19	47.17				
44	Particle Size by Volume	micron			0.86(87%), 8.22(13%)			
45	Particle Size by Number	micron			0.80			
46	Kin. Viscosity	cSt				12	11	
47	Dyn. Visc./Consistency	cP				17	16	
48	Yield Stress	Pa				12	7.6	
49	Density	g/mL						
50	Density	g/mL	n/a	1.430				
51	Turbidity	NTU						
52	Comment - Note (1)	Note (2)			bimodal by volume			
53	Note(1)-Notes precede this table							

Table G2:AN-102 simulant analytical and other data, Page 5

	AP	AQ	AR	AS	AT	AU	AV	AW
1	Test Run ----->>		Wash-3B	Wash-3B	Wash-3B	Wash-3B	Wash-3B	Wash-3B
2	Sample Taken Date ----->>		October 30, 2002	October 30, 2002	October 30, 2002	October 30, 2002	October 30, 2002	October 30, 2002
3	Sample Taken Time ----->>		prewash 20 wt%	prewash 20 wt%	prewash 20 wt%	wash cycle 5	wash cycle 10	wash cycle 15
4	Sample ID (Prefix = rpp-pxu) ->>		fil20%-prewash-3b-solids	slu20%-prewash-3b-solids	slu20%-prewash-3b-psd	fil20%-wash-5-3b-ICPES	fil20%-wash-10-3b-ICPES	fil20%-wash-15-3b-ICPES
5	ADS Sample ID ----->>		300189087	300189088	300189271	300189083	300189084	300189085
6	Type Sample ----->>		filtrate	slurry	slurry	filtrate	filtrate	filtrate
7	Sample Size (mL) ----->>		15	15	15	15	15	15
8	Item Measured	Units*						
9	Al	ug/mL				6620	4940	3460
10	B	ug/mL						
11	Ba	ug/mL						
12	Ca	ug/mL				72.6	57.1	42.9
13	Cd	ug/mL				32.1	24.7	17.6
14	Ce	ug/mL						
15	Cl <sup>-</sup>	ug/mL						
16	Co	ug/mL						
17	Cr	ug/mL				70	53	38
18	Cu	ug/mL				3.8	2.9	2.0
19	Fe	ug/mL				1.0	0.6	0.3
20	K	ug/mL				1410	1030	714
21	La	ug/mL						
22	Mg	ug/mL						
23	Mn	ug/mL				4.5	2.7	1.2
24	Mo	ug/mL						
25	Na	ug/mL				123000	95000	68900
26	Nd	ug/mL				1.4	1.1	<0.52
27	Ni	ug/mL				188	140	101
28	NO3 (Nitrate)	ug/mL						
29	P	ug/mL				900	1190	1630
30	PO4 (Phosphate)	ug/mL						
31	Pb	ug/mL				21.2	13.7	8.3
32	S	ug/mL				2530	1920	1390
33	Si	ug/mL						
34	Sn	ug/mL						
35	SO4 (Sulfate)	ug/mL						
36	Sr	ug/mL				16.9	15.2	5.0
37	W	ug/mL						
38	Zn	ug/mL				2.2	1.4	0.9
39	Zr	ug/mL						
40	Total Organic Carbon	ug/mL						
41	Total Inorganic Carbon	ug/mL						
42	Suspended Solids	wt%		18.95				
43	Total Solids	wt%	32.66	45.42				
44	Particle Size by Volume	micron			1.34(98%), 5.89(2%)			
45	Particle Size by Number	micron			1.21			
46	Kin. Viscosity	cSt						
47	Dyn. Visc./Consistency	cP						
48	Yield Stress	Pa						
49	Density	g/mL						
50	Density	g/mL	1.280	1.355				
51	Turbidity	NTU						
52	Comment - Note (1)	Note (2)			bimodal by volume			
53	Note(1)-Notes precede this table							

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	AX	AY	AZ	BA	BB	BC	BD	BE
1	Test Run ----->>		Wash-3B	Wash-3B	Wash-3B	Wash-3B	Wash-3B	130-3B
2	Sample Taken Date ----->>		October 30, 2002	October 30, 2002	October 30, 2002	October 30, 2002	October 30, 2002	October 31, 2002
3	Sample Taken Time ----->>		postwash	postwash	postwash	postwash	postwash	test end
4	Sample ID (Prefix = rpp-pxu-) ->>		slu-postwash-3b-rheology	filt-postwash-3b-table1	filt-postwash-3b-solids	slu-postwash-3b-solids	slu-postwash-3b-psd	filt-end1.30-3b-solids
5	ADS Sample ID ----->>		none	300189079	300189089	300189090	300189272	300189091
6	Type Sample ----->>		slurry	filtrate	filtrate	slurry	slurry	filtrate
7	Sample Size (mL) ----->>		250	15	15	15	15	15
8	Item Measured	Units*						
9	Al	ug/mL		2230				
10	B	ug/mL		n/a				
11	Ba	ug/mL		n/a				
12	Ca	ug/mL		30.7				
13	Cd	ug/mL		10.4				
14	Ce	ug/mL		n/a				
15	Cl <sup>-</sup>	ug/mL		945				
16	Co	ug/mL		n/a				
17	Cr	ug/mL		25				
18	Cu	ug/mL		1.3				
19	Fe	ug/mL		0.2				
20	K	ug/mL		438				
21	La	ug/mL		n/a				
22	Mg	ug/mL		n/a				
23	Mn	ug/mL		1.0				
24	Mo	ug/mL		n/a				
25	Na	ug/mL		45500				
26	Nd	ug/mL		<0.52				
27	Ni	ug/mL		66				
28	NO3 (Nitrate)	ug/mL		33700				
29	P	ug/mL		792				
30	PO4 (Phosphate)	ug/mL		2390				
31	Pb	ug/mL		5.5				
32	S	ug/mL		894				
33	Si	ug/mL		n/a				
34	Sn	ug/mL		n/a				
35	SO4 (Sulfate)	ug/mL		2460				
36	Sr	ug/mL		12.4				
37	W	ug/mL		n/a				
38	Zn	ug/mL		<0.74				
39	Zr	ug/mL		n/a				
40	Total Organic Carbon	ug/mL		2910				
41	Total Inorganic Carbon	ug/mL		2470				
42	Suspended Solids	wt%				18.83		
43	Total Solids	wt%				28.50		10.07
44	Particle Size by Volume	micron					1.48(93%), 6.89(7%)	
45	Particle Size by Number	micron					1.25	
46	Kin. Viscosity	cSt	6.2					
47	Dyn. Visc./Consistency	cP	7.1					
48	Yield Stress	Pa	14					
49	Density	g/mL						
50	Density	g/mL			1.090	1.150		1.070
51	Turbidity	NTU						
52	Comment - Note (1)	Note (2)					bimodal by volume	
53	Note(1)-Notes precede this table							

Table G2:AN-102 simulant analytical and other data, Page 7

	BF	BG	BH	BI	BJ	BK	BL	BM	BN
1	Test Run ----->>		130-3B	130-3B	130-3B	130-3B		1.16-3A	1.16-3A
2	Sample Taken Date ----->>		October 31, 2002	October 31, 2002	October 31, 2002	October 31, 2002		November 6, 2002	November 6, 2002
3	Sample Taken Time ----->>		test end	test end	test end	test end		before test	before test
4	Sample ID (Prefix = rpp-pxu-) -->>		filt-end1.30-3b-table1	slu-end1.30-3b-rheology	slu-end1.30-3b-table1	slu-end1.30-3b-solids		slu-pre1.16-3a-rheology	slu-pre1.16-3a-solids1
5	ADS Sample ID ----->>		300189080	none	300189086	300189092		none	300188474
6	Type Sample ----->>		filtrate	slurry	slurry (units=ug/g)	slurry		slurry	slurry
7	Sample Size (mL) ----->>		15	250	15	15		250	15
8	Item Measured	Units*							
9	Al	ug/mL	1850		2970				
10	B	ug/mL	n/a		n/a				
11	Ba	ug/mL	n/a		590.0				
12	Ca	ug/mL	27.6		3590.0				
13	Cd	ug/mL	6.9		n/a				
14	Ce	ug/mL	n/a		410.0				
15	Cl <sup>-</sup>	ug/mL	782		557				
16	Co	ug/mL	n/a		n/a				
17	Cr	ug/mL	22		155				
18	Cu	ug/mL	0.8		193.0				
19	Fe	ug/mL	0.2		607.0				
20	K	ug/mL	359		335				
21	La	ug/mL	n/a		346.0				
22	Mg	ug/mL	n/a		209.0				
23	Mn	ug/mL	0.5		37700.0				
24	Mo	ug/mL	n/a		n/a				
25	Na	ug/mL	38400		39000				
26	Nd	ug/mL	<0.52		668.0				
27	Ni	ug/mL	55		663				
28	NO3 (Nitrate)	ug/mL	28200		21400				
29	P	ug/mL	208		1880				
30	PO4 (Phosphate)	ug/mL	736		1140				
31	Pb	ug/mL	2.8		1260.0				
32	S	ug/mL	751		742				
33	Si	ug/mL	n/a		49.0				
34	Sn	ug/mL	n/a		<6.0				
35	SO4 (Sulfate)	ug/mL	2070		1700				
36	Sr	ug/mL	6.4		88700.0				
37	W	ug/mL	n/a		n/a				
38	Zn	ug/mL	<0.74		27.8				
39	Zr	ug/mL	n/a		84.5				
40	Total Organic Carbon	ug/mL	2570		3450				
41	Total Inorganic Carbon	ug/mL	2340		3960				
42	Suspended Solids	wt%				25.25			1.56
43	Total Solids	wt%				33.06			33.02
44	Particle Size by Volume	micron							
45	Particle Size by Number	micron							
46	Kin. Viscosity	cSt		11				3.2	
47	Dyn. Visc./Consistency	cP		14				4.1	
48	Yield Stress	Pa		44				0.0	
49	Density	g/mL						1.286	
50	Density	g/mL				1.250			1.280
51	Turbidity	NTU							
52	Comment - Note (1)	Note (2)							
53	Note(1)-Notes precede this table								

Table G2:AN-102 simulant analytical and other data, Page 8

	BO	BP	BQ	BR	BS	BT	BU	BV	BW
1	Test Run ----->>>		1.16-3A	1.16-3A	1.16-3A	1.16-3A	1.16-3A	1.16-3A	1.16-3A
2	Sample Taken Date ----->>		November 6, 2002	November 6, 2002	November 6, 2002	November 6, 2002	November 7, 2002	November 7, 2002	November 7, 2002
3	Sample Taken Time ----->>>		before test	before test	1 hr into test	1 hr into test	14 wt% / 15:00 hours	14 wt% / 15:00 hours	14 wt% / 15:00 hours
4	Sample ID (Prefix = rpp-pxu-) ->>		slu-pre1.16-3a-solids2	slu-pre1.16-3a-psd	filt-pre1.16-3a-turbidity	filt-pre1.16-3a-table1	filt-end1.16-3a-turbidity	filt-end1.16-3a-solids	filt-end1.16-3a-rheology
5	ADS Sample ID ----->>>		300188475	300189273	none	300189081	none	none	none
6	Type Sample ----->>>		slurry	slurry	filtrate	filtrate	filtrate	filtrate	slurry
7	Sample Size (mL) ----->>>		15	15	15	15	250	15	250
8	Item Measured	Units*							
9	Al	ug/mL				7880			
10	B	ug/mL				n/a			
11	Ba	ug/mL				n/a			
12	Ca	ug/mL				51.8			
13	Cd	ug/mL				32.9			
14	Ce	ug/mL				n/a			
15	Cf	ug/mL				2830			
16	Co	ug/mL				n/a			
17	Cr	ug/mL				128			
18	Cu	ug/mL				0.6			
19	Fe	ug/mL				2.5			
20	K	ug/mL				1610			
21	La	ug/mL				n/a			
22	Mg	ug/mL				n/a			
23	Mn	ug/mL				5.3			
24	Mo	ug/mL				n/a			
25	Na	ug/mL				137000			
26	Nd	ug/mL				10.1			
27	Ni	ug/mL				221			
28	NO3 (Nitrate)	ug/mL				117000			
29	P	ug/mL				675			
30	PO4 (Phosphate)	ug/mL				2000			
31	Pb	ug/mL				16.5			
32	S	ug/mL				2860			
33	Si	ug/mL				n/a			
34	Sn	ug/mL				n/a			
35	SO4 (Sulfate)	ug/mL				7680			
36	Sr	ug/mL				89.5			
37	W	ug/mL				n/a			
38	Zn	ug/mL				2.9			
39	Zr	ug/mL				n/a			
40	Total Organic Carbon	ug/mL				9280			
41	Total Inorganic Carbon	ug/mL				6320			
42	Suspended Solids	wt%	1.62						
43	Total Solids	wt%	33.04						
44	Particle Size by Volume	micron		2.82(58%), 9.79(42%)					
45	Particle Size by Number	micron		1.98					
46	Kin. Viscosity	cSt			2.9		3.0		7.9
47	Dyn. Visc./Consistency	cP			3.7		3.8		11.0
48	Yield Stress	Pa							2.1
49	Density	g/mL			1.276		1.280		1.386
50	Density	g/mL	1.300					1.280	
51	Turbidity	NTU			0.18		0.13		
52	Comment - Note (1)	Note (2)		bimodal by volume					
53	Note(1)-Notes precede this table								

Table G2:AN-102 simulant analytical and other data, Page 9

	BX	BY	BZ	CA	CB	CC	CD	CE
1	Test Run ----->>		1.16-3A	1.16-3A	1.16-3A	1.16-3A	1.16-3A	1.16-3A
2	Sample Taken Date ----->>		November 7, 2002	November 7, 2002	November 7, 2002	November 11, 2002	November 11, 2002	November 11, 2002
3	Sample Taken Time ----->>		14 wt% / 15:00 hours	14 wt% / 15:00 hours	14 wt% / 15:00 hours	25 wt% / 11:30 hours	25 wt% / 11:30 hours	25 wt% / 11:30 hours
4	Sample ID (Prefix = rpp-pxu-) ->>		slu-end1.16-3a-solids1	slu-end1.16-3a-solids2	slu-end1.16-3a-psd	filt-final1.16-3a-turbidity	filt-final1.16-3a-solids	slu-final1.16-3a-rheology
5	ADS Sample ID ----->>		300188585	300188586	300189274	none	none	none
6	Type Sample ----->>		slurry	slurry	slurry	filtrate	filtrate	slurry
7	Sample Size (mL) ----->>		15	15	15	250	15	250
8	Item Measured	Units*						
9	Al	ug/mL						
10	B	ug/mL						
11	Ba	ug/mL						
12	Ca	ug/mL						
13	Cd	ug/mL						
14	Ce	ug/mL						
15	Cl	ug/mL						
16	Co	ug/mL						
17	Cr	ug/mL						
18	Cu	ug/mL						
19	Fe	ug/mL						
20	K	ug/mL						
21	La	ug/mL						
22	Mg	ug/mL						
23	Mn	ug/mL						
24	Mo	ug/mL						
25	Na	ug/mL						
26	Nd	ug/mL						
27	Ni	ug/mL						
28	NO3 (Nitrate)	ug/mL						
29	P	ug/mL						
30	PO4 (Phosphate)	ug/mL						
31	Pb	ug/mL						
32	S	ug/mL						
33	Si	ug/mL						
34	Sn	ug/mL						
35	SO4 (Sulfate)	ug/mL						
36	Sr	ug/mL						
37	W	ug/mL						
38	Zn	ug/mL						
39	Zr	ug/mL						
40	Total Organic Carbon	ug/mL						
41	Total Inorganic Carbon	ug/mL						
42	Suspended Solids	wt%	14.14	13.97				
43	Total Solids	wt%	41.67	41.55				
44	Particle Size by Volume	micron			2.79			
45	Particle Size by Number	micron			1.79			
46	Kin. Viscosity	cSt				3.5		17
47	Dyn. Visc./Consistency	cP				4.5		24
48	Yield Stress	Pa						24
49	Density	g/mL				1.283		1.469
50	Density	g/mL	1.3 (too low?)	1.26 (too low?)			1.270	
51	Turbidity	NTU				0.23		
52	Comment - Note (1)	Note (2)						
53	Note(1)-Notes precede this table							

Table G2:AN-102 simulant analytical and other data, Page 10

	CG	CH	CI	CJ	CK	CL	CM	CN	CO
1	Test Run ----->>		1.16-3A	1.16-3A	1.16-3A		1.16-4A	1.16-4A	1.16-4A
2	Sample Taken Date ----->>		November 11, 2002	November 11, 2002	November 11, 2002		March 12, 2003	March 12, 2003	March 12, 2003
3	Sample Taken Time ----->>		25 wt% / 11:30 hours	25 wt% / 11:30 hours	25 wt% / 11:30 hours		before test	before test	before test
4	Sample ID (Prefix = rpp-pxu-) -->>		slu-final1.16-3a-solids1	slu-final1.16-3a-solids2	slu-final1.16-3a-psd		slu-pre1.16-4a-rheology	slu-pre1.16-4a-archive	slu-pre1.16-4a-solids1
5	ADS Sample ID ----->>		300188587	300188588	300189275		none	none	300192924
6	Type Sample ----->>		slurry	slurry	filtrate		slurry	slurry	slurry
7	Sample Size (mL) ----->>		15	15	15		250	250	15
8	Item Measured	Units*							
9	Al	ug/mL							
10	B	ug/mL							
11	Ba	ug/mL							
12	Ca	ug/mL							
13	Cd	ug/mL							
14	Ce	ug/mL							
15	Cf	ug/mL							
16	Co	ug/mL							
17	Cr	ug/mL							
18	Cu	ug/mL							
19	Fe	ug/mL							
20	K	ug/mL							
21	La	ug/mL							
22	Mg	ug/mL							
23	Mn	ug/mL							
24	Mo	ug/mL							
25	Na	ug/mL							
26	Nd	ug/mL							
27	Ni	ug/mL							
28	NO3 (Nitrate)	ug/mL							
29	P	ug/mL							
30	PO4 (Phosphate)	ug/mL							
31	Pb	ug/mL							
32	S	ug/mL							
33	Si	ug/mL							
34	Sn	ug/mL							
35	SO4 (Sulfate)	ug/mL							
36	Sr	ug/mL							
37	W	ug/mL							
38	Zn	ug/mL							
39	Zr	ug/mL							
40	Total Organic Carbon	ug/mL							
41	Total Inorganic Carbon	ug/mL							
42	Suspended Solids	wt%	25.24	25.39					1.40
43	Total Solids	wt%	49.27	49.37					33.34
44	Particle Size by Volume	micron			2.53				
45	Particle Size by Number	micron			1.83				
46	Kin. Viscosity	cSt				3.3			
47	Dyn. Visc./Consistency	cP				4.2			
48	Yield Stress	Pa				0.0			
49	Density	g/mL					1.289		
50	Density	g/mL	1.470	1.430					
51	Turbidity	NTU							
52	Comment - Note (1)	Note (2)							
53	Note(1)-Notes precede this table								

Table G2:AN-102 simulant analytical and other data, Page 11

	CP	CQ	CR	CS	CT	CU	CV	CW	CX	
1	Test Run ----->>		1.16-4A	1.16-4A	1.16-4A	1.16-4A	1.16-4A	1.16-4A	1.16-4A	
2	Sample Taken Date ----->>		March 12, 2003	March 12, 2003	March 12, 2003	March 12, 2003	March 12, 2003	March 12, 2003	March 13, 2003	
3	Sample Taken Time ----->>		before test	before test	1 hr into test	1 hr into test	1 hr into test	1 hr into test	18 wt% / 04:11 hours	
4	Sample ID (Prefix = rpp-pxu-) ----->>		slu-pre1.16-4a-solids2	slu-pre1.16-4a-psd	filt-pre1.16-4a-turbidity	filt-pre1.16-4a-table1a	filt-pre1.16-4a-table1b	filt-pre1.16-4a-table1c	filt-end1.16-4a-turbidity	
5	ADS Sample ID ----->>		300192925	300192929	none	300192931	300192932	300192933	none	
6	Type Sample ----->>		slurry	slurry	filtrate	filtrate	filtrate	filtrate	filtrate	
7	Sample Size (mL) ----->>		15	15	250	15	15	15	250	
8	Item Measured	Units*								
9	A1	ug/mL				7648				
10	B	ug/mL				n/a				
11	Ba	ug/mL				n/a				
12	Ca	ug/mL				60.6				
13	Cd	ug/mL				n/a				
14	Ce	ug/mL				n/a				
15	Cl	ug/mL						3280		
16	Co	ug/mL				n/a				
17	Cr	ug/mL				135				
18	Cu	ug/mL				5.3				
19	Fe	ug/mL				1.8				
20	K	ug/mL				1453				
21	La	ug/mL				<1.4				
22	Mg	ug/mL				<0.17				
23	Mn	ug/mL				9.7				
24	Mo	ug/mL				n/a				
25	Na	ug/mL				132512				
26	Nd	ug/mL				3.4				
27	Ni	ug/mL				229				
28	NO3 (Nitrate)	ug/mL						119000		
29	P	ug/mL				n/a				
30	PO4 (Phosphate)	ug/mL						3550		
31	Pb	ug/mL				66.5				
32	S	ug/mL				n/a				
33	Si	ug/mL				n/a				
34	Sn	ug/mL				n/a				
35	SO4 (Sulfate)	ug/mL						8890		
36	Sr	ug/mL				27.6				
37	W	ug/mL				n/a				
38	Zn	ug/mL				3.4				
39	Zr	ug/mL				n/a				
40	Total Organic Carbon	ug/mL					9470			
41	Total Inorganic Carbon	ug/mL					7030			
42	Suspended Solids	wt%	1.61							
43	Total Solids	wt%	33.35							
44	Particle Size by Volume	micron		2.67						
45	Particle Size by Number	micron		1.79						
46	Kin. Viscosity	cSt			2.9				3.0	
47	Dyn. Visc./Consistency	cP			3.7				3.8	
48	Yield Stress	Pa								
49	Density	g/mL			1.278					
50	Density	g/mL				1.273				
51	Turbidity	NTU			0.06				0.18	
52	Comment - Note (1)	Note (2)				density at start				
53	Note(1)-Notes precede this table									

Table G2:AN-102 simulant analytical and other data, Page 12

	CY	CZ	DA	DB	DC	DD	DE	DF
1	Test Run ----->>		1.16-4A	1.16-4A	1.16-4A	1.16-4A	1.16-4A	
2	Sample Taken Date ----->>		March 13, 2003	March 13, 2003	March 13, 2003	March 13, 2003	March 13, 2003	
3	Sample Taken Time ----->>		18 wt% / 04:11 hours	18 wt% / 04:11 hours				
4	Sample ID (Prefix = rpp-pxu-) -->		filt-end1.16-4a-solids	slu-end1.16-4a-archive	slu-end1.16-4a-solids1	slu-end1.16-4a-solids2	slu-end1.16-3a-psd	
5	ADS Sample ID ----->>		300192928	none	300192926	300192927	300192930	
6	Type Sample ----->>		filtrate	filtrate	slurry	slurry	slurry	
7	Sample Size (mL) ----->>		15	250	15	15	15	
8	Item Measured	Units*						
9	Al	ug/mL						
10	B	ug/mL						
11	Ba	ug/mL						
12	Ca	ug/mL						
13	Cd	ug/mL						
14	Ce	ug/mL						
15	Cl	ug/mL						
16	Co	ug/mL						
17	Cr	ug/mL						
18	Cu	ug/mL						
19	Fe	ug/mL						
20	K	ug/mL						
21	La	ug/mL						
22	Mg	ug/mL						
23	Mn	ug/mL						
24	Mo	ug/mL						
25	Na	ug/mL						
26	Nd	ug/mL						
27	Ni	ug/mL						
28	NO3 (Nitrate)	ug/mL						
29	P	ug/mL						
30	PO4 (Phosphate)	ug/mL						
31	Pb	ug/mL						
32	S	ug/mL						
33	Si	ug/mL						
34	Sn	ug/mL						
35	SO4 (Sulfate)	ug/mL						
36	Sr	ug/mL						
37	W	ug/mL						
38	Zn	ug/mL						
39	Zr	ug/mL						
40	Total Organic Carbon	ug/mL						
41	Total Inorganic Carbon	ug/mL						
42	Suspended Solids	wt%			18.71	18.71		
43	Total Solids	wt%	33.31		45.79	45.82		
44	Particle Size by Volume	micron					2.13	
45	Particle Size by Number	micron					1.76	
46	Kin. Viscosity	cSt		11				
47	Dyn. Visc./Consistency	cP		15				
48	Yield Stress	Pa		7.6				
49	Density	g/mL		1.315				
50	Density	g/mL	1.270		1.320	1.330		
51	Turbidity	NTU						
52	Comment - Note (1)	Note (2)		submitted for rheology	Note (6)	Note (6)		
53	Note(1)-Notes precede this table							

Table G2:AN-102 simulant analytical and other data, Page 13

## Rheology

At the beginning and the end (and at other points) of each pilot-scale cross-flow ultrafiltration test with AN-102 simulant slurry, samples were taken to measure some rheological properties, like shear stress versus shear rate, viscosity, or if non-Newtonian, consistency. The preceding table lists the viscosity, or consistency and yield shear stress, for each of the samples. This section shows graphical representation of the data used to determine those number.

Those simulant slurry samples at 25°C are: (Consistency, cP; Yield Stress, Pa)

Fig.G\_

1. AN-102R2, Batch 3C at 0.8 wt% insoluble solids	(3.6; 0.0)
2. AN-102R2, Batch 3C at 8.4 wt% insoluble solids	(9.8; 1.7)
3. AN-102R2, Batch 3B at 1.2 wt% insoluble solids	(4.0; 0.0)
4. AN-102R2, Batch 3B at 22 wt% insoluble solids	(21; 8.8)
5. AN-102R2, Batch 3B at 19 wt% insoluble solids:	(16, 7.6)
6. AN-102R2, Batch 3B (post-washed) at 18 wt% insoluble solids:	(7.1; 14)
7. AN-102R2, Batch 3B (post-washed) at 25 wt% insoluble solids:	(14; 44)
8. AN-102R2, Batch 3A at 1.6 wt% insoluble solids:	(4.1; 0.0)
9. AN-102R2, Batch 3A at 14 wt% insoluble solids:	(11; 2.1)
10. AN-102R2, Batch 3A at 25 wt% insoluble solids:	(24; 24)
11. AN-102R2, Batch 4A at 1.5 wt% insoluble solids:	(4.2; 0.0)
12. AN-102R2, Batch 4A at 18 wt% insoluble solids:	(15; 7.6)

### Note on rheological character of the AN-102R2 slurry simulant

As will be seen in the flowing shear stress versus shear strain curves the simulants do not generally produce a straight line. The slurries are actually a time dependent pseudoplastics (a thixotropic, like ink and some paints). However, when the insoluble solids concentration is low (e.g., < 2 wt%) the stress versus strain curves are approximately straight (see the next note) there is not significant shear stress at zero shear strain. That is, they behave like Newtonian fluids for which the concept viscosity is defined and are listed above when the yield stress is zero. When the concentration of the insoluble solids increases the non-Newtonian nature of the slurries becomes evident. However, for engineering purposes the slurries can be fit to a Bingham-type fluid model where over more of the strain range the stress is close to a straight line except that as the strain approaches zero there remains a finite stress, which is referred to as the Yield stress. This is the stress that must be overcome for the slurry to begin to flow; its yield point.

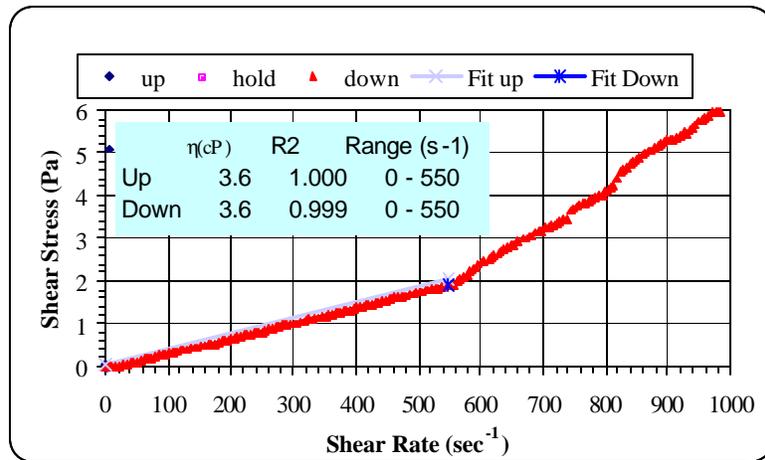
### Note on the less viscous slurry solutions: Taylor Vortices

The straight line for the lowest viscosity simulants is limited by the type of viscometer used. For the simulants with the lowest viscosities, i.e., less than 5 cP, the shear stress versus shear strain curves show a knee somewhere between a shear strain of 550 and 650 sec<sup>-1</sup>. The data for shear strains above the knee are not used in calculating slurry viscosity because the measurement is being affected by Taylor vortices. The type of

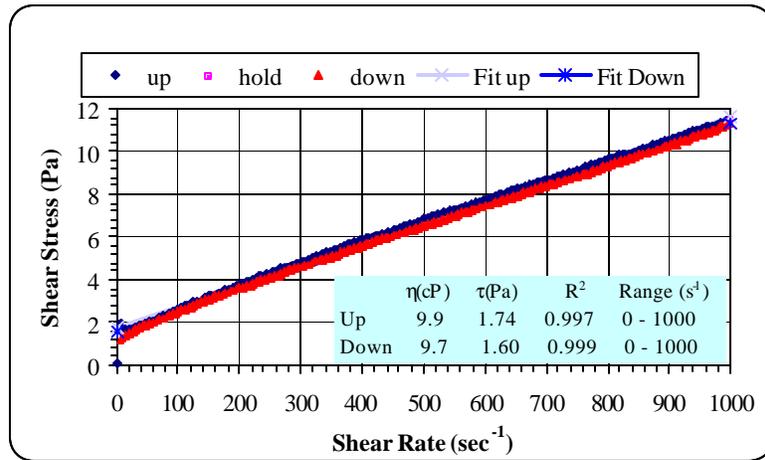
viscometer used for this work utilizes concentric cylinders. The solution to be measured filled the annular gap between two cylinder; the outer cylinder is stationary while the inner one rotates. As the inner cylinder increases with speed it imparts a centrifugal force on the solution through shear and the closer the solution to the cylinder the larger the force. That is, the solution closest to the inner cylinder feels a larger force to move away from the inner surface than the liquid further away. This secondary flow causes what is called Taylor vortices and at some point they affect and corrupt the rheological measurement. That point is evidenced by the knee in the data as seen in Figs. G1, G3, G8, and G11. This knee is not seen for the high viscosity solutions because it would occur beyond the shear strains measure for this work. To illustrate the Taylor vortices see Fig. G11. The shear stress caused by the Taylor vortices has been calculated and while the stress is below the inherent shear stress of the solution itself the solution viscosity is unaffected. However, when the shear stress of the Taylor vortices is on the same order of magnitude or large, then the rheometer measures this larger shear field, thus the knee and steeper slope of the data. If the Taylor vortices were not present the shear stress versus shear strain slope would be unaffected.

Note on choice of data included

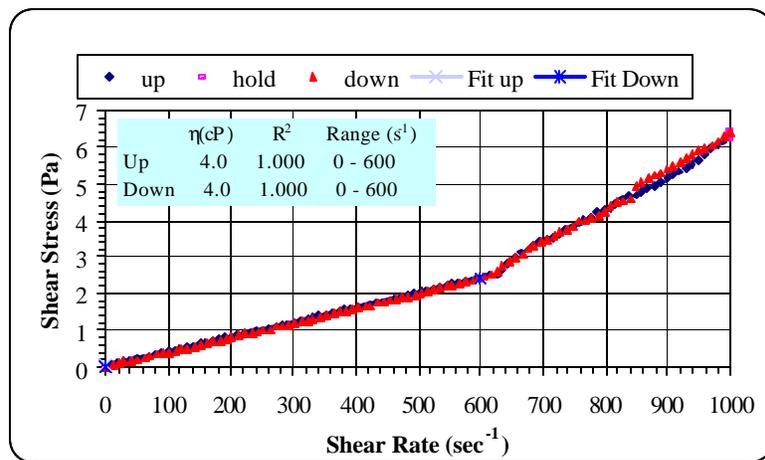
For each slurry the rheological measurements were done at least twice. However, only one graph for each data set is included since the extra data do not add more information. None of the repeated measurements showed significant differences from those shown in this sections.



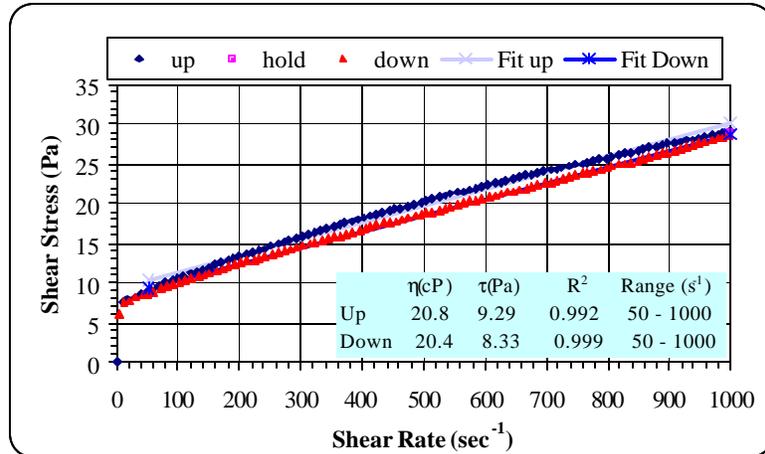
G1. AN-102R2, Batch 3C at 0.8 wt% I.S. at 25°C (Consistency = 3.6 cP; Yield Stress = 0.0 Pa)



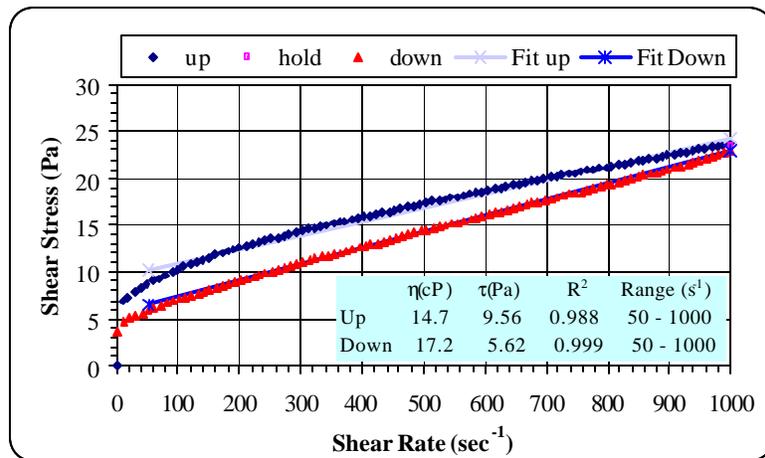
G2. AN-102R2, Batch 3C at 8.4 wt% I.S. at 25°C (Consistency = 9.8 cP; Yield Stress = 1.7 Pa)



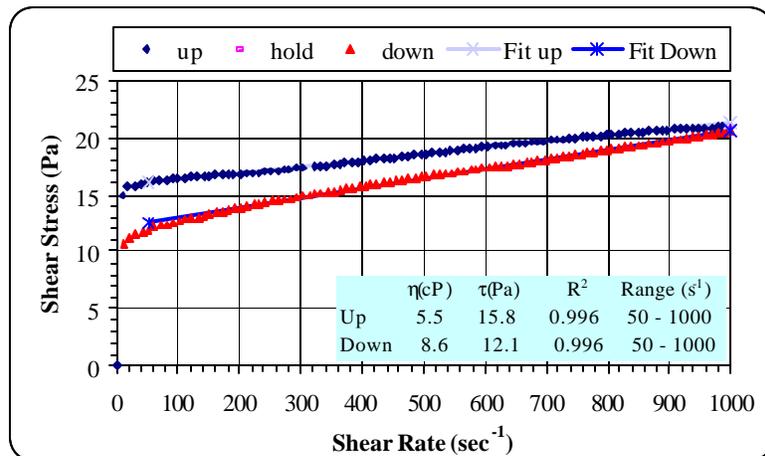
G3. AN-102R2, Batch 3B at 1.2 wt% I.S. at 25°C (Consistency = 4.0 cP; Yield Stress = 0.0 Pa)



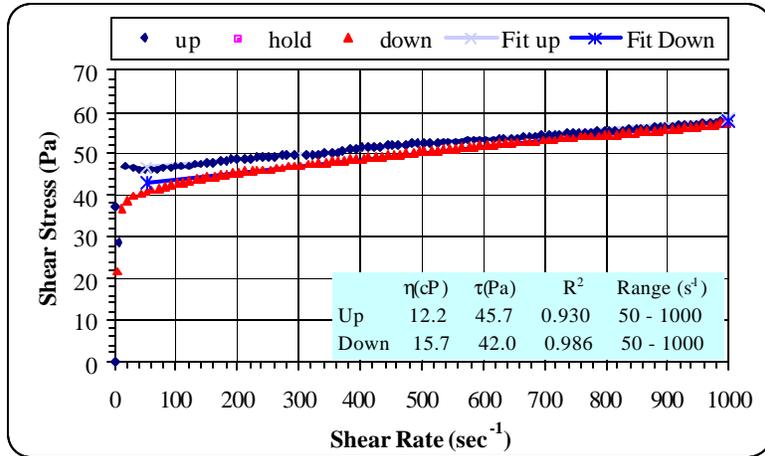
G4. AN-102R2, Batch 3B at 22 wt% I.S. at 25°C (Consistency = 21 cP; Yield Stress = 8.8 Pa)



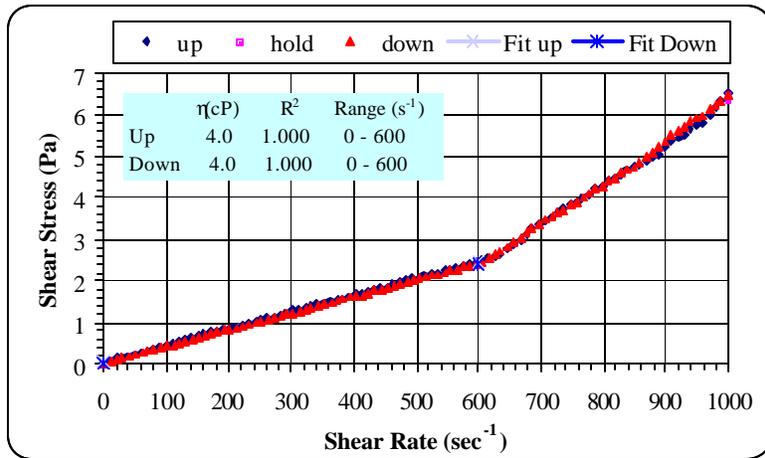
G5. AN-102R2, Batch 3B at 19 wt% I.S. at 25°C (Consistency = 16 cP; Yield Stress = 7.6 Pa)



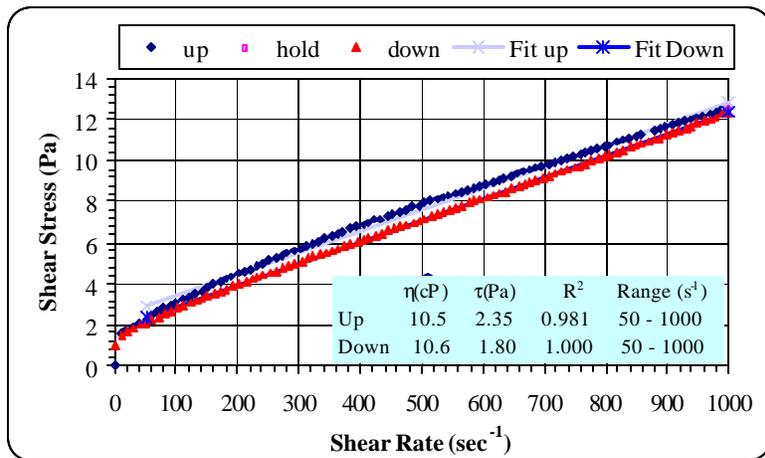
G6. AN-102R2, Batch 3B (washed) at 18 wt% I.S. at 25°C (Consistency = 7.1 cP; Yield Stress = 14 Pa)



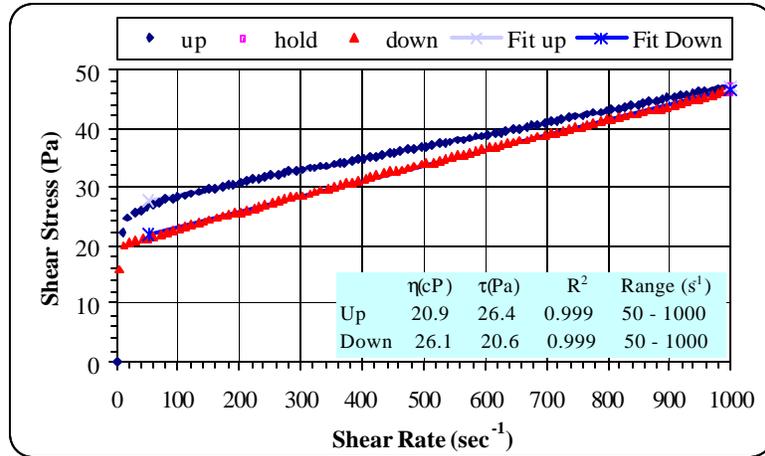
G7. AN-102R2, Batch 3B (washed) at 25 wt% I.S. at 25°C (Consistency = 14 cP; Yield Stress = 44 Pa)



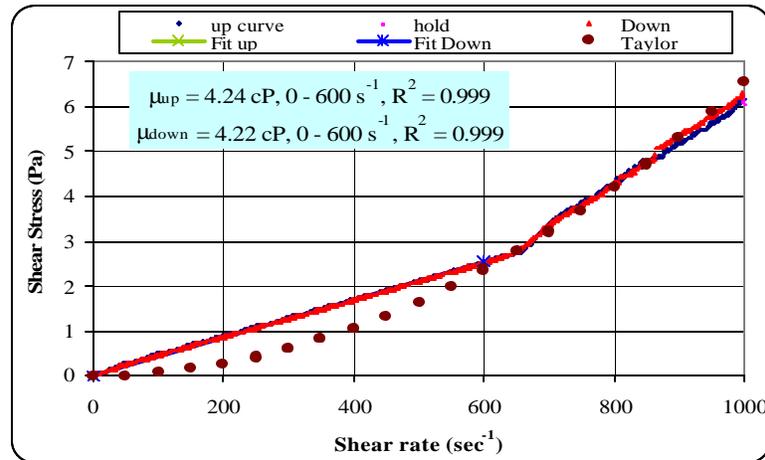
G8. AN-102R2, Batch 3A at 1.6 wt% I.S. at 25°C (Consistency = 4.0 cP; Yield Stress = 0.0 Pa)



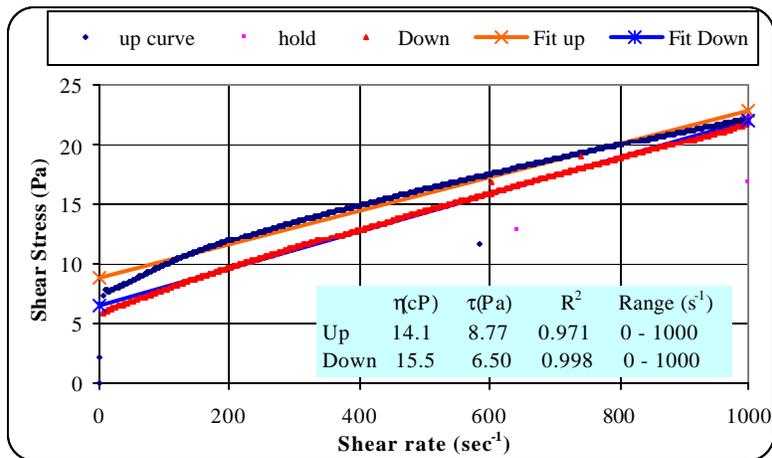
G9. AN-102R2, Batch 3A at 14 wt% I.S. at 25°C (Consistency = 11 cP; Yield Stress = 2.1 Pa)



G10. AN-102R2, Batch 3A at 25 wt% I.S. at 25°C (Consistency = 24 cP; Yield Stress = 24 Pa)



G11. AN-102R2, Batch 4A at 1.5 wt% I.S. at 25°C (Consistency = 4.2 cP; Yield Stress = 0.0 Pa)



G12. AN-102R2, Batch 4A at 18 wt% I.S. at 25°C (Consistency = 15 cP; Yield Stress = 7.6 Pa)

## Particle Size Distribution

Samples were taken at the beginning and the end (and at other points) of each pilot-scale cross-flow ultrafiltration test with AN-102 simulant slurry, to measure some rheological properties, like shear stress versus shear rate, viscosity, or if non-Newtonian, consistency. The preceding table lists the viscosity, or consistency and yield shear stress, for each of the samples. This section shows graphical representation of the data used to determine those number.

Those simulant slurry samples at 25°C are:

Fig.G\_

13. AN-102R2, Batch 3C at 0.8 wt% insoluble solids:	Volume Distribution
14. AN-102R2, Batch 3C at 0.8 wt% insoluble solids:	Number Distribution
15. AN-102R2, Batch 3C at 8.4 wt% insoluble solids:	Volume Distribution
16. AN-102R2, Batch 3C at 8.4 wt% insoluble solids:	Number Distribution
17. AN-102R2, Batch 3B at 1.2 wt% insoluble solids:	Volume Distribution
18. AN-102R2, Batch 3B at 1.2 wt% insoluble solids:	Number Distribution
19. AN-102R2, Batch 3B at 22 wt% insoluble solids:	Volume Distribution
20. AN-102R2, Batch 3B at 22 wt% insoluble solids:	Number Distribution
21. AN-102R2, Batch 3B at 19 wt% insoluble solids:	Volume Distribution
22. AN-102R2, Batch 3B at 19 wt% insoluble solids:	Number Distribution
23. AN-102R2, Batch 3B (post-washed) at 18 wt% insoluble solids:	Volume Distribution
24. AN-102R2, Batch 3B (post-washed) at 18 wt% insoluble solids:	Number Distribution
25. AN-102R2, Batch 3A at 1.6 wt% insoluble solids:	Volume Distribution
26. AN-102R2, Batch 3A at 1.6 wt% insoluble solids:	Number Distribution
27. AN-102R2, Batch 3A at 14 wt% insoluble solids:	Volume Distribution
28. AN-102R2, Batch 3A at 14 wt% insoluble solids:	Number Distribution
29. AN-102R2, Batch 3A at 25 wt% insoluble solids:	Volume Distribution
30. AN-102R2, Batch 3A at 25 wt% insoluble solids:	Number Distribution
31. AN-102R2, Batch 4A at 1.5 wt% insoluble solids:	Volume Distribution
32. AN-102R2, Batch 4A at 1.5 wt% insoluble solids:	Number Distribution
33. AN-102R2, Batch 4A at 18 wt% insoluble solids:	Volume Distribution
34. AN-102R2, Batch 4A at 18 wt% insoluble solids:	Number Distribution

### Note on Particle Size Distribution Method

Three of the methods available at the Savannah River Site to evaluate the particle size distribution (PSD) are performed by equipment made by Microtrac. They are:

Mono-laser diffraction analysis:

- a. SRA150 standard range, 20 channels: 0.7 to 700 microns
- b. SRA150 extended range, 40 channels: 0.2 to 700 microns

Tri-laser diffraction analysis

- a. X100 high resolution, 40 channels: 0.04 to 700 microns

Each method has its strong and weak points.

*SRA150 standard range*

Strong point: No knowledge of particle transparency is needed and gives immediate results.

Weak point: There is not enough resolution to discern between particle sizes and is on the threshold of the minimum particle size of interest.

*SRA150 extended range*

Strong point: It covers the range of particle size of interest

Weak point: Some knowledge of particle transparency is needed for submicron particles, however, the apparatus will make an educated guess if not known.

*X100 high resolution*

Strong point: Can measure to very small sizes

Weak point: The accuracy of the results is highly dependent on knowledge of particle transparency and the index of refraction of the fluid. The measurement is very sensitive and much more prone to measurement uncertainty without a detailed knowledge of the slurry's and solids' optical characteristics.

Because particle transparencies and simulants' index of refractions were not known the SRA150 extended range method was chosen. It covered the expected range of particle sizes and gave very consistent results with minimal input. On testing the first slurry, batch 3C, tests were done by choosing all three particle transparencies options, i.e., transparent, absorptive (opaque), or reflective. For the tests with one slurry sample all three choices gave very similar results and within the significance of measurement the difference were not important. That is, a particle size averages did not vary more that 15% amongst themselves and distribution characteristics remain the same, e.g., a bimodal distribution was obtain independent of the transparency. Table G3 shows ther results of the sample, AN-102R2, Batch 3C, at 0.8 wt% insoluble solids. (Figs. G13 and G14 are the full Microtrac results of the absorptive PSDs.)

Particle Transparency	Reflective	Transparent	Absorptive	Reflective	Transparent	Absorptive
Type Distribution	Volume	Volume	Volume	Number	Number	Number
Distribution Characteristic	Bimodal	Bimodal	Bimodal	Single	Single	Single
Large Average Particle Size	8.5 microns	8.6 microns	8.6 microns	2.3 microns	2.4 microns	2.1 microns
% of Particles in Average	69%	71%	68%	100%	100%	100%
Small Average Particle Size	2.6 microns	2.7 microns	2.6 microns	not applicable	not applicable	not applicable
% of Particles in Average	31%	29%	32%	not applicable	not applicable	not applicable
Particle Range (microns)	1.6 to 74	1.6 to 74	1.0 to 74	1.6 to 22	1.6 to 22	1.0 to 22

Table G3. Comparing particle transparency results using Microtrac SRA150 extended range with a simulant sample from AN-102R2, Batch 3C (No. 300188111)

All the following PSD analyses were done with an absorptive particle transparency because that method seemed to indicate slightly smaller particle than the other methods.

*Minimum size for SRA150 extended range*

The stated range for this method, as given above, is 0.2 to 700 micron. However, as seen in the following Microtrac data sheets is appears that the lower setting was set at

0.688 micron for an unknown reason. While the smaller size was intended, a scan of the data show that for all but a few of the samples measured the PSD data tails smoothly taper off for the smallest particles, which implies that most, if not all, particle sizes were measured. However, there are a few exceptions like for the sample of Batch 3B at its highest concentration of 22 wt%, i.e., Figs 19 and 20. In most cases, the 0.688 micron cutoff was sufficient.

Note on Sample Preparation to perform a Microtrac Evaluation

Besides the methods to choose in evaluating sample it is also important to prepare the sample properly to obtain accurate results.

*Diluent*

The slurry sample is suspended in a large volume (~0.3 liter) of dilute. The standard diluent is distilled water but due to the neutral pH and the solubility of solids in water the slurry sample were suspended in it respective filtrate. Filtrate was usually optically transparent and free of solids was used.

*Sonication*

In the past the insoluble solids in slurry samples that sat while waiting for process tended to clump and give falsely large particle measurements. To minimize this each sample was mildly agitated with sonic waves to break up such clumps. For this task the samples were sonicated four times at 15 seconds each at a power setting of 30 watts. All samples received the same treatment.

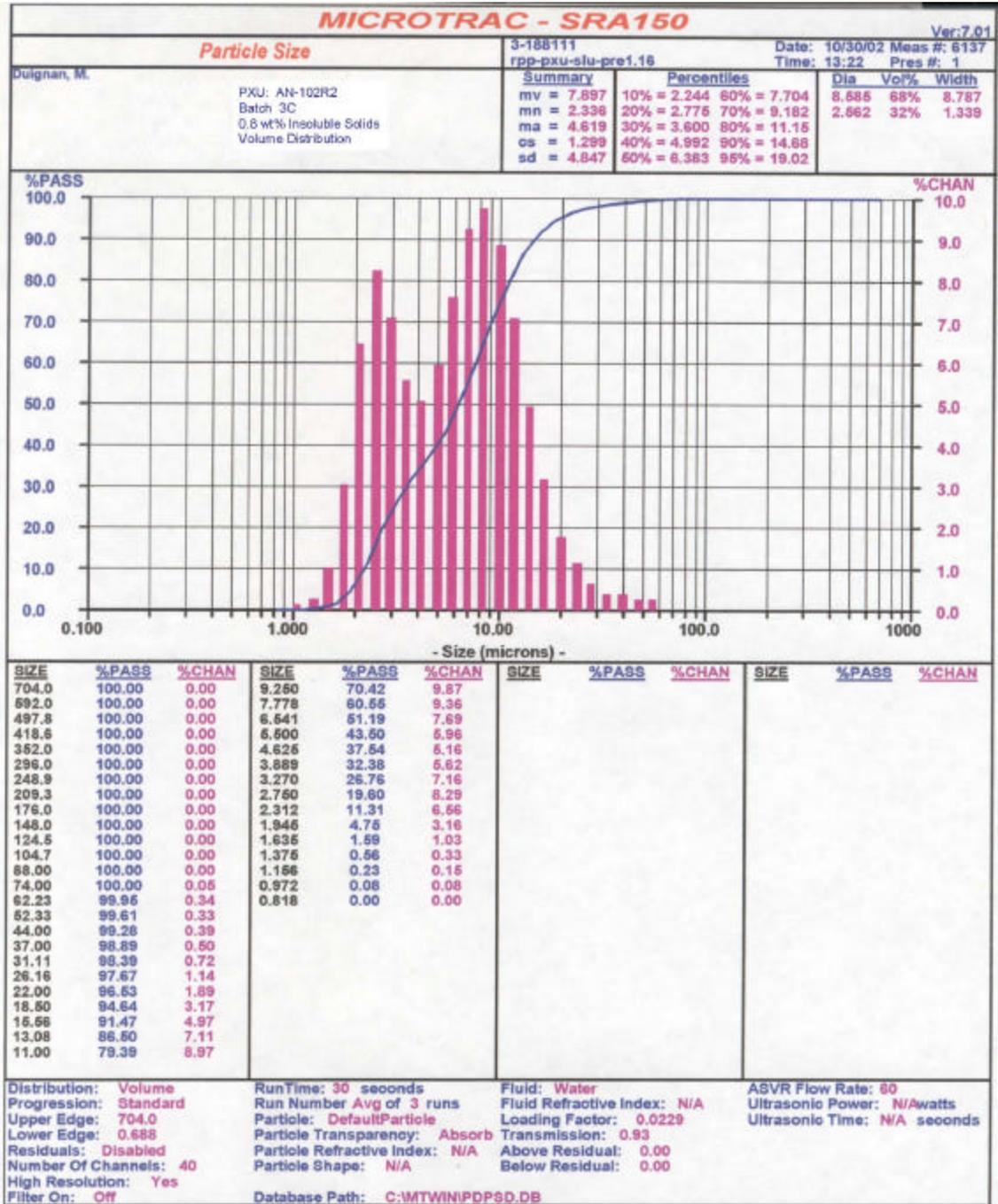


Figure G13. At start of Batch 3C dewatering: 0.8 wt% Insoluble Solids (VOLUME Distribution)

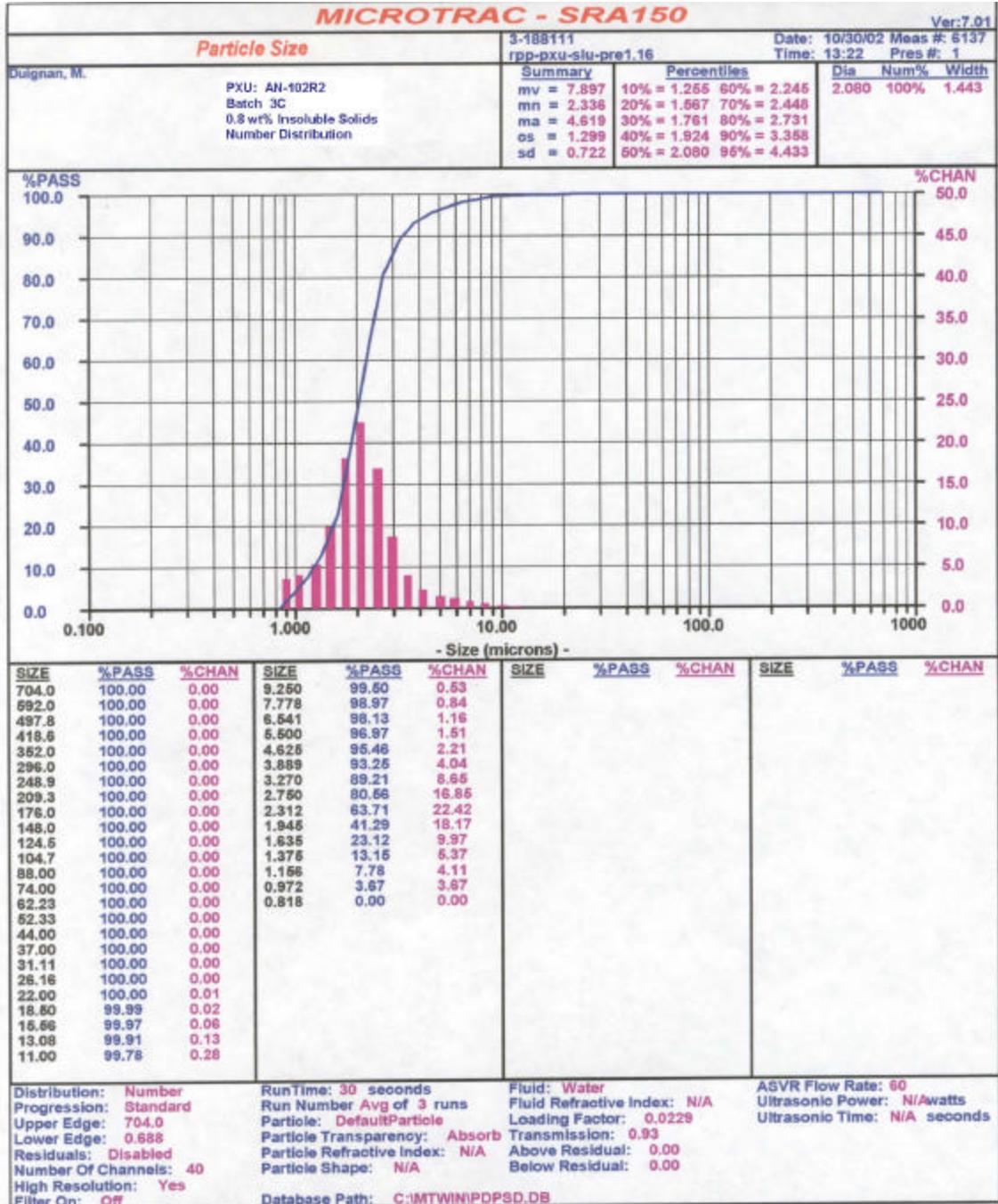


Figure G14. At start of Batch 3C dewatering: 0.8 wt% Insoluble Solids (NUMBER Distribution)

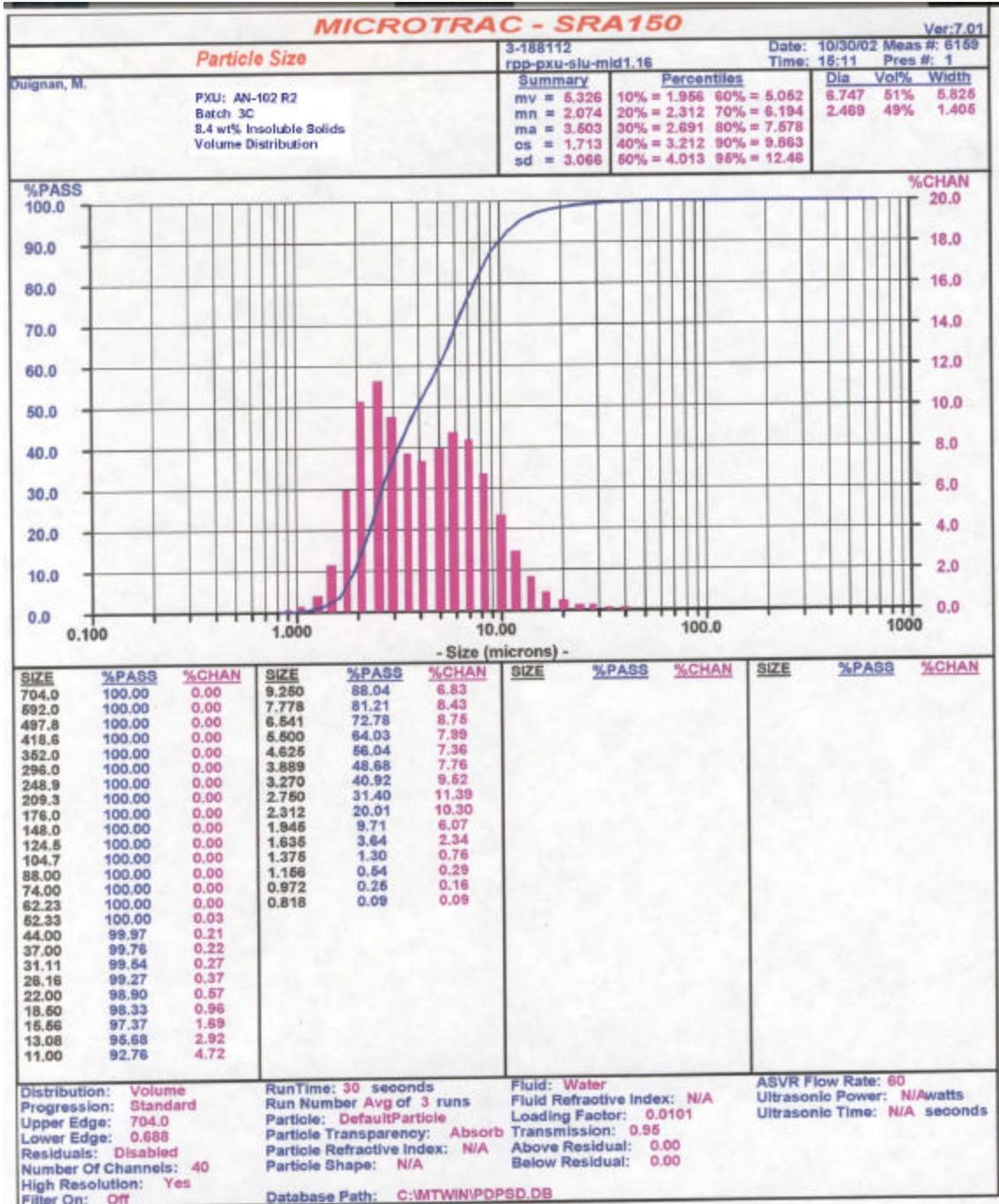


Figure G15. After 45 hours of Batch 3C dewatering: 8.4 wt% Insoluble Solids (VOLUME Distribution)

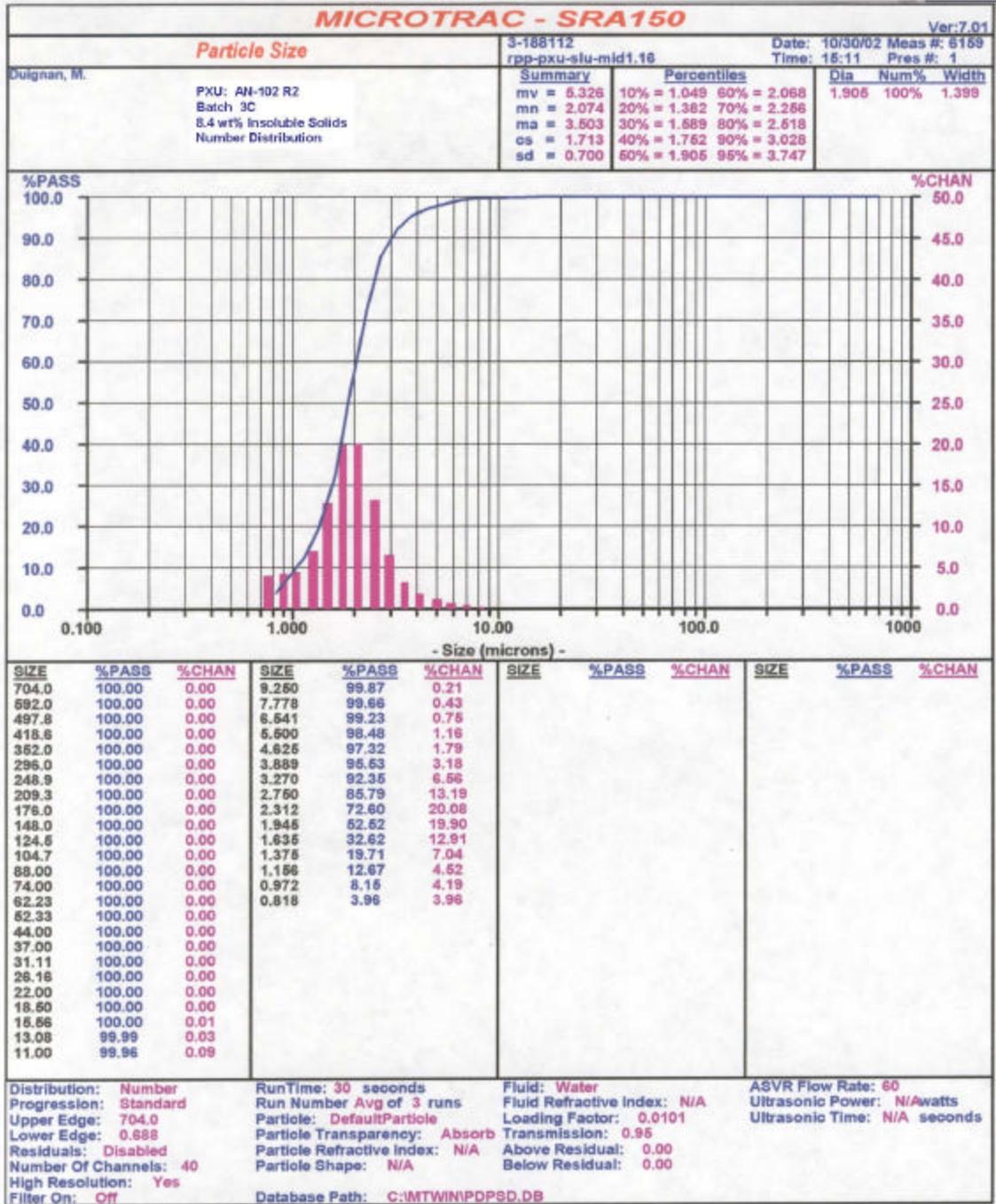


Figure G16. After 45 hours of Batch 3C dewatering: 8.4 wt% Insoluble Solids (NUMBER Distribution)

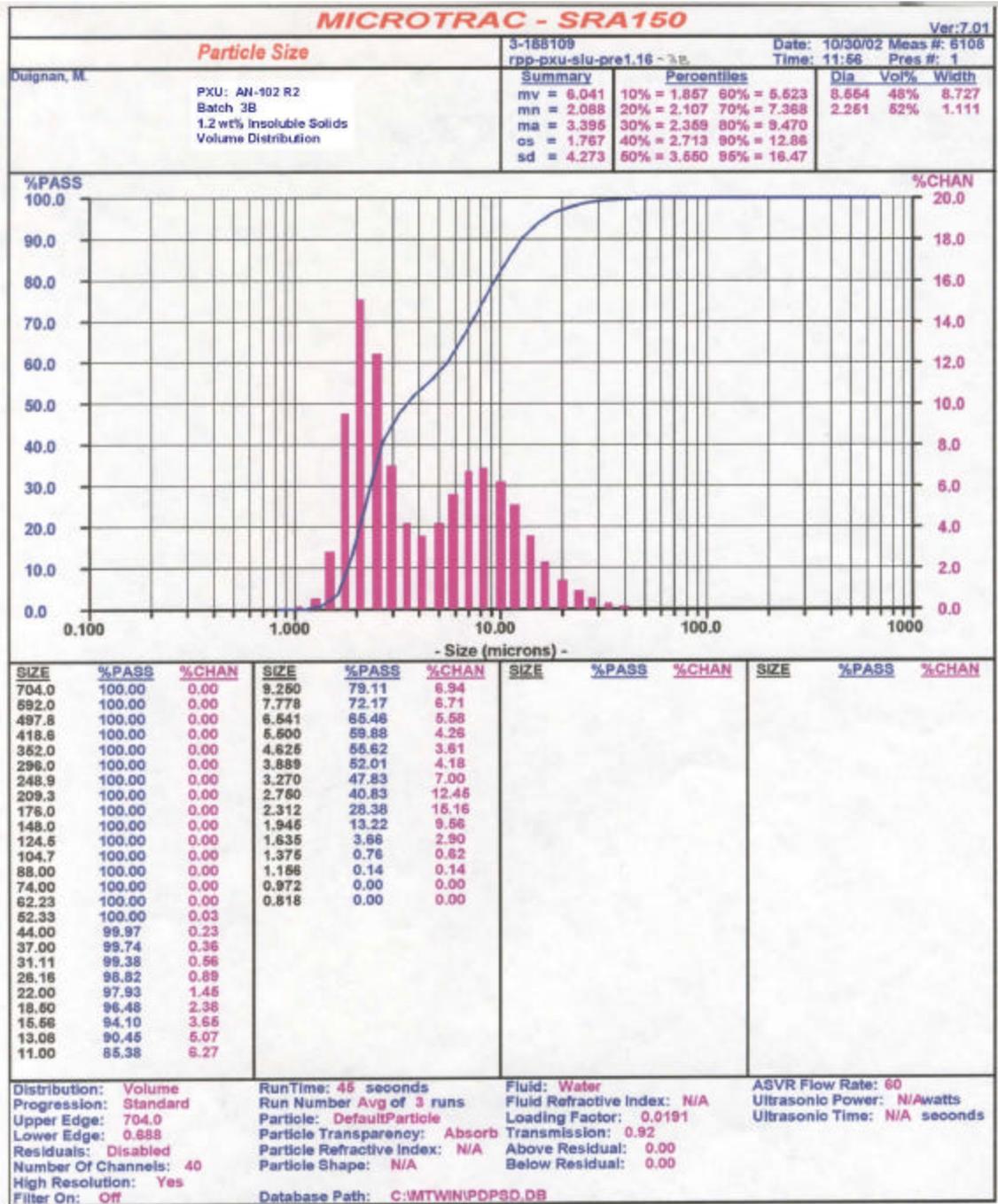


Figure G17. At start of Batch 3B dewatering: 1.2 wt% Insoluble Solids (VOLUME Distribution)

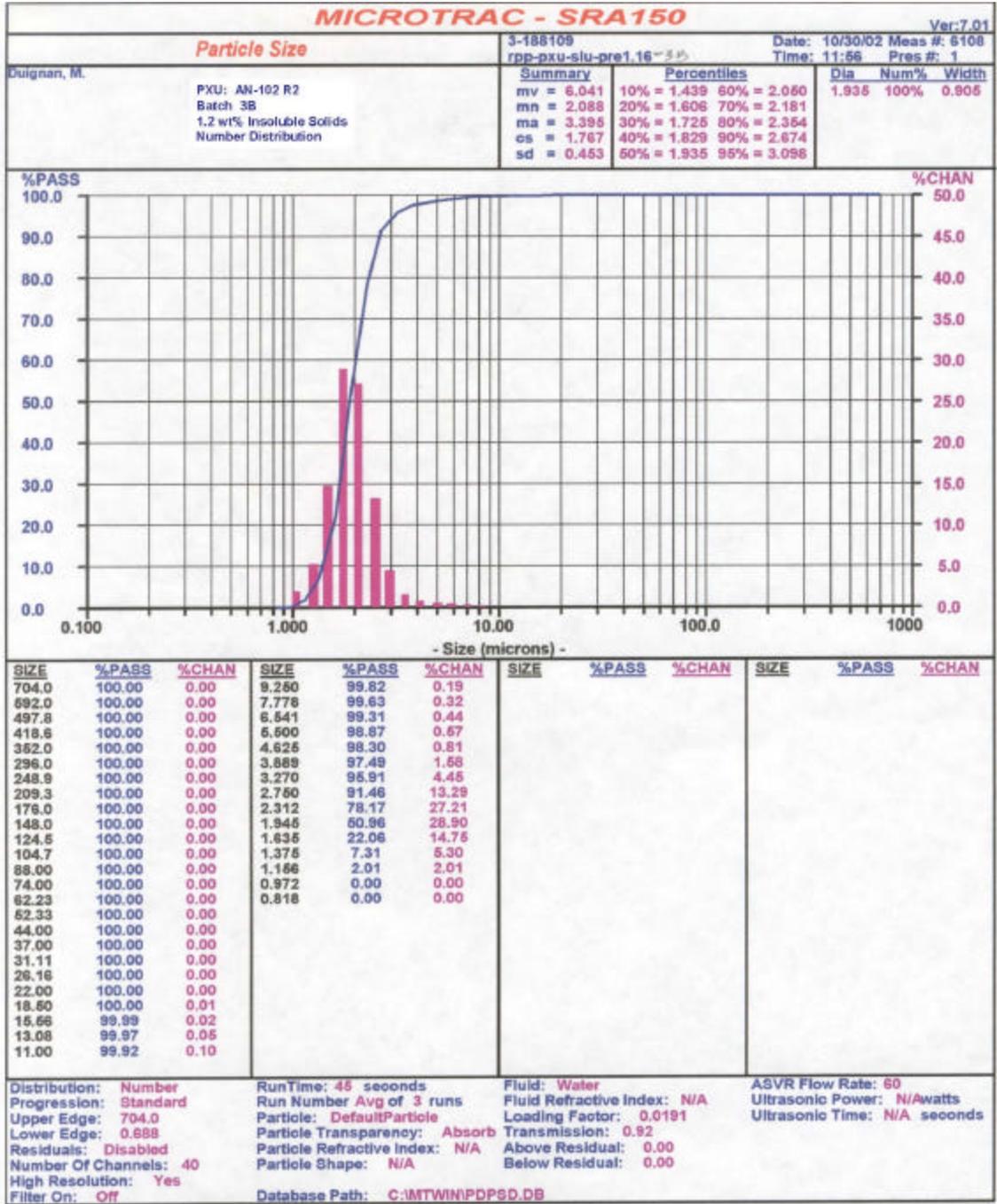


Figure G18. At start of Batch 3B dewatering: 1.2 wt% Insoluble Solids (NUMBER Distribution)

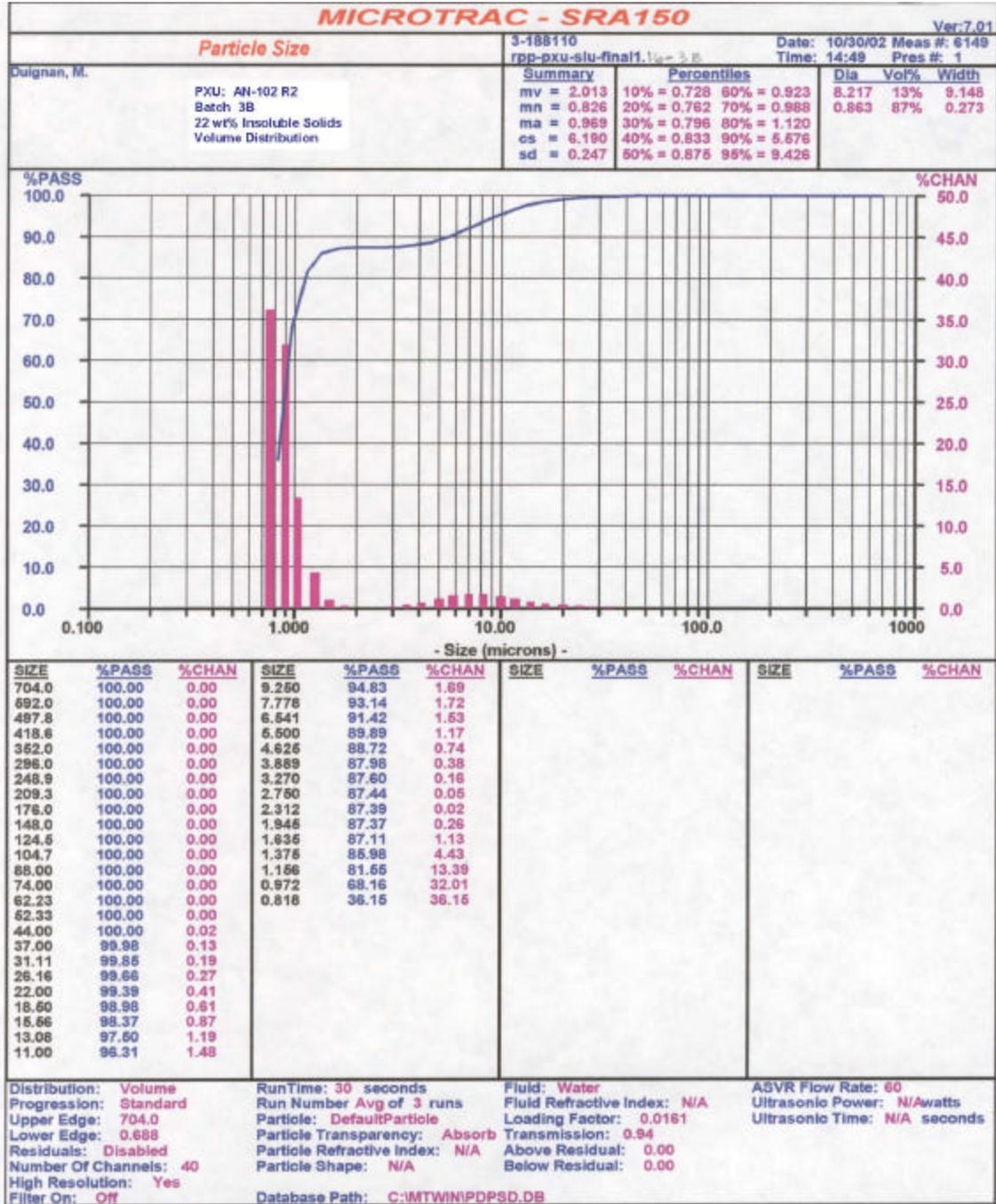


Figure G19. After 12 hours of Batch 3B dewatering: 22 wt% Insoluble Solids (VOLUME Distribution)

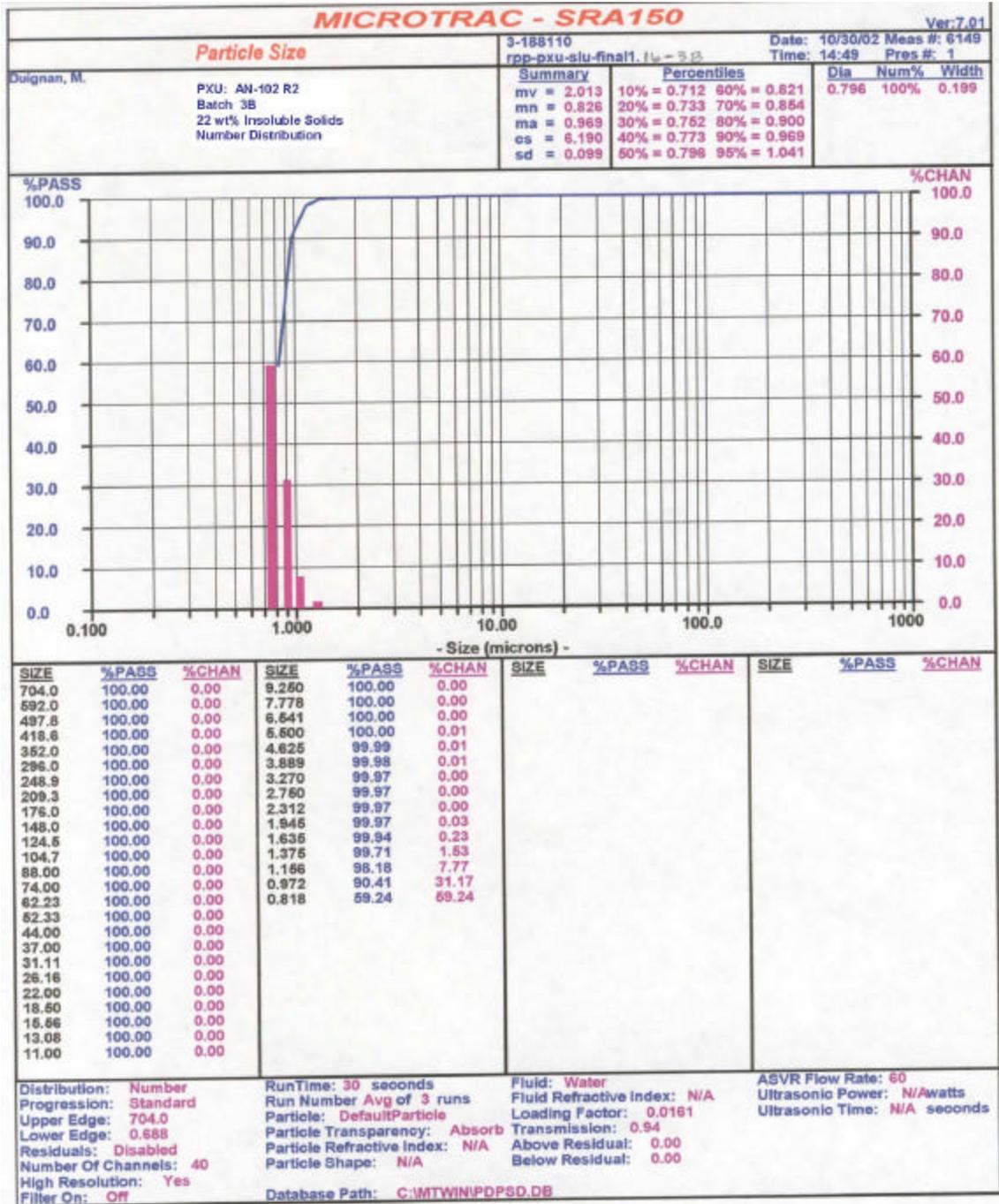


Figure G20. After 12 hours of Batch 3B dewatering: 22 wt% Insoluble Solids (NUMBER Distribution)

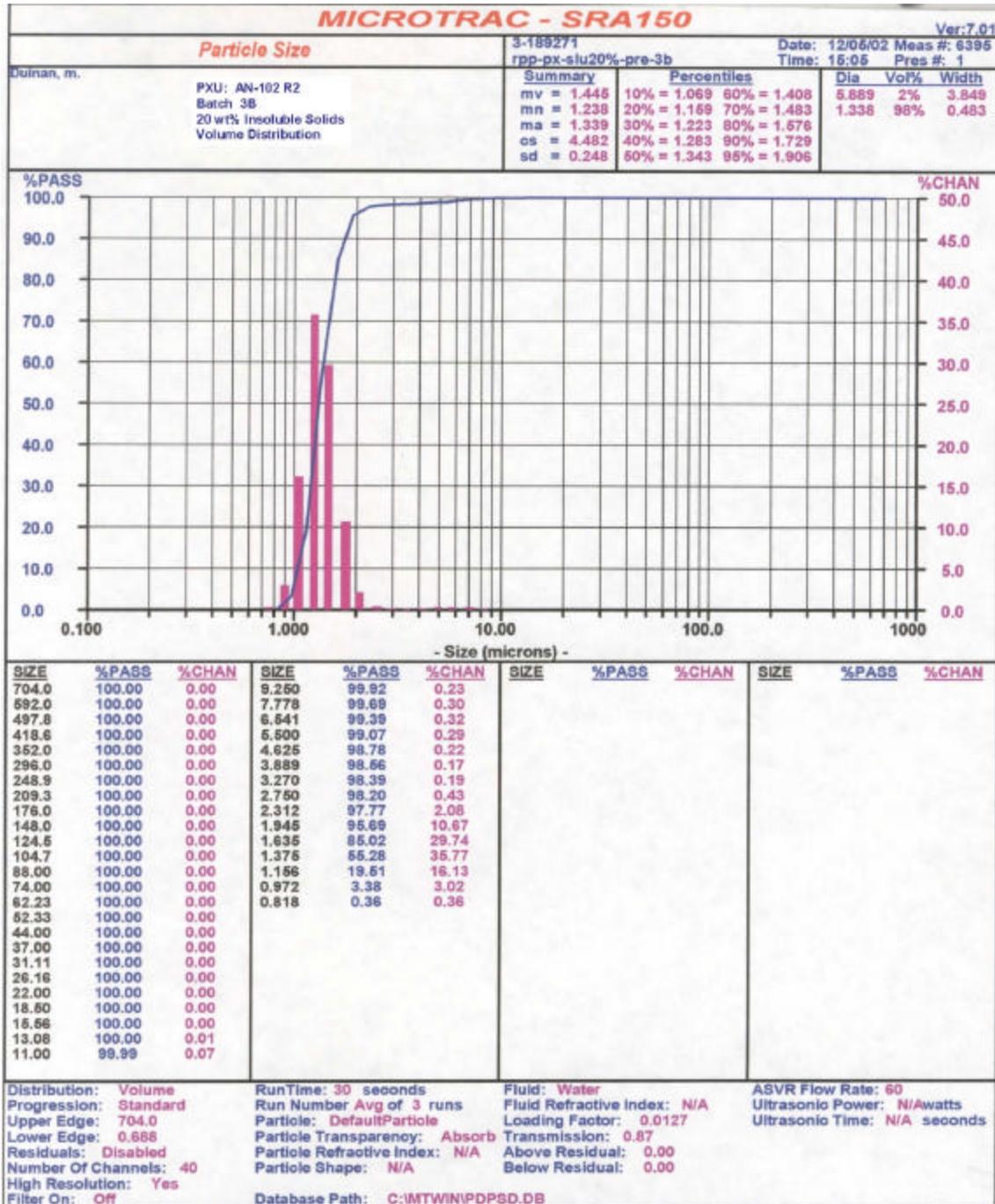


Figure G21. After 12 hours of Batch 3B dewatering: 19 wt% Insoluble Solids (VOLUME Distribution) – Diluted with filtrate to prepare for washing

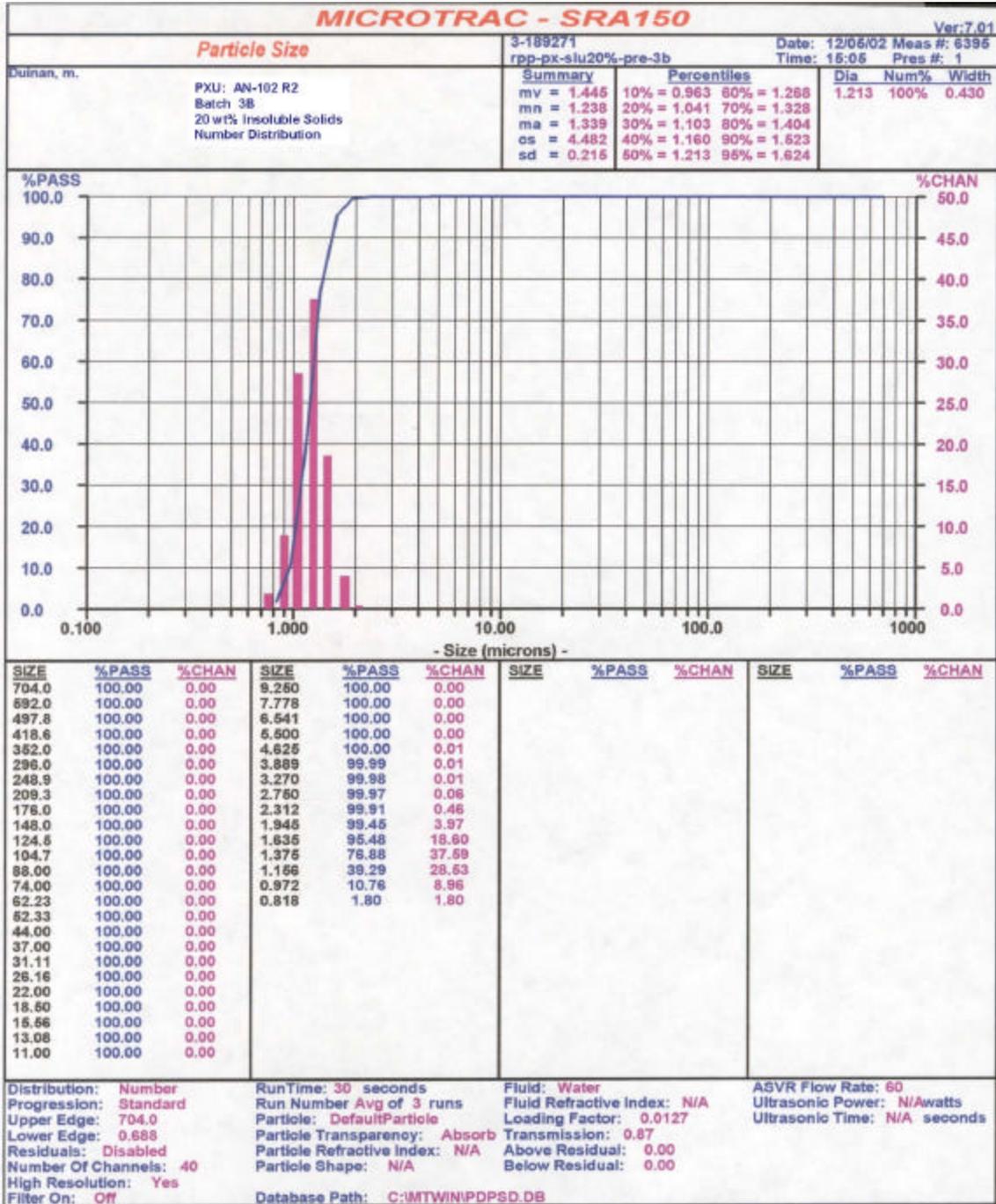


Figure G22. After 12 hours of Batch 3B dewatering: 19 wt% Insoluble Solids (NUMBER Distribution) – Diluted with filtrate to prepare for washing

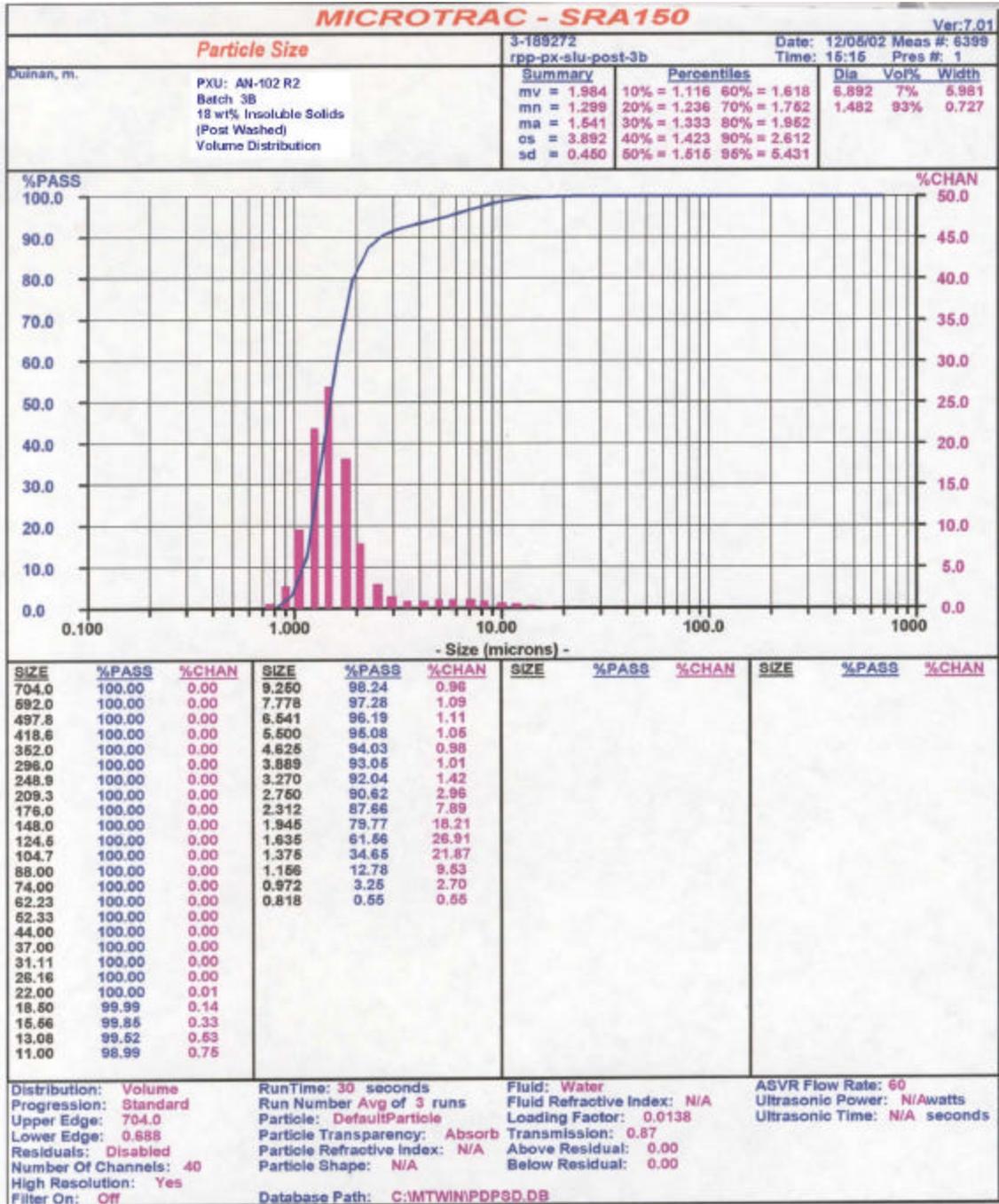


Figure G23. After washing of Batch 3B: 18 wt% Insoluble Solids  
 (VOLUME Distribution)

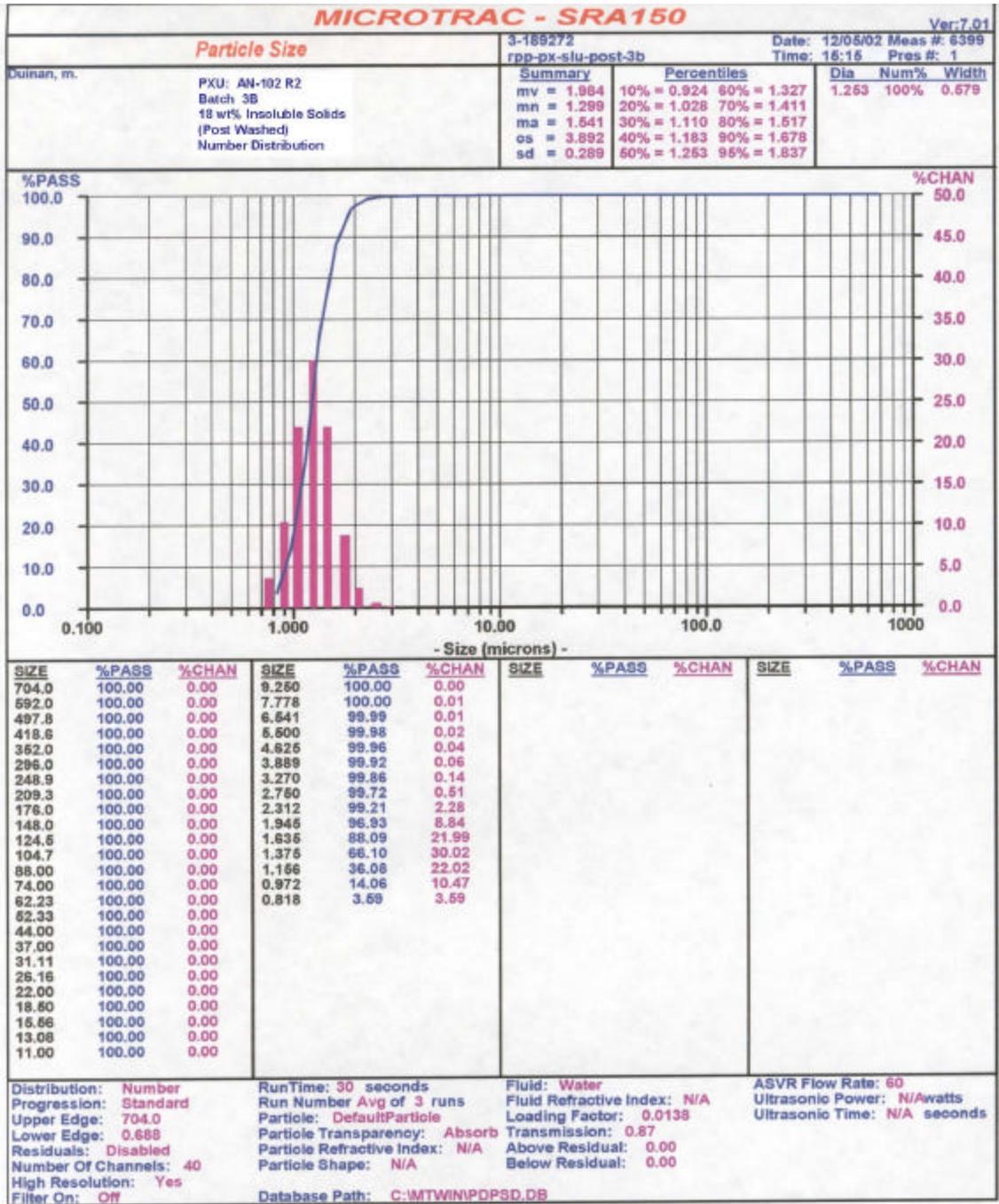


Figure G24. After washing of Batch 3B: 18 wt% Insoluble Solids  
 (NUMBER Distribution)

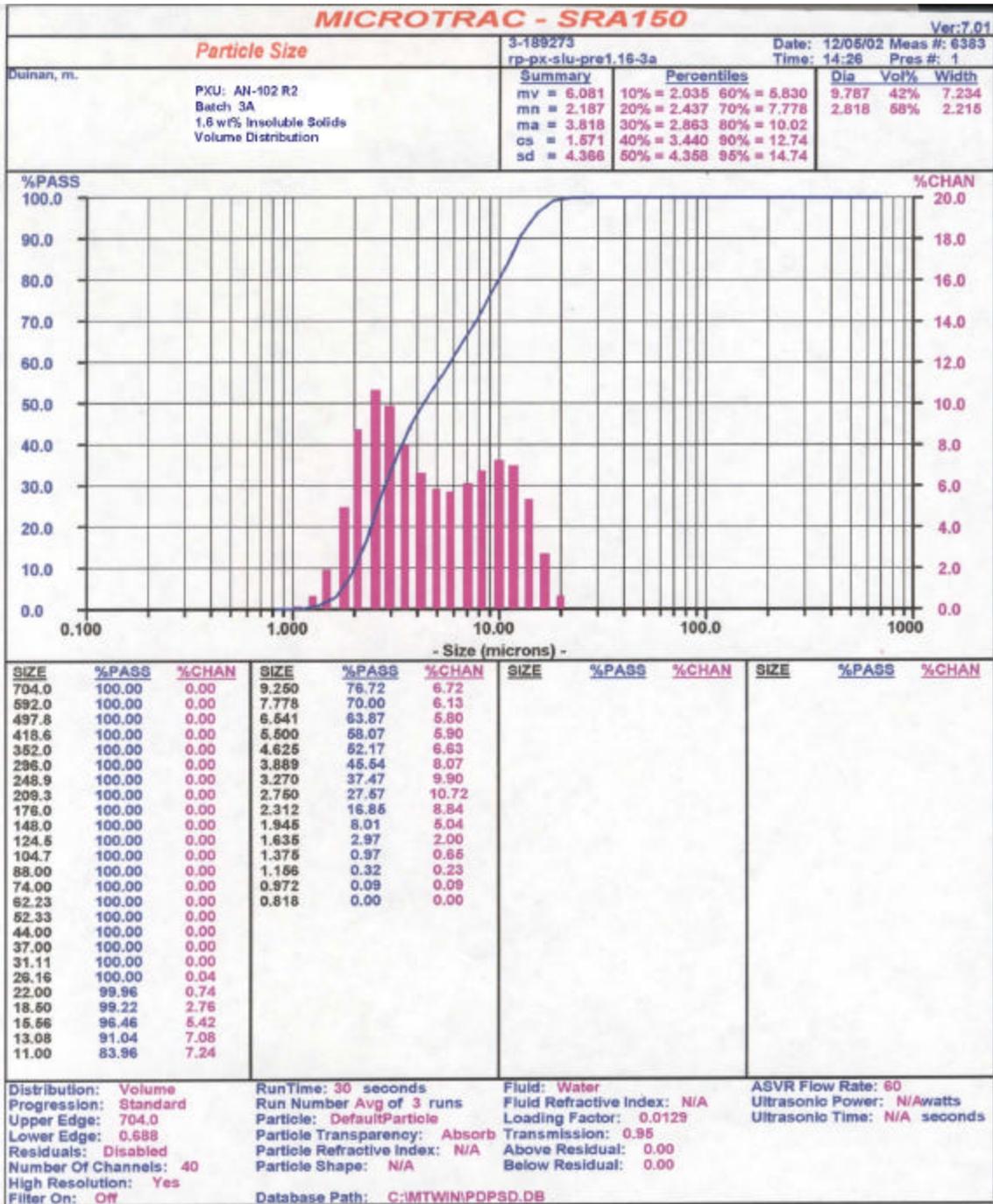


Figure G25. At start of Batch 3A dewatering: 1.6 wt% Insoluble Solids (VOLUME Distribution)

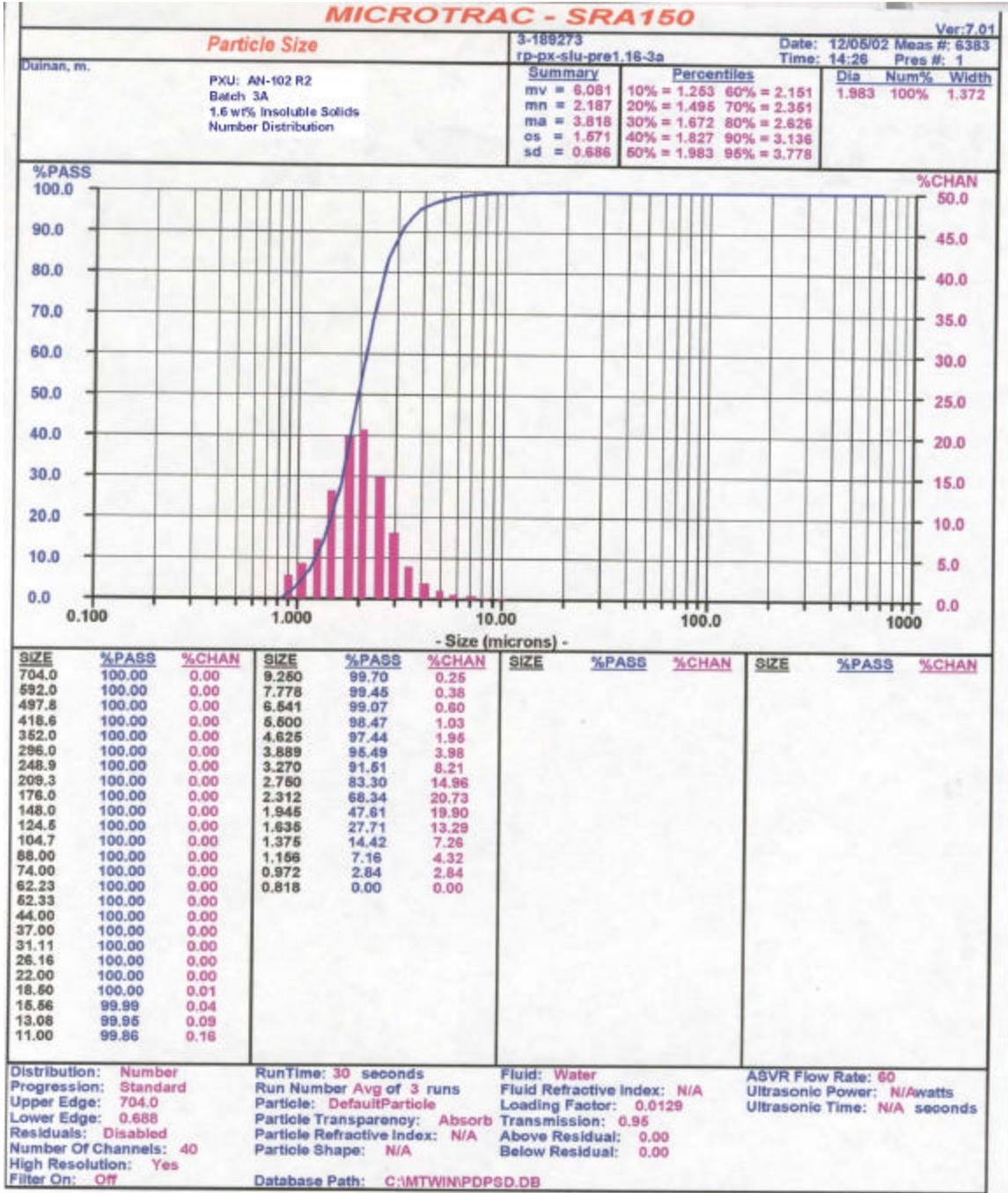


Figure G26. At start of Batch 3A: 1.6 wt% Insoluble Solids  
 (NUMBER Distribution)

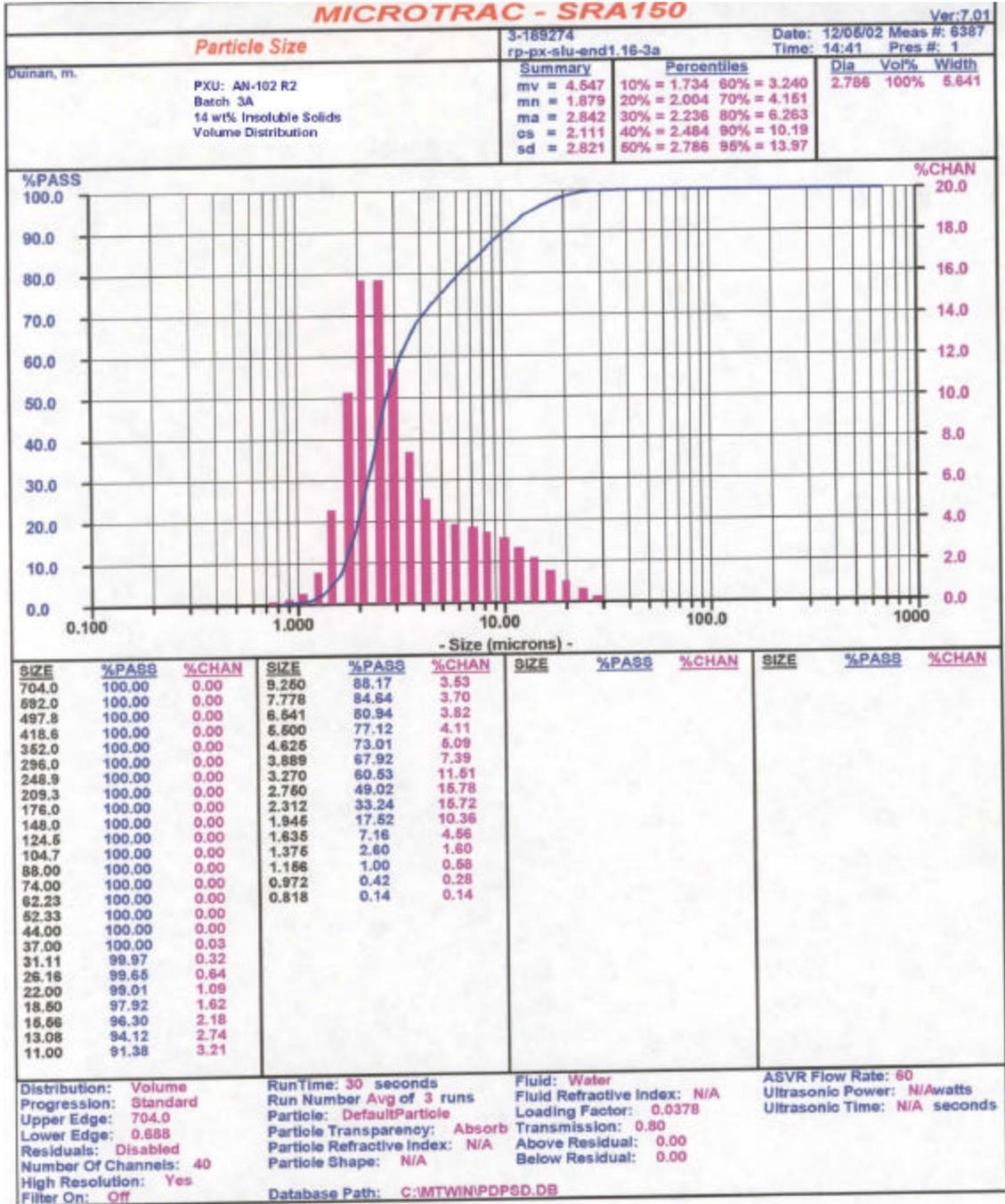


Figure G27. After 26 hours of Batch 3A dewatering: 14 wt% Insoluble Solids (VOLUME Distribution)

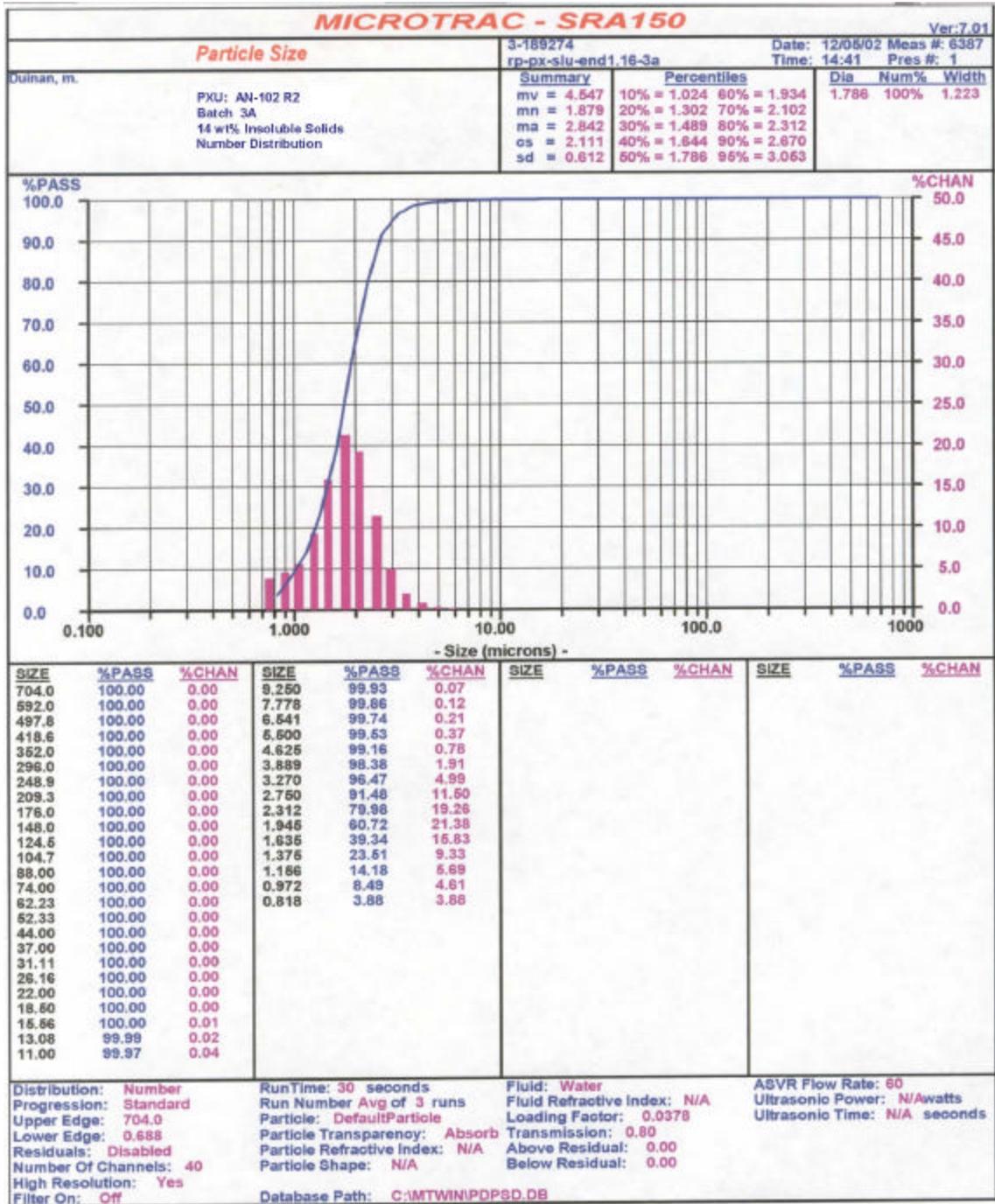


Figure G28. After 26 hours of Batch 3A: 14 wt% Insoluble Solids  
 (NUMBER Distribution)

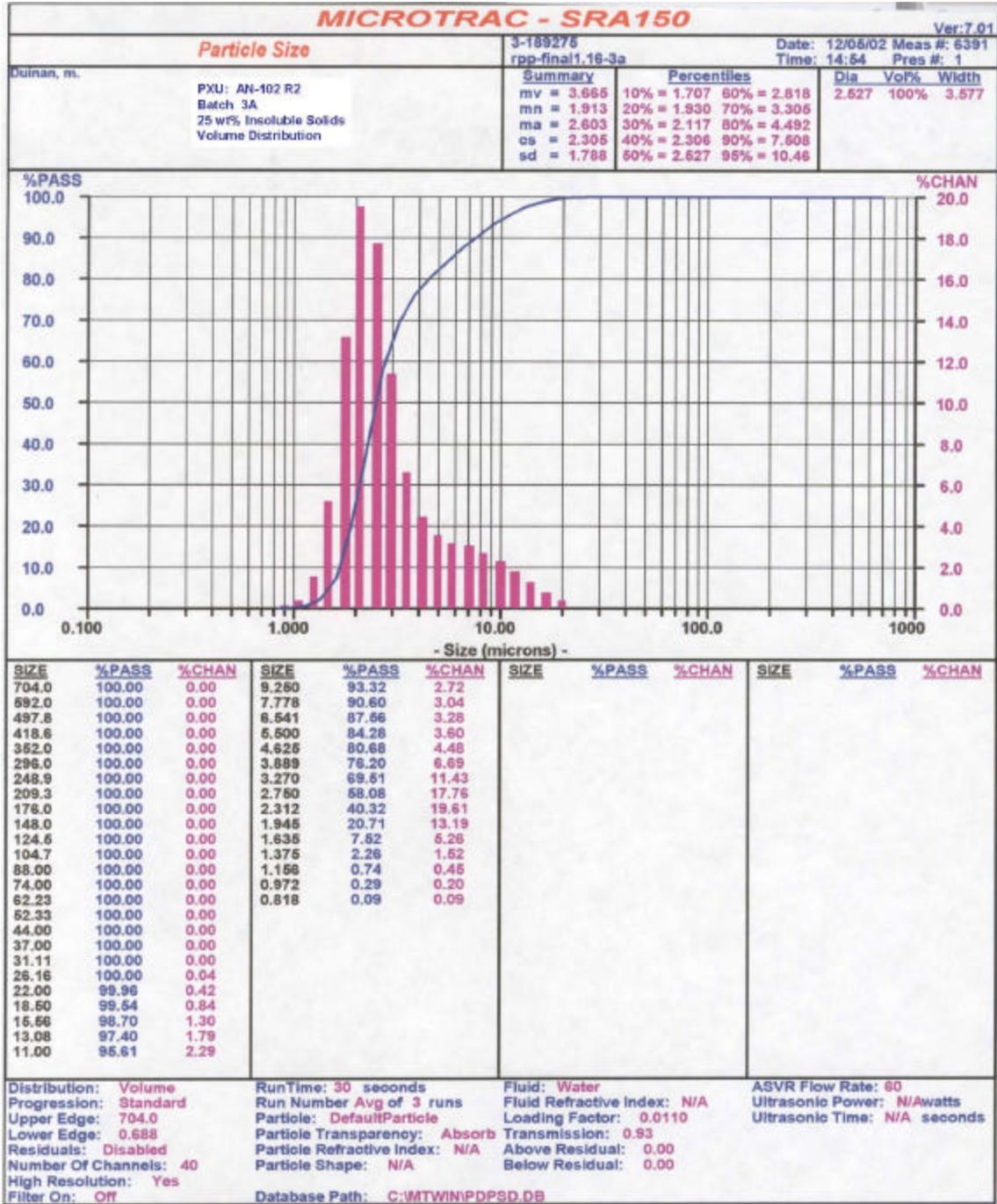


Figure G29. After 29 hours of Batch 3A dewatering: 25 wt% Insoluble Solids (VOLUME Distribution)

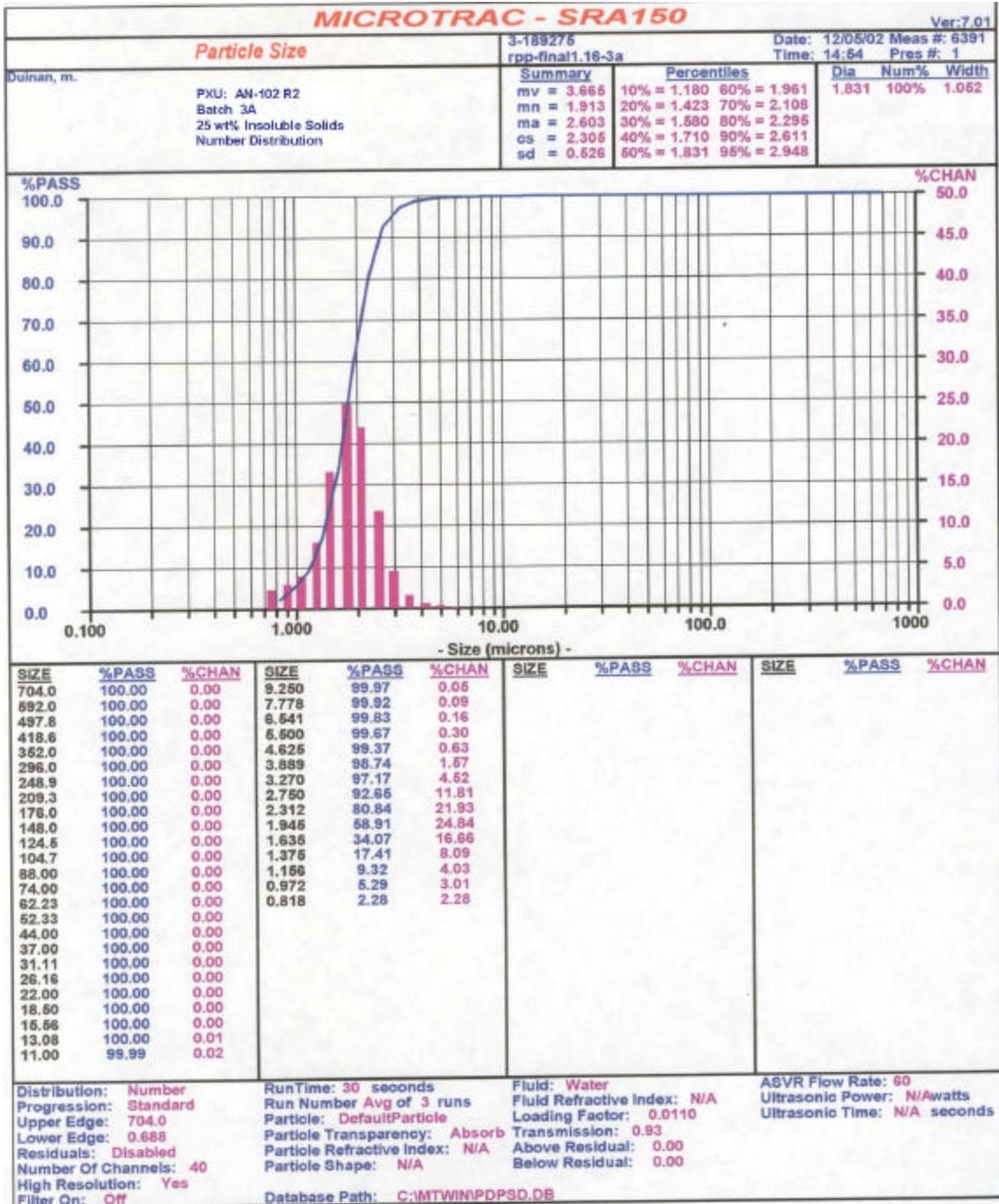


Figure G30. After 29 hours of Batch 3A: 25 wt% Insoluble Solids (NUMBER Distribution)

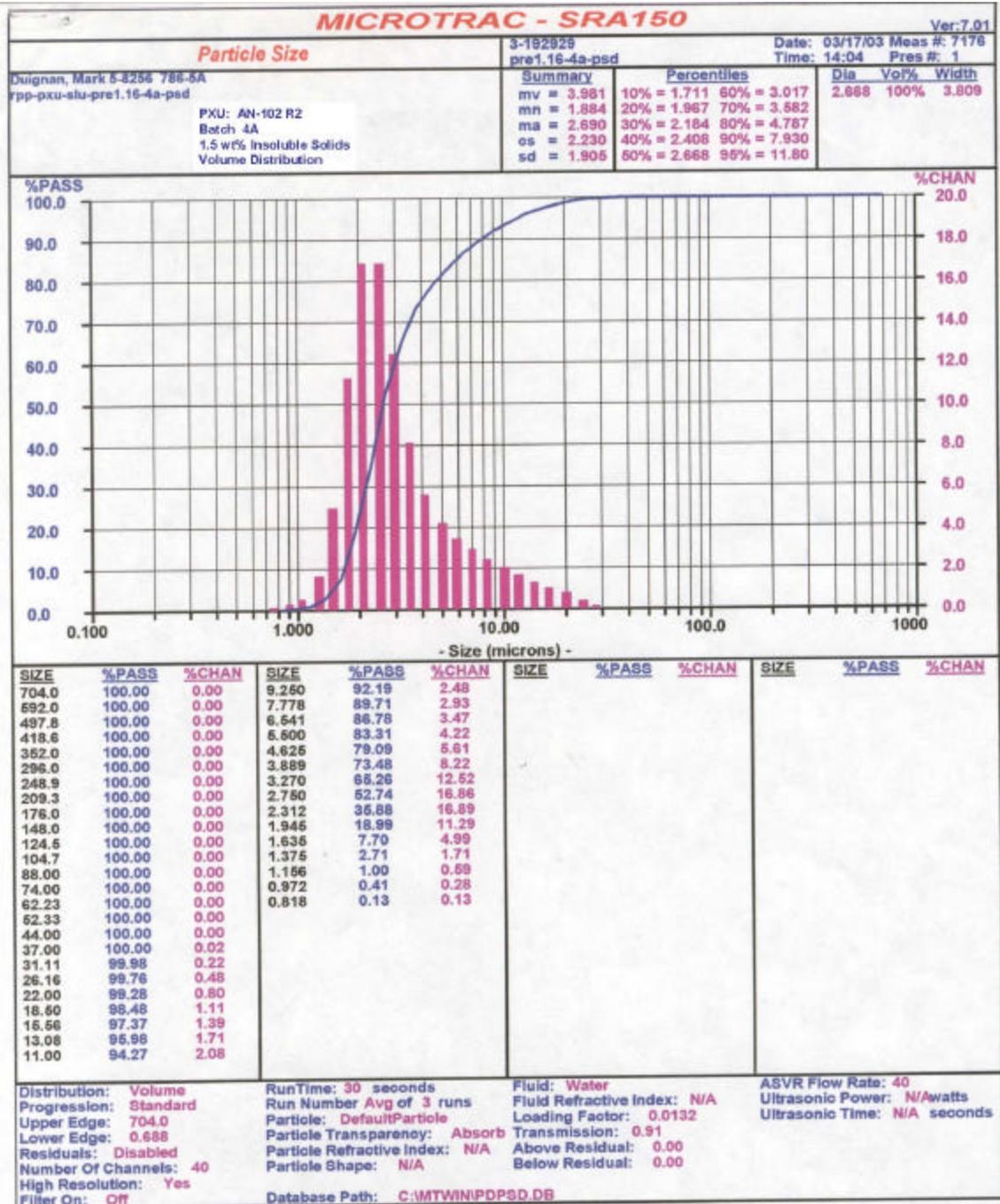


Figure G31. At start of Batch 4A dewatering: 1.5 wt% Insoluble Solids (VOLUME Distribution)

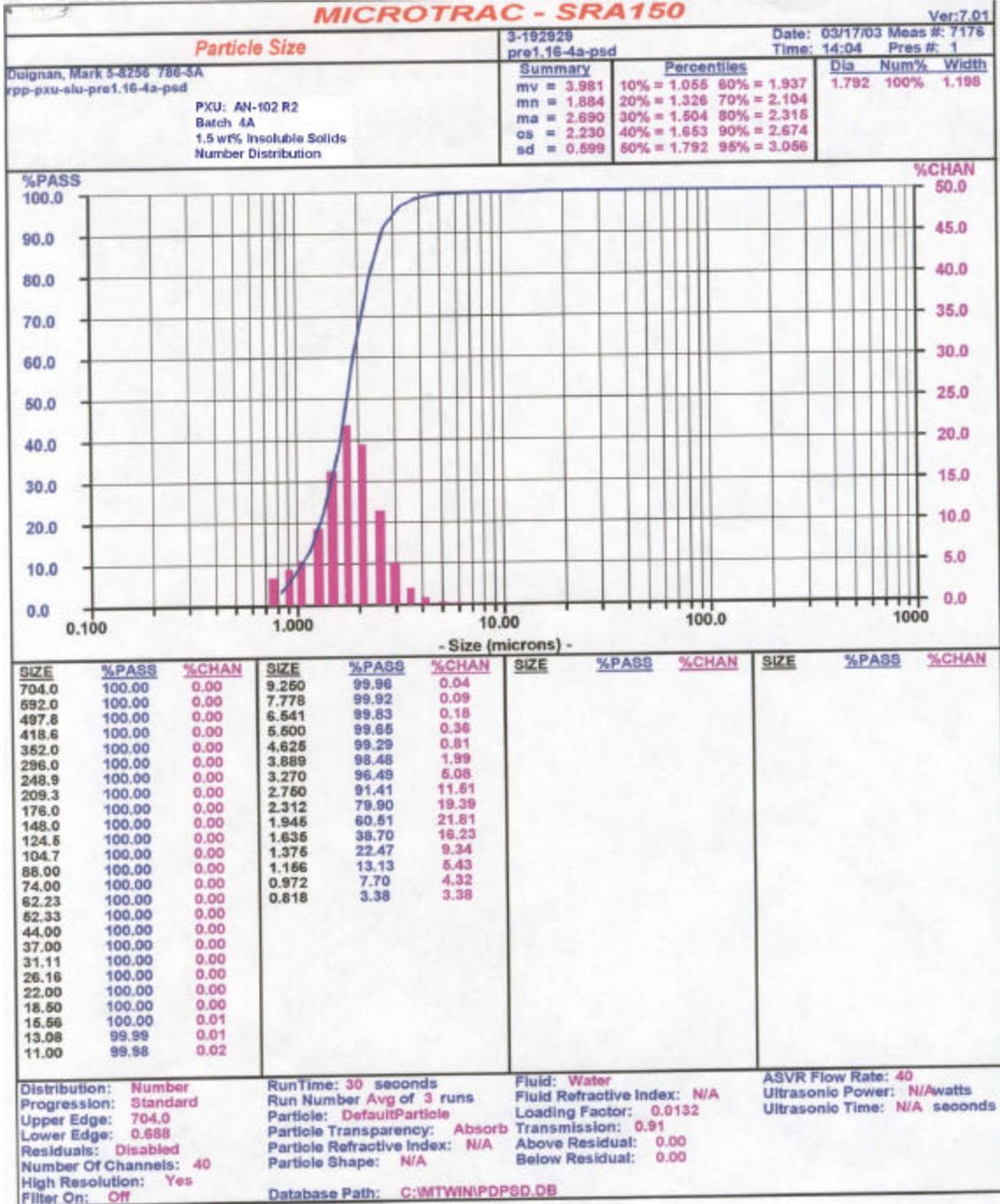


Figure G32. At start of Batch 4A: 1.5 wt% Insoluble Solids  
 (NUMBER Distribution)

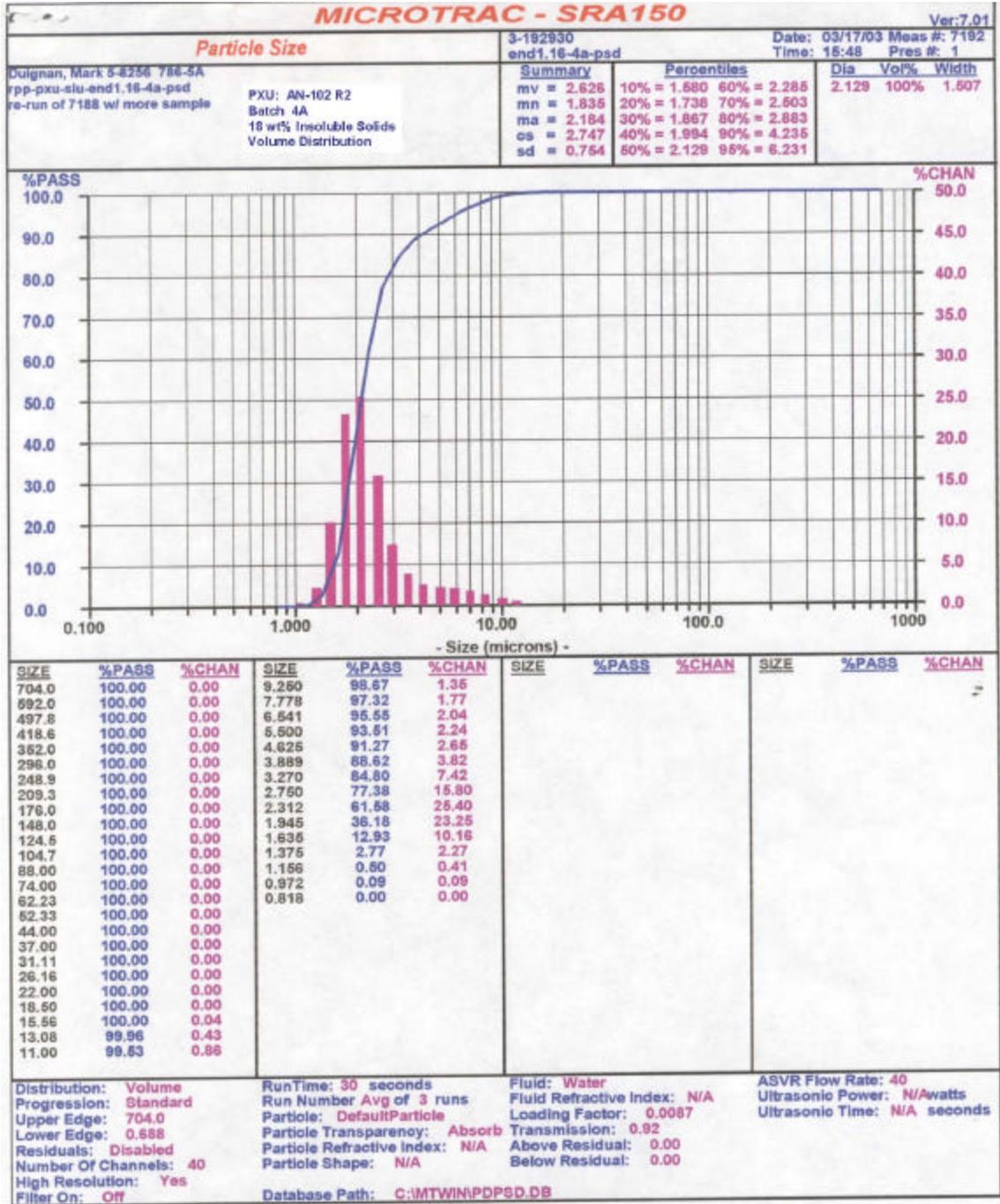


Figure G33. After 20 hours of Batch 4A dewatering: 18 wt% Insoluble Solids (VOLUME Distribution)

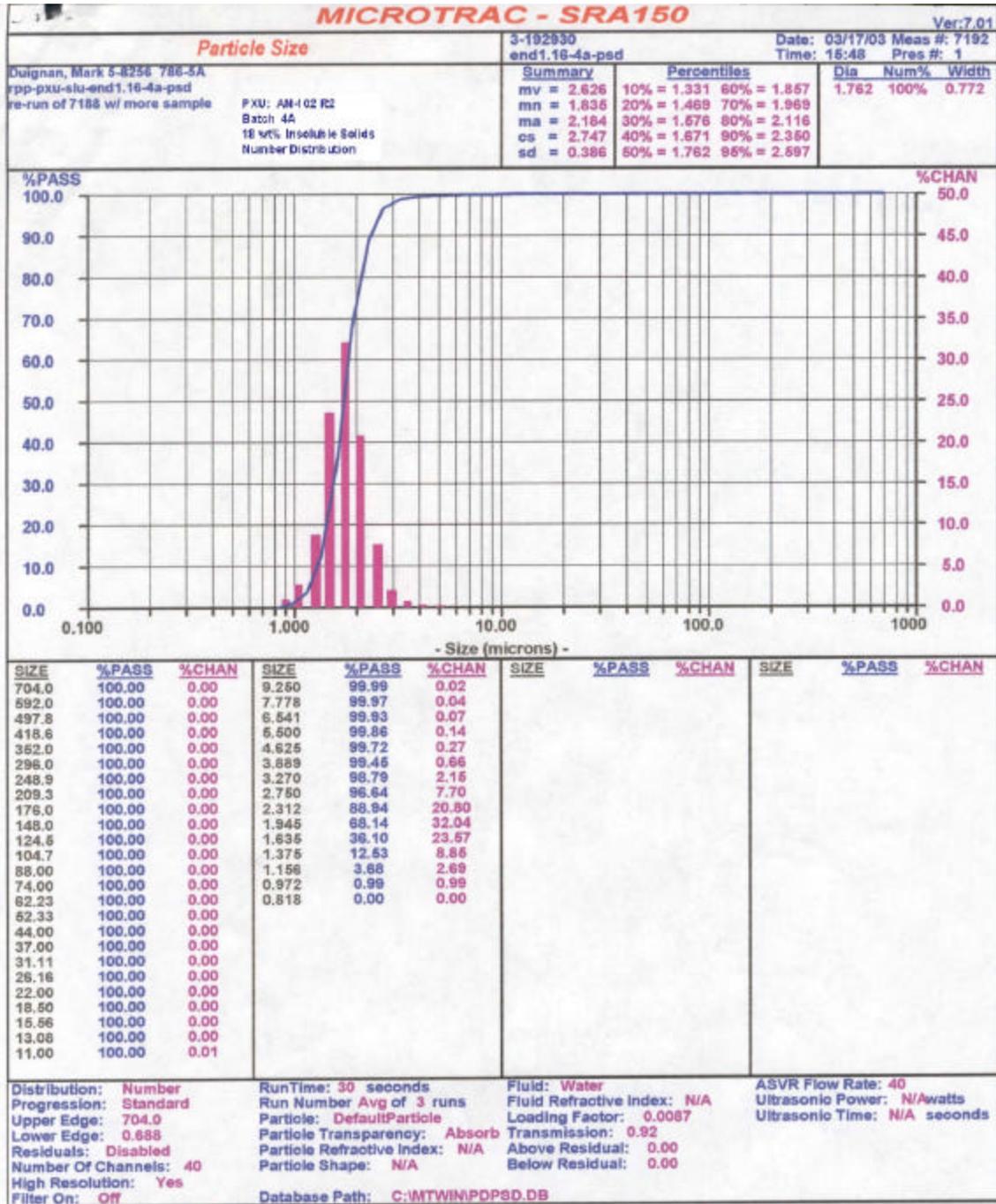


Figure G34. After 20 hours of Batch 4A: 18 wt% Insoluble Solids  
 (NUMBER Distribution)

## APPENDIX H

### INSTRUMENTATION AND MEASUREMENT UNCERTAINTY

#### *Appendix Contents*

1. Experimental measurement uncertainty
2. Figure H1. Instrumentation used with their transfer functions
3. Figure H2. Pressure transducer locations
4. Figures H3 to H17. Pre-test calibration sheets<sup>†</sup> for the 15 instruments

#### Special Note:

As mentioned in Appendix F, there are no measurement uncertainties listed for the analytical data because those uncertainties are beyond the scope and control of this task. There is reason to believe that all analytical data can be at least 15% accurate, but no quantitative data are given to this effect.

---

<sup>†</sup> To save space the post-test calibration sheets have not been included. They show no more information than what is shown on the pre-test sheets. Moreover, the transfer functions for the pre-test calibration were used through the testing; therefore it is more appropriate to include those calibrations. However, the top table in Fig. H1 shows the measurement uncertainties for both calibrations and the resulting uncertainty used for this task.

## EXPERIMENTAL MEASUREMENT UNCERTAINTY

As always, any measurement made has an attributed error which must be known before a level of confidence can be attained for the results obtained. This error may come from one or all of the following: the measurement instrument, the way an instrument is set up to make a measurement in relation to the experimental phenomenon to be measured, and the person using the instrument. It is not the purpose of this section to exhaust all possible avenues of measurement uncertainty, but rather to illustrate the level of measurement uncertainty in the results presented in Appendices A, B, C, D, E. (Outside of density and capillary-viscometer measurements taken, the measurement uncertainty of the analytical data in Appendix F is beyond the scope of this task.) In general, the measurement uncertainties present here are for a reading or calculation at any instant. That is, the fluctuations that occur during experimentation are not addressed here. The magnitude of measurement fluctuations with time that occur during an experimental run can be seen at the bottom of each data table from the preceding appendices. Each column of data includes the average value of those data and their standard deviation.

In all the data sheets included in Appendices A, B, C, D, E there are raw data columns (for instruments, five thermocouples: T1-T5, six pressure transducers: dP1-dP3 and P1-P3, and four flow meters: Q1-Q3, and Qbp) and there are calculated data columns (all columns to the right Column Qbp). The uncertainty of a raw data measurement is the calibrated uncertainty of the individual instrument to a 95% confidence level, Figs. H3 to H17.

Example to find the measurement uncertainty of a raw data point:

1. Find the data column entitled, T1, any Appendix A through E.
2. Look up Thermocouple T1 on Fig. H1 in this Appendix to see that the calibrated uncertainty is 1.2°C (95% confidence level\*). If a closer look on how that specific systematic error was obtained is desired, then check the appropriate calibration sheet. Thermocouple T2 is shown as Fig. H4. (The calibration sheets are in order of the fifteen instruments that are listed in Fig. H1, with the first instrument T1 shown in Fig. H3 and the last instrument Q4 (or Qbp) shown in Fig. H17.)  
[\*The confidence level comes from the Student's  $t$  distribution function used in determining an instrument uncertainty.]
3. The magnitude of the random error can be obtained from the standard deviation shown at the bottom of each column of raw data. (The values shown are twice the magnitude of the standard deviation of the data which represents a 95% confidence level. The standard deviation from the average value, obtained from a specific instrument for a specific test run, will be a good indication of random error for all but the filtrate flowrates, Q2, Q3, Qbp. Temperatures, pressures, and slurry flowrates were maintained constant, therefore the fluctuations around the mean should be normally distributed. The filtrate flowrates decreased with time, due to the nature of the experiment. Therefore, the random error for Q2 and Q3 should only be obtained when the filtrate flowrates reach some asymptote. (In some cases, for a thick slurry the temperature could not be held constant, but increased with time. In these cases the standard deviation will not properly represent random fluctuations. To facilitate

the evaluation of such occurrences each column of data also has the maximum, minimum, and median values along with 2 x the standard deviation. Note that the number of points used to determine these values is also given. Extreme points, like when backpulsing occurs were excluded.). Finally, the backpulse flowrate, Qbp, was never in steady state, as per design, therefore the standard deviation means nothing.

Measurement uncertainties for the calculated results can be obtained by the general method of the Law of Propagation of Errors (section 4.7 of Mandel, 1964). The derivation will not be given here and the following is just one example for one type of relation, albeit a common relation.

For example, a calculated entity has an uncertainty of  $\delta a$ . The entity a is a function of three measured quantities: b, c, and d by the following relationship:  $a = b \times c / d$  and these quantities have measurement uncertainties of  $\delta b$ ,  $\delta c$ , and  $\delta d$ , respectively. The uncertainty can be shown as:

$$(\delta a)^2 = [(\partial a / \partial b) \delta b]^2 + [(\partial a / \partial c) \delta c]^2 + [(\partial a / \partial d) \delta d]^2,$$

if the error terms are independent and symmetrical. The term  $\delta a$  is squared to capture both the negative and positive error terms.

Then for the relation  $a = bc/d$  the relative uncertainty can be shown to be:

$$\delta a/a = [(\delta b/b)^2 + (\delta c/c)^2 + (\delta d/d)^2]^{1/2}. \quad (1)$$

Using the above the relation (1) an uncertainty for velocity, transmembrane pressure, filtrate flux, and permeability are determined. The method of determining the measurement uncertainty of any of the calculated results will be the same as the following analyses. However, only one example of each calculated result is shown below. To show an example, any specific calculated quantity is sufficient. An arbitrary choice (but having a low TMP to obtain a bounding high uncertainty) of a representative group of results is: Run 1.01A at the 10.70<sup>th</sup> minute [The data for Run 1.01A can be found in Appendix B in the Fig. B18 and the 10.70<sup>th</sup> minute is row 23<sup>rd</sup> row from the top or 8<sup>th</sup> from sub-table "Data – Per Minute.]

The measurement uncertainty for the following values will be shown:

V, ft/s	TMP, psi	Fc (at 25°C*), gpm/ft <sup>2</sup> ,	P, gpm/ft <sup>2</sup> /psi
11.6	10.4	0.028	0.003

\*actual temperature was 25.1°C but was adjusted to 25.0°C as per the customer specification, Ref. 3, therefore Fc means the corrected filtrate flux.

The results of the measurement uncertainties found below at the 95% confidence level are:

$$\text{Slurry Velocity} = \mathbf{V} \pm \mathbf{6.3 \%}$$

Transmembrane Pressure	=	<b>TMP</b>	$\pm 2.2 \%$
Temperature Corrected Filtrate Flux	=	<b>Fc</b>	$\pm 5.4 \%$
Permeability	=	<b>P</b>	$\pm 5.8\%$

### H.1 Velocity [ $V = Q1 / A_{\text{cross-section}}$ ]

This uncertainty is combination of the instrument, Q1, uncertainty and from the lack of knowledge of the exact inside diameters of the filter tubes. The instrument uncertainty is obtained for that instrument's calibrated uncertainty. An accurate measurement of the average inside diameter of the filtrate tubes was impossible since it may vary down the length for each filter tube and may vary from tube to tube. Even measuring the diameter at the filter tube ends is difficult because of the weldments to the tube sheets. For a Mott 1/2-inch tube the diameter was measured to be 0.488 inch and the tolerances were measured at +0.002 inch and -0.003 inch. The diameter could only be measured at the tube ends and the vendor stated tolerances for the overall tubes are +0.025 and -0.005 and the diameter of the filter tubes can presumably vary anywhere between those tolerances therefore for this task the diameter uncertainty will be taken as the average tolerance, i.e.,  $\pm 0.015$  inch.

The measurement uncertainty estimate:

Calibrated uncertainty (Figs. H1 and H14):  $\delta Q1 = \pm 0.5$  gpm

Slurry flow rate:  $Q1 = 47.23$  gpm [Run 1.01A, Row 23, Q1 Column: Appendix B]

Filter tube inside diameter:  $\delta d = \pm 0.015$  inch

Filter tube inside diameter:  $d = 0.488$  inch

$$V = Q / A = Q1 / (\pi d^2/2)$$

$$\text{In the form of Eq. (1): } \delta V/V = [(\delta Q1/Q1)^2 + 4(\delta d/d)^2]^{1/2}$$

[Note the multiplier 4. This results from the derivation  $\partial V/\partial d$  because of the exponent]

$$\text{Therefore, } [(0.5/47.23)^2 + 4(0.015/0.488)^2]^{1/2} \times 100\% = \pm 6.24 \%$$

The uncertainty of the example **V** is: **11.5  $\pm$  0.7 ft/s**

[since  $11.5 \times 0.0624 \sim 0.72$ ]

### H.2 Transmembrane Pressure [ $TMP = (dP2 + dP3) / 2$ ]

This uncertainty will come from two instruments, dP2 and dP3. Also, there is another uncertainty due to location of the pressure taps. As seen in Figs. H1 and H2, dP2 is located at the bottom to the filter housing (upstream to the filter) and dP3 is located at the top of the filter housing (downstream to the filter). Due to fluid being in the pressure lines (water) a liquid-filled system will give approximately\* the correct pressure drops,

however, the slurry pressures lost upstream to the filter and gained downstream of the filter are not symmetrical and therefore do not cancel out. With this said, this addition to the uncertainty is small compared to the assumption that true TMP is represented by the average of two pressures at the ends of a filter. Because the filter is oriented perpendicular to gravity and the flow causes a pressure and concentration gradient along the entire tube wall it is not clear what TMP would be representative of the entire filter unit. On the other hand, the way measurements were taken probably will be similar to the field use of this filter and therefore a good measurement for design purposes. The uncertainty is actually the uncertainty of two measurement devices, and nothing more. Finally, the Law of Propagation of Errors by Eq. (1) does not lend itself to additive contributions to uncertainties. Fortunately, the two quantities are similar in magnitude and calibrated uncertainty. Equation (1) will be used as long as it gives an uncertainty larger than the largest calibrated uncertainty for the two pressure transducers.

[\*The correct pressure drop, for any dP, is obtained when the test liquid is the same as the liquid in the pressure lines. Since the slurry was more dense than the water the readings are affected accordingly. For instance, the pressure lines to obtain dP3 are lines 3 and 4, Fig. H2, and their heights were 139.63 inches and 131.88 inches, respectively. With NO flow in a completely water-filled system, then  $dP3 = 0$ , (that is, the two water columns cancel each other) but with a different density fluid in the test rig there is a differential pressure  $dP3 = P_{line3} - P_{line4} = (139.63 - 131.88) \times (\text{density difference})$ . In the worst case the slurry density was approximately 1.4 g/cc, therefore the offset could be a maximum of 7.75 inches  $\times$  0.4 = 3.1 inches H<sub>2</sub>O or 0.11 psid. However, the actual magnitude of the offset was probably smaller because the differential height, 7.8 inches, was a combination of slurry and filtrate, which had a lower density. Combining this complication of obtaining the true contribution to the overall uncertainty, along with the measurement fluctuations and other factors, then this quantity to the uncertainty was neglected.]

The measurement uncertainty estimate:

Calibrated uncertainty (Figs. H1 and H12):  $\delta dP2 = \pm 0.11$  psi

Pressure drop:  $dP2 = 12.669$  psid [Run 1.01A, Row 23, dP2 Column: Appendix B]

Calibrated uncertainty (Figs. H1 and H13):  $\delta dP3 = \pm 0.16$  psi

Pressure drop:  $dP3 = 8.23$  psid [Run 1.01A, Row 23, dP3 Column: Appendix B]

$$TMP = (dP2 + dP3) / 2$$

In the form of Eq. (1):  $\delta TMP / TMP = [(\delta dP2 / dP2)^2 + (\delta dP3 / dP3)^2]^{1/2}$

Therefore,  $[(0.11/12.67)^2 + (0.16/8.23)^2]^{1/2} \times 100\% = \pm 2.13 \%$

The uncertainty of the example **TMP** is: **10.5  $\pm$  0.3 psid**

[since  $TMP = (12.669 + 8.23) / 2 = 10.45$  psid and  $10.45 \times 0.0213 \sim 0.223$ ]

### H.3 Filtrate Flux [ $F = Q2 / A_{\text{inner-surface}}$ ]

This uncertainty is combination of the instrument, Q2, uncertainty and from the lack of knowledge of the exact inside diameters and length of the filter tubes. The instrument uncertainty is obtained for that instrument's calibrated uncertainty. The uncertainty of the inside diameter of the filter tubes has already been addressed in section H.1 and it was estimated at 0.015 inch from the manufacturer's stated tolerance. The uncertainty of the length of the filter tubes was estimate from in-house measurements. The requested tube length from the manufacturer was 90 inches. Because of the center weldments (the 90-inch length was made of four 22.5-inch tube sections) the active length measured closer to 89 5/8 inches; take the each of the three central weldments to by 1/8 inch long. Due to bowing and weldment variations an overall length uncertainty will be taken as the length of one weldment, i.e., 1/8-inch.

The measurement uncertainty estimate:

Calibrated uncertainty (Figs. H1 and H15):  $\delta Q2 = \pm 0.005$  gpm

Filtrate flow rate:  $Q2 = 0.186$  gpm [Run 1.01A, Row 23, Q2 Column: Appendix B]

Tube inside diameter uncertainty:  $\delta d = \pm 0.015$  inch (from manufacturer)

Tube inside diameter:  $d = 0.488$  inch

Tube length uncertainty:  $\delta L = \pm 0.125$  inch

Tube length:  $L = 89.625$  inches

$$F = Q/A = Q2 / \pi d L$$

In the form of Eq. (1):  $\delta F/F = [(\delta Q2/dQ2)^2 + (\delta d/d)^2 + (\delta L/L)^2]^{1/2}$

Therefore,  $[(0.005/0.186)^2 + (0.015/0.488)^2 + (0.125/89.625)^2]^{1/2} \times 100\% = \pm 4.09\%$

The uncertainty of the example **F** is: **0.19 ± 0.008 gpm/ft<sup>2</sup>**

[since  $0.186 \times 0.0409 \sim 0.0076$ ]

#### H.3.1 Effect of Temperature on the Measurement Uncertainty on F

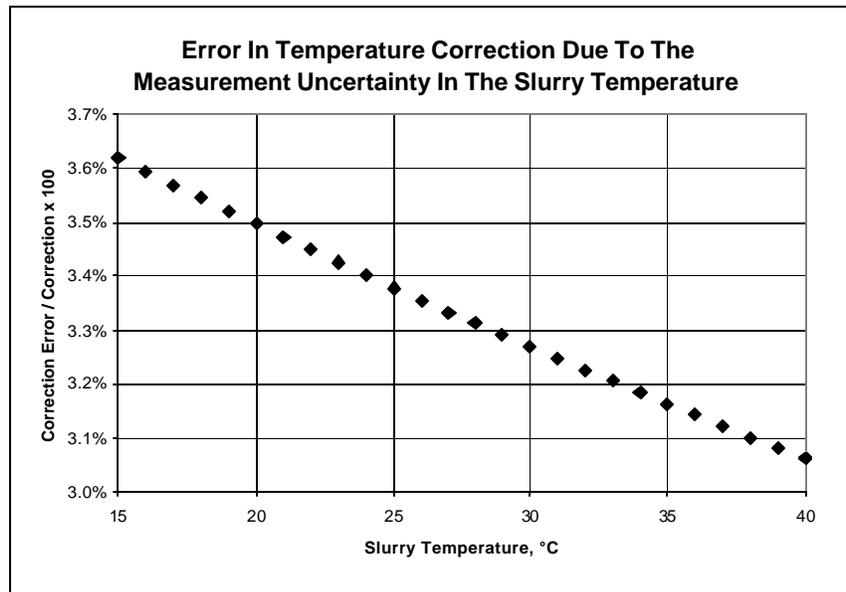
As per the customer specification the filtrate flux was to adjusted such that it would give a result at 25°C. The equation as was stated is:

$$F = Q2(\text{Temperature}) / \text{Area} = Q2 \times \text{Correction Factor} / \text{Area}$$

$$CF = e^{[2500((1/273 + \text{Slurry Temperature}) - (1/298))]}$$

Only the correction factor's effect on measurement uncertainty is dealt with here. The equation is accepted as error free, i.e., method, constants, etc. Only the uncertainty of the temperature measurement, which leads to the correction, will be addressed.

Generally, the adjustment to filtrate flux, **F**, is small because, whenever possible, the slurry's operational temperature was maintained at 25°C, which would result in a zero adjustment. However, the example chosen to show measurement uncertainty had a temperature difference of 0.2°C. That is, for Run 1.01A at the 20<sup>th</sup> minute the slurry temperature was 25.076°C. Unfortunately, the fact that a temperature correction is applied means the temperature uncertainty will effect the calculated result at any temperature. That is, even if the slurry temperature were exactly 25°C, which would make the correction = 1.0, the uncertainty of that temperature and thereby the correction, leads to an inherent uncertainty of value that is being corrected, i.e, **F**. For this task the slurry temperature was measured with thermocouple T1, which had a calibrated measurement uncertainty of ±1.2°C [see Fig. H1]. If at 25°C the temperature has an uncertainty of ±1.2°C, then the correction can be either 0.9669 to 1.0345, or approximately ±3.38% [i.e., ((1-0.9669)+(1.0345-1))/2 / 1.00 = 0.0338]. To show the measurement uncertainty mathematically from the correction equation is beyond the scope of this task, however it can be shown graphically. For a range of slurry temperatures from 15°C to 40°C, then the correction can be shown to change from 1.34 to 0.65, respectively. However, with a measurement uncertainty of ±1.2°C this factor can be in error from approximately 3.62% to 3.06%, respectively, see the Figure below:



Therefore, for the sake of this example the relative uncertainty of the correction factor due to the temperature will be assumed to be 3.4%, since most of the data were obtained at 25°C. Using this constant value is not a bad assumption because between 20°C and 30°C this uncertainty only fluctuates by approximately 0.1%.

This increased uncertainty to the filtrate flux is then a combination of two uncertainties already calculated above for **F** (section H.3) and the correction factor. The analyses still follows Eq. (1) therefore:

The measurement uncertainty estimate:

Filtrate flux relative uncertainty:  $\delta F/F = \pm 4.09\%$  [section H.3]

Correction factor relative uncertainty:  $\delta CF/CF = \pm 3.38\%$  [section H.3.1]

$$F_c = F_{\text{corrected}} = F \times CF$$

In the form of Eq. (1):  $\delta F_c/F_c = [(\delta F/F)^2 + (\delta CF/CF)^2]^{1/2}$

Therefore,  $[(4.09\%)^2 + (3.38\%)^2]^{1/2} = \pm 5.31\%$

The uncertainty of the example **F<sub>c</sub>** is: **0.186 ± 0.010 gpm/ft<sup>2</sup>**

[since  $0.186 \times 0.0531 \sim 0.0099$ ]

#### **H.4 Permeability [ P = F<sub>c</sub> / TMP ]**

This uncertainty is combination of two uncertainties already calculated above, in sections H.2 and H.3. The analyses still follows Eq. (1) therefore:

The measurement uncertainty estimate:

Filtrate flux relative uncertainty:  $\delta F_c/F_c = \pm 5.31\%$  [section H.3.1]

TMP relative uncertainty:  $\delta TMP/TMP = \pm 2.13\%$  [section H.2]

$$P = F_c / TMP$$

In the form of Eq. (1):  $\delta P/P = [(\delta F_c/F_c)^2 + (\delta TMP/TMP)^2]^{1/2}$

Therefore,  $[(5.31\%)^2 + (2.13\%)^2]^{1/2} = \pm 5.72\%$

The uncertainty of the example **P** is: **0.003 ± 0.0002 gpm/ft<sup>2</sup>/psi**

[since  $0.003 \times 0.0572 \sim 0.00017$ ]

## H.5 Second-Order Effects to Measurement Uncertainty

There were other effects on the measurement uncertainty, which are not included because they are thought to be of second order. For example, since the test rig was very tall, approximately 30 feet, it was subjected an ambient temperature gradient. Ambient temperatures at the bottom of the rig were usually less than at the top. For the example used in this section, [Run 1.01A, Row 23, T4 and T5 Columns: Appendix B], the temperatures were 24.9°C and 22.8°C, respectively. This gradient varied hourly and daily for several reasons. Most importantly, the 2.1°C temperature variation shown in this example is on the same order of magnitude as the calibrated uncertainties for the thermocouples. Further, the slurry in the loop generally flowed fast, so the residence time in any one section of the rig was small. For Run 1.01A the flow rate was,  $Q_1 = 47.3$  gpm. The loop volume was approximately 6 gallons so a fluid particle traversed the loop every  $6/47.3 \times 60 \sim 7.6$  seconds. [Note that the slurry flow rate for Run 1.01A was typical of most test runs.] In this example, the slurry temperature was measured to be 25.1°C, from one thermocouple located in the suction line of the pumps. While it is certain that the ambient temperatures had an effect on the slurry temperature it was small, and at steady state the effect is incorporated in the slurry temperature. The same is true for the ambient temperature gradient but to a lesser extent and therefore not considered.

INSTRUMENTS USED ON THE RPP-WTP PILOT-SCALE CROSS-FLOW FILTRATION TEST									
(Printed: April 17, 2003)									
DAS Chan.	Test Rig No.	Instrument	M&TE #	Make	Model / Serial	Calibrated Range	Uncertainty (pre-test)	Uncertainty (post-test)	Average
0	T2	Thermocouple	TR-02927	OMEGA	TJ36-CXSS-18U-6-SB-OST-M/None	0 to 100C	1.3°C	0.7°C	1.0
1	T3	Thermocouple	TR-02930	OMEGA	TJ36-CXSS-18U-6-SB-OST-M/None	0 to 100C	1.4°C	0.6°C	1.0
2	T1	Thermocouple	TR-02929	OMEGA	TJ36-CXSS-18U-6-SB-OST-M/None	0 to 100C	1.2°C	0.6°C	0.9
3	T4	Thermocouple	TR-02925	OMEGA	TJ36-CXSS-18U-6-SB-OST-M/None	0 to 100C	1.4°C	0.6°C	1.0
4	T5	Thermocouple	TR-02926	OMEGA	TJ36-CXSS-18U-6-SB-OST-M/None	0 to 100C	1.5°C	0.5°C	1.0
6	dP2	Pres. Transducer	TR-03553	Rosemount	1151DP6E22/1368962	0 to 101 PSID	0.11 PSIG	0.10 PSIG	0.11
7	P1	Pres. Transducer	TR-02917	Rosemount	1151GP6/409543	0 to 101 PSIG	0.10 PSIG	0.10 PSIG	0.10
8	dP1	Pres. Transducer	TR-03495	Rosemount	1151DP6E22/1368962	0 to 26 PSID	0.044 PSID	0.046 PSID	0.045
9	dP3	Pres. Transducer	TR-03109	Rosemount	1151DP6E22/1368963	-11 to 91 PSID	0.16 PSIG	0.12 PSIG	0.14
10	P2	Pres. Transducer	TR-03115	Rosemount	1151DP7E22M3B1/402987	0 to 151 PSIG	0.36 PSIG	0.41 PSIG	0.39
11	P3(backpulse)	Pres. Transducer	TR-00532	Rosemount	1151DP7E22M3B1P1/1038513	0 to 151 PSIG	0.15 PSIG	0.20 PSIG	0.18
12	Q2	Mag. Flowmeter	TR-20353	Fischer-Porter	10D1475EN01PF29KW12CAC1/93W011793	0 to 1.2 GPM	0.005 GPM	0.005 GPM	0.005
13	Q1	Mag. Flowmeter	TR-20350	Fischer-Porter	10D1475DK11PL29KD11CAC/90W007609	0 TO 100 GPM	0.5 GPM	0.5 GPM	0.5
14	Q3	Mag. Flowmeter	TR-03562	Fischer-Porter	10D1475CDBC11BBL1/8710A0242A3	0 to 5 GPM	0.02 GPM	0.02 GPM	0.02
15	Q4 = Qbackpulse	Mag. Flowmeter	TR-03276	Fischer-Porter	10D1475EN06PL29KD11CAC1/92W446636	0 to 5 GPM	0.02 GPM	0.02 GPM	0.02
					DAS Calibration				
					Transfer Functions for DAS (Conversion from mA to Volts)				
DAS Channel	Instrument		Slope (V/mA)	Intercept (V)	Output	Slope (unit/V)	Intercept (unit)		
6	dP2		0.4975	0.0000	Pressure (psid)	12.6673	x V +		-25.1790
7	P1		0.4975	0.0000	Pressure (psig)	12.6814	x V +		-25.1980
8	dP1		0.4988	0.0030	Pressure (psid)	3.2562	x V +		-6.5230
9	dP3		0.4983	0.0050	Pressure (psid)	12.8077	x V +		-36.5748
10	P2		0.4983	0.0050	Pressure (psig)	18.9324	x V +		-37.9977
11	P3		0.4975	0.0000	Pressure (psig)	18.9688	x V +		-37.7140
12	Q2		0.4975	0.0100	Flow (gpm)	0.1487	x V +		-0.2955
13	Q1		0.4990	0.0020	Flow (gpm)	12.5210	x V +		-25.0350
14	Q3		0.4993	-0.0030	Flow (gpm)	0.6249	x V +		-1.2381
15	Q4 = Qbackpulse		0.4988	0.0070	Flow (gpm)	0.6195	x V +		-1.2373

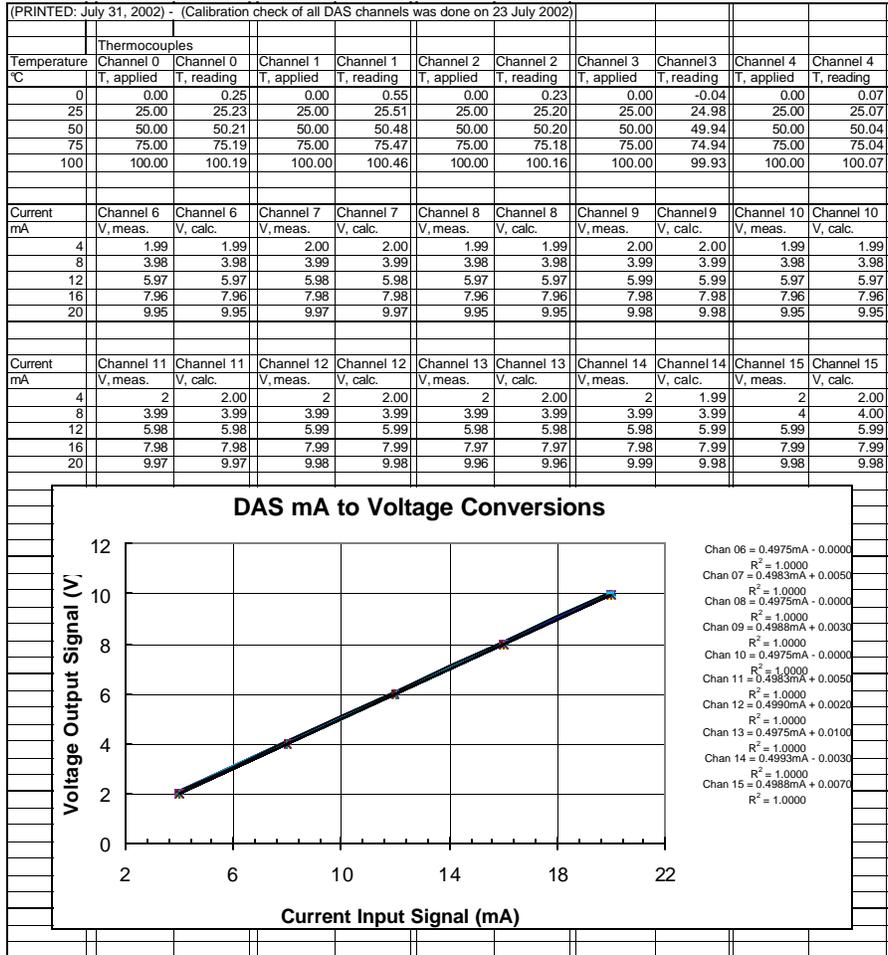


Figure H1. Instrumentation Used with their Transfer Functions

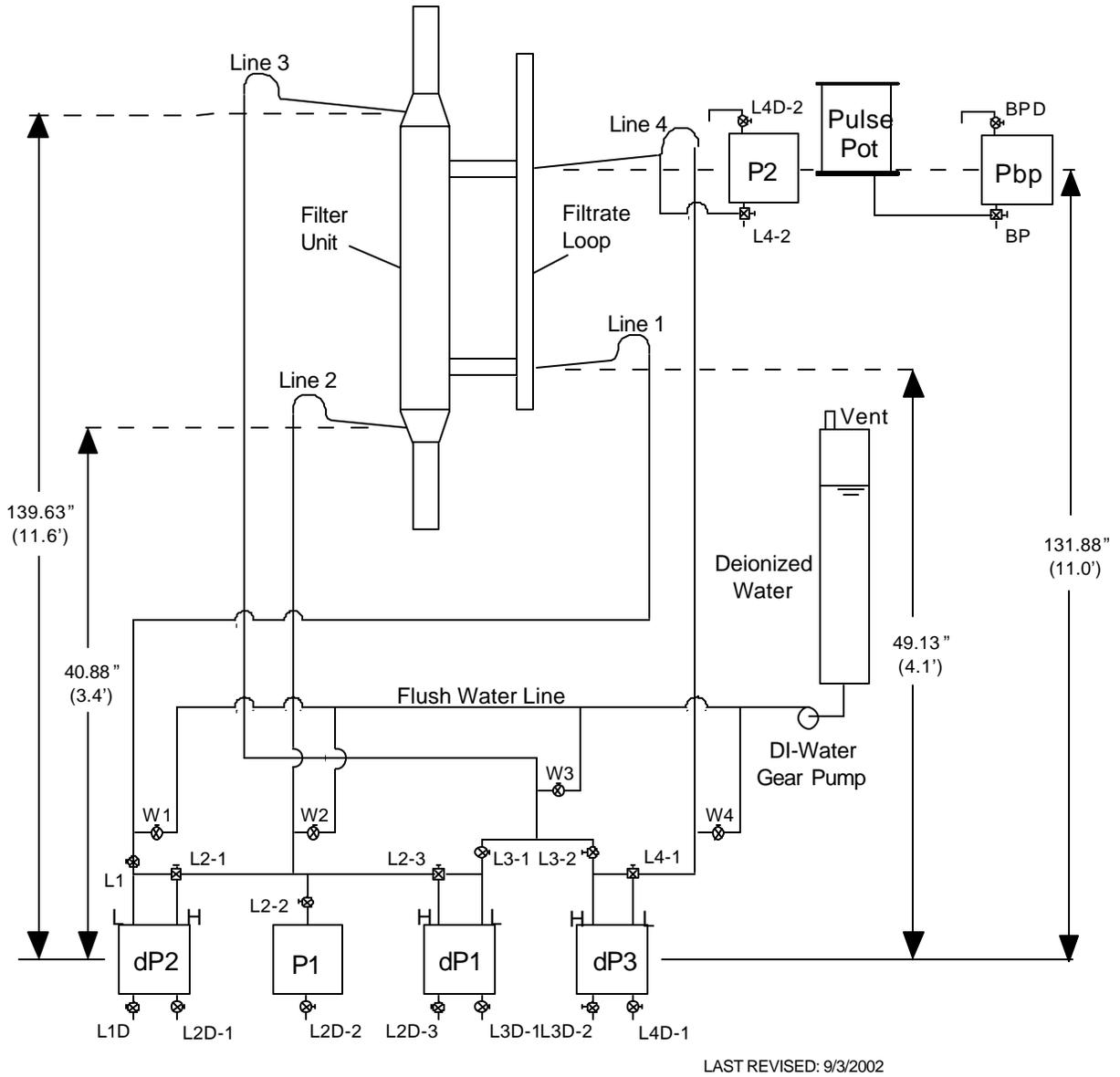


Figure H2. Pressure Transducer Locations

UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106

TR-2929

cal date: 16 April 2001

(Note: This uncertainty is the variance of the actual T from the NIST curve (Eq.1) based on the output mV)

Temperature Medium	Calibration Data		Calculated Temperature	
	Standard Temp (C)	Voltage Output (mV)	(eq. 1) (C)	Error (C)
Ice Point	0.00	-0.010	-0.17	-0.2
Ice Point	0.00	-0.025	-0.42	-0.4
Ice Point	0.00	-0.025	-0.42	-0.4
Ice Point	0.00	-0.025	-0.42	-0.4
Room Temp	22.79	1.313	22.00	-0.8
Room Temp	23.23	1.439	24.08	0.8
Room Temp	24.58	1.435	24.01	-0.6
Room Temp	24.07	1.421	23.78	-0.3
Boiling Water	99.53	6.330	100.16	0.6
Boiling Water	99.53	6.330	100.16	0.6
Boiling Water	99.44	6.317	99.97	0.5
Boiling Water	99.45	6.317	99.97	0.5

$T (C) = 0.00483 + 17.040918 * mV - 0.224284 * mV^2 + 0.005038 * mV^3$  (eq. 1)  
(Limited Curve Fit, 0-100 C. From N.I.S.T. Reference Tables)

Uncertainty of the Standards:	Temperature Curve Fit: +/-	0.010	C
	Thermometer: +/-	0.40	C
	Ice Bath: +/-	0.10	C
	Multimeter: +/- (	0.0045	% RDG +
	= +/-	0.012	C @ 6.33 mV

Accepted Tolerance: +/- 1.7 C

Statistical Info.

a	b	n	T	Xbar (C)	Sxx (C^2)	SEE (C^2)	MSE (C^2)
-0.39	1.01	12.00	2.228	41.05	21610.7	1.660	0.1660

Calculated Uncertainties:

standard uncertainty (C)	curve-fit uncertainty (C)	fixed uncertainty (C)	total uncertainty (C)
0.41	1.00	0.57	1.2

**PASS CALIBRATION? YES**

Figure H3. Pre-test Calibration Data of Thermocouple T1

**UNCERTAINTY ANALYSIS**  
**REF. WSRC-TR-91-106**

**TR-2927**

cal date: 16 April 2001

(Note: This uncertainty is the variance of the actual T from the NIST curve (Eq.1) based on the output mV)

Temperature Medium	Calibration Data		Calculated Temperature	
	Standard Temp (C)	Voltage Output (mV)	(eq. 1) (C)	Error (C)
Ice Point	0.00	-0.009	-0.15	-0.1
Ice Point	0.00	-0.014	-0.23	-0.2
Ice Point	0.00	-0.015	-0.25	-0.3
Ice Point	0.00	-0.012	-0.20	-0.2
Room Temp	22.79	1.315	22.04	-0.8
Room Temp	23.23	1.438	24.06	0.8
Room Temp	24.58	1.450	24.26	-0.3
Room Temp	24.07	1.449	24.24	0.2
Boiling Water	99.53	6.344	100.37	0.8
Boiling Water	99.53	6.345	100.39	0.9
Boiling Water	99.46	6.328	100.14	0.7
Boiling Water	99.48	6.329	100.15	0.7

$T (C) = 0.00483 + 17.040918 * mV - 0.224284 * mV^2 + 0.005038 * mV^3$  (eq. 1)  
(Limited Curve Fit, 0-100 C. From N.I.S.T. Reference Tables)

Uncertainty of the Standards:	Temperature Curve Fit: +/-	0.010	C
	Thermometer: +/-	0.40	C
	Ice Bath: +/-	0.10	C
	Multimeter: +/- (	0.0045	% RDG + 0.0005 mV)
	= +/-	0.012	C @ 6.35 mV

Accepted Tolerance: +/- 1.7 C

Statistical Info.

a	b	n	T	Xbar (C)	Sxx (C^2)	SEE (C^2)	MSE (C^2)
-0.23	1.01	12.00	2.228	41.06	21616.6	1.429	0.1429

Calculated Uncertainties:

standard uncertainty (C)	curve-fit uncertainty (C)	fixed uncertainty (C)	total uncertainty (C)
0.41	0.93	0.75	1.3

**PASS CALIBRATION? YES**

Figure H4. Pre-test Calibration Data of Thermocouple T2



UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106

TR-2925

cal date: 12 April 2001

(Note: This uncertainty is the variance of the actual T from the NIST curve (Eq.1) based on the output mV)

Temperature Medium	Calibration Data		Calculated Temperature	
	Standard Temp (C)	Voltage Output (mV)	(eq. 1) (C)	Error (C)
Ice Point	0.00	-0.013	-0.22	-0.2
Ice Point	0.00	-0.009	-0.15	-0.1
Ice Point	0.00	-0.009	-0.15	-0.1
Ice Point	0.00	-0.009	-0.15	-0.1
Room Temp	23.30	1.384	23.17	-0.1
Room Temp	24.99	1.400	23.44	-1.6
Room Temp	23.48	1.356	22.71	-0.8
Room Temp	25.57	1.500	25.08	-0.5
Boiling Water	99.94	6.342	100.34	0.4
Boiling Water	99.94	6.345	100.39	0.4
Boiling Water	99.70	6.338	100.28	0.6
Boiling Water	99.71	6.339	100.30	0.6

$T (C) = 0.00483 + 17.040918 * mV - 0.224284 * mV^2 + 0.005038 * mV^3$  (eq. 1)  
(Limited Curve Fit, 0-100 C. From N.I.S.T. Reference Tables)

Uncertainty of the Standards:	Temperature Curve Fit: +/-	0.010	C
	Thermometer: +/-	0.40	C
	Ice Bath: +/-	0.10	C
	Multimeter: +/- (	0.0045	% RDG + 0.0005 mV)
	= +/-	0.012	C @ 6.35 mV

Accepted Tolerance: +/- 1.7 C

Statistical Info.

a	b	n	T	Xbar (C)	Sxx (C^2)	SEE (C^2)	MSE (C^2)
-0.50	1.01	12.00	2.228	41.39	21677.3	2.464	0.2464

Calculated Uncertainties:

standard uncertainty (C)	curve-fit uncertainty (C)	fixed uncertainty (C)	total uncertainty (C)
0.41	1.22	0.50	1.4

**PASS CALIBRATION? YES**

Figure H6. Pre-test Calibration Data of Thermocouple T4

UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106

TR-2926

cal date: 18 July 2001

(Note: This uncertainty is the variance of the actual T from the NIST curve (Eq.1) based on the output mV)

Temperature Medium	Calibration Data		Calculated Temperature	
	Standard Temp (C)	Voltage Output (mV)	(eq. 1) (C)	Error (C)
Ice Point	0.00	-0.017	-0.28	-0.3
Ice Point	0.00	-0.015	-0.25	-0.3
Ice Point	0.00	-0.015	-0.25	-0.3
Ice Point	0.00	-0.016	-0.27	-0.3
Room Temp	24.37	1.402	23.47	-0.9
Room Temp	24.33	1.401	23.45	-0.9
Room Temp	24.43	1.367	22.89	-1.5
Room Temp	21.54	1.308	21.92	0.4
Boiling Water	100.20	6.344	100.37	0.2
Boiling Water	100.20	6.344	100.37	0.2
Boiling Water	100.10	6.345	100.39	0.3
Boiling Water	100.10	6.343	100.36	0.3

$T (C) = 0.00483 + 17.040918 * mV - 0.224284 * mV^2 + 0.005038 * mV^3$  (eq. 1)  
(Limited Curve Fit, 0-100 C. From N.I.S.T. Reference Tables)

Uncertainty of the Standards:	Temperature Curve Fit: +/-	0.010	C
	Thermometer: +/-	0.40	C
	Ice Bath: +/-	0.10	C
	Multimeter: +/- (	0.0045	% RDG + 0.0005 mV)
	= +/-	0.012	C @ 6.35 mV

Accepted Tolerance: +/- 1.7 C

Statistical Info.

a	b	n	T	Xbar (C)	Sxx (C^2)	SEE (C^2)	MSE (C^2)
-0.53	1.01	12.00	2.228	41.27	21925.7	2.825	0.2825

Calculated Uncertainties:

standard uncertainty (C)	curve-fit uncertainty (C)	fixed uncertainty (C)	total uncertainty (C)
0.41	1.31	0.53	1.5

**PASS CALIBRATION? YES**

Figure H7. Pre-test Calibration Data of Thermocouple T5

UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106, REV. 0

TR-02917

cal. date: 22 April 2001

Calibration Data

Nominal Pressure (psig)	Applied Pressure (psig)	Gage Reading (mADC)	Curve Fit (mADC)	Error (mADC)	Error (psig)
0.00	0.00	4.00	3.99	-0.006	-0.04
21.00	21.00	7.32	7.32	0.003	0.02
41.00	41.00	10.49	10.49	0.003	0.02
61.00	61.00	13.66	13.66	0.003	0.02
81.00	81.00	16.83	16.83	0.003	0.02
101.00	101.00	20.01	20.00	-0.006	-0.04
0.00	0.00	4.00	3.99	-0.006	-0.04
21.00	21.00	7.32	7.32	0.003	0.02
41.00	41.00	10.49	10.49	0.003	0.02
61.00	61.00	13.66	13.66	0.003	0.02
81.00	81.00	16.83	16.83	0.003	0.02
101.00	101.00	20.01	20.00	-0.006	-0.04
0.00	0.00	4.00	3.99	-0.006	-0.04
21.00	21.00	7.32	7.32	0.003	0.02
41.00	41.00	10.49	10.49	0.003	0.02
61.00	61.00	13.66	13.66	0.003	0.02
81.00	81.00	16.83	16.83	0.003	0.02
101.00	101.00	20.01	20.00	-0.006	-0.04
0.00	0.00	4.00	3.99	-0.006	-0.04
21.00	21.00	7.32	7.32	0.003	0.02
41.00	41.00	10.49	10.49	0.003	0.02
61.00	61.00	13.66	13.66	0.003	0.02
81.00	81.00	16.83	16.83	0.003	0.02
101.00	101.00	20.01	20.00	-0.006	-0.04

<u>Standard Uncertainties:</u>	Multimeter: +/- (	0.04	% RDG +	0.001	mADC)
	Dead Weight Tester: +/- (	0.03	% RDG +	0.03	psig)

<u>Statistical Info:</u>				Xbar	Sxx	SEE	MSE
a	b	n	T	psig	psig <sup>2</sup>	mADC <sup>2</sup>	mADC <sup>2</sup>
3.9941	0.1585	24.00	2.07	50.83	28403.33	0.0005	0.0000

<u>Calculated Uncertainties:</u>			<u>Total Uncertainty</u>	
$\sigma_C$	$\sigma_E$		$\sigma_F$	$\sigma_T$
psig	psig		psig	psig
0.08	0.06		0.00	0.10

Accepted Tolerance: +/- 2 psig

**PASS CALIBRATION? YES**  
**TRANSFER EQUATION PSIG = 6.309 \*mA -25.198**

Figure H8. Pre-test Calibration Data of Gauge Pressure Transducer P1



UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106, REV. 0

TR-00532

cal. date: 23 May 2002

Calibration Data

Nominal Pressure (psig)	Applied Pressure (psig)	Gage Reading (mADC)	Curve Fit (mADC)	Error (mADC)	Error (psig)
0.00	0.00	4.00	4.00	-0.004	-0.04
31.00	31.00	7.28	7.28	0.001	0.01
61.00	61.00	10.46	10.46	0.000	0.00
91.00	91.00	13.63	13.64	0.009	0.08
121.00	121.00	16.82	16.82	-0.002	-0.02
151.00	151.00	20.00	20.00	-0.004	-0.03
0.00	0.00	4.00	4.00	-0.004	-0.04
31.00	31.00	7.28	7.28	0.001	0.01
61.00	61.00	10.46	10.46	0.000	0.00
91.00	91.00	13.63	13.64	0.009	0.08
121.00	121.00	16.82	16.82	-0.002	-0.02
151.00	151.00	20.00	20.00	-0.004	-0.03
0.00	0.00	4.00	4.00	-0.004	-0.04
31.00	31.00	7.28	7.28	0.001	0.01
61.00	61.00	10.46	10.46	0.000	0.00
91.00	91.00	13.63	13.64	0.009	0.08
121.00	121.00	16.82	16.82	-0.002	-0.02
151.00	151.00	20.00	20.00	-0.004	-0.03
0.00	0.00	4.00	4.00	-0.004	-0.04
31.00	31.00	7.28	7.28	0.001	0.01
61.00	61.00	10.46	10.46	0.000	0.00
91.00	91.00	13.63	13.64	0.009	0.08
121.00	121.00	16.82	16.82	-0.002	-0.02
151.00	151.00	20.00	20.00	-0.004	-0.03

<u>Standard Uncertainties:</u>	Multimeter: +/- (	0.04	% RDG +	0.001	mADC)
	Dead Weight Tester: +/- (	0.03	% RDG +	0.03	psig)

<u>Statistical Info:</u>				Xbar	Sxx	SEE	MSE
a	b	n	T	psig	psig <sup>2</sup>	mADC <sup>2</sup>	mADC <sup>2</sup>
3.9962	0.1060	24.00	2.07	75.83	63603.33	0.0004	0.0000

<u>Calculated Uncertainties:</u>			<u>Total Uncertainty</u>	
$\sigma_C$	$\sigma_E$		$\sigma_F$	$\sigma_T$
psig	psig		psig	psig
0.11	0.09		0.00	0.15

Accepted Tolerance: +/- 1.5 psig

**PASS CALIBRATION? YES**  
**TRANSFER EQUATION PSIG = 9.437 \*mA -37.714**

Figure H10. Pre-test Calibration Data of Gauge Pressure Transducer P3







**UNCERTAINTY ANALYSIS**  
**REF. WSRC-TR-91-106**

**TR-20350**

page \_\_\_\_ of \_\_\_\_  
 calibration date: 29 April 2001

**Calibration Data**

**Calculated Data**

Meter Output (mA)	Water Temp (C)	Water Weight (lbs)	Time Duration (min)	Mass Flow (lbs/min)	Water Density (lb/ft <sup>3</sup> )	Volume Flow (ft <sup>3</sup> /min)	Volume Flow (GPM)	Curve Fit Output (mA)	Error (mA)	Error (GPM)
4.00	26.20	0.00	0.001	0.00	62.22	0.00	0.00	4.00	0.00	0.030
7.27	27.06	1020	6.01	169.72	62.21	2.73	20.41	7.27	0.00	-0.005
10.43	27.53	1336	4.00	334.00	62.20	5.37	40.17	10.43	0.00	0.010
13.63	27.49	1501	3.01	498.67	62.20	8.02	59.97	13.60	-0.03	-0.181
16.86	26.07	2006	3.01	666.45	62.22	10.71	80.12	16.83	-0.03	-0.214
19.98	26.50	2493	3.01	828.24	62.22	13.31	99.58	19.94	-0.04	-0.248
7.20	26.90	1005	6.01	167.22	62.21	2.69	20.11	7.22	0.02	0.131
10.49	26.64	1345	4.00	336.25	62.22	5.40	40.43	10.47	-0.02	-0.103
13.65	26.11	1505	3.00	501.67	62.22	8.06	60.31	13.66	0.01	0.033
16.88	25.90	2010	3.00	670.00	62.23	10.77	80.54	16.89	0.01	0.085
20.05	25.48	2507	3.00	835.67	62.23	13.43	100.45	20.08	0.03	0.183
7.23	24.91	1010	6.01	168.05	62.24	2.70	20.20	7.24	0.01	0.034
10.45	23.17	1340	4.00	335.00	62.27	5.38	40.25	10.44	-0.01	-0.036
13.70	25.21	1512	3.00	504.00	62.24	8.10	60.58	13.70	0.00	-0.012
16.80	25.76	1997	3.00	665.67	62.23	10.70	80.02	16.81	0.01	0.061
20.06	28.33	2508	3.00	836.00	62.19	13.44	100.56	20.10	0.04	0.232

Water Density:  $\rho = 62.441 - 1.374E-3 \cdot T - 271.818E-6 \cdot T^2 + 194.093E-9 \cdot T^3$   
 7.4805 gallons = 1 ft<sup>3</sup>

Uncertainty of the Standards:

Weight: +/-	7.0	lbs		
Temperature: +/-	0.40	C		
Density: +/-	0.06	lbm/ft <sup>3</sup>		
Time: +/- (	0.20	sec +	500.00	µsec/sec)
Multimeter: +/- (	0.04	% RDG +	0.001	mADC

Accepted Tolerance: +/- 0.5 GPM

Statistical Info.				Xbar	Sxx	SEE	MSE
a	b	n	T	(GPM)	(GPM <sup>2</sup> )	(mA <sup>2</sup> )	(mA <sup>2</sup> )
4.003	0.160	16.00	2.145	56.48	15387.47	0.0069	0.0005

Calculated Uncertainties:	standard uncertainty (GPM)	curve-fit uncertainty (GPM)	fixed uncertainty (GPM)	total uncertainty (GPM)
	0.336	0.336	0.000	0.475

**PASS CALIBRATION? YES**  
**TRANSFER EQUATION: GPM = 6.248 mA -25.010**

Figure H14. Pre-test Calibration Data of Magnetic Flowmeter Q1

**UNCERTAINTY ANALYSIS**  
**REF. WSRC-TR-91-106**

**TR-20353**

page \_\_\_\_ of \_\_\_\_  
 calibration date: 29 April 2001

**Calibration Data**

**Calculated Data**

Meter Output (mA)	Water Temp (C)	Water Weight (lbs)	Time Duration (min)	Mass Flow (lbs/min)	Water Density (lb/ft <sup>3</sup> )	Volume Flow (ft <sup>3</sup> /min)	Volume Flow (GPM)	Curve Fit Output (mA)	Error (mA)	Error (GPM)
4.00	21.64	0.00	0.001	0.00	62.29	0.00	0.00	3.96	-0.04	-0.003
7.23	20.92	10.12	5.00	2.02	62.30	0.03	0.24	7.23	0.00	0.000
10.48	21.24	12.09	3.00	4.03	62.29	0.06	0.48	10.48	0.00	0.000
13.65	21.38	17.97	3.00	5.99	62.29	0.10	0.72	13.66	0.01	0.000
16.78	21.57	19.76	2.50	7.90	62.29	0.13	0.95	16.75	-0.03	-0.002
20.05	21.60	19.86	2.00	9.93	62.29	0.16	1.19	20.03	-0.02	-0.001
7.17	21.39	9.95	5.01	1.99	62.29	0.03	0.24	7.17	0.00	0.000
10.43	21.77	12.11	3.01	4.02	62.28	0.06	0.48	10.47	0.04	0.003
13.61	21.42	17.93	3.01	5.96	62.29	0.10	0.72	13.60	-0.01	-0.001
16.79	21.77	19.83	2.50	7.93	62.28	0.13	0.95	16.80	0.01	0.001
20.03	21.93	19.86	2.00	9.93	62.28	0.16	1.19	20.03	0.00	0.000
7.17	21.81	9.96	5.01	1.99	62.28	0.03	0.24	7.18	0.01	0.001
10.44	22.01	12.07	3.01	4.01	62.28	0.06	0.48	10.45	0.01	0.001
13.65	22.14	17.98	3.00	5.99	62.28	0.10	0.72	13.66	0.01	0.001
16.86	22.02	19.93	2.50	7.97	62.28	0.13	0.96	16.87	0.01	0.000
19.96	21.61	19.77	2.00	9.89	62.29	0.16	1.19	19.96	0.00	0.000

Water Density:  $\rho = 62.441 - 1.374E-3 \cdot T - 271.818E-6 \cdot T^2 + 194.093E-9 \cdot T^3$   
 7.4805 gallons = 1 ft<sup>3</sup>

Uncertainty of the Standards:

Weight: +/-	0.02	lbs		
Temperature: +/-	0.40	C		
Density: +/-	0.06	lbm/ft <sup>3</sup>		
Time: +/- (	0.20	sec +	500.00	µsec/sec)
Multimeter: +/- (	0.04	% RDG +	0.00	mADC)

Accepted Tolerance: +/- 0.500 GPM

Statistical Info.				Xbar	Sxx	SEE	MSE
a	b	n	T	(GPM)	(GPM <sup>2</sup> )	(mA <sup>2</sup> )	(mA <sup>2</sup> )
3.958	13.480	16.00	2.145	0.67	2.17	0.0050	0.0004

Calculated Uncertainties:	standard uncertainty (GPM)	curve-fit uncertainty (GPM)	fixed uncertainty (GPM)	total uncertainty (GPM)
	0.0031	0.0034	0.0000	0.0046

**PASS CALIBRATION? YES**

<b>TRANSFER EQUATION:</b>	<b>GPM =</b>	<b>0.074</b>	<b>mA</b>	<b>-0.294</b>
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Figure H15. Pre-test Calibration Data of Magnetic Flowmeter Q2

**UNCERTAINTY ANALYSIS**  
**REF. WSRC-TR-91-106**

**TR-03562**

page \_\_\_\_ of \_\_\_\_  
 calibration date: 07 May 2001

**Calibration Data**

**Calculated Data**

Meter Output (mA)	Water Temp (C)	Water Weight (lbs)	Time Duration (min)	Mass Flow (lbs/min)	Water Density (lb/ft^3)	Volume Flow (ft^3/min)	Volume Flow (GPM)	Curve Fit Output (mA)	Error (mA)	Error (GPM)
4.00	21.65	0.00	0.001	0.00	62.29	0.00	0.00	3.98	-0.02	-0.006
7.24	22.09	50.91	6.00	8.49	62.28	0.14	1.02	7.25	0.01	0.003
10.37	22.13	66.34	4.00	16.59	62.28	0.27	1.99	10.37	0.00	0.001
13.18	22.08	71.69	3.00	23.90	62.28	0.38	2.87	13.19	0.01	0.003
16.77	22.14	99.58	3.01	33.08	62.28	0.53	3.97	16.73	-0.04	-0.012
19.87	22.59	123.73	3.00	41.24	62.27	0.66	4.95	19.88	0.01	0.003
7.30	21.19	51.43	6.00	8.57	62.29	0.14	1.03	7.28	-0.02	-0.005
10.42	21.71	66.84	4.00	16.71	62.29	0.27	2.01	10.42	0.00	0.000
13.75	21.65	76.15	3.00	25.38	62.29	0.41	3.05	13.76	0.01	0.004
16.77	21.32	99.71	3.01	33.13	62.29	0.53	3.98	16.75	-0.02	-0.007
19.97	20.89	124.55	3.00	41.52	62.30	0.67	4.99	19.98	0.01	0.003
7.20	21.01	50.55	6.01	8.41	62.29	0.14	1.01	7.22	0.02	0.006
10.40	20.61	66.80	4.00	16.70	62.30	0.27	2.01	10.41	0.01	0.005
13.61	21.71	74.95	3.00	24.98	62.29	0.40	3.00	13.61	0.00	0.000
16.82	21.03	100.01	3.00	33.34	62.29	0.54	4.00	16.83	0.01	0.002
20.07	22.59	125.23	3.00	41.74	62.27	0.67	5.01	20.07	0.00	0.001

Water Density:  $\rho = 62.441 - 1.374E-3 \cdot T - 271.818E-6 \cdot T^2 + 194.093E-9 \cdot T^3$   
 7.4805 gallons = 1 ft^3

Uncertainty of the Standards:

Weight: +/-	0.2	lbs		
Temperature: +/-	0.40	C		
Density: +/-	0.06	lbm/ft^3		
Time: +/- (	0.20	sec +	500.00	µsec/sec)
Multimeter: +/- (	0.04	% RDG +	0.001	mADC)

Accepted Tolerance: +/- 0.10 GPM

Statistical Info.				Xbar	Sxx	SEE	MSE
a	b	n	T	(GPM)	(GPM^2)	(mA^2)	(mA^2)
3.979	3.209	16.00	2.145	2.81	37.90	0.0039	0.0003

Calculated Uncertainties:	standard uncertainty (GPM)	curve-fit uncertainty (GPM)	fixed uncertainty (GPM)	total uncertainty (GPM)
	0.012	0.013	0.000	0.018

**PASS CALIBRATION? YES**  
**TRANSFER EQUATION: GPM = 0.312 mA - 1.240**

Figure H16. Pre-test Calibration Data of Magnetic Flowmeter Q3

UNCERTAINTY ANALYSIS  
REF. WSRC-TR-91-106

TR-03276

page \_\_\_\_ of \_\_\_\_  
calibration date: 21 May 2002

Calibration Data

Calculated Data

Meter Output (mA)	Water Temp (C)	Water Weight (lbs)	Time Duration (min)	Mass Flow (lbs/min)	Water Density (lb/ft <sup>3</sup> )	Volume Flow (ft <sup>3</sup> /min)	Volume Flow (GPM)	Curve Fit Output (mA)	Error (mA)	Error (GPM)
4.00	20.70	0.00	0.001	0.00	62.30	0.00	0.00	3.99	-0.01	-0.002
7.27	18.90	84.35	10.005	8.43	62.32	0.14	1.01	7.27	0.00	-0.001
10.42	19.20	82.87	5.004	16.56	62.32	0.27	1.99	10.43	0.01	0.002
13.66	20.60	99.50	4.003	24.86	62.30	0.40	2.98	13.65	-0.01	-0.003
16.78	21.30	98.82	3.004	32.90	62.29	0.53	3.95	16.78	0.00	0.000
20.04	21.30	123.96	3.002	41.29	62.29	0.66	4.96	20.04	0.00	0.000
7.25	21.10	84.00	10.002	8.40	62.29	0.13	1.01	7.26	0.01	0.002
10.40	21.10	82.66	5.001	16.53	62.29	0.27	1.98	10.42	0.02	0.005
13.69	21.40	99.77	4.009	24.89	62.29	0.40	2.99	13.66	-0.03	-0.008
16.80	21.50	98.99	3.002	32.98	62.29	0.53	3.96	16.81	0.01	0.003
20.05	21.50	124.17	3.006	41.30	62.29	0.66	4.96	20.05	0.00	-0.001
7.26	20.80	84.11	10.001	8.41	62.30	0.13	1.01	7.26	0.00	0.000
10.41	20.70	82.72	5.004	16.53	62.30	0.27	1.98	10.42	0.01	0.002
13.65	19.80	99.49	4.005	24.84	62.31	0.40	2.98	13.64	-0.01	-0.002
16.85	19.20	99.37	3.002	33.10	62.32	0.53	3.97	16.85	0.00	0.001
20.05	22.10	124.13	3.004	41.33	62.28	0.66	4.96	20.06	0.01	0.002

Water Density:  $\rho = 62.441 - 1.374E-3 \cdot T - 271.818E-6 \cdot T^2 + 194.093E-9 \cdot T^3$   
7.4805 gallons = 1 ft<sup>3</sup>

Uncertainty of the Standards:

Weight: +/-	0.2	lbs
Temperature: +/-	0.20	C
Density: +/-	0.06	lbm/ft <sup>3</sup>
Time: +/- (	0.20	sec +
Multimeter: +/- (	0.04	% RDG +
	500.00	μsec/sec)
	0.001	mADC

Accepted Tolerance: +/- 0.025 GPM

Statistical Info.	a	b	n	T	Xbar (GPM)	Sxx (GPM <sup>2</sup> )	SEE (mA <sup>2</sup> )	MSE (mA <sup>2</sup> )
	3.992	3.236	15.00	2.160	2.79	37.60	0.0013	0.0001

Calculated Uncertainties:	standard uncertainty (GPM)	curve-fit uncertainty (GPM)	fixed uncertainty (GPM)	total uncertainty (GPM)
	0.012	0.008	0.000	0.014

**PASS CALIBRATION? YES**  
**TRANSFER EQUATION: GPM = 0.309 mA - 1.233**

Figure H17. Pre-test Calibration Data of Magnetic Flowmeter Q4 or Qbp